

Estudo das deformações

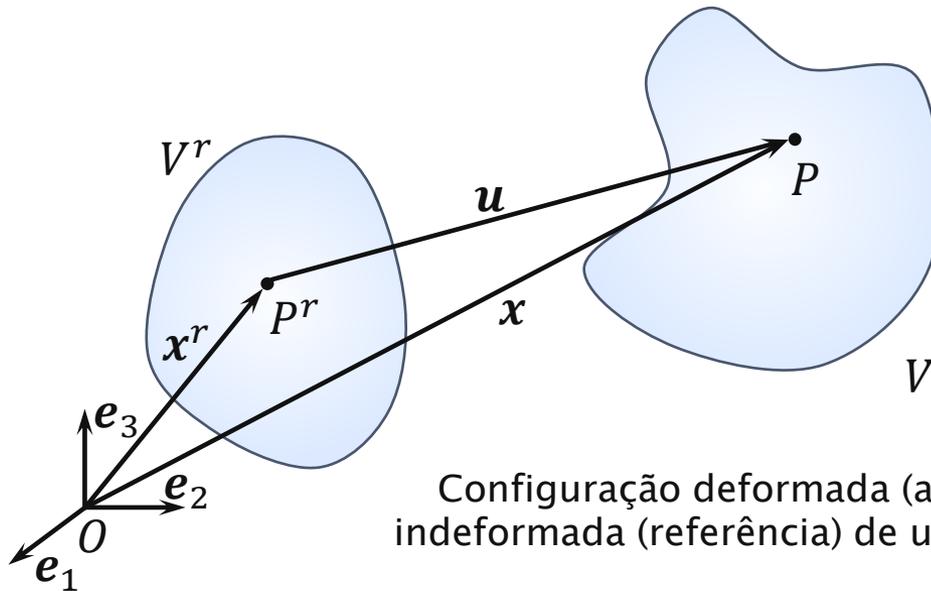
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**PEF 3302 – Mecânica das
Estruturas I**



Configuração deformada (atual) e indeformada (referência) de um sólido

$$\mathbf{x}^r = \sum_{i=1}^3 x_i^r \mathbf{e}_i = x_1^r \mathbf{e}_1 + x_2^r \mathbf{e}_2 + x_3^r \mathbf{e}_3 = \mathbf{x}_i^r \mathbf{e}_i \quad (1)$$

$$\mathbf{x} = \sum_{i=1}^3 x_i \mathbf{e}_i = x_1 \mathbf{e}_1 + x_2 \mathbf{e}_2 + x_3 \mathbf{e}_3 = \mathbf{x}_i \mathbf{e}_i \quad (2)$$

Notação de Einstein

Campo de deslocamentos: $\mathbf{u} = \mathbf{x} - \mathbf{x}^r \quad (3)$

A deformação fica totalmente caracterizada conhecendo-se a função:

$$\mathbf{x} = \mathbf{x}(\mathbf{x}^r) \quad (4)$$

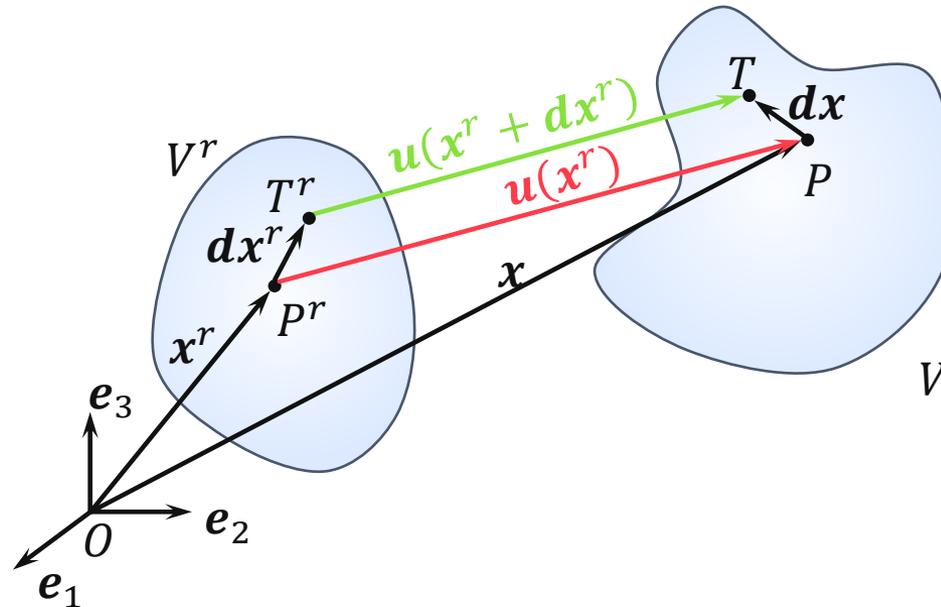
que fornece a posição de uma partícula material na configuração deformada a partir de sua posição na configuração indeformada.

