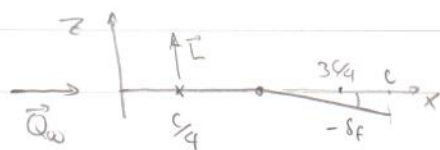


P5.3 Find the Hinge moment of the flapped air foil of Eq. (5.90)

$$\frac{dM_c}{dx} = \begin{cases} 0 & \text{for } 0 < x < k_c \\ -\delta_f & \text{for } k_c < x < c \end{cases}$$



from eqs. (5.94) and (5.96)

$$\alpha = 0 \Rightarrow \begin{cases} C_e = [2(\pi - \theta_k) + 2 \sin \theta_k] \delta_f \\ C_{m_{c/4}} = \left[ \frac{1}{4} \sin(2\theta_k) - \frac{1}{2} \sin \theta_k \right] \delta_f \end{cases}$$

where  $k_c = \frac{c}{2} (1 - \cos \theta_k) \Rightarrow \cos \theta_k = 1 - 2k$

The hinge moment: ( $C_{m_{k_c}}$ ) should be equal to the moment about the aerodynamic center, which does not depend on  $\alpha$  and where the Lift force acts — for this torque is transferred to the hinge point ( $k_c$ ) without any change — plus the moment of the lift force with respect to the hinge point:

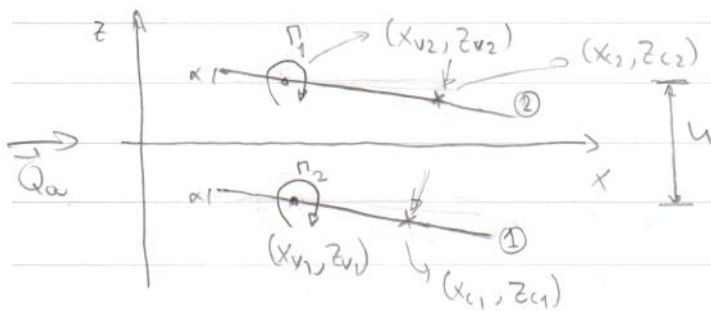
$$M_{k_c} = M_{c/4} + L \cdot \left( k_c - \frac{c}{4} \right)$$

$$C_{m_{k_c}} = C_{m_{c/4}} + \frac{C_e}{c} \left( k_c - \frac{c}{4} \right)$$

$$C_{m_{k_c}} = C_{m_{c/4}} + C_e \left( k - \frac{1}{4} \right)$$

$$C_{m_{k_c}} = \left\{ \frac{1}{4} \sin(2\theta_k) - \frac{1}{2} \sin \theta_k + \left( k - \frac{1}{4} \right) [2(\pi - \theta_k) + 2 \sin \theta_k] \right\} \delta_f$$

P.5.5.  $Q_{\infty}, \alpha \Rightarrow$  Biplane



$$U = \frac{\Gamma}{2\pi} \frac{(z - z_0)}{[(z - z_0)^2 + (x - x_0)^2]}$$

$$W = \frac{-\Gamma}{2\pi} \frac{(x - x_0)}{[(z - z_0)^2 + (x - x_0)^2]}$$

Vortex points: (1)  $\Rightarrow (x_{v1}, z_{v1}) = (0, -h/2)$

(2)  $\Rightarrow (x_{v2}, z_{v2}) = (0, +h/2)$

Collocation Points: (1)  $\Rightarrow (x_{c1}, z_{c1}) = \left( \frac{c \cos \alpha}{2}, -\frac{(h + c \sin \alpha)}{2} \right)$

(2)  $\Rightarrow (x_{c2}, z_{c2}) = \left( \frac{c \cos \alpha}{2}, \frac{(h - c \sin \alpha)}{2} \right)$

$$\hat{n}_1, \hat{n}_2 = \sin \alpha \hat{i} + \cos \alpha \hat{k}$$

Self-induced velocities at the collocation points are normal to each chord:

$$\begin{cases} U_{111} = -\frac{\Gamma_1}{\pi c} \end{cases}$$

$$\begin{cases} U_{222} = -\frac{\Gamma_2}{\pi c} \end{cases}$$

Mutually induced velocities are given by: (at the collocation points)

$$U_{12} = \frac{\Gamma_2}{2\pi} \frac{(h - \frac{c \sin \alpha}{2})}{\left[ \left( \frac{h - \frac{c \sin \alpha}{2} \right)^2 + \frac{c^2 \cos^2 \alpha}{4} \right]} = \frac{\Gamma_2}{2\pi} \frac{2h - c \sin \alpha}{2 \left[ h^2 - ch \sin \alpha + \frac{c^2}{4} \right]}$$

$$W_{12} = -\frac{\Gamma_2}{2\pi} \frac{c \cos \alpha}{2 \left[ h^2 - ch \sin \alpha + \frac{c^2}{4} \right]}$$

$$U_{n12} = U_{12} \sin \alpha + W_{12} \cos \alpha$$

$$U_{n12} = \frac{\sqrt{2}}{4\pi} \left[ \frac{(2h - c \sin \alpha) \sin \alpha}{(h^2 - ch \sin \alpha + c^2/4)} - \frac{c \cos^2 \alpha}{(h^2 - ch \sin \alpha + c^2/4)} \right]$$

$$U_{n12} = \frac{\sqrt{2}}{4\pi} \frac{(2h \sin \alpha - c)}{(h^2 - ch \sin \alpha + c^2/4)} \quad \checkmark$$

