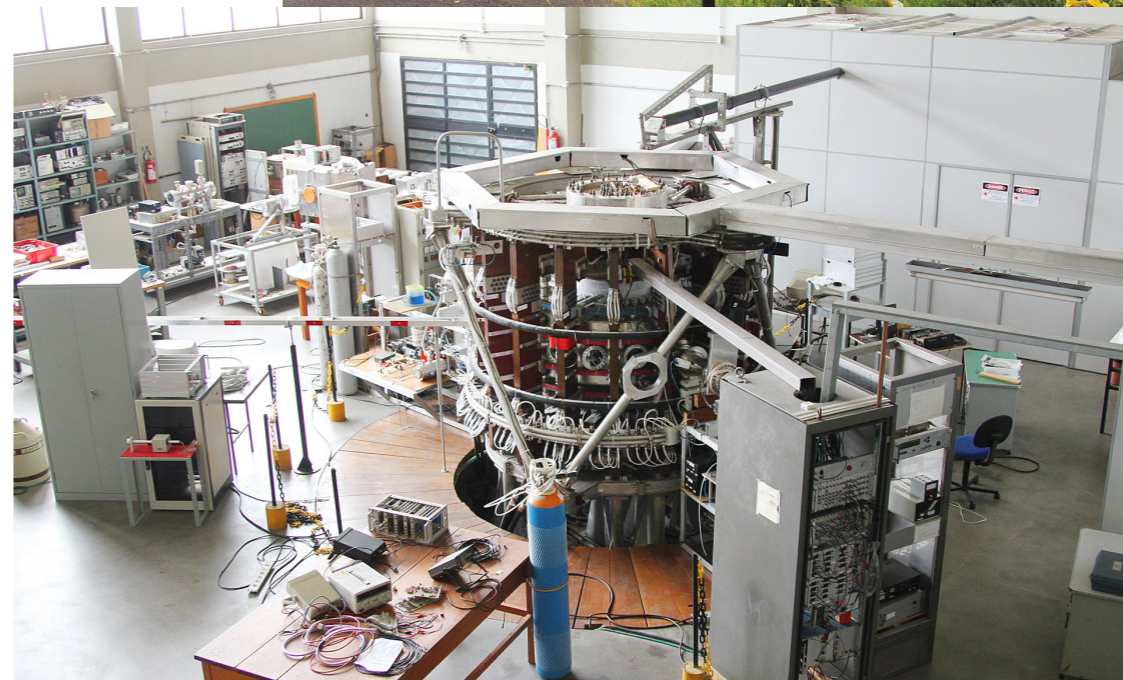


PGF5112 - Plasma Physics I

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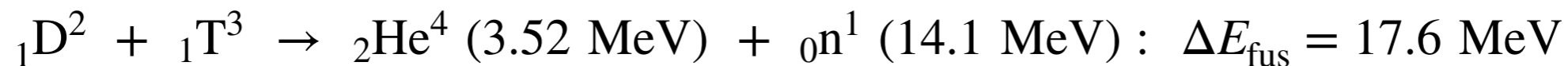
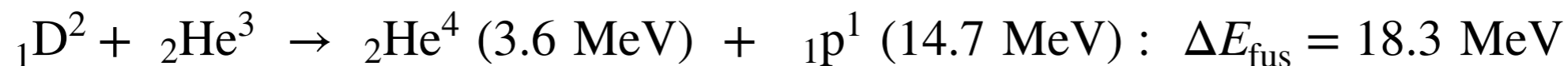
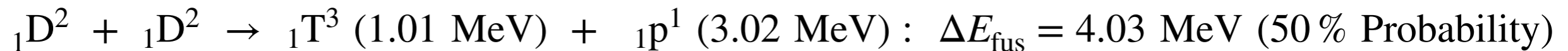
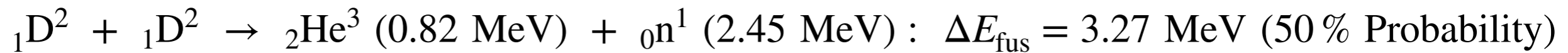


- **Nuclear fusion and tokamak physics**
 - *Nuclear fusion reactions*
 - *Thermonuclear fusion*
 - *Breakeven and the Lawson criterion for ignition*
 - *Scaling laws*

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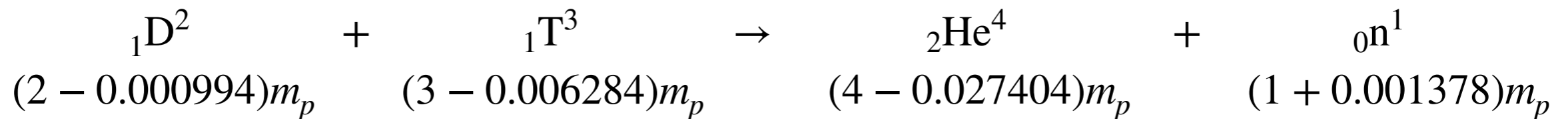
Nuclear fusion reactions

- Among nuclear fusion reactions, the exothermic are the ones of interest



- The energies given here are the kinetic energies of the reaction products
- By far, the most promising reactions are the D-T and D-He³

- The mass-energy balance from the mass deficit δm in the reaction below

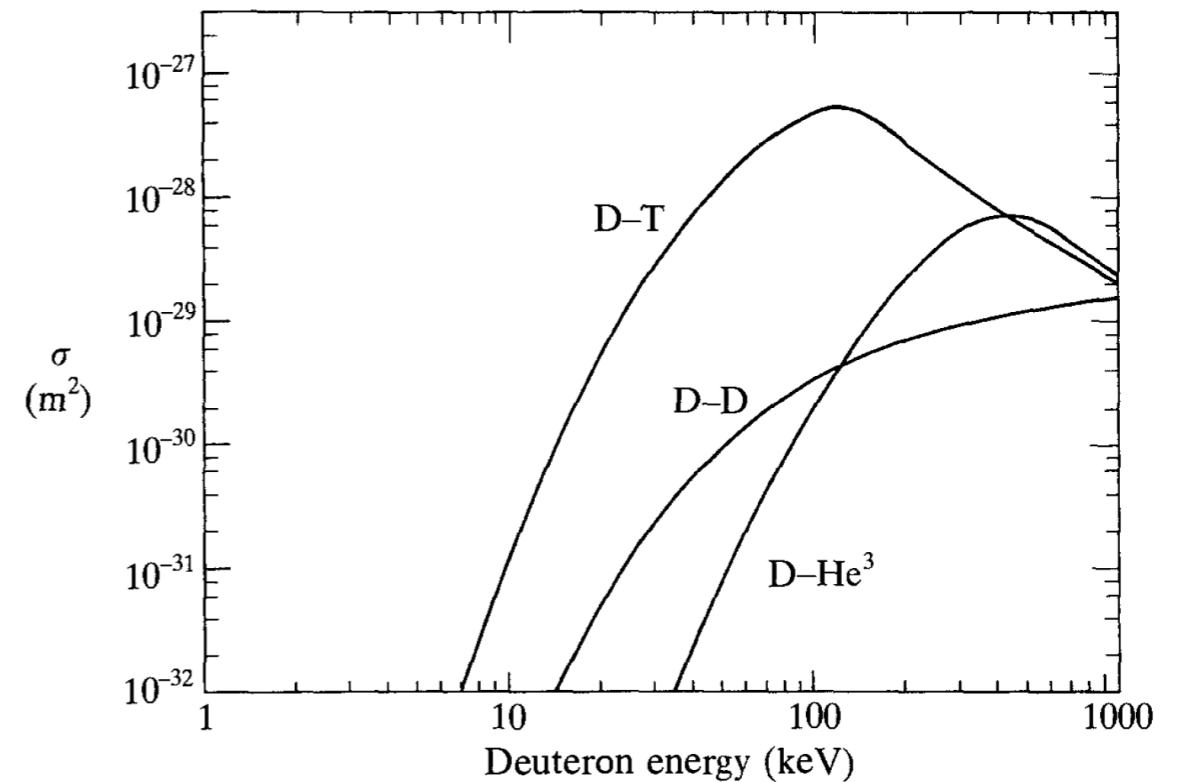
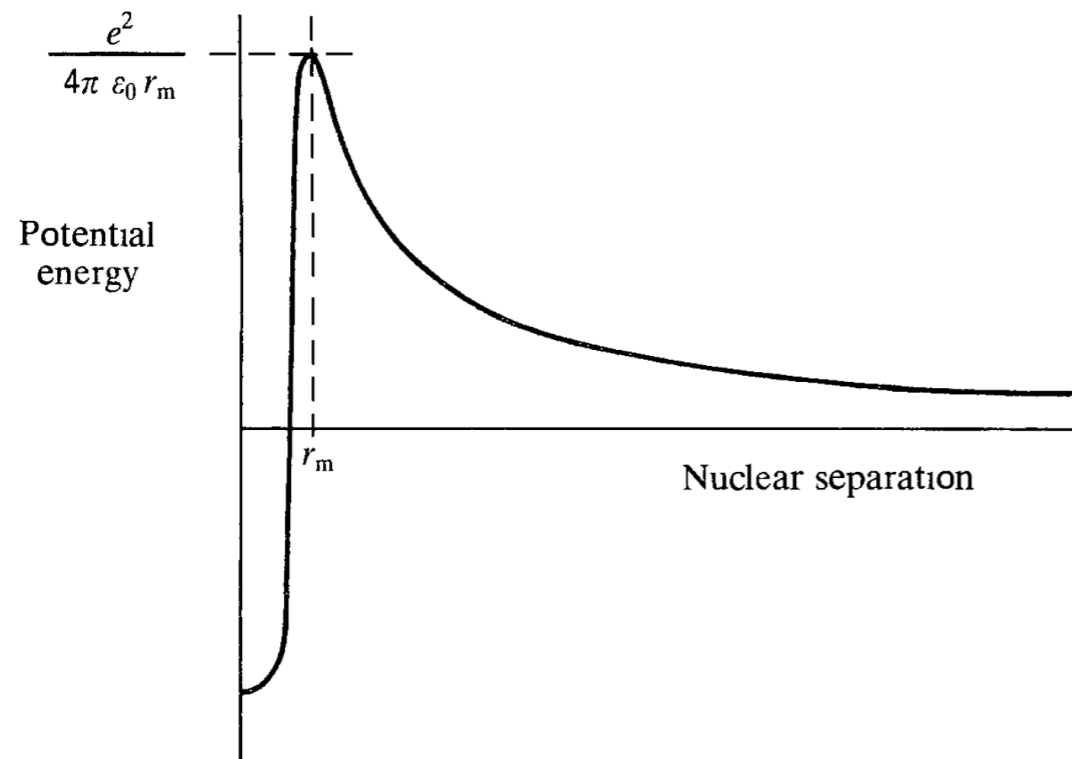


Here, $\delta m = 0.01875 m_p$ with $m_p = 1.6726 \times 10^{-27} \text{ kg}$ being the proton mass

$$\Delta E_{\text{fus}} = \delta m c^2 = 0.01875 \times 1.6726 \times 10^{-27} \times (2.9979 \times 10^8)^2 = 2.8186 \times 10^{-12} \text{ J} = 17.59 \text{ MeV}$$