Em componentes:

$$\begin{aligned} x_1 &= x_1(x_1^r, x_2^r, x_3^r) \\ x_2 &= x_2(x_1^r, x_2^r, x_3^r) \\ x_3 &= x_3(x_1^r, x_2^r, x_3^r) \end{aligned} \quad (5)$$

e para o campo de deslocamentos: (6)

$$\begin{aligned} u_1 &= u_1(x_1^r, x_2^r, x_3^r) \\ u_2 &= u_2(x_1^r, x_2^r, x_3^r) \\ u_3 &= u_3(x_1^r, x_2^r, x_3^r) \end{aligned}$$



Fibras na configuração deformada e indeformada:

$$dx = dx^r + u(x^r + dx^r) - u(x^r) \quad (7)$$

Em componentes:

$$dx_i = dx_i^r + u_i(x_1^r + dx_1^r, x_2^r + dx_2^r, x_3^r + dx_3^r) - u_i(x_1^r, x_2^r, x_3^r) \quad (8)$$

Lembrando do cálculo com múltiplas variáveis:

$$u_i(x_1^r + dx_1^r, x_2^r + dx_2^r, x_3^r + dx_3^r) - u_i(x_1^r, x_2^r, x_3^r) = \frac{\partial u_i}{\partial x_1^r} dx_1^r + \frac{\partial u_i}{\partial x_2^r} dx_2^r + \frac{\partial u_i}{\partial x_3^r} dx_3^r \quad (9)$$

Substituindo (9) em (8)

$$dx_i = dx_i^r + \frac{\partial u_i}{\partial x_1^r} dx_1^r + \frac{\partial u_i}{\partial x_2^r} dx_2^r + \frac{\partial u_i}{\partial x_3^r} dx_3^r \quad (10)$$

que em forma matricial:

$$\begin{bmatrix} dx_1 \\ dx_2 \\ dx_2 \end{bmatrix} = \begin{bmatrix} dx_1^r \\ dx_2^r \\ dx_2^r \end{bmatrix} + \begin{bmatrix} \frac{\partial u_1}{\partial x_1^r} & \frac{\partial u_1}{\partial x_2^r} & \frac{\partial u_1}{\partial x_3^r} \\ \frac{\partial u_2}{\partial x_1^r} & \frac{\partial u_2}{\partial x_2^r} & \frac{\partial u_2}{\partial x_3^r} \\ \frac{\partial u_3}{\partial x_1^r} & \frac{\partial u_3}{\partial x_2^r} & \frac{\partial u_3}{\partial x_3^r} \end{bmatrix} \begin{bmatrix} dx_1^r \\ dx_2^r \\ dx_2^r \end{bmatrix} \quad (11)$$

ou

$$\begin{bmatrix} dx_1 \\ dx_2 \\ dx_2 \end{bmatrix} = \begin{bmatrix} 1 + \frac{\partial u_1}{\partial x_1^r} & \frac{\partial u_1}{\partial x_2^r} & \frac{\partial u_1}{\partial x_3^r} \\ \frac{\partial u_2}{\partial x_1^r} & 1 + \frac{\partial u_2}{\partial x_2^r} & \frac{\partial u_2}{\partial x_3^r} \\ \frac{\partial u_3}{\partial x_1^r} & \frac{\partial u_3}{\partial x_2^r} & 1 + \frac{\partial u_3}{\partial x_3^r} \end{bmatrix} \begin{bmatrix} dx_1^r \\ dx_2^r \\ dx_2^r \end{bmatrix} \quad (12)$$

São definidos:

