## SECTION 9

## SCUBA TANK





## SCUBA TANK

- Topics covered in this section
- Axisymmetric modeling techniques
- Importing Geometry
- Mesh Density Control
- Perform quality checks on stress results
- Create and manipulate viewports


## SCUBA TANK

- Problem Description
- Scuba tanks are designed to withstand cyclic pressurization and depressurization loads. They must also survive loads induced during transportation and actual service. You are asked to analyze a new scuba tank design.
- Analysis Objectives
- Determine stresses in the scuba tank under an internal pressure of 3000 psi. The maximum stress must be below the yield point of the tank material.


## SCUBA TANK

- Getting started on the scuba tank analysis
- The scuba tank is a thick shell structure. We expect the state of stress to be 3 dimensional in the tank shell. Solid elements should be used.
- Solid element models tend to get large and take a lot of CPU time to solve. This is especially true for non-linear or transient analysis. It is often advisable to simplify the model in order to speed up the analysis process.
- Several ways to simplify finite element models are presented next.


## SCUBA TANK

- Simplifying Finite Element Models
- Finite element models can be simplified by using a 2D (planar) representation of a 3D model. There are three ways to do this:
- Plane Stress
- Plane Strain
- Axisymmetric
- Finite element models can also be simplified by taking advantage of symmetry. There are two primary types of symmetry - reflective symmetry and cyclic symmetry. Symmetry techniques will be presented in detail in the advanced course.


## SCUBA TANK

- The Plane Stress Model
- Assumptions:
- $Z$ stress is zero
- Stresses do no vary through the thickness
- One way to identify a plane stress model is to look for structures in which the thickness is small compared to the other two dimensions.



## SCUBA TANK

- The Plane Strain Model
- Assumptions:
- Z strain is zero
- The depth of the plane strain model is large compared to the cross section.
- Plane strain problems are common in civil engineering and are used to model retaining walls or dams.


Retaining Wall


Earth Dam

$$
\begin{gathered}
\varepsilon_{Z}=0 \quad \gamma_{X Z}=\gamma_{Y Z}=0 \\
\left\{\begin{array}{l}
\sigma_{X} \\
\sigma_{Y} \\
\sigma_{Z}
\end{array}\right\}=\frac{E}{(1+\psi)(1-2 \psi)}\left[\begin{array}{ccc}
1-\psi & \psi & 0 \\
\psi & 1-\psi & 0 \\
0 & 0 & 1-\psi
\end{array}\right]\left\{\begin{array}{l}
\varepsilon_{X} \\
\varepsilon_{Y} \\
\gamma_{X Y}
\end{array}\right\}
\end{gathered}
$$



## SCUBA TANK

- The Axisymmetric Model
- Assumptions:
- The geometry, loads, and boundary conditions are not a function of $q$.
- Another way to state this is
 and boundary conditions do not vary in the circumferential direction.
- Axisymmetry is commonly used to analyze pressure vessels and tanks.

$$
\left\{\begin{array}{l}
\sigma_{f} \\
\sigma_{Z} \\
\sigma_{\theta} \\
\tau_{\mathrm{IZ}}
\end{array}\right\}=\frac{E}{(1+\psi)(1-2 v)}\left[\begin{array}{cccc}
1-\psi & \psi & v & 0 \\
v & 1-\psi & v & 0 \\
v & v & 1-v & 0 \\
0 & 0 & 0 & 1-\psi
\end{array}\right]\left\{\begin{array}{l}
\varepsilon_{\mathrm{I}} \\
\varepsilon_{\mathrm{I}} \\
\varepsilon_{\theta} \\
\gamma_{\mathrm{IZ}}
\end{array}\right\}
$$



## SCUBA TANK

- Simplification of the scuba tank model
- Since the scuba tank is axisymmetric and the pressure load is axisymmetric, we can simplify the problem using axisymmetry. We will solve this problem using two different axisymmetric methods:
- Build a sector of the tank using 3D solid elements
- Build the tank cross section using 2D solid elements


## SCUBA TANK

- Creating the geometry for the tank
- A geometry file for the scuba tank generated by a CAD package is available so there is no need to re-create the geometry.
- Use File/lmport to import the geometry file directly into PATRAN.


## SCUBA TANK




## SCUBA TANK

- Models created by the following CAD packages can be imported into PATRAN:
- CATIA
- Unigraphics
- Pro/ENGINEER
- EUCLID 3
- I-DEAS


## SCUBA TANK

- Additional types of geometry files can also be imported into PATRAN
- ACIS solid geometry files
- Typical file extension is .sat
- Generated by CAD systems such as Autocad, SolidEdge, and Mechanical Desktop
- Parasolid solid geometry files
- Typical file extension is .xmt
- Generated by CAD systems such as SolidWorks
- IGES geometry files
- Typical file extension is .igs
- Generated by most CAD systems
- STEP geometry files
- Typical file extension is .stp
- Generated by CAD systems such as CATIA



## SCUBA TANK

- The scuba tank geometry file we have is a parasolid solid geometry model. Let's import this file into PATRAN.