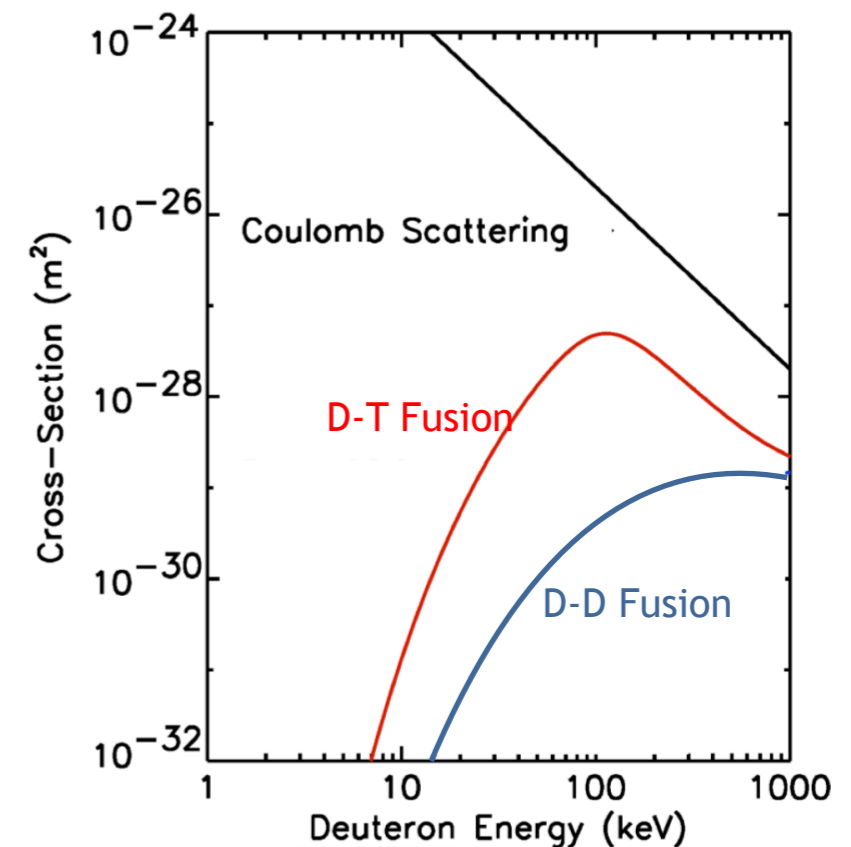
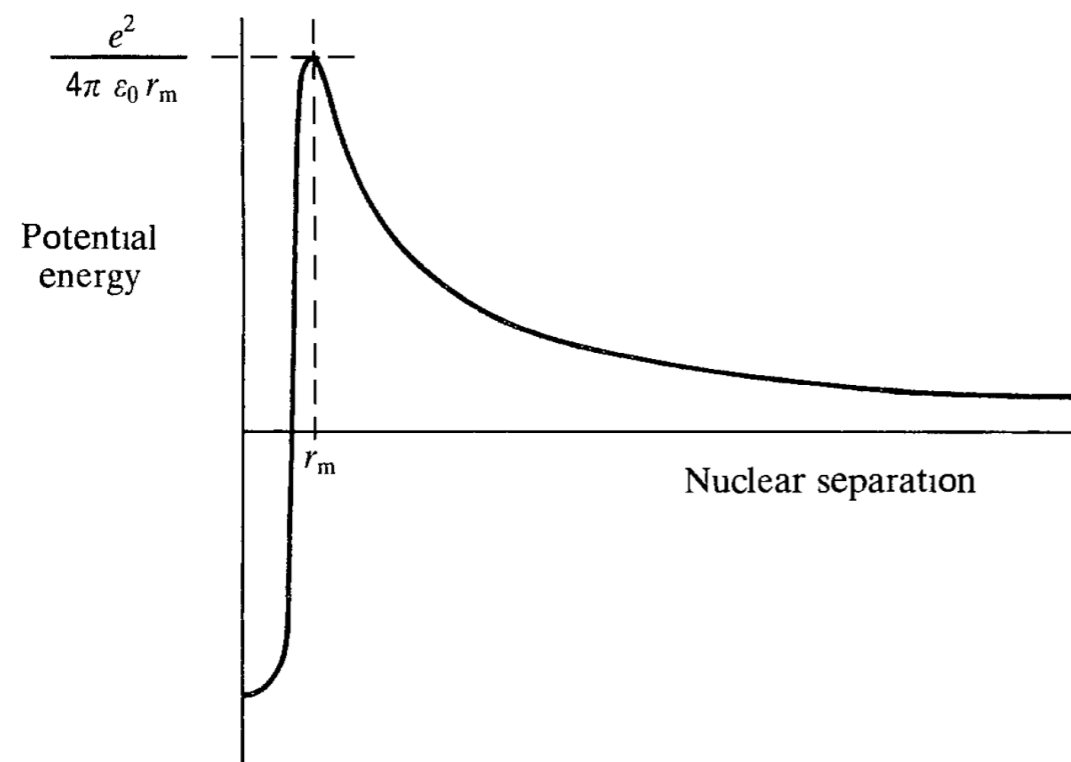
Nuclear fusion reactions

- Among the nuclear fusion reactions just mentioned, the D-T reaction is the one that has the largest cross section at lower energies
 - Quantum tunneling allows fusion to occur at significantly lower energies



Nuclear fusion reactions

- Among the nuclear fusion reactions just mentioned, the D-T reaction is the one that has the largest cross section at lower energies
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- The cross section of a D-T reaction is, for an ion average energy of 10 keV, about 10⁷ time smaller than that associated with a Coulomb scattering

- **Nuclear fusion and tokamak physics**

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Thermonuclear fusion

- **The most promising approach to fuse D and T is by heating a mixture of these to high enough temperature**

- *Particles in the velocity distribution tail can undergo fusion reactions*

- **Let's calculate the D-T fusion reaction rate,**

$$R_{DT} = \int_{v_D} \int_{v_T} \sigma_{DT} (|\mathbf{v}_D - \mathbf{v}_T|) |\mathbf{v}_D - \mathbf{v}_T| f_D(v_D) f_T(v_T) d^3v_D d^3v_T$$

- **In addition, let's suppose that D and T have a Maxwellian distribution**

$$f_j(v_j) = n_j \left(\frac{m_j}{2\pi k_B T} \right)^{3/2} \exp \left(-\frac{mv_j^2}{2k_B T} \right)$$

Thermonuclear fusion

- By writing

$$u = |\mathbf{v}_D - \mathbf{v}_T| \quad (\text{relative velocity})$$

$$\mu = \frac{m_D + m_T}{m_D m_T} \quad (\text{reduced mass})$$

$$\text{and} \quad V = \frac{v_D + v_T}{2}$$

the reaction rate can be rewritten as

$$R_{DT} = n_D n_T \langle \sigma u \rangle_{DT} = n_D n_T \frac{(m_D m_T)^{3/2}}{(2\pi k_B T)^3} \int_u \int_V \exp \left[-\frac{m_D + m_T}{2k_B T} \left(V + \frac{(m_D - m_T)u}{2(m_D + m_T)} \right)^2 \right] \times \\ \times \sigma_{DT}(u) u \exp \left(-\frac{\mu u^2}{2k_B T} \right) d^3 V d^3 u$$

- The integral in V can be carried out and results in

$$R_{DT} = 4\pi n_D n_T \left(\frac{\mu}{2\pi k_B T} \right)^{3/2} \int \sigma_{DT}(u) u^3 \exp \left(-\frac{\mu u^2}{2k_B T} \right) d^3 u$$

Thermonuclear fusion

- Cross sections measured in laboratory experiments are usually given in terms of the energy of the projectile particles. Therefore, taking D as the projectile particle (we could have chosen T without any problem), and defining

$$\epsilon = \frac{1}{2} m_D u^2$$

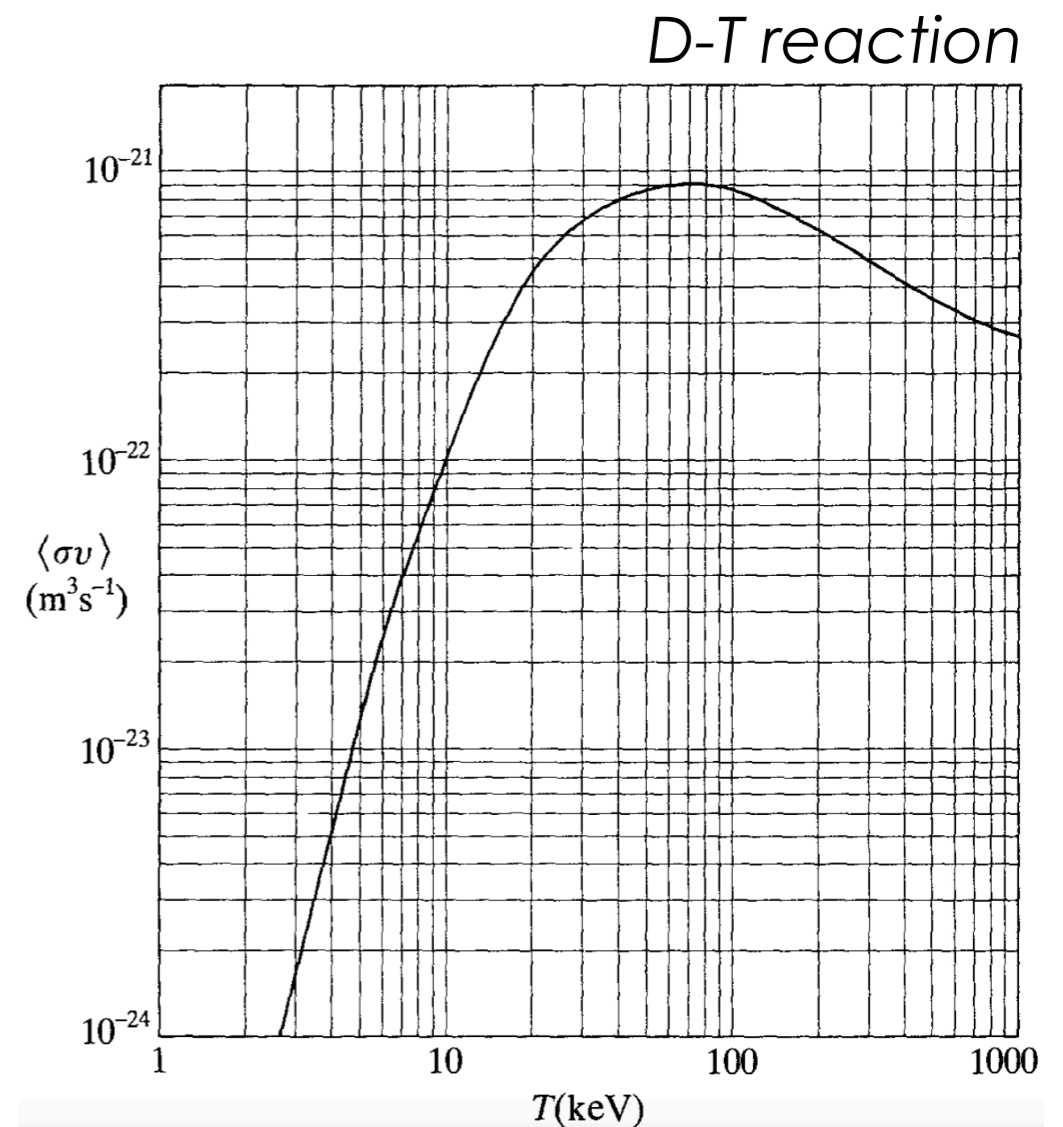
allows us to write the reaction rate as

$$R_{DT} = n_D n_T \langle \sigma u \rangle_{DT}$$

with

$$\langle \sigma u \rangle_{DT} = \sqrt{\frac{8}{\pi}} \frac{1}{m_D^2} \left(\frac{\mu}{k_B T} \right)^{3/2} \times \int_0^{\infty} \sigma_{DT}(\epsilon) \epsilon \exp\left(-\frac{\mu \epsilon}{m_D k_B T}\right) d\epsilon$$