Gradiente dos deslocamentos:

$$\nabla \mathbf{u} = \begin{bmatrix} \frac{\partial u_1}{\partial x_1^r} & \frac{\partial u_1}{\partial x_2^r} & \frac{\partial u_1}{\partial x_3^r} \\ \frac{\partial u_2}{\partial x_1^r} & \frac{\partial u_2}{\partial x_2^r} & \frac{\partial u_2}{\partial x_3^r} \\ \frac{\partial u_3}{\partial x_1^r} & \frac{\partial u_3}{\partial x_2^r} & \frac{\partial u_3}{\partial x_3^r} \end{bmatrix} \quad (13)$$

Gradiente das deformações:

$$\mathbf{F} = \begin{bmatrix} 1 + \frac{\partial u_1}{\partial x_1^r} & \frac{\partial u_1}{\partial x_2^r} & \frac{\partial u_1}{\partial x_3^r} \\ \frac{\partial u_2}{\partial x_1^r} & 1 + \frac{\partial u_2}{\partial x_2^r} & \frac{\partial u_2}{\partial x_3^r} \\ \frac{\partial u_3}{\partial x_1^r} & \frac{\partial u_3}{\partial x_2^r} & 1 + \frac{\partial u_3}{\partial x_3^r} \end{bmatrix} = \mathbf{I} + \nabla \mathbf{u} \quad (14)$$

Logo, pode-se escrever que:

$$d\mathbf{x} = d\mathbf{x}^r + \nabla \mathbf{u} d\mathbf{x}^r \quad (15)$$

e

$$d\mathbf{x} = (\mathbf{I} + \nabla \mathbf{u}) d\mathbf{x}^r = \mathbf{F} d\mathbf{x}^r \quad (16)$$

Alternativamente, o gradiente das deformações pode ser definido como:

$$\mathbf{u} = \mathbf{x} - \mathbf{x}^r \Rightarrow \mathbf{x} = \mathbf{x}^r + \mathbf{u}$$

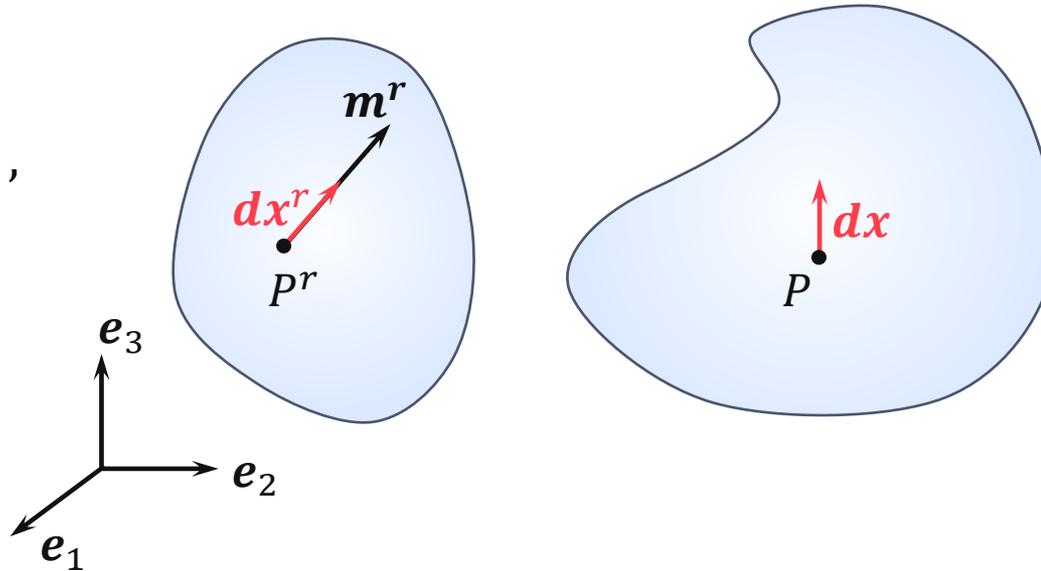
Em componentes: $x_i = u_i + x_i^r$

$$\frac{\partial x_i}{\partial x_j^r} = \frac{\partial x_i^r}{\partial x_j^r} + \frac{\partial u_i}{\partial x_j^r}$$

delta de Kronecker

$$\mathbf{F} = \begin{bmatrix} \frac{\partial x_1}{\partial x_1^r} & \frac{\partial x_1}{\partial x_2^r} & \frac{\partial x_1}{\partial x_3^r} \\ \frac{\partial x_2}{\partial x_1^r} & \frac{\partial x_2}{\partial x_2^r} & \frac{\partial x_2}{\partial x_3^r} \\ \frac{\partial x_3}{\partial x_1^r} & \frac{\partial x_3}{\partial x_2^r} & \frac{\partial x_3}{\partial x_3^r} \end{bmatrix} \quad (17)$$

$$\mathbf{m}^r = \frac{d\mathbf{x}^r}{\|d\mathbf{x}^r\|},$$
$$\|\mathbf{m}^r\| = 1$$



