

7,0

6º Trabalho em Grupo - Comportamento dinâmico de sistemas de 2ª. ordem

Grupo: 8

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1) Uma mudança em degrau na pressão de um vaso de 15 para 24 psi resulta em uma resposta no medidor de pressão de acordo com a Figura 1. Assuma dinâmica de segunda ordem, calcule todos os parâmetros importantes e escreva a FT na forma:

$$\frac{\overline{Rm}(s)}{P(s)} = \frac{K}{\tau^2 s^2 + 2\zeta\tau s + 1}$$

Em que Rm → instrumento de medida (mm); P → pressão (psi)

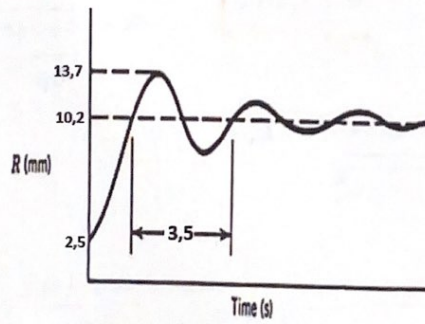


Figura 1: Resposta dinâmica do sistema de medida

2) Encontre a função de transferência, de um sistema composto por 2 tanques em série como mostrado na Figura 2, que descreva o comportamento do sistema ( $h_2(t)$ ) frente a uma perturbação na vazão de entrada ( $F_0(t)$ ).

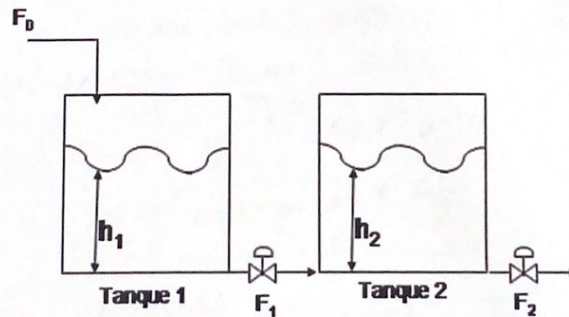


Figura 2: Tanques em série

Considere:  $F_1 = \beta\sqrt{h_1 - h_2}$        $F_2 = \beta\sqrt{h_2}$       em que  $\beta$  é o termo

associado às resistências aos fluxos volumétricos  $F_1$  e  $F_2$ , respectivamente.

1)  $P_{res\tilde{c}o} \rightarrow 15 \rightarrow 24 \rightarrow 9 \text{ psi}$

$$K_p = \frac{\Delta y}{\Delta c} \quad K_p = \frac{7,7}{9} = 0,855$$

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$$\begin{cases} T = 3,5 \\ B = 50,2 - 2,5 = 7,7 \\ A = 53,7 - 50,2 = 3,5 \\ \Delta y = 50,2 - 2,5 = 7,7 \\ \Delta c = 9 \end{cases}$$

$$D_{res\tilde{c}o} = \frac{A}{B} = \exp\left(\frac{-\tilde{\pi} b}{\sqrt{1-b^2}}\right) \rightarrow \frac{3,5}{7,7} = \exp\left(\frac{-\tilde{\pi} b}{\sqrt{1-b^2}}\right)$$

$$\ln\left(\frac{3,5}{7,7}\right) = \ln\left(\exp\left(\frac{-\tilde{\pi} b}{\sqrt{1-b^2}}\right)\right) \rightarrow \sqrt{1-b^2} = \frac{-\tilde{\pi} b}{\ln\left(\frac{3,5}{7,7}\right)} \quad -1-b^2 = \left(\frac{-\tilde{\pi} b}{-0,7884}\right)^2$$

$$-1-b^2 = \frac{9,8596 b^2}{0,62157} \quad -1-b^2 = 15,8624 \cdot b^2 \rightarrow (-1+(-15,8624)) \cdot b^2 + 1 = 0$$

$$+16,8624 \cdot b^2 = 1 \quad \therefore b^2 = \frac{1}{16,8624} \quad b^2 = 0,059303 \quad b = 0,2435$$

$$\bullet T = \frac{2\tilde{\pi}}{\omega} \rightarrow 3,5 = \frac{2\tilde{\pi}}{\omega} \quad \omega = 3,794$$

$$\omega = \frac{\sqrt{1-b^2}}{\zeta_p} \rightarrow 3,794 = \frac{\sqrt{1-(0,2435)^2}}{\zeta_p}$$