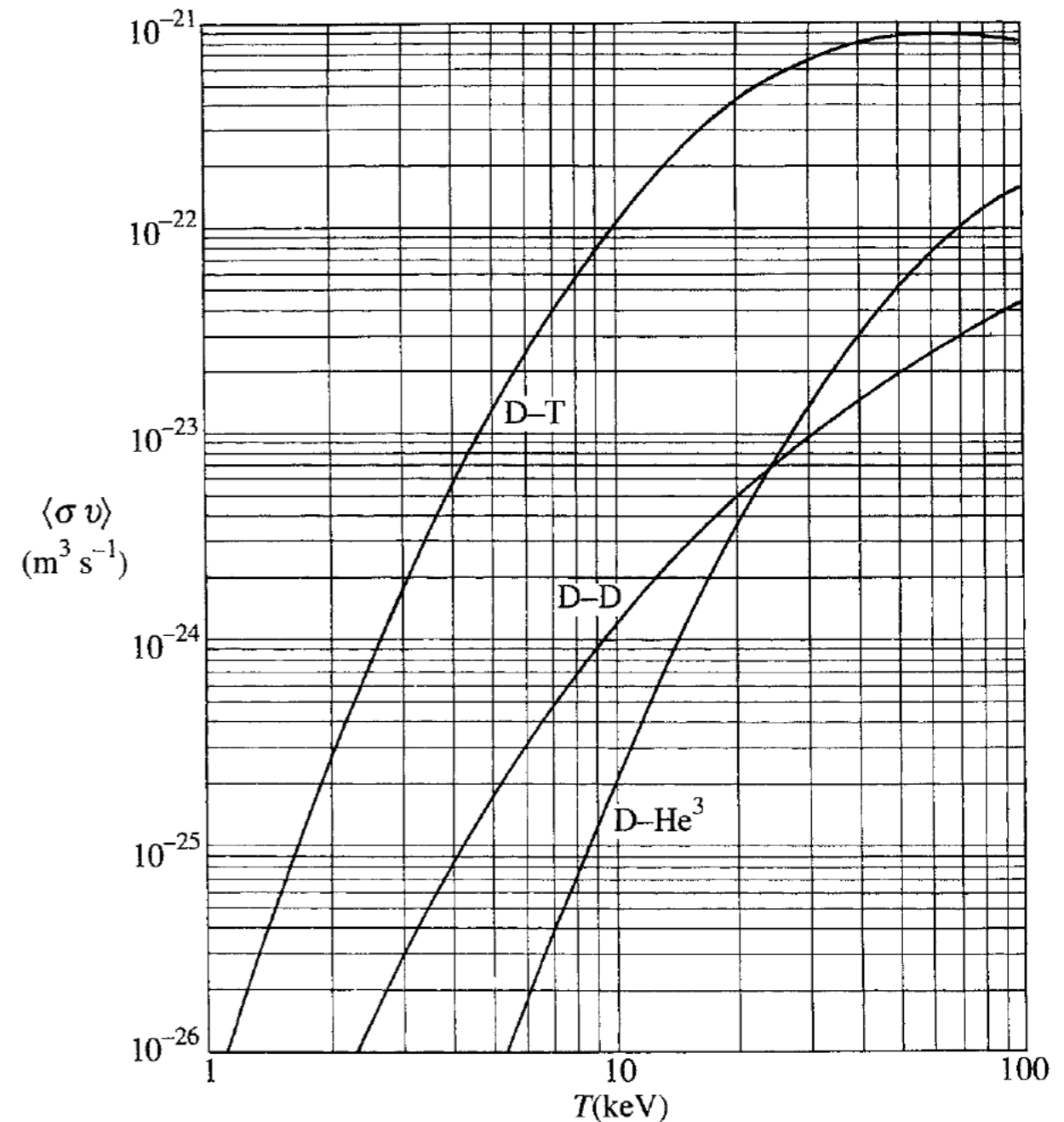
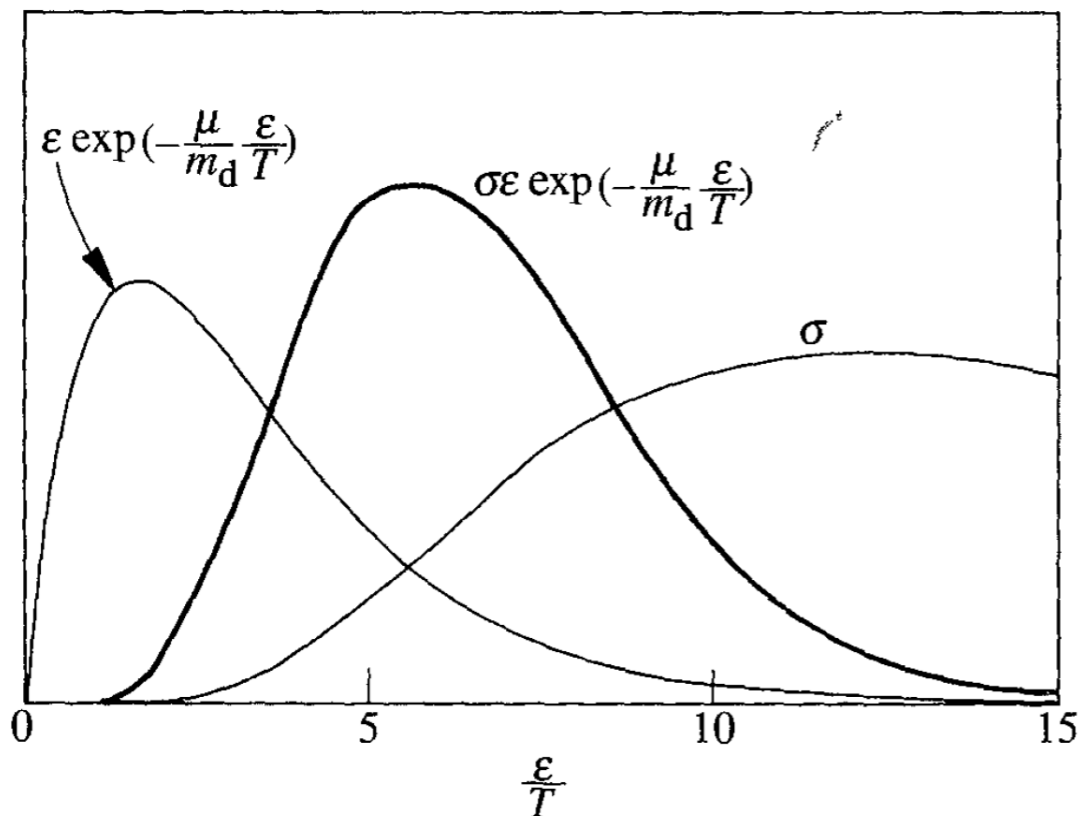
- For a given ion density the maximum rate is achieved for $n_D = n_T$



Thermonuclear fusion

- The $\langle \sigma u \rangle$ parameter can also be calculated for other nuclear fusion reactions

$$\langle \sigma u \rangle_{12} = \sqrt{\frac{8}{\pi}} \frac{1}{m_1^2} \left(\frac{\mu}{k_B T} \right)^{3/2} \times \int_0^\infty \sigma_{12}(\epsilon) \epsilon \exp\left(-\frac{\mu \epsilon}{m_1 k_B T}\right) d\epsilon$$



Thermonuclear fusion power density

- With the $\langle \sigma u \rangle$ parameter in hands, one can now calculate the fusion power density produced by the any fusion reaction by

$$p_{\text{fus}} = R_{12} \Delta E_{\text{fus}} = n_1 n_2 \langle \sigma u \rangle_{12} \Delta E_{\text{fus}}$$

- For the case a D-T reaction, and writing the ion density $n_D = n_T = n/2$, one has

$$p_{\text{fus}} = \frac{n^2}{4} \langle \sigma u \rangle_{DT} \Delta E_{DT}$$

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Breakeven and the Lawson criterion for ignition

- **An important aspect that must be taken into account in designing a fusion reactor is the so-called power balance**
 - *In a tokamak, there is a continuous loss of energy from the plasma, which has to be replenished through additional plasma heating*
- **Using the equipartition energy theorem, we have that the local energy density in the plasma is**

$$w = n_D \frac{3}{2} k_B T + n_T \frac{3}{2} k_B T + n_e \frac{3}{2} k_B T = 3nk_B T$$

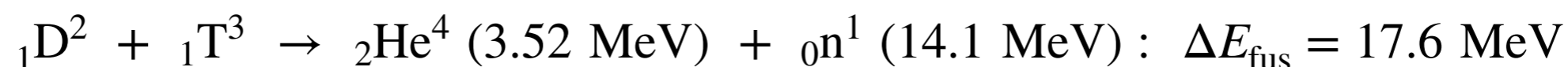
- *Here, one used that $n_e = n_D/2 = n_T/2 = n$ (quasi-neutrality condition)*
- **Therefore, the total plasma stored energy is**

$$W_P = \int w dV = \int 3nk_B T dV = 3\bar{p}V$$

where $\bar{p} = \overline{nk_B T} = \frac{1}{V} \int nk_B T dV$ is the volume-averaged plasma pressure

Breakeven and the Lawson criterion for ignition

- **The power P_{fus} has contributions from two species: α -particles and neutrons**
 - Neutrons leave the plasma (not charged particles) while the α -particles (charged particles) remain confined by the magnetic field



- Note that for a D-T reaction, $\Delta E_{\text{fus}} = \Delta E_n + \Delta E_\alpha$
 - Note that $\Delta E_\alpha = \Delta E_{\text{fus}}/5$
 - The α -particles, therefore, transfer 1/5 of total fusion energy to the plasma
- **The α -particles heating density is, therefore,**

$$p_\alpha = \frac{P_{\text{fus}}}{5} = \frac{n^2}{4} \langle \sigma u \rangle \frac{\Delta E_{\text{fus}}}{5} = \frac{n^2}{4} \langle \sigma u \rangle \Delta E_\alpha$$

and the total α -heating is

$$P_\alpha = \int p_\alpha dV = \frac{1}{4} \overline{n^2 \langle \sigma u \rangle} \Delta E_\alpha V \quad \text{with} \quad \overline{n^2 \langle \sigma u \rangle} = \frac{1}{V} \int n^2 \langle \sigma u \rangle dV$$

Breakeven and the Lawson criterion for ignition

- The rate of energy loss (power loss) is characterized in terms of an energy confinement time, which is defined as

$$P_L = \frac{W_P}{\tau_E}$$

- In a tokamak, external/auxiliary heating must be applied to compensate P_L
- In most of present day tokamaks, the fusion power is negligible
 - Therefore, under steady state, one usually have

$$P_L = \frac{W_P}{\tau_E} = P_H \quad \text{and, therefore,} \quad \tau_E \equiv \frac{W_P}{P_H}$$

- This relation allows us to determine τ_E from experimentally know quantities
- In the overall power balance in future fusion reactors, however, the power loss is balanced by external/auxiliary heating plus the α -particles heating

$$P_H + P_\alpha = P_L$$

Breakeven and the Lawson criterion for ignition

- Substitution into the previous equation yields

$$P_H + \frac{1}{4} \overline{n^2 \langle \sigma u \rangle} \Delta E_\alpha V = \frac{3 \overline{nk_B T} V}{\tau_E}$$