Fibras infinitesimais nas configurações deformada e indeformada

Pode-se escrever:

$$ds^r = \|d\mathbf{x}^r\| = (d\mathbf{x}^r \cdot d\mathbf{x}^r)^{1/2} = \left((dx_1^r)^2 + (dx_2^r)^2 + (dx_3^r)^2 \right)^{1/2} \quad (18)$$

$$ds = \|d\mathbf{x}\| = \left((dx_1)^2 + (dx_2)^2 + (dx_3)^2 \right)^{1/2} \quad (19)$$

Define-se alongamento linear por:

$$\varepsilon_l = \frac{ds - ds^r}{ds^r} = \frac{ds}{ds^r} - 1 \quad (20)$$

e o estiramento por:

$$\lambda = \frac{ds}{ds^r} \quad (21)$$

Portanto:

$$\varepsilon_l = \lambda - 1 \quad (22)$$

Tem-se:

$$ds = \|\mathbf{dx}\| = \sqrt{\mathbf{dx} \cdot \mathbf{dx}} = \sqrt{\mathbf{F}d\mathbf{x}^r \cdot \mathbf{F}d\mathbf{x}^r} \quad (23)$$

Define-se o transposto de um operador A como o operador A^T que verifica:

$$\mathbf{a} \cdot A \mathbf{b} = \mathbf{b} \cdot A^T \mathbf{a} \quad (24)$$

Considerando a relação (24) em (23), temos:

$$ds = \sqrt{\underbrace{\mathbf{F}d\mathbf{x}^r \cdot \mathbf{F}d\mathbf{x}^r}_v} = \sqrt{d\mathbf{x}^r \cdot \mathbf{F}^T \mathbf{v}} = \sqrt{d\mathbf{x}^r \cdot \mathbf{F}^T \mathbf{F}d\mathbf{x}^r} \quad (25)$$

Resulta:

$$\varepsilon_l = \frac{ds}{ds^r} - 1 = \frac{\sqrt{d\mathbf{x}^r \cdot \mathbf{F}^T \mathbf{F}d\mathbf{x}^r}}{\sqrt{d\mathbf{x}^r \cdot d\mathbf{x}^r}} - 1 \quad (26)$$

e como

$$d\mathbf{x}^r = ds^r \mathbf{m}^r \quad (27)$$

$$\|\mathbf{m}^r\| = 1$$

Resulta:

$$\varepsilon_l = \frac{ds}{ds^r} - 1 = \frac{ds^r \sqrt{\mathbf{m}^r \mathbf{F}^T \mathbf{F} \mathbf{m}^r}}{ds^r \sqrt{\mathbf{m}^r \cdot \mathbf{m}^r}} - 1 \quad (28)$$

ou

$$\varepsilon_l = \sqrt{\mathbf{m}^r \cdot \mathbf{F}^T \mathbf{F} \mathbf{m}^r} - 1 = \sqrt{\mathbf{m}^{rT} \mathbf{F}^T \mathbf{F} \mathbf{m}^r} - 1 \quad (29)$$

Alongamento linear para uma fibra infinitesimal que tem direção dada pelo versor \mathbf{m}^r na configuração de referência.

Tem-se:

$$\mathbf{F}^T \mathbf{F} = (\mathbf{I} + \nabla \mathbf{u})^T (\mathbf{I} + \nabla \mathbf{u}) = \mathbf{I} + \nabla \mathbf{u} + \nabla \mathbf{u}^T + \nabla \mathbf{u}^T \nabla \mathbf{u} \quad (30)$$

