

Laboratório 5

Osciladores Harmônicos

Roteiro Experimental

SEL393 – Laboratório de Instrumentação Eletrônica I
Departamento de Engenharia Elétrica e de Computação

Laboratório 5 – Osciladores Harmônicos
(Oscilador Senoidal com Ponte de Wien)

Neste laboratório serão avaliados em protoboard e em simulação osciladores senoidais utilizando ponte de WIEN. A primeira topologia utiliza um oscilador com resistores lineares na malha de realimentação negativa (sem controle automático de ganho - CAG) para se verificar a dificuldade de estabilização da oscilação e conseqüente necessidade de utilização do CAG. A segunda topologia utiliza um CAG com diodos para o controle e estabilização da oscilação.

Implementação em Protoboard

Oscilador com Ponte de Wien com CAG

a) No circuito da Fig. 5.1 observe no osciloscópio o sinal em V_s .

Utilize os op amps LM741, LF351 e LT1022 e os diodos 1N4148 (silício) ou 1N60 (germânio). Utilize o comando `uic` do LTSpice para simular a energização do circuito quando é ligado.

b) Verifique o erro relativo entre a frequência teórica e a medida.

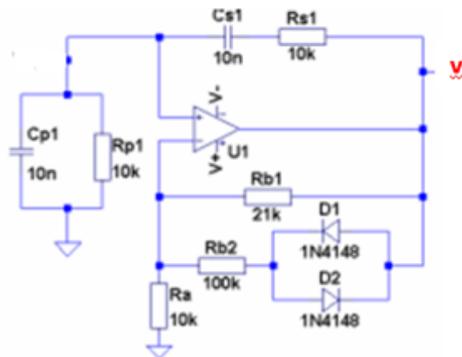


Fig.5.1 - Oscilador com Ponte de Wien com CAG

Simulação em LT Spice

Oscilador com Ponte de Wien sem CAG

a) No circuito da Fig. 5.2 observe o sinal em V_s , durante um intervalo de tempo de 5ms, para os valores de R_A e R_B mostrados na Tabela 1. Utilize o comando `uic` do LTSpice para simular a energização do circuito quando é ligado.

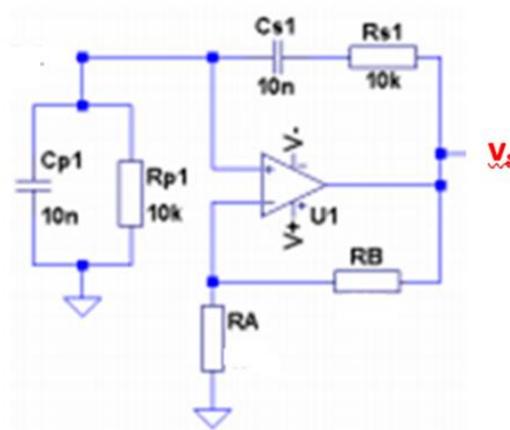


Fig. 5.2 - Oscilador com Ponte de Wien sem CAG

Tabela 6.1

Simulação	R_A (Ω)	R_B (Ω)
1	10K	19k
2	10k	20k
3	10k	21k

b) Comente os resultados obtidos.

Oscilador com Ponte de Wien com CAG

a) No circuito da Fig. 5.3 observe o sinal em V_s durante um intervalo de tempo de 12ms.

Utilize os op amps LM741, LF351 e LT1022 e os diodos 1N4148 (silício) ou 1N60 (germânio). Utilize o comando `uic` do LTSpice para simular a energização do circuito quando é ligado.

b) Verifique o erro relativo entre a frequência teórica e a medida.

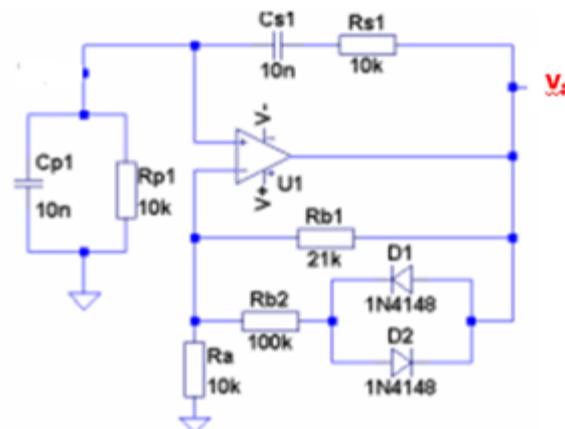


Fig.5.3 - Oscilador com Ponte de Wien com CAG

Fundamentos Teóricos