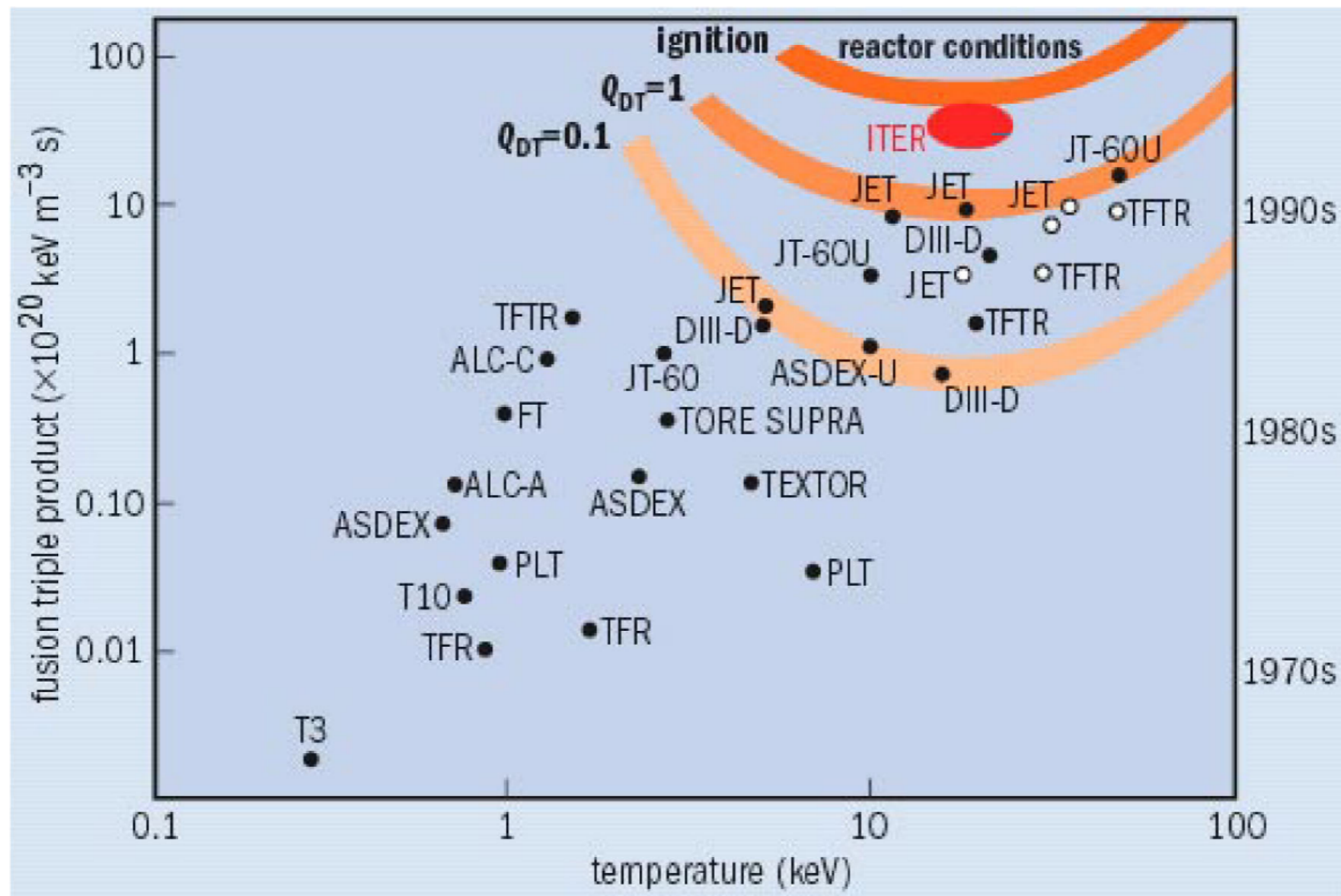
- Assuming constant plasma density and temperature profiles, for simplicity, yields

$$P_H = \left(\frac{3 nk_B T}{\tau_E} - \frac{n^2 \langle \sigma u \rangle \Delta E_\alpha}{4} \right) V$$

- An important parameter used to measure the performance of a fusion plasma is the fusion factor gain as $Q = P_{\text{fus}}/P_H$
 - The condition at which $P_H = P_{\text{fus}}$, i.e. $Q = 1$, is called the breakeven
 - The breakeven condition corresponds to the point at which the total (neutron plus α -particles) fusion power produced equals the necessary external/auxiliary heating power
- Since $P_{\text{fus}} = 5P_{\alpha'}$, the $Q = 1$ condition corresponds to an α -particle heating power that is only 20% of the externally applied heating power

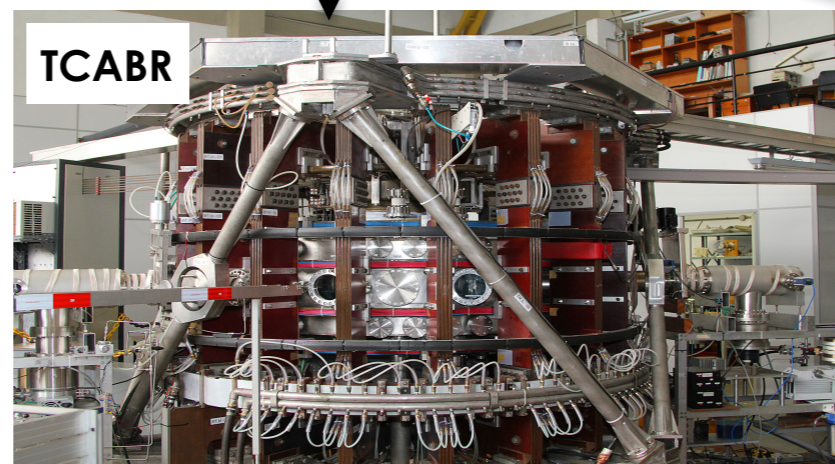
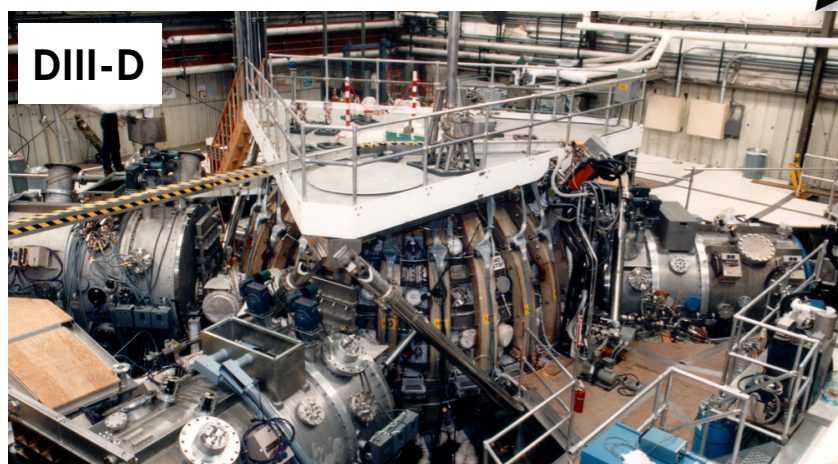
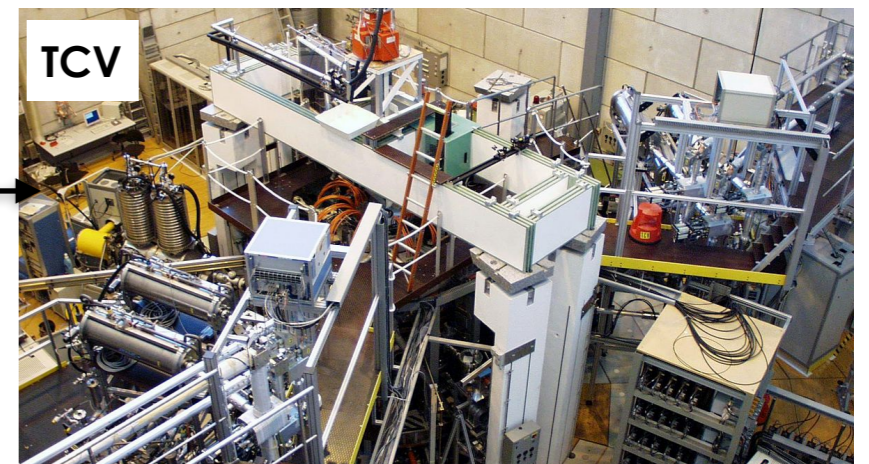
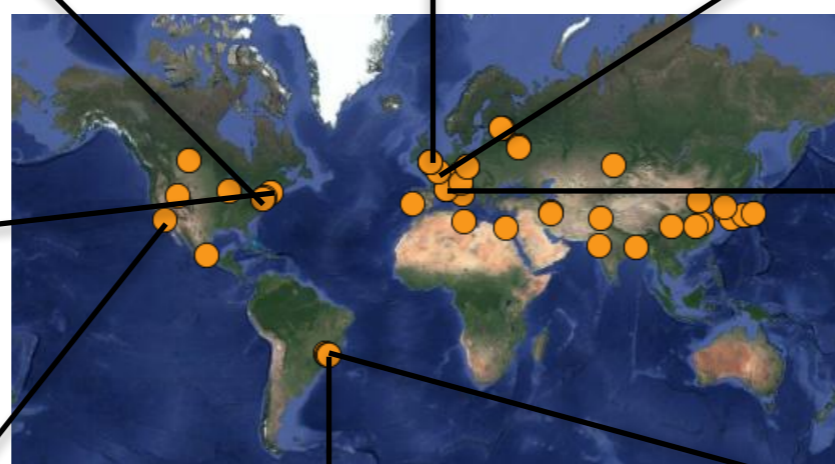
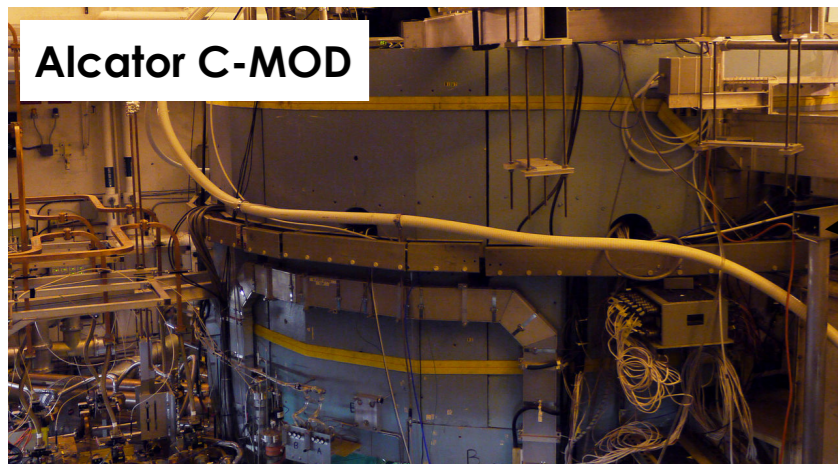
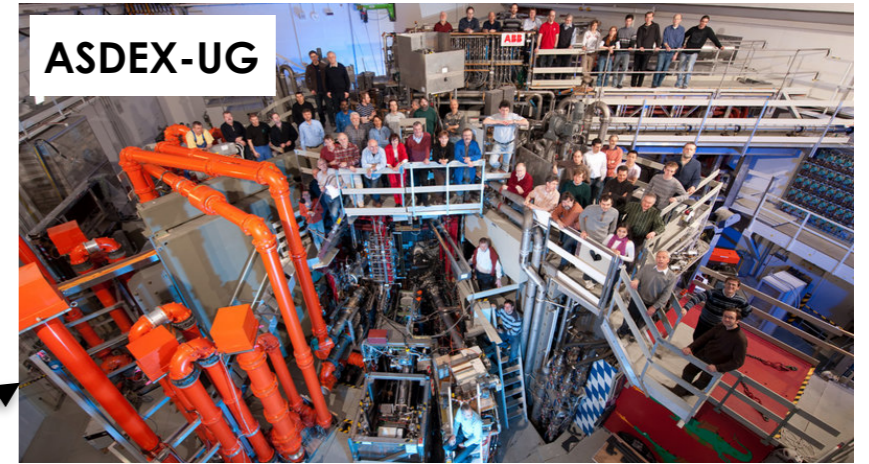
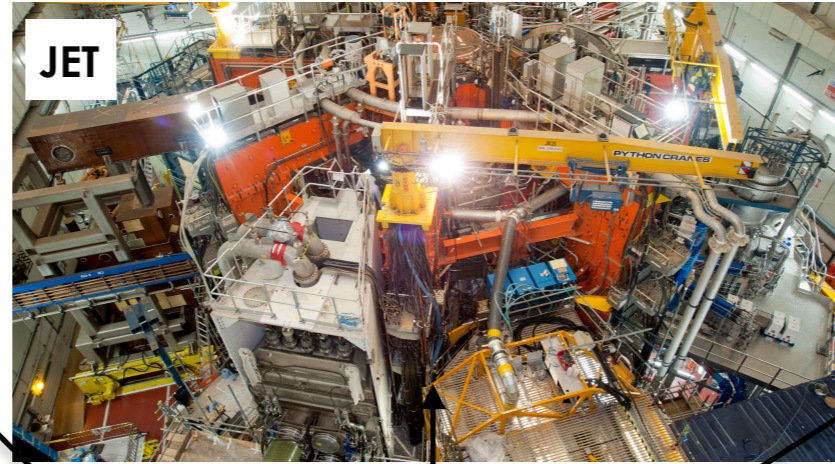
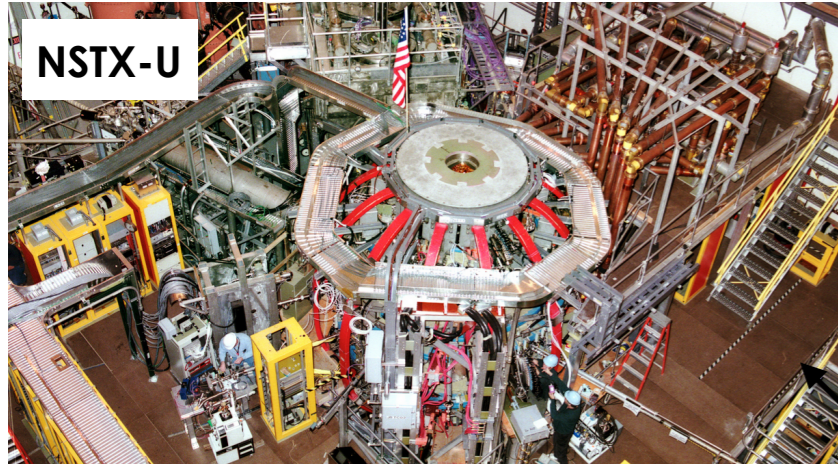
Breakeven and the Lawson criterion for ignition