Quando se tem deslocamentos infinitesimais, pode-se desprezar $\nabla u_{ij}^T \nabla u_{ij} \frac{\partial u_i}{\partial x_j^r} \frac{\partial u_j}{\partial x_i^r}$ em relação a ∇u_{ij} e ∇u_{ij}^T , onde:

$$\begin{aligned} \nabla u_{ij}^T \nabla u_{ij} &= \frac{\partial u_k}{\partial x_i^r} \frac{\partial u_k}{\partial x_j^r} = \frac{\partial u_1}{\partial x_i^r} \frac{\partial u_1}{\partial x_j^r} + \frac{\partial u_2}{\partial x_i^r} \frac{\partial u_2}{\partial x_j^r} + \frac{\partial u_3}{\partial x_i^r} \frac{\partial u_3}{\partial x_j^r} \\ \nabla u_{ij} &= \frac{\partial u_i}{\partial x_j^r} \text{ e } \nabla u_{ij}^T = \frac{\partial u_j}{\partial x_i^r} \end{aligned}$$

Portanto,

$$\mathbf{F}^T \mathbf{F} = \mathbf{I} + \nabla \mathbf{u} + \nabla \mathbf{u}^T \quad (31)$$

Define-se então o tensor das deformações infinitesimais como:

$$\mathbf{E} = \frac{1}{2} (\nabla \mathbf{u} + \nabla \mathbf{u}^T) \quad (32)$$

Em notação indicial:

$$E_{ij} = \frac{1}{2} \left(\frac{\partial u_i}{\partial x_j^r} + \frac{\partial u_j}{\partial x_i^r} \right)$$

Em componentes:

$$\mathbf{E} = \begin{bmatrix} \frac{\partial u_1}{\partial x_1^r} & \frac{1}{2} \left(\frac{\partial u_1}{\partial x_2^r} + \frac{\partial u_2}{\partial x_1^r} \right) & \frac{1}{2} \left(\frac{\partial u_1}{\partial x_3^r} + \frac{\partial u_3}{\partial x_1^r} \right) \\ \frac{1}{2} \left(\frac{\partial u_1}{\partial x_2^r} + \frac{\partial u_2}{\partial x_1^r} \right) & \frac{\partial u_2}{\partial x_2^r} & \frac{1}{2} \left(\frac{\partial u_2}{\partial x_3^r} + \frac{\partial u_3}{\partial x_2^r} \right) \\ \frac{1}{2} \left(\frac{\partial u_1}{\partial x_3^r} + \frac{\partial u_3}{\partial x_1^r} \right) & \frac{1}{2} \left(\frac{\partial u_2}{\partial x_3^r} + \frac{\partial u_3}{\partial x_2^r} \right) & \frac{\partial u_3}{\partial x_3^r} \end{bmatrix} \quad (33)$$

$$\mathbf{E} = \mathbf{E}^T \quad (34)$$

De (31): $\mathbf{F}^T \mathbf{F} = \mathbf{I} + 2\mathbf{E}$

e a equação (29) pode ser reescrita como:

$$\varepsilon_l = \sqrt{\mathbf{m}^{rT} (\mathbf{I} + 2\mathbf{E}) \mathbf{m}^r} - 1 = \left(1 + 2\mathbf{m}^{rT} \mathbf{E} \mathbf{m}^r \right)^{1/2} - 1 \quad (35)$$

$$\mathbf{m}^{rT} \mathbf{E} \mathbf{m}^r = \sum_{i=1}^3 \sum_{j=1}^3 \frac{\partial u_i}{\partial x_j^r} m_i^r m_j^r \quad (36)$$

Considere a identidade matemática:

$$(1 + \delta)^s = 1 + s\delta + \frac{s(s-1)}{2}\delta^2 + \dots \quad (37)$$

Substituindo $\delta = 2\mathbf{m}^{rT} \mathbf{E} \mathbf{m}^r$ e $s = 1/2$, obtém-se:

$$(1 + 2\mathbf{m}^{rT} \mathbf{E} \mathbf{m}^r)^{1/2} = 1 + \mathbf{m}^{rT} \mathbf{E} \mathbf{m}^r + \text{termos de alta ordem em } \mathbf{m}^{rT} \mathbf{E} \mathbf{m}^r \quad (38)$$