$$\bullet \zeta_p = \frac{\tilde{\pi} \zeta_p}{\sqrt{1-b^2}} \quad \zeta_p = \frac{\tilde{\pi} \cdot 0,54}{\sqrt{1-0,2435^2}} \quad \zeta_p = 1,75$$

$$\zeta_p = 0,54$$

Função de Transferência

$$\frac{\bar{R}_m(s)}{\bar{P}(s)} = \frac{K_p}{\zeta_p^2 s^2 + 2\zeta_p \omega_p s + \omega_p^2}$$

$$\frac{\bar{R}_m(s)}{\bar{P}(s)} = \frac{0,855}{0,12916 \cdot s^2 + 2 \cdot 0,2434 \cdot 0,545 + 1}$$

$$\frac{\bar{R}_m(s)}{\bar{P}(s)} = \frac{0,855}{0,12916 s^2 + 0,2635 s + 1}$$

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2) Hipótese pl Torque

- mistura completa
- densidade constante
- área da seção transversal

Balanco de massa no Torque

$$F_0 = F_1 = F_2 = \frac{dM}{dt} = d(\rho \cdot A_1 \cdot h_1) = \rho \cdot A_1 \cdot \frac{d(h_1)}{dt}$$

$$F_0(t) - F_1(t) = A_2 \cdot \frac{dh_2}{dt}$$

$$F_0(t) - \beta \sqrt{h_2(t) - h_{2M}} = A \frac{dh_2}{dt} \quad (\text{EDO n\u00b0 linear})$$

Linearização por Taylor

$$\sqrt{h_1(t) - h_{2M}} \approx \sqrt{h_{1M} - h_{2M}} + \frac{1}{2\sqrt{h_{1M} - h_{2M}}} (h_1(t) - h_{1M}) - \frac{1}{2\sqrt{h_{1M} - h_{2M}}} (h_2(t) - h_{2M})$$

substituindo (2) em (1)

$$F_0(t) - \beta \left( \sqrt{h_{1M} - h_{2M}} + \frac{1}{2\sqrt{h_{1M} - h_{2M}}} (h_1(t) - h_{1M}) - \frac{1}{2\sqrt{h_{1M} - h_{2M}}} (h_2(t) - h_{2M}) \right) = A \frac{dh_2}{dt}$$

estado estacion\u00e1rio

$$F_{0M} - \beta \sqrt{h_{1M} - h_{2M}} = 0 \quad \text{subtra\u00eddo (4) de (3)}$$

$$(F_0(t) - F_{0M}) - \beta \left( \sqrt{h_{1M} - h_{2M}} + \frac{1}{2\sqrt{h_{1M} - h_{2M}}} (h_1(t) - h_{1M}) - \frac{1}{2\sqrt{h_{1M} - h_{2M}}} (h_2(t) - h_{2M}) \right) +$$

$$\beta \sqrt{h_{1M} - h_{2M}} = A \frac{dh_2}{dt} \quad \text{continua\u00e7\u00e3o}$$

D	S	T	Q	Q	S	S
C	L	M	M	J	V	S

$$(F_0(x) - F_{0M}) - \beta \left( \frac{1}{2\sqrt{h_{1M} \cdot h_{2M}}} (h_1(x) - h_{1M}) - 1 \right) \left( h_2(x) - h_{2M} \right)$$

$$= A \cdot \frac{dh_1}{dt} \quad (5)$$

Forma da variável de estado

$$F_0'(x) - \beta \cdot \frac{1}{2\sqrt{h_{1M} \cdot h_{2M}}} (h_1'(x) - h_2'(x)) = A \cdot \frac{dh_1}{dt} \quad (6)$$

Laplace

$$L\{F_0'(x)\} = L\left\{ \beta \frac{1}{2\sqrt{h_{1M} \cdot h_{2M}}} \cdot h_2'(x) \right\} + L\left\{ \beta \frac{1}{2\sqrt{h_{1M} \cdot h_{2M}}} \right\}$$

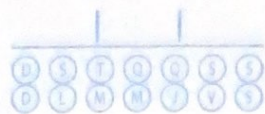
$$= L\left\{ A \cdot \frac{dh_1}{dt} \right\} \quad \text{NÃO LINEARIZOU}$$

$$\bar{F}_0(s) - \beta \cdot \frac{1}{2\sqrt{h_{1M} \cdot h_{2M}}} \cdot \bar{h}_2(s) + \beta \frac{1}{2\sqrt{h_{1M} \cdot h_{2M}}} \bar{h}_2(s) = A \cdot \bar{h}_1(s) \cdot s$$