- Several tokamaks were built over the past aiming at the breakeven condition



- The International Thermonuclear Experimental Reactor (ITER) aims at $Q = 10$

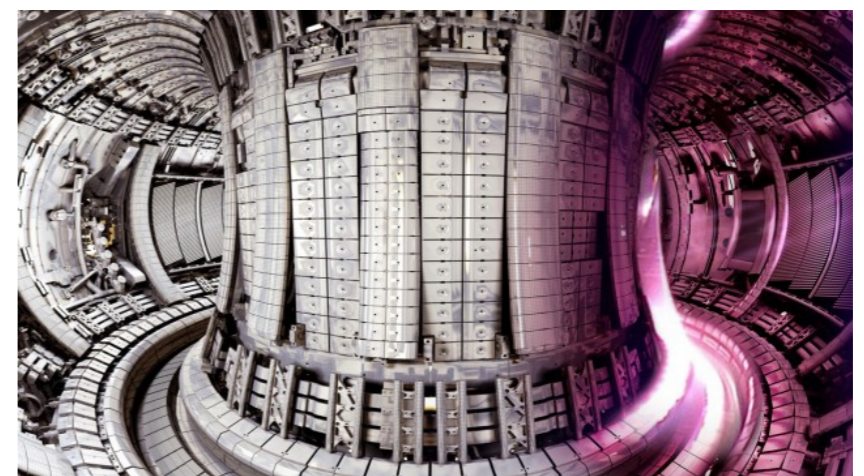
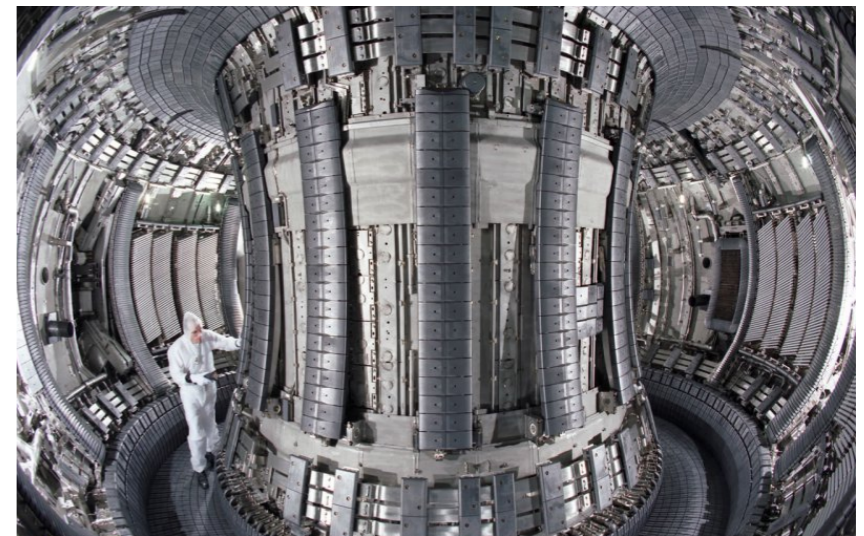
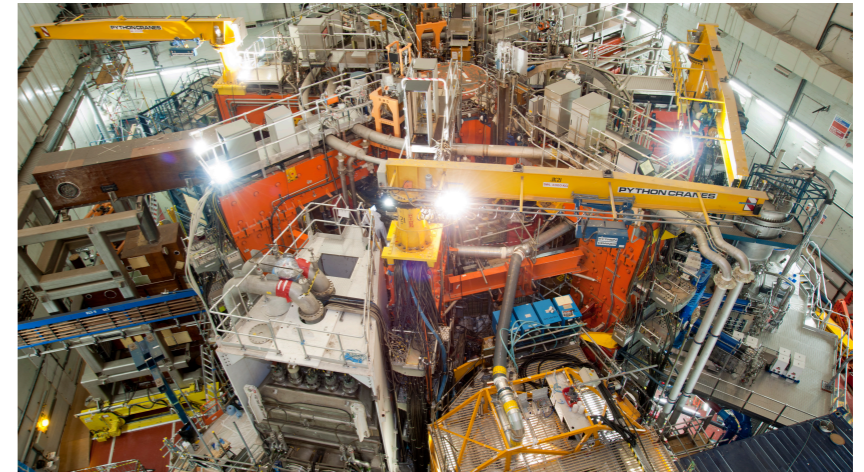
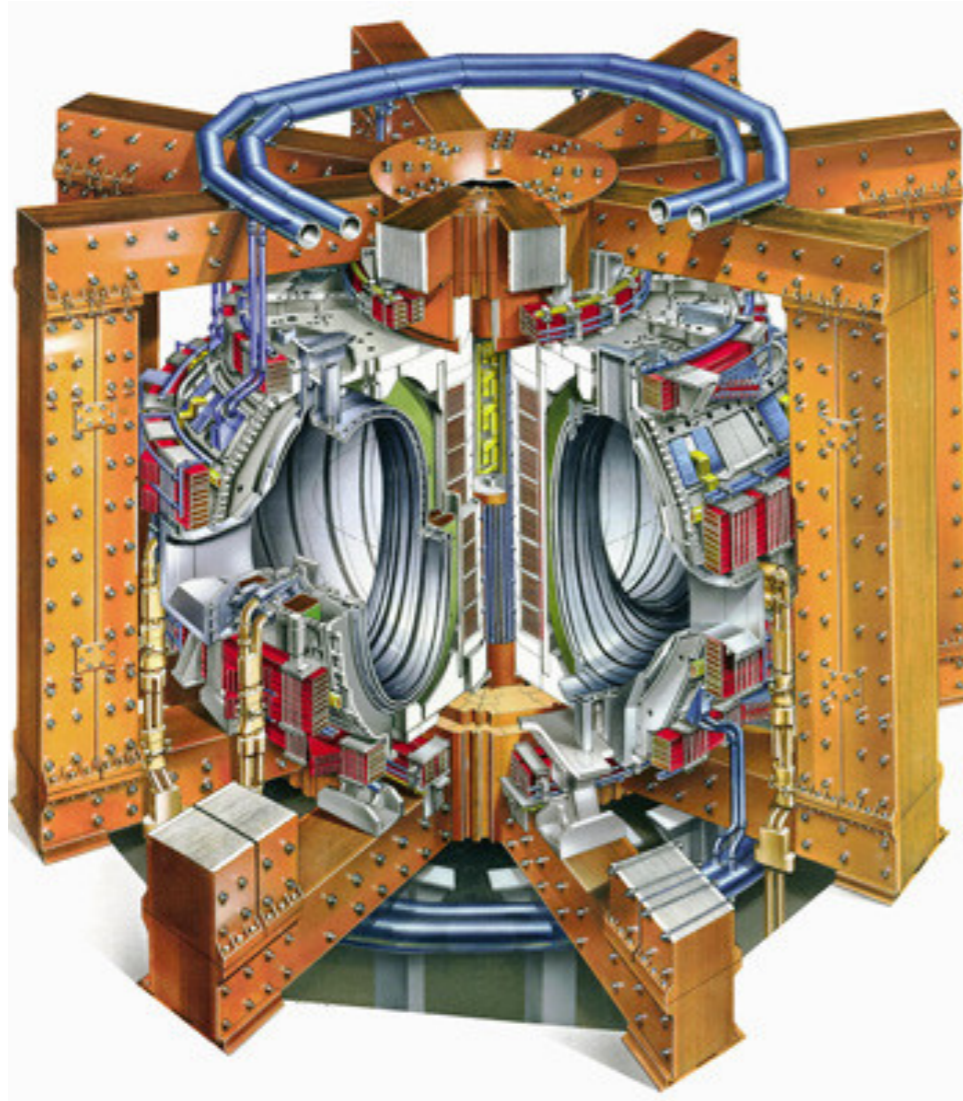
Tokamaks in operation around the world