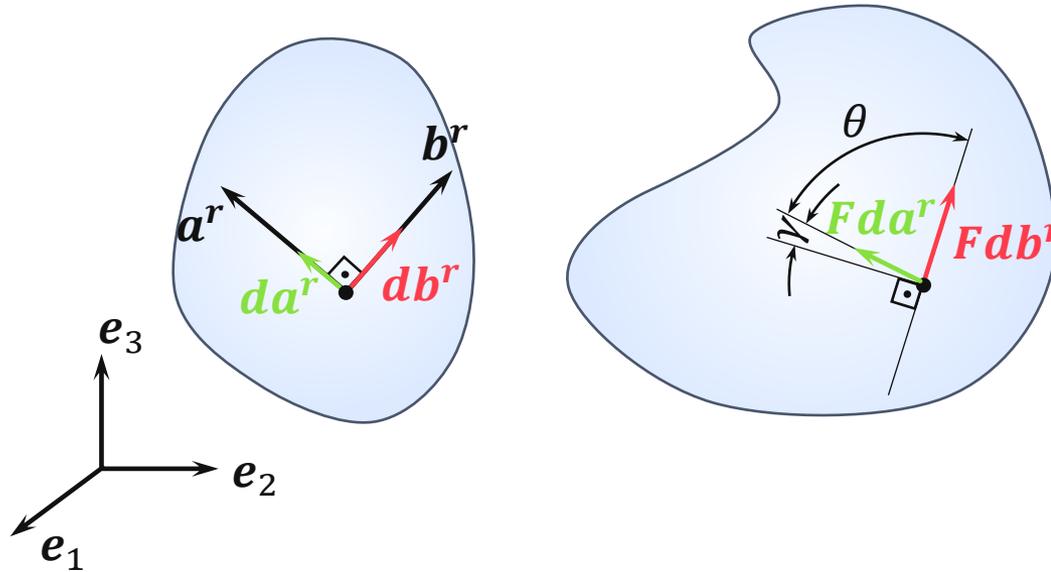
Desprezando termos de alta ordem em $\frac{\partial u_i}{\partial x_j^r}$:

$$(1 + 2\mathbf{m}^{rT} \mathbf{E} \mathbf{m}^r)^{1/2} = 1 + \mathbf{m}^{rT} \mathbf{E} \mathbf{m}^r \quad (39)$$

De (35) resulta:

$$\varepsilon_l(\mathbf{m}) = \mathbf{m}^{rT} \mathbf{E} \mathbf{m}^r = \mathbf{m}^r \cdot \mathbf{E} \mathbf{m}^r \quad (40)$$

Alongamento linear para uma fibra infinitesimal \mathbf{m}^r considerando deformações infinitesimais.



Fibras infinitesimais nas configurações deformada e indeformada.

Pode-se escrever, considerando a definição de produto escalar:

$$F da^r \cdot F db^r = \|F da^r\| \|F db^r\| \cos \theta \quad (41)$$

e

$$\cos \theta = \text{sen } \gamma = \frac{F da^r \cdot F db^r}{\|F da^r\| \|F db^r\|} = \frac{da^r \cdot F^T F db^r}{\|F da^r\| \|F db^r\|} \quad (42)$$

Sabemos que:

$$\|F da^r\| = \sqrt{F da^r \cdot F da^r} \text{ e } \|F db^r\| = \sqrt{F db^r \cdot F db^r} \quad (43)$$
$$da^r = da^r a^r \text{ e } db^r = db^r b^r$$

Substituindo a equação (43) na equação (42):

$$\sin \gamma = \frac{da^r a^r \cdot F^T F db^r b^r}{da^r \sqrt{F a^r \cdot F a^r} db^r \sqrt{F b^r \cdot F b^r}} = \frac{a^r \cdot F^T F b^r}{\sqrt{F a^r \cdot F a^r} \sqrt{F b^r \cdot F b^r}} \quad (44)$$

que também pode ser escrita como:

$$\sin \gamma = \frac{a^{rT} F^T F b^r}{\sqrt{a^{rT} F^T F a^r} \sqrt{b^{rT} F^T F b^r}}$$

Lembrando que:

$$1 + \varepsilon_l(\mathbf{a}^r) = \sqrt{\mathbf{a}^{rT} \mathbf{F}^T \mathbf{F} \mathbf{a}^r} \quad e \quad 1 + \varepsilon_l(\mathbf{b}^r) = \sqrt{\mathbf{b}^{rT} \mathbf{F}^T \mathbf{F} \mathbf{b}^r} \quad (45)$$

podemos então também expressar a equação (44) que calcula a distorção entre duas fibras infinitesimais ($d\mathbf{a}^r$ e $d\mathbf{b}^r$), inicialmente ortogonais, cujas direções são definidas pelos versores \mathbf{a}^r e \mathbf{b}^r , da seguinte forma:

$$\sin \gamma(\mathbf{a}^r, \mathbf{b}^r) = \frac{\mathbf{a}^{rT} \mathbf{F}^T \mathbf{F} \mathbf{b}^r}{(1 + \varepsilon_l(\mathbf{a}^r))(1 + \varepsilon_l(\mathbf{b}^r))} \quad (46)$$