## SCUBA TANK




## SCUBA TANK



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## SCUBA TANK

Finish importing the parasolid model



## SCUBA TANK



## Rotate and shade the model

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## SCUBA TANK

|  |  |  |  | Geometry |  | Properties | Loads/BCs |  | Meshing | Analysis Results |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\sim$ | $\square$ | 5 | $\xrightarrow{n}$ |  | $\uparrow$ | $\square$ | 8 | 四 | (0) |  |  |  | \$2 |  |  |
| Select | Select | Select | Select | Select | Select | Select | Select | 5 | 1 | Show | Edit | Verify | Renumber | Delete | Associate | Disassociate |
| Points | Curves | Surfaces | Solids | Coordinates | Planes | Vectors | P-Shapes |  | ansform |  |  |  | Geometry | tions |  |  |



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## SCUBA TANK





## SCUBA TANK



## Break the remaining

 tank into two halves


## SCUBA TANK




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## SCUBA TANK




$\square$

## SCUBA TANK



A relatively coarse mesh is created


## SCUBA TANK

- Create Boundary Conditions
- Since the scuba tank is axisymmetric, we need to create a cylindrical coordinate system to define the symmetry boundary conditions.



## SCUBA TANK




## SCUBA TANK




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## SCUBA TANK



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## SCUBA TANK






## SCUBA TANK

| [ |  |  |  |  |  |  |  | Loads/BCs |  | Meshing | Analysis | Results |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Displacement Constraint | Force | Temp <br> No |  | Velocity | Accel |  | Element Uniform | Element Variable | Contact Bodies * | Initial Conditions * | LBC Actions * | Create Load Case <br> Load Cases | $\begin{gathered} \text { LBC } \\ \text { Fields } \end{gathered}$ |



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## SCUBA TANK




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## SCUBA TANK




## SCUBA TANK

|  |  |  |  |  |  | Loads/BCs |  | Meshing Analysis |  | Results |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Displacement Constraint | Force | Tempe <br> No | Velocity | Acceleration | Element Uniform | Element <br> Variable | Contact Bodies * | Initial Conditions * | LBC Actions | Create Load Case Load Cases | $\begin{gathered} \text { LBC } \\ \text { Fields } \end{gathered}$ |



## SCUBA TANK

|  |  |  |  |  |  | Loads/BCs |  | Meshing Analysis |  | Results |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Displacement Constraint | Force | Tempe <br> No | Velocity | Acceleration | Element Uniform | Element Variable | Contact Bodies * | Initial Conditions * | LBC <br> Actions * | Create <br> Load Case <br> Load Cases | $\begin{gathered} \text { LBC } \\ \text { Fields } \end{gathered}$ |

Finish creating the radial constraint.



## SCUBA TANK

|  |  |  |  |  |  | Loads/BCs |  | Meshing Analysis |  | Results |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Displacement Constraint | Force | Tempe <br> No | Velocity | Acceleration | Element Uniform | Element Variable | Contact <br> Bodies * | Initial Conditions * | LBC <br> Actions * | Create Load Case Load Cases | LBC <br> Fields * |




## SCUBA TANK



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## SCUBA TANK

|  |  |  |  |  |  | Loads/BCs |  | Meshing Analysis |  | Results |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Displacement Constraint | Force | Tempe <br> No | Velocity | Acceleration | Element Uniform | Element Variable * | Contact Bodies * | Initial Conditions * | LBC <br> Actions * | 3 $=$ <br> Create Load Case <br> Load Cases. | $\begin{gathered} \text { LBC } \\ \text { Fields } \end{gathered}$ |



## SCUBA TANK

|  |  |  |  | Geometry Properties |  | Loads/BCs |  | Meshing | Analysis | Results |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Displacement Constraint | Force | Tempe <br> No | Velocity | Acceleration | Element Uniform | Element Variable | Contact Bodies | Initial Conditions * | LBC Actions * | Create Load Case Load Cases | $\begin{gathered} \text { LBC } \\ \text { Fields } \end{gathered}$ |




## SCUBA TANK

|  |  |  | Geometry |  | Properties | Loads/BCs |  | Meshing | Analysis Resu |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Displacement Constraint | Force | Tempe | Velocity | Acceler | Displa |  | Pressure | Temperature | il <br> Inertial Load | Distributed Load | CID Distributed Load | Total Load |
| Nodal |  |  |  |  | Element Uniform |  |  |  |  |  |  |  |

Create a pressure load.