INPE PESQUISA EM PLASMA DE FUSÃO EXPERIMENTO TOKAMAK ESFÉRICO LAF

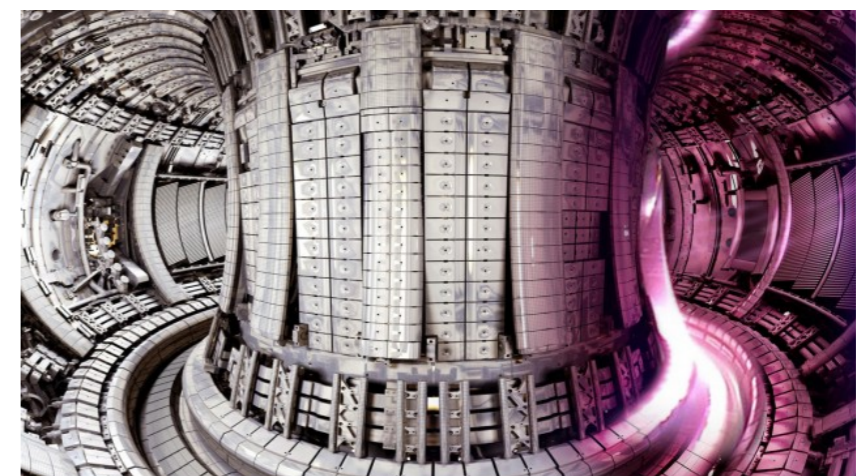
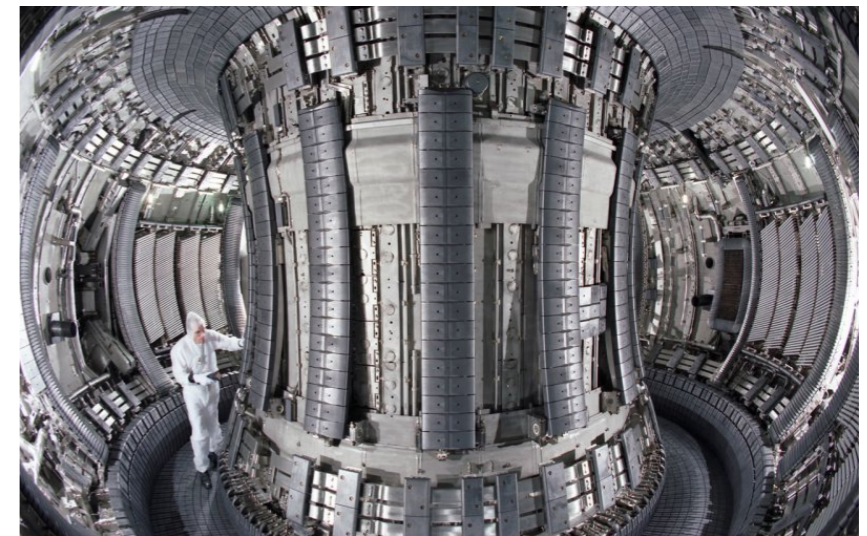
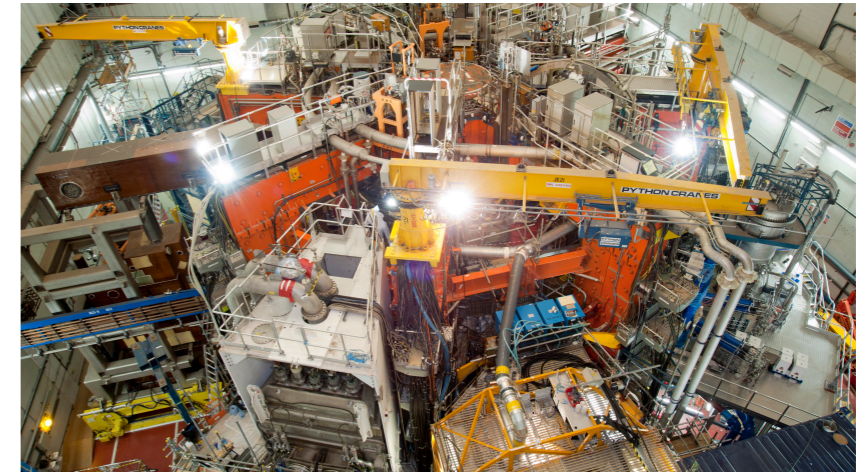
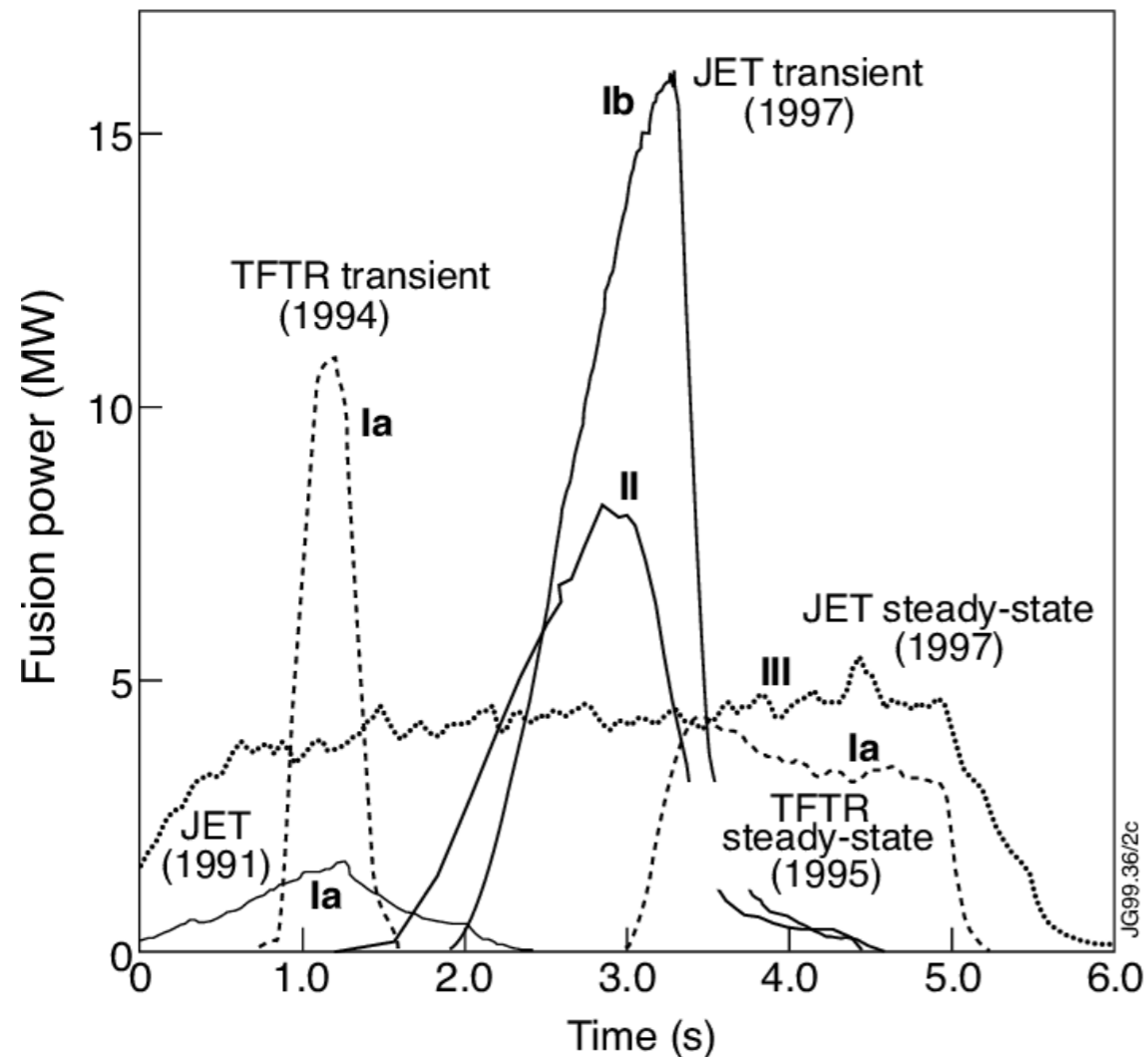
The Joint European Torus (JET) is the largest tokamak ever built and it is located in Oxfordshire - UK

- JET features $R_0 = 2.96$ m, $a = 1.25$ - 2.10 m, $I_p = 4.8$ MA, $B_0 = 3.45$ T and pulse duration 10 s
 - JET holds the world record for fusion power produced. In 1997, JET achieved $Q = 0.67$



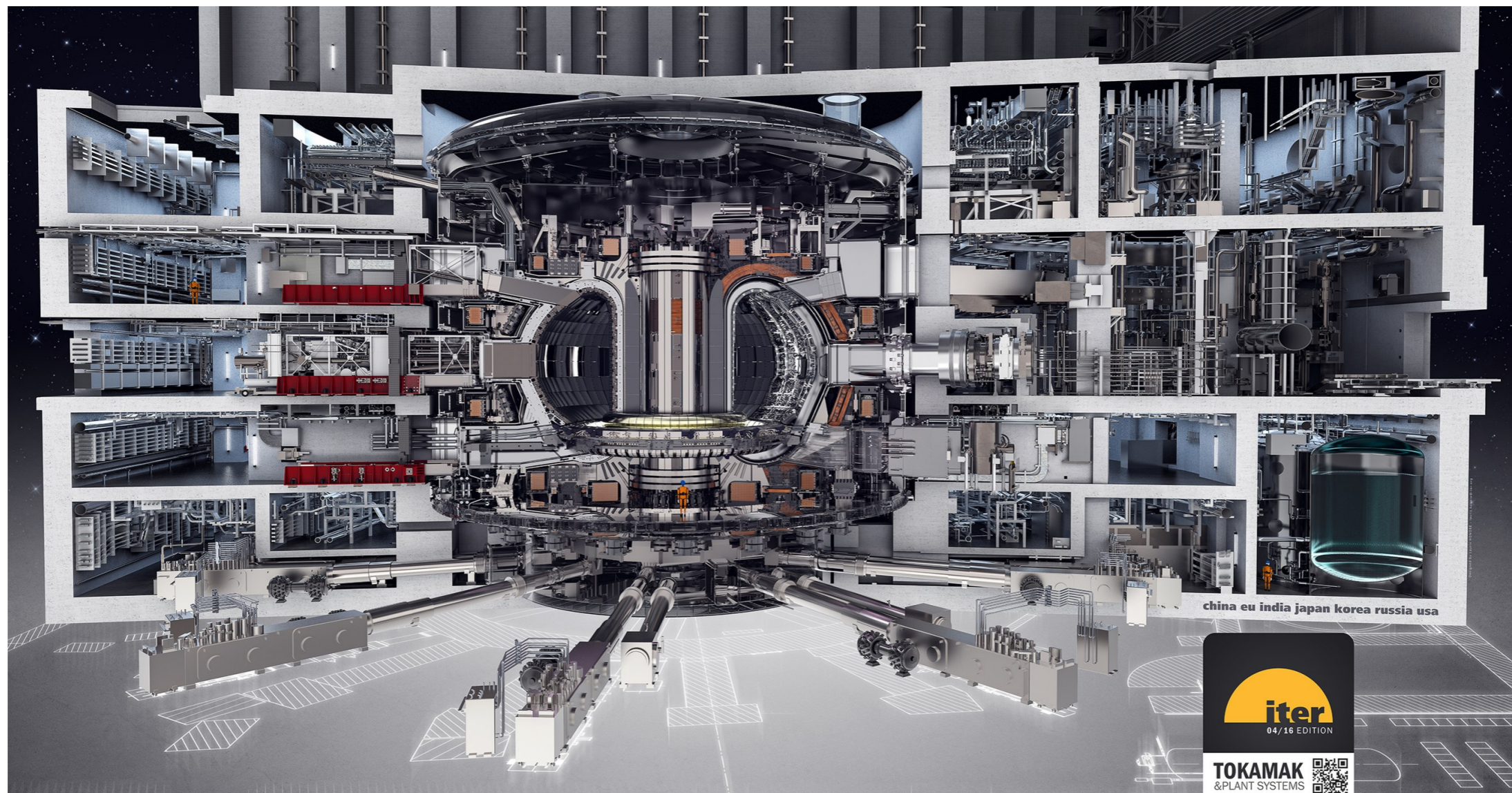
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ITER will be the largest, and most complex, experiment ever built by mankind

- ITER is being constructed in France through a consortium composed by several countries: European Union, India, Japan, China, Russia, South Korea e USA
 - ITER features $R_0 = 6.2$ m, $a = 2.0$ m, $I_P = 15$ MA, $B_0 = 12$ T, pulse duration up to 1000 s and it was designed to achieve $Q = 10$



Breakeven and the Lawson criterion for ignition

- From the power balance equation

$$P_H = \left(\frac{3 n k_B T}{\tau_E} - \frac{n^2 \langle \sigma u \rangle \Delta E_\alpha}{4} \right) V$$

the condition at which $P_H = 0$ is called the ignition condition. To have the plasma temperature being set alone by self-heating due to α -particles heating,