Para deformações infinitesimais resulta:

$$\sin \gamma = \gamma = \mathbf{a}^{rT} (\mathbf{I} + 2\mathbf{E}) \mathbf{b}^r = 2\mathbf{a}^{rT} \mathbf{E} \mathbf{b}^r + \mathbf{a}^{rT} \mathbf{b}^r$$

$$\gamma(\mathbf{a}^r, \mathbf{b}^r) = 2\mathbf{a}^{rT} \mathbf{E} \mathbf{b}^r$$

(47)

Distorção entre fibras infinitesimais ($d\mathbf{a}^r$ e $d\mathbf{b}^r$) considerando deformações infinitesimais.

Quadro resumido de alongamento linear e distorção

| | Deformações finitas | Deformações infinitesimais |
|---|---|---|
| Alongamento linear para fibra na direção dada por \mathbf{m}^r | $\varepsilon_l(\mathbf{m}^r) = \sqrt{\mathbf{m}^{rT} \mathbf{F}^T \mathbf{F} \mathbf{m}^r} - 1$ | $\varepsilon_l(\mathbf{m}^r) = \mathbf{m}^{rT} \mathbf{E} \mathbf{m}^r$ |
| Distorção de um par de fibras ortogonais definidas nas direções \mathbf{a}^r e \mathbf{b}^r | $\sin \gamma(\mathbf{a}^r, \mathbf{b}^r) = \frac{\mathbf{a}^{rT} \mathbf{F}^T \mathbf{F} \mathbf{b}^r}{(1 + \varepsilon_l(\mathbf{a}^r))(1 + \varepsilon_l(\mathbf{b}^r))}$ | $\gamma(\mathbf{a}^r, \mathbf{b}^r) = 2\mathbf{a}^{rT} \mathbf{E} \mathbf{b}^r$ |

Considerando:

$$[\mathbf{E}] = \begin{bmatrix} E_{11} & E_{12} & E_{13} \\ E_{21} & E_{22} & E_{23} \\ E_{31} & E_{32} & E_{33} \end{bmatrix} \quad (48)$$

Seja

$$\varepsilon_1 = \varepsilon_l(\mathbf{e}_1) = \mathbf{e}_1^T \mathbf{E} \mathbf{e}_1 \quad (49)$$

$$\varepsilon_1 = [1 \quad 0 \quad 0] \begin{bmatrix} E_{11} & E_{12} & E_{13} \\ E_{21} & E_{22} & E_{23} \\ E_{31} & E_{32} & E_{33} \end{bmatrix} \begin{bmatrix} 1 \\ 0 \\ 0 \end{bmatrix} \quad (50)$$

$$\boxed{\varepsilon_1 = E_{11}} \quad (51)$$

Analogamente:

$$\boxed{\begin{aligned} \varepsilon_2 &= E_{22} \\ \varepsilon_3 &= E_{33} \end{aligned}} \quad (52)$$

Seja

$$\gamma_{12} = \gamma(\mathbf{e}_1, \mathbf{e}_2) = 2\mathbf{e}_1^T \mathbf{E} \mathbf{e}_2 \quad (53)$$

$$\gamma_{12} = 2 \begin{bmatrix} 1 & 0 & 0 \end{bmatrix} \begin{bmatrix} E_{11} & E_{12} & E_{13} \\ E_{21} & E_{22} & E_{23} \\ E_{31} & E_{32} & E_{33} \end{bmatrix} \begin{bmatrix} 0 \\ 1 \\ 0 \end{bmatrix} \quad (54)$$

$$\boxed{\gamma_{12} = 2E_{12}} \quad (55)$$

Analogamente:

$$\boxed{\begin{aligned} \gamma_{13} &= 2E_{13} = 2E_{31} = \gamma_{31} \\ \gamma_{23} &= 2E_{23} = 2E_{32} = \gamma_{32} \end{aligned}} \quad (56)$$

- ▶ **BUCALEM, M. L.; BATHE, K. J. The mechanics of solids and structures: hierarchical modeling and the finite element solution, p.95–112. Heidelberg: Springer, 2011.**