~~$$\bar{F}_0(s) + \beta \frac{1}{2\sqrt{h_{1M} \cdot h_{2M}}} \bar{h}_2(s) = \left( A \cdot s \cdot \beta \frac{1}{2\sqrt{h_{1M} \cdot h_{2M}}} \right) \bar{h}_1(s)$$~~

~~$$\bar{h}_1(s) = \frac{1}{A \cdot s + \beta \frac{1}{2\sqrt{h_{1M} \cdot h_{2M}}}} \cdot \bar{F}_0(s) + \frac{\beta}{2\sqrt{h_{1M} \cdot h_{2M}}} \frac{1}{A \cdot s + \beta \frac{1}{2\sqrt{h_{1M} \cdot h_{2M}}}} \cdot \bar{h}_2(s)$$~~

~~$$\bar{h}_1(s) = \frac{2\sqrt{h_{1M} \cdot h_{2M}}}{2 \cdot A \sqrt{h_{1M} \cdot h_{2M}} \cdot s + \beta} \cdot \bar{F}_0(s) + \frac{1}{2A \sqrt{h_{1M} \cdot h_{2M}} \cdot s + \beta} \cdot \bar{h}_2(s) \quad (7)$$~~



$$K_{ps} = \frac{2 \sqrt{h_{1M} - h_{2M}}}{\beta} \quad \tau_{ps} = \frac{2 \cdot A \cdot \sqrt{h_{1M} - h_{2M}}}{\beta}$$

• Balanço de massa p/ Torque (2)

$$F_1(t) \cdot \rho_1 - F_2(t) \cdot \rho_2 = \frac{dm(t)}{dt} = \frac{d(\rho A h_2(t))}{dt} = \rho A \frac{d(h_2(t))}{dt}$$

$$F_1(t) - F_2(t) = A \cdot \frac{dh_2(t)}{dt}$$

$$\beta \sqrt{h_1(t) - h_2(t)} - \beta \sqrt{h_2(t)} = A \frac{dh_2(t)}{dt} \quad (8) \text{ EDO - n\u00e3 linear}$$

Linearizar

$$\sqrt{h_1(t) - h_2(t)} \therefore \sqrt{h_{1M} - h_{2M}} + \frac{(h_1(t) - h_{1M}) - 1}{2\sqrt{h_{1M} - h_{2M}}}$$

$$\sqrt{h_2(t) - h_{2M}} \quad (9) \rightarrow \sqrt{h_2(t)} \therefore \sqrt{h_{2M}} + \frac{(h_2(t) - h_{2M})}{2\sqrt{h_{2M}}} \quad (10)$$

Substituindo (9) e (10) na eq (8)

$$\beta \left( \frac{\sqrt{h_{1M} - h_{2M}} + 1}{2\sqrt{h_{1M} - h_{2M}}} (h_1(t) - h_{1M}) - \frac{1}{2\sqrt{h_{1M} - h_{2M}}} (h_2(t) - h_{2M}) \right) -$$

$$\beta \left( \sqrt{h_{2M}} + \frac{(h_2(t) - h_{2M})}{2\sqrt{h_{2M}}} \right) = A \frac{dh_2(t)}{dt} \quad (11)$$

M\u00e9todo Ortogonal

$$\beta \sqrt{h_{1M} - h_{2M}} - \beta \sqrt{h_{2M}} = 0 \quad (12)$$

Substituindo (12) da (11)

$$\beta \left( \frac{1}{2\sqrt{h_{1M} - h_{2M}}} (h_1(t) - h_{1M}) - \frac{1}{2\sqrt{h_{1M} - h_{2M}}} (h_2(t) - h_{2M}) \right) - \beta \left( \frac{1}{2\sqrt{h_{2M}}} (h_2(t) - h_{2M}) \right) = A \frac{dh_2(t)}{dt} \quad (13)$$

Variable derivo

$$\beta \left( \frac{1}{2\sqrt{h_{1M} - h_{2M}}} \cdot h_1'(t) - \frac{1}{2\sqrt{h_{1M} - h_{2M}}} \cdot h_2'(t) - \beta \left( \frac{1}{2\sqrt{h_{2M}}} \cdot h_2'(t) \right) = A \cdot \frac{dh_2(t)}{dt} \right) \quad (14)$$