## SCUBA TANK

|  |  |  | Geometry |  | Properties | Loads/BCs |  | Meshing | Analysis Resu |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Displacement Constraint | Force | Tempe | Velocity | Accele | Displa |  | Pressure | Temperature | il <br> Inertial Load | Distributed Load | CID Distributed Load | $\begin{aligned} & \sum_{\text {nal }} \\ & \text { Total } \\ & \text { Load } \end{aligned}$ |
| Nodal |  |  |  |  | Element Uniform |  |  |  |  |  |  |  |



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## SCUBA TANK

|  |  |  | Geometry |  | Properties | Loads/BCs |  | Meshing | Analysis | s Results |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Displacement Constraint | Force | Tempe | Velocity | Acceler | Displa |  | Pressure | Temperature | il <br> Inertial Load | Distributed Load | CID Distributed Load | Total Load |
| Nodal |  |  |  |  | Element Uniform |  |  |  |  |  |  |  |



| Load/Boundary Conditions ${ }^{\text {a }}$ |  |  |
| :---: | :---: | :---: |
| LoadBoundary Condtions |  |  |
| Action: | Create - | $\wedge$ |
| obiect | Pressure - |  |
| Type |  |  |
| Current Load Case: |  |  |
| $\square$ |  |  |
| Type: Static |  |  |
| Existing Sets 易 |  |  |
| New Set Name |  |  |
| internal_pressure |  |  |
| Target Element Type: 30 |  |  |
| Input Data... |  |  |
| Select Application Region... |  |  |
| -Apply- |  |  |
|  |  | $\checkmark$ |

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## SCUBA TANK

- Create the scuba tank material properties
- The tank is made from 17-4 PH stainless steel forging, heat treated to the H 1025 condition.
- $\mathrm{E}=28.5 \times 10^{6} \mathrm{psi}$
- $v=0.27$
- Ultimate strength $=155 \mathrm{ksi}$
- Yield strength $=145 \mathrm{ksi}$


## SCUBA TANK



Create an isotropic material named 17-4PH.
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## SCUBA TANK



## SCUBA TANK




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## SCUBA TANK



Submit the model to MD NASTRAN for a static analysis.


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## SCUBA TANK




Group
Method: Result Entities
Available Jobs
scuba

Job Name
scuba
Job Description (TTitLE) MD Nastran iob created
O6-Apr-10 at 21:59:30

SUBTITLE
Label

Select Results File. Translation Parameters...

Apply

$$
\begin{aligned}
& \text { Code: MO Nastran } \\
& \text { Type: Structural }
\end{aligned}
$$

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## SCUBA TANK



## Object Deformation - <br> 是图图圆

Seiect रesuit Cases EX Default，A1：Stetic Subcase；－MD NASTF
（ ）III
Select Deformation Resut
Constrint Forces，Translational

```
Displacements, Translational
```

```
Displacements, Translational
```


Postion...((NON-LAYERED))

Resultant -
$\square$ Aninate
Apply
Reset


## SCUBA TANK



## SCUBA TANK



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## SCUBA TANK

- Next, let's plot the stresses
- By default, the solid element stresses are computed in the basic coordinate system.
- For the scuba tank, we are interested in the radial, hoop, and axial stresses which are defined in a cylindrical system. We need to transform the stresses from the basic coordinate system to the cylindrical coordinate system no. 1.


## SCUBA TANK



Click the Plot Options icon.

Select CID and coordinate system no.

1. This transforms the stresses into
coordinate system 1.


## SCUBA TANK




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## SCUBA TANK

|  | 事 $=\mathrm{H}$ |  | Geometry | Pro | perties | Loads/E | Cs Mes | hing |  | Analysis | Results |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fringe/Deformation | Deformation | Fringe | $\underset{\text { Vector }}{\rightarrow \stackrel{1}{7}}$ | Tensor | cursor | Contour | Isosurface | Free | dy | Graph | Animation | Report | - |  \% <br>  a | Insight | XY Plots | Imaging |
| Quick Plot | Result Plots |  |  |  |  |  |  |  |  |  |  |  |  | Result A.... | Insight |  |  |




## SCUBA TANK





## SCUBA TANK




## SCUBA TANK



$\square$

## SCUBA TANK



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## SCUBA TANK



## SCUBA TANK

- Scuba tank coarse-mesh model analysis summary:
- The maximum Von Mises stress is 31,800 psi at the base of the tank near the fillet radius.
- The stress gradient through the tank wall thickness is high. It ranges from 31,800 psi on the inside wall to about 5,000 psi on the outside wall. This stress gradient is captured by a single tet10 element through the thickness.
- The un-averaged stress fringe plot is jagged, an indication that the mesh is too coarse.
- The stress difference plot shows a maximum stress jump of 13,700 psi. This suggests that the mesh is too coarse in this area.
- This first scuba tank model was relatively coarse. It helped us identify the critical area in the tank. We will now create a second model with a finer mesh in the critical area.