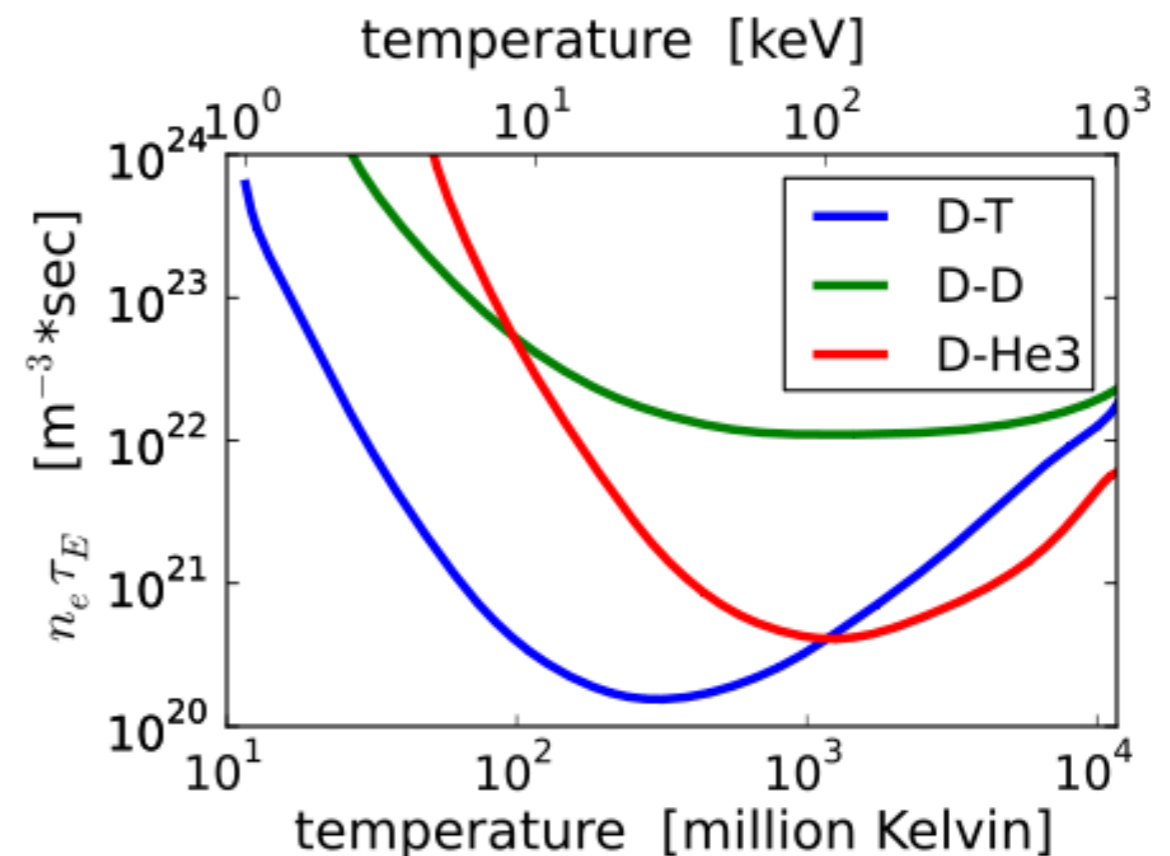
$$n\tau_E \geq \frac{12k_B}{\Delta E_\alpha} \frac{T}{\langle \sigma u \rangle}$$

- In the range 10-20 keV, the $\langle \sigma u \rangle$ parameter can be approximated (to within 10%) by

$$\langle \sigma u \rangle = 1.1 \times 10^{-24} T^2 \text{ m}^3/\text{s} \quad (\text{with } T \text{ in keV})$$

- The expression $T/\langle \sigma u \rangle$ has a minimum at $T = 26 \text{ keV}$. At this temperature,

$$n\tau_E \geq 1.5 \times 10^{20} \text{ s/m}^3 \quad (\text{The Lawson Criterion})$$



Breakeven and the Lawson criterion for ignition

- In tokamaks, the maximum achievable plasma pressure is limited, to a major extent, by its toroidal magnetic field. Therefore, to account for this limitation, the Lawson criterion is multiplied by the plasma temperature leading to

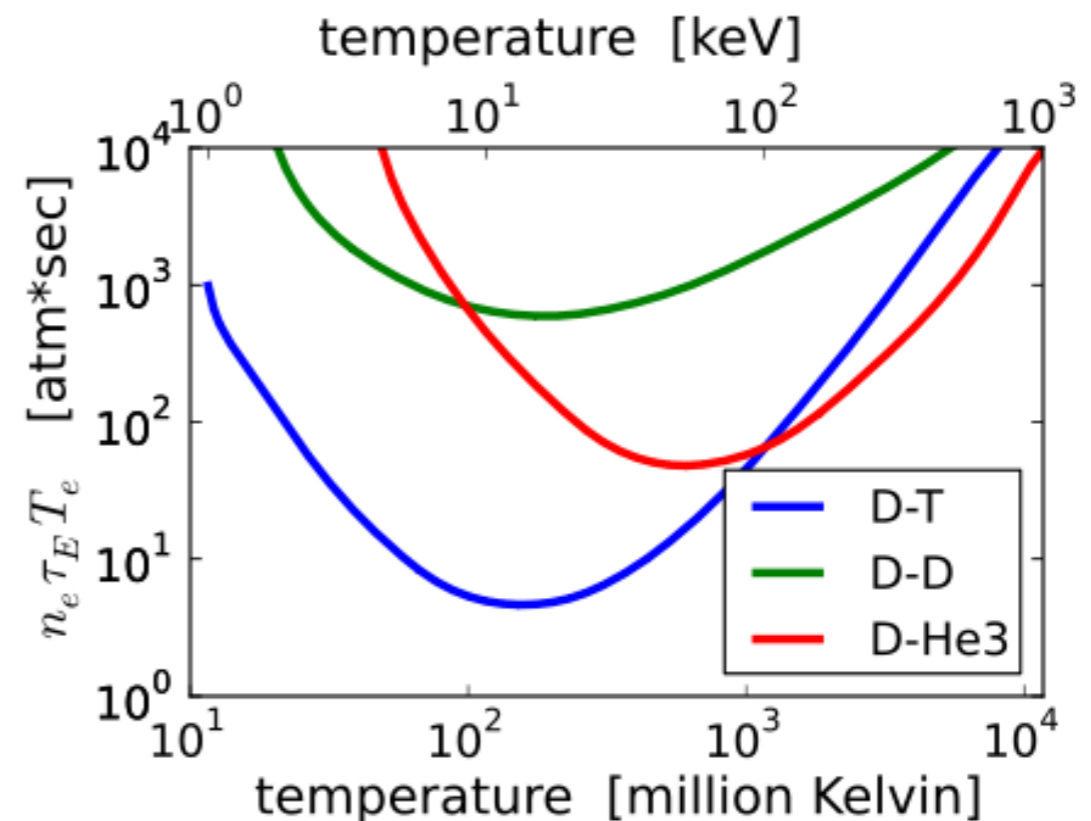
$$nT\tau_E \geq \frac{12k_B}{\Delta E_\alpha} \frac{T^2}{\langle \sigma u \rangle}$$

- The expression $T^2/\langle \sigma u \rangle$ also has a minimum, but at a slightly lower temperature, i.e. at $T \sim 10$ keV. At this temperature,

$$nT\tau_E \geq 3 \times 10^{21} \text{ keV} \cdot \text{s/m}^3$$

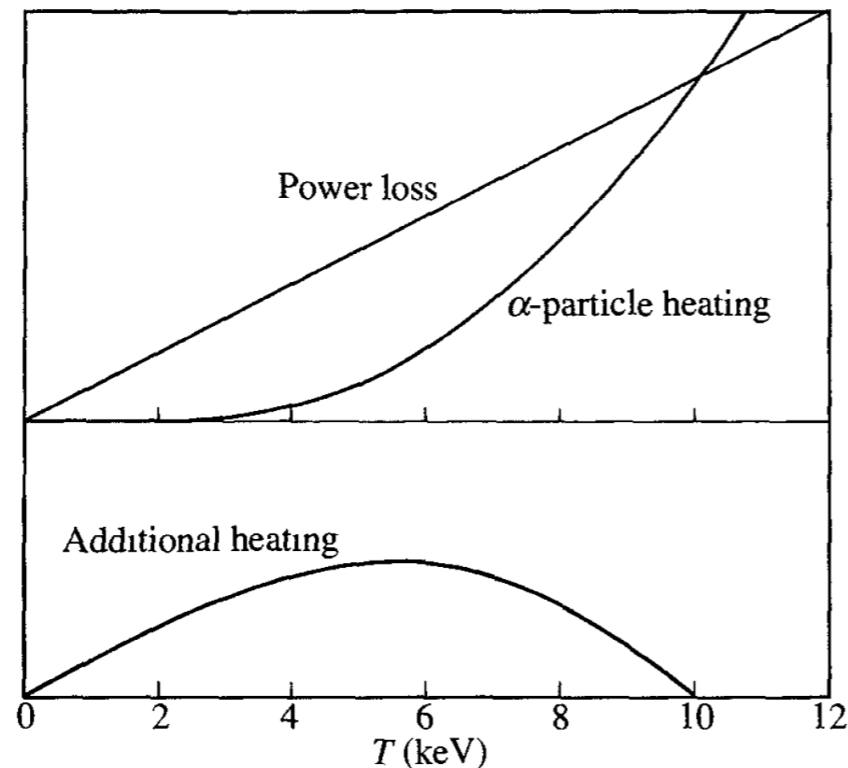
(The Triple Product)

- For a tokamak plasma with
 - $n = 1 \times 10^{20} \text{ m}^{-3}$
 - $T = 10 \text{ keV}$
 - The energy confinement time must be, at least, $\tau_E = 3 \text{ s}$

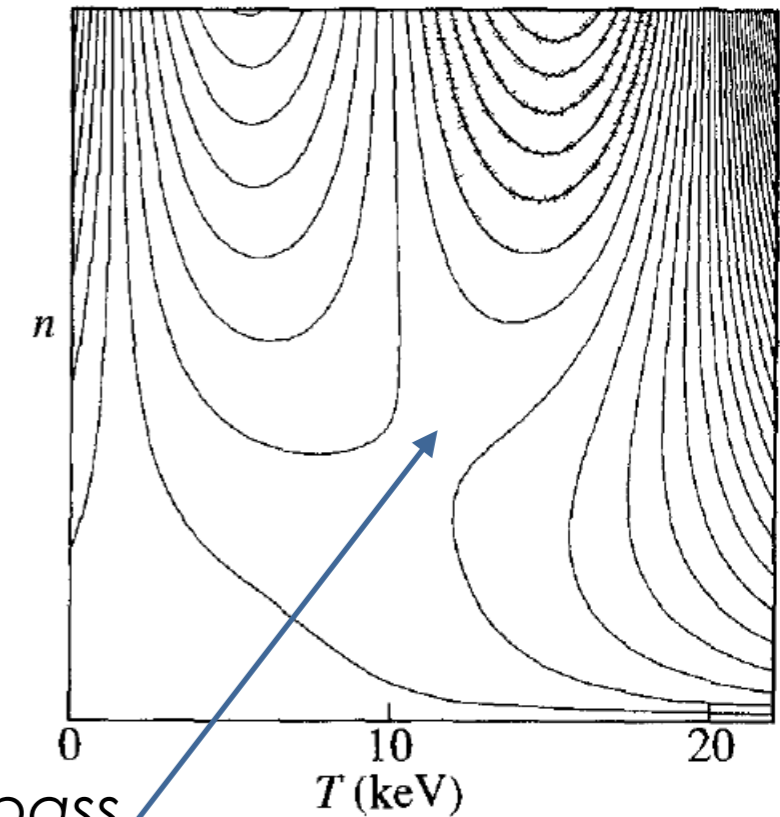


Breakeven and the Lawson criterion for ignition

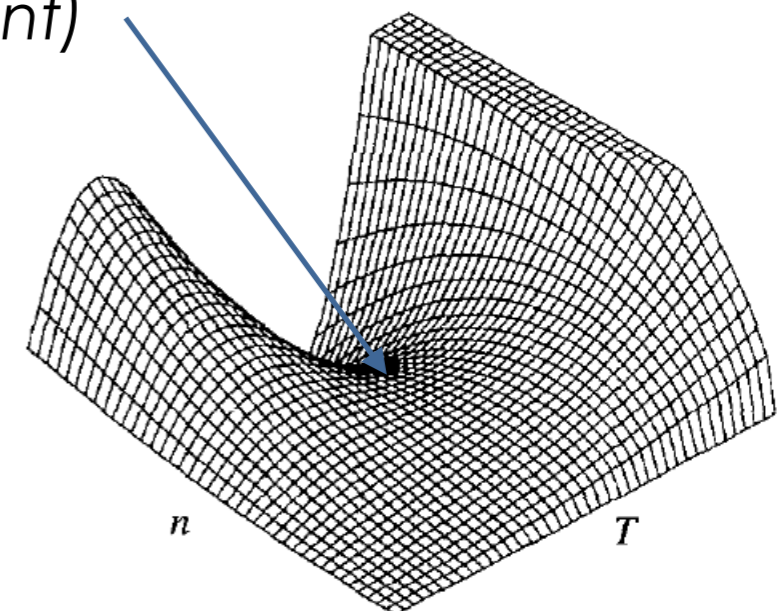
- As the ignition condition is approached, the fusion gain factor tends to infinity, i.e. as $P_H \rightarrow 0$ one has that $Q = P_{\text{fus}}/P_H \rightarrow \infty$