Similarly, we can compute  $U_{n21}$

$$U_{21} = \frac{\sqrt{2}}{2\pi} \frac{-(h + \frac{c \sin \alpha}{2})}{\left[ (h + \frac{c \sin \alpha}{2})^2 + \frac{c^2 \cos^2 \alpha}{4} \right]} = -\frac{\sqrt{2}}{4\pi} \frac{(2h + c \sin \alpha)}{(h^2 + ch \sin \alpha + c^2/4)}$$

$$W_{21} = -\frac{\sqrt{2}}{4\pi} \frac{c \cos \alpha}{(h^2 + ch \sin \alpha + c^2/4)} \quad \checkmark$$

$$U_{n21} = U_{21} \sin \alpha + W_{21} \cos \alpha$$

$$U_{n21} = \frac{\sqrt{2}}{4\pi} \left[ \frac{-(2h + c \sin \alpha) \sin \alpha - c \cos \alpha \cos \alpha}{(h^2 + ch \sin \alpha + c^2/4)} \right]$$

$$U_{n21} = +\frac{\sqrt{2}}{4\pi} \frac{(-2h \sin \alpha - c)}{(h^2 + ch \sin \alpha + c^2/4)} = -\frac{\sqrt{2}}{4\pi} \frac{(2h \sin \alpha + c)}{(h^2 + ch \sin \alpha + c^2/4)} \quad \checkmark$$

The boundary conditions at the collocation points comprise the set:

$$\begin{cases} U_{n11} + U_{n21} + Q_{00} \sin \alpha = 0 \\ U_{n22} + U_{n12} + Q_{00} \sin \alpha = 0 \end{cases}$$

$$\left\{ \begin{array}{l} -\frac{\Gamma_1}{\pi c} - \frac{(c + 2h \sin \alpha)}{\pi(4h^2 + 4ch \sin \alpha + c^2)} \Gamma_2 = -Q_{\infty} \sin \alpha \\ \frac{(2h \sin \alpha - c)}{\pi(4h^2 - 4ch \sin \alpha + c^2)} \Gamma_1 - \frac{\Gamma_2}{\pi c} = -Q_{\infty} \sin \alpha \end{array} \right.$$

On having "Mathematica" solve this set, we get for the circulations: <sup>(+)</sup>

$$\Gamma_1 = \pi Q_{\infty} \sin(\alpha) c \frac{[8h^3 + 2c^2 h \cos(2\alpha) + c(c^2 - 4h^2) \sin(\alpha)]}{h[c^2 + 8h^2 + 3c^2 \cos(2\alpha)]}$$

$$\Gamma_2 = -\pi Q_{\infty} \sin(\alpha) c \frac{[8h^3 + 2c^2 h \cos(2\alpha) - c(c^2 - 4h^2) \sin(\alpha)]}{h[c^2 + 8h^2 + 3c^2 \cos(2\alpha)]}$$

And, on accounting for the fact that  $\alpha \ll 1$ , it implies the following assumptions:

$$\left. \begin{array}{l} \sin \alpha \approx \alpha \\ \cos \alpha \approx 1 \end{array} \right\} \Rightarrow \begin{array}{l} \sin^2 \alpha \approx \alpha^2 \rightarrow 0, \sin^3 \alpha \approx 0 \\ \cos(2\alpha) = 1 - 2\sin^2 \alpha = 2\cos^2 \alpha - 1 \approx 1 \end{array}$$

which lead to the following small disturbance expressions for the circulations:

$$\Gamma_1 \approx \pi \alpha Q_{\infty} c \frac{(c^2 + 4h^2)}{2(c^2 + 2h^2)}$$

$$\Gamma_2 \approx \pi \alpha Q_{\infty} c \frac{(c^2 + 4h^2)}{2(c^2 + 2h^2)}$$

Having found the sdt values for the circulations, it is easy to get the velocities each vortex induces on the other; with the



normal direction, which in this case is the  $x$  direction:

$$U_{1v2v} = \frac{\Gamma_1}{2\pi h} \approx Q_{\infty} \alpha c \frac{(c^2 + 4h^2)}{4h(c^2 + 2h^2)}$$

$$U_{2v1v} = \frac{-\Gamma_2}{2\pi h} \approx -Q_{\infty} \alpha c \frac{(c^2 + 4h^2)}{4h(c^2 + 2h^2)}$$

On substituting these results into the generalized form of the Kutta - Joukowski theorem, we get:

$$L = \rho Q_{\infty} \Gamma \left( 1 + \frac{\vec{Q}_{\infty} \cdot \vec{a}_T}{Q_{\infty}^2} \right), \text{ where } \vec{Q}_{\infty} \cdot \vec{a}_T = U_{1v2v}$$

$$L_1 = \rho Q_{\infty} \alpha c \frac{(c^2 + 4h^2)}{(c^2 + 2h^2)} \left[ \frac{-\alpha c (c^2 + 4h^2)}{8h(c^2 + 2h^2)} + \frac{Q_{\infty}}{2} \right]$$

$$L_2 = \rho Q_{\infty} \alpha c \frac{(c^2 + 4h^2)}{(c^2 + 2h^2)} \left[ \frac{+\alpha c (c^2 + 4h^2)}{8h(c^2 + 2h^2)} + \frac{Q_{\infty}}{2} \right]$$

$$L_T = L_1 + L_2 = \rho Q_{\infty}^2 \alpha c \frac{(c^2 + 4h^2)}{(c^2 + 2h^2)}$$

It is worth noting that the lift for a single flat plate is given by:  $L_{FP} = \rho Q_{\infty}^2 \alpha c$ ; and the ratio  $L_T/L_{FP}$  yields

$$\frac{L_T}{L_{FP}} = 2 \frac{c^2}{c^2 + 2h^2}$$

which implies that the influence each plate exerts on one another lessens the total lift from what it could be, provided that the plates are further apart:  $h \rightarrow \infty$ .