## SCUBA TANK




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## SCUBA TANK




## SCUBA TANK





## SCUBA TANK




## SCUBA TANK




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## SCUBA TANK


from the dome/cylinder transition point and create a plane there.
Break the solid using this plane.


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## SCUBA TANK



> Mesh the dome portion of the tank
> with an element size of 0.25 inch.



## SCUBA TANK




## SCUBA TANK






## SCUBA TANK




## SCUBA TANK





## SCUBA TANK



## SCUBA TANK



Plot the Von Mises stress



## SCUBA TANK




$\square$

## SCUBA TANK






## SCUBA TANK




| Results |  |
| :---: | :---: |
| Action: | Create - |
| Object | Fringe - |
| 骂 | - 5 |

Coordinate Transtormation
$\mathrm{ClD}-$
Select Coordinate Frame
Coord 1

Scale Factor
Filter Values: None -

Averaging Definition:
Domair: All Entities -
Method: Difference $\nabla$
Extrapolation: Shape Fn. -
$\square$ use PCL Expression

| Define PCL Expression... |
| :--- |
| Existing Fringe Flots... |

Save Fringe Plot $A s$ :


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## SCUBA TANK

- Scuba tank fine-mesh model analysis summary:
- The maximum Von Mises stress is 30,300 psi at the base of the tank near the fillet radius.
- There are 5 elements through the thickness in this critical area. The stress gradient is represented reasonably well through the thickness.
- The un-averaged stress fringe plot is relatively smooth, indicating that the re-meshing effort paid off.
- The stress difference plot shows a maximum stress jump of 4300 psi. Is further mesh refinement necessary?
- A total of 98,830 nodes and 66,504 elements were used to model this problem.
- Let's analyze the tank again using 2D axisymmetric elements.


## SCUBA TANK

- Using 2D Axisymmetric Elements
- This converts a 3D problem into a planar problem by using 2D elements.
- Only half of the tank cross section is modeled.
- Geometry, boundary condition, and loads must all be axisymmetric.
- A much finer mesh can be used to solve this problem.



## SCUBA TANK




## SCUBA TANK




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## SCUBA TANK





## SCUBA TANK



Change the view by using Viewing Angles.


## SCUBA TANK



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## SCUBA TANK



The use of planar elements allowed us to use a much finer mesh.

There are now 10 elements through the thickness in the critical area.


## SCUBA TANK



The T2, R1, R2, and R3 degrees of freedom are not used in this axisymmetric problem. Constrain these unused degrees of freedom.



## SCUBA TANK



Constrain the model in the $z$ direction.


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## SCUBA TANK



Apply the pressure to all the internal curves.

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## SCUBA TANK



Create an isotropic material named 17-4PH.


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## SCUBA TANK



## SCUBA TANK

|  |  |  | Geometry |  |  |  | Properties Loads/BCs |  |  | Meshing | alysis Results |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $+$ |  | 4 |  | $\square$ | $\square \square$ |  |  | $8$ |  | $\prod_{\text {plot }}^{33}$ |  | (4) 5 |
| Entire Model | Selected Group | Analysis Deck |  | Read | Submit |  | + 8 | XDB | Output2 | $\begin{aligned} & \text { MASTER/ } \\ & \text { DBALL } \end{aligned}$ | t16/t19 | d3plot |  | 6evi 4 |
| Analyze |  | Create | Existing Deck |  |  | Optimize | Toptomize | Access Results |  |  |  |  | Delete | Actions |



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## SCUBA TANK



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## SCUBA TANK




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## SCUBA TANK




| Results |
| :---: |
| Results |
| Action: Create - |
| Object: Fringe - |
|  |
| Coordinate Transformation: $\square$ <br> CID |
| Select Coordinate Frame |
| Coord 1 |
| Scale Factor 1.0 |
| Filter Values: None - |
| Averaging Definition: <br> Domain: All Entities <br> Method: Difference |
| Extrapolation: Shape Fn. |
| $\square$ Use PCL Expression |
| Define PCL Expression.. |
| Existing Fringe Plots... |
| Save Fringe Plot As: |
| Apply $\quad$ Reset |

## SCUBA TANK

- Scuba tank 2D axisymmetric analysis summary
- The maximum Von Mises stress is 29,100 psi at the base of the tank near the fillet radius.
- There are 10 elements through the thickness in this critical area. The stress gradient is represented reasonably well through the thickness.
- The un-averaged stress fringe plot is very smooth, indicating that the mesh density is adequate.
- The stress difference plot shows near zero values.
- Using a 2D representation of the scuba tank, we were able to create a smaller model with a finer mesh compared to the 3D model.


## EXERCISE

- Perform Workshop 9 "Support Bracket" in your exercise workbook.
- Optional:
- Analyze the Scuba Tank covered in this section.