- However, operation beyond ignition is not desired due to a thermal instability
- Although an ignited plasma does not need external heating to maintain the plasma, high fusion powers can be achieved at still finite values of Q



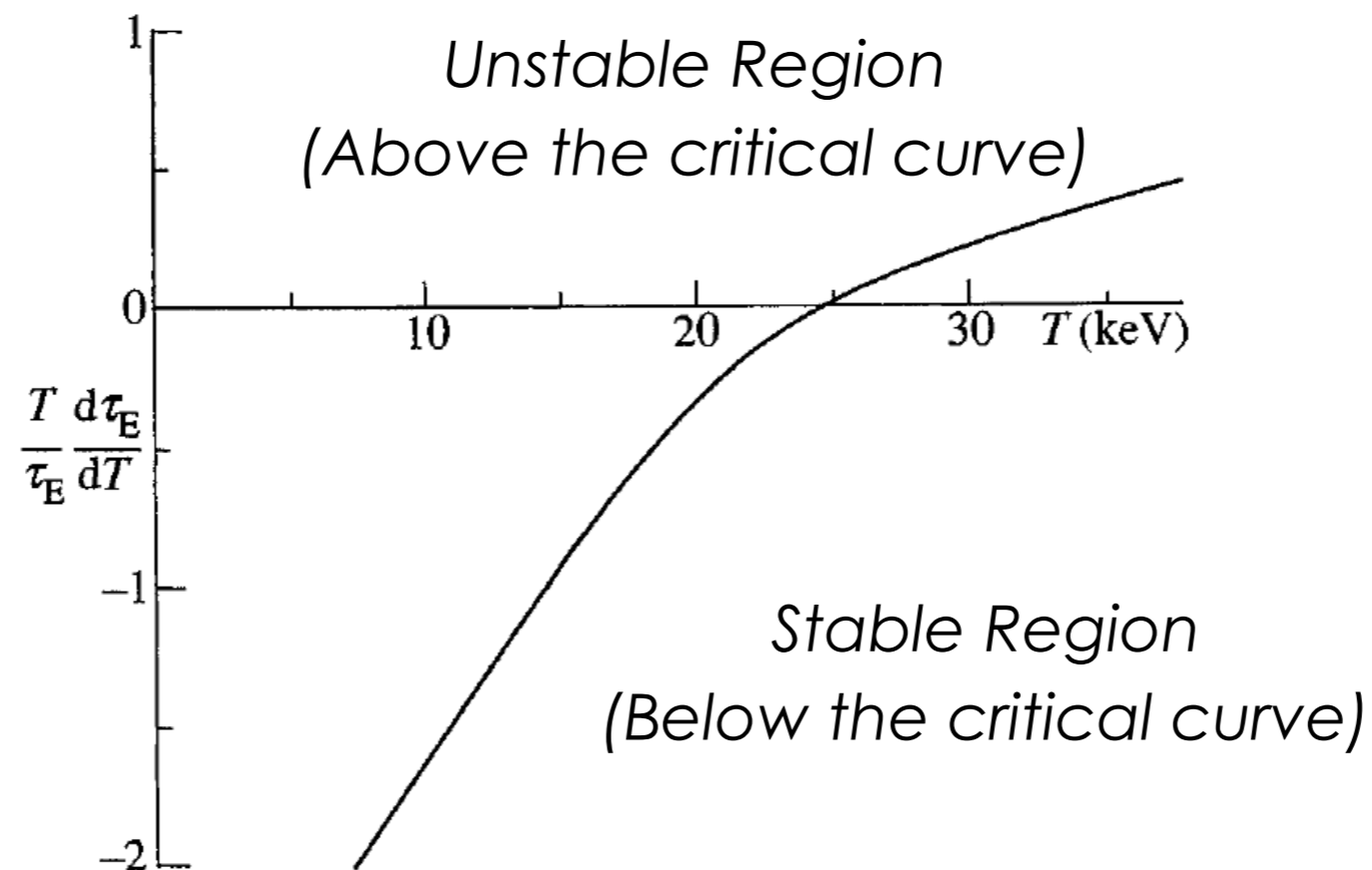
The Cordey pass
(Saddle point)



Exercise

- Show that the condition for thermal stability of a plasma with α -particle heating is given by (see Wesson, Ch. 1, at the end of section 5):

$$\frac{T}{\tau_E} \frac{d\tau_E}{dT} < 1 - \frac{T}{\langle \sigma v \rangle} \frac{d\langle \sigma v \rangle}{dT}$$



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Scaling laws

- From kinetic theory, the Vlasov equation must be invariant under just 3 scaling transformations [J.W. Connor and J.B. Taylor, Nuclear Fusion 17, 1047 (1977)]:

- T1: $f_j \rightarrow \alpha f_j$

- T2: $t \rightarrow \beta^{-1}t, \quad v \rightarrow \beta v, \quad B \rightarrow \beta B, \quad E \rightarrow \beta^2 E$

- T3: $t \rightarrow \gamma t, \quad x \rightarrow \gamma x, \quad E \rightarrow \gamma^{-1}E, \quad B \rightarrow \gamma^{-1}B$

$$\frac{\partial f_j}{\partial t} + \mathbf{v} \cdot \nabla f_j + \frac{q_j}{m_j} (\mathbf{E} + \mathbf{v} \times \mathbf{B}) \cdot \nabla_{\mathbf{v}} f_j = 0$$

- Let's suppose that the thermal energy confinement time depends on engineering parameters, for example, as

$$\tau_{E,th} = C n^p B^q T^r a^s$$

- Remember that $n = \int f d^3v$ and $T = \frac{1}{n} \int \frac{1}{2} m v^2 f d^3v$

Scaling laws

- Equating the powers α , β and γ on the two sides of the resulting equation leads to 3 different constraints for the powers p , q , r , and s

- T1: $\tau_{E,th} = C (\alpha n)^p B^q T^r a^s \rightarrow \alpha^p = 1$

- T2: $\beta^{-1} \tau_{E,th} = C (\beta^3 n)^p (\beta B)^q (\beta^2 T)^r a^s \rightarrow \beta^{-1} = \beta^{3p+q+2r}$

- T3: $\gamma \tau_{E,th} = C n^p (\gamma^{-1} B)^q T^r (\gamma a)^s \rightarrow \gamma = \gamma^{s-q}$

- This set of equations has as solution: $p = 0$, $q + 2r = -1$ and $s - q = 1$

- Substitution of these constraints in the proposed form of $\tau_{E,th}$ yields

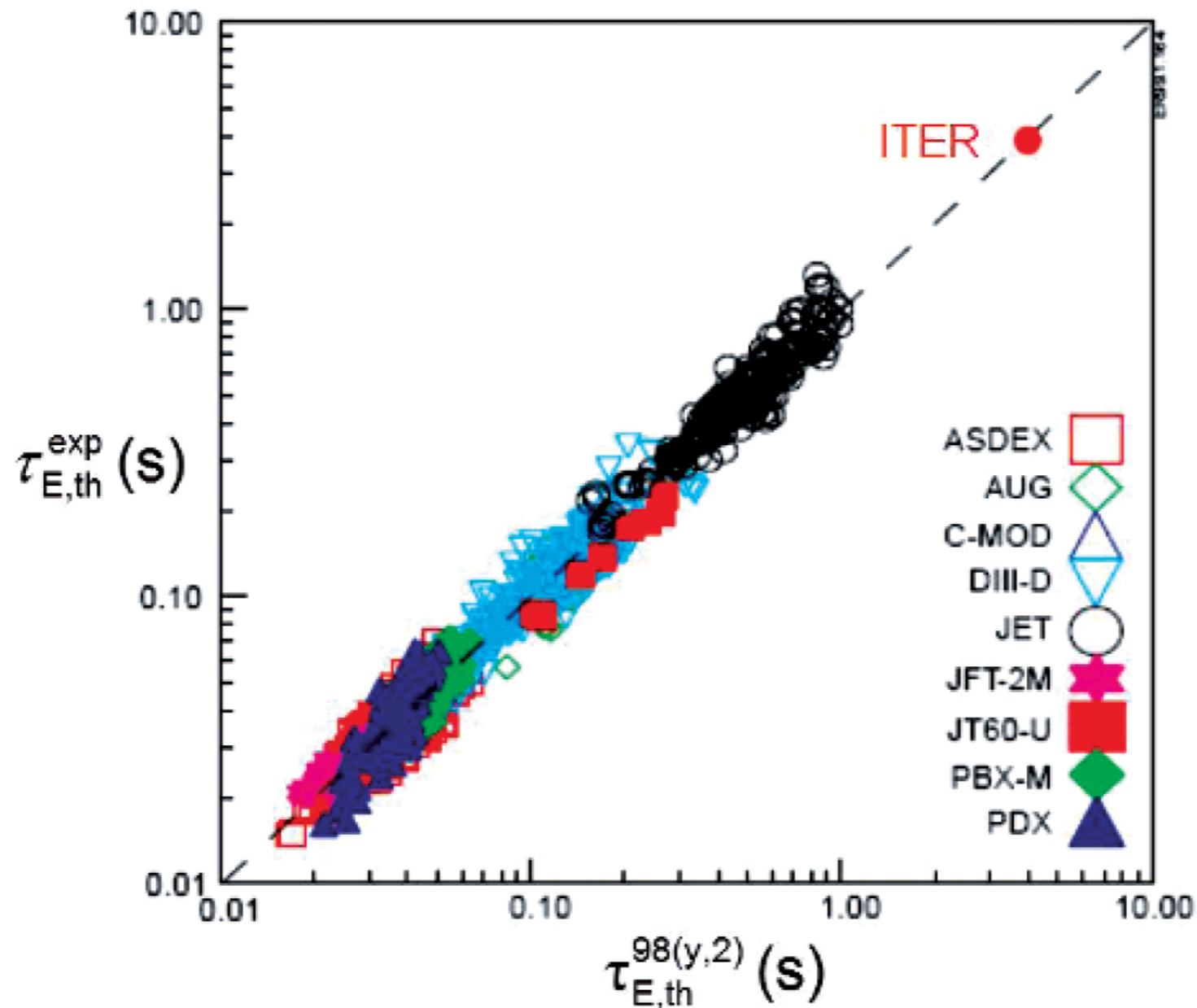
$$\tau_{E,th} = C B^q T^{-(1+q)/2} a^{1+q} \quad \text{(Note that, in this simple case, there is only one free parameter left for the data fitting)}$$

- This method does not give information about geometrical ratios, such as a/R_0
- This method is of less value when atomic processes play a significant role
- A more complex model, and, consequently, a more complete form for $\tau_{E,th}$, would lead to less constraints

Scaling laws

- The thermal energy confinement time scaling law (the IPB98(y,2) scaling) is

$$\tau_{E,th} = 0.0562 I_P^{0.93} B_0^{0.15} n_{19}^{0.41} P_H^{-0.69} R_0^{1.97} \epsilon^{0.58} \kappa_a^{0.78} M^{0.19}$$



References

- **Nuclear fusion and tokamak physics**
 - *Nuclear fusion reactions: Wesson, Ch. 1*
 - *Thermonuclear fusion: Wesson, Ch. 1*
 - *Breakeven and the Lawson criterion for ignition: Wesson, Ch. 1*
 - *Scaling laws: Wesson, Ch. 4, section 15*