Laplace

$$\beta \left( \frac{1}{2\sqrt{h_{1M} - h_{2M}}} \cdot \bar{h}_1(s) - \frac{1}{2\sqrt{h_{1M} - h_{2M}}} \cdot \bar{h}_2(s) - \beta \left( \frac{1}{2\sqrt{h_{2M}}} \cdot \bar{h}_2(s) \right) = A \cdot \bar{h}_2(s) \cdot s \right) \quad (15)$$

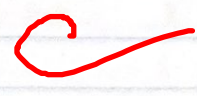
$$\beta \frac{1}{2\sqrt{h_{1M} - h_{2M}}} \cdot \bar{h}_1(s) - \beta \frac{1}{2\sqrt{h_{1M} - h_{2M}}} \cdot \bar{h}_2(s) - \beta \frac{1}{2\sqrt{h_{2M}}} \cdot \bar{h}_2(s) = A \cdot \bar{h}_2(s) \cdot s$$

$$\beta \frac{1}{2\sqrt{h_{1M} - h_{2M}}} \cdot \bar{h}_1(s) = A \cdot \bar{h}_2(s) \cdot s + \beta \frac{1}{2\sqrt{h_{1M} - h_{2M}}} \cdot \bar{h}_2(s) + \beta \frac{1}{2\sqrt{h_{2M}}} \cdot \bar{h}_2(s)$$

$$\bar{h}_2(s) = \left( \beta \frac{1}{2\sqrt{h_{1M} - h_{2M}}} \right) \cdot \bar{h}_1(s) \cdot \left( A \cdot s + \beta \frac{1}{2\sqrt{h_{1M} - h_{2M}}} + \beta \frac{1}{2\sqrt{h_{2M}}} \right)$$

$$\bar{h}_2(s) = \left( \beta \frac{1}{2\sqrt{h_{1M} - h_{2M}}} \right) \cdot \left( A \cdot s + \beta \frac{\sqrt{h_{2M}}}{2\sqrt{h_{2M}}} + \frac{\sqrt{h_{1M} - h_{2M}}}{\sqrt{h_{1M} - h_{2M}}} \right) \cdot \bar{h}_1(s)$$

$$\bar{h}_2(s) = \beta \frac{1}{2\sqrt{h_{1M} - h_{2M}}} \cdot \bar{h}_1(s) \cdot \left( \frac{2A\sqrt{h_{2M}}\sqrt{h_{1M} - h_{2M}} \cdot s + 1}{\beta(\sqrt{h_{2M}} + \sqrt{h_{1M} - h_{2M}})} \right) \quad (16)$$



$$K_{p2} = \left( \beta \frac{1}{2\sqrt{h_{1M} - h_{2M}}} \right) \quad \tau_{p2} = \frac{2 \cdot A \sqrt{h_{2M}} \sqrt{h_{1M} - h_{2M}}}{\beta (\sqrt{h_{2M}} + \sqrt{h_{1M} - h_{2M}})}$$

Relacionamos (7) com (6)

$$\bar{h}_2(s) = K_{p2} \cdot \left[ \frac{K_{p1}}{\tau_{p1} \cdot s + 1} \cdot \bar{F}_0(s) + \frac{1}{\tau_{p1} \cdot s + 1} \cdot \bar{h}_2(s) \right]$$

$$\bar{h}_2(s) - K_{p2} \cdot \frac{1}{(\tau_{p1} \cdot s + 1)} \cdot \bar{h}_2(s) = \frac{K_{p2}}{(\tau_{p1} \cdot s + 1)} \cdot K_{p1} \cdot \bar{F}_0(s)$$

$$\bar{h}_2(s) \cdot \left[ \frac{1 - K_{p2}}{\tau_{p1} \cdot \tau_{p2} \cdot s^2 + (\tau_{p2} + \tau_{p1}) \cdot s + 1} \right] = \frac{K_{p1} \cdot K_{p2}}{\tau_{p1} \cdot \tau_{p2} \cdot s^2 + (\tau_{p2} + \tau_{p1}) \cdot s + 1} \cdot \bar{F}_0(s)$$

$$\bar{h}_2(s) \cdot \left[ \frac{(\tau_{p1} \tau_{p2} s^2 + (\tau_{p2} + \tau_{p1}) \cdot s + 1) - K_{p2}}{\tau_{p1} \tau_{p2} s^2 + (\tau_{p2} + \tau_{p1}) \cdot s + 1} \right] = \frac{K_{p1} \cdot K_{p2}}{\tau_{p1} \tau_{p2} s^2 + (\tau_{p2} + \tau_{p1}) \cdot s + 1} \cdot \bar{F}_0(s)$$

$$\bar{h}_2(s) = \frac{K_{p1} \cdot K_{p2}}{(\tau_{p1} \cdot \tau_{p2} \cdot s^2 + (\tau_{p2} + \tau_{p1}) \cdot s + 1) - K_{p2}} \cdot \bar{F}_0(s)$$

$$\bar{h}_2(s) = \frac{K_{p1} \cdot K_{p2}}{\left( \frac{\tau_{p1} \cdot \tau_{p2}}{1 - K_{p2}} \right) \cdot s^2 + \left( \frac{\tau_{p1} \cdot \tau_{p2}}{1 - K_{p2}} \right) \cdot s + 1} \cdot \bar{F}_0(s)$$

$$K_{p1} \cdot K_{p2} = \left( \frac{2 \sqrt{h_{1M} - h_{2M}}}{\beta} \right) \cdot \left( \beta \frac{1}{2\sqrt{h_{1M} - h_{2M}}} \right) = 1$$

$$\frac{\tau_{p1} \cdot \tau_{p2}}{1 - K_{p2}} = \left( \frac{2 \cdot A \sqrt{h_{1M} - h_{2M}}}{\beta} \right) \cdot \left( \frac{2 \cdot A \sqrt{h_{2M}} \sqrt{h_{1M} - h_{2M}}}{\beta (\sqrt{h_{2M}} + \sqrt{h_{1M} - h_{2M}})} \right) = \frac{4A^2 (h_{1M} - h_{2M}) \sqrt{h_{2M}}}{\beta^2 (\sqrt{h_{2M}} + \sqrt{h_{1M} - h_{2M}})}$$

$$1 \cdot \left( \beta \frac{1}{2\sqrt{h_{1M} - h_{2M}}} \right) \quad 1 \cdot \left( \beta \frac{1}{2\sqrt{h_{2M} - h_{2M}}} \right)$$

$$\frac{T_{p1} + T_{p2}}{1 - K_{p2}} = \frac{2A \sqrt{h_{1M} - h_{2M}}}{\beta} + \frac{2A \sqrt{h_{2M}} \sqrt{h_{1M} - h_{2M}}}{\beta (\sqrt{h_{2M}} + \sqrt{h_{1M} - h_{2M}})}$$

$$1 - \left( \beta \frac{1}{2\sqrt{h_{1M} - h_{2M}}} \right)$$

$$= \frac{2A \sqrt{h_{1M} - h_{2M}} (\sqrt{h_{2M}} + \sqrt{h_{1M} - h_{2M}}) + 2A \sqrt{h_{2M}} \sqrt{h_{1M} - h_{2M}}}{\beta (\sqrt{h_{2M}} + \sqrt{h_{1M} - h_{2M}})}$$

$$1 - \left( \beta \frac{1}{2\sqrt{h_{1M} - h_{2M}}} \right)$$

$$\frac{T_{p1} + T_{p2}}{1 - K_{p2}} = \frac{2A \sqrt{h_{1M} - h_{2M}} \sqrt{h_{2M}} + 2A (h_{1M} - h_{2M}) + 2A \sqrt{h_{2M}} \sqrt{h_{1M} - h_{2M}}}{\beta (\sqrt{h_{2M}} + \sqrt{h_{1M} - h_{2M}})}$$

$$1 - \left( \beta \frac{1}{2\sqrt{h_{1M} - h_{2M}}} \right)$$

$$= \frac{2A (\sqrt{h_{1M} - h_{2M}} \sqrt{h_{2M}} + (h_{1M} - h_{2M}) + \sqrt{h_{2M}} \sqrt{h_{1M} - h_{2M}})}{\beta (\sqrt{h_{2M}} + \sqrt{h_{1M} - h_{2M}})}$$

$$1 - \left( \beta \frac{1}{2\sqrt{h_{1M} - h_{2M}}} \right)$$

$$h_2(s) = \frac{1}{\left( \frac{4R^2 (h_{1M} - h_{2M}) \sqrt{h_{2M}}}{\beta^2 (\sqrt{h_{2M}} + \sqrt{h_{1M} - h_{2M}})} \right) \cdot s^2 + \left( \frac{2A (\sqrt{h_{1M} - h_{2M}} \sqrt{h_{2M}} + \sqrt{h_{2M}} \sqrt{h_{1M} - h_{2M}})}{\beta (\sqrt{h_{2M}} + \sqrt{h_{1M} - h_{2M}})} \right)}$$

$$1 - \left( \beta \frac{1}{2\sqrt{h_{1M} - h_{2M}}} \right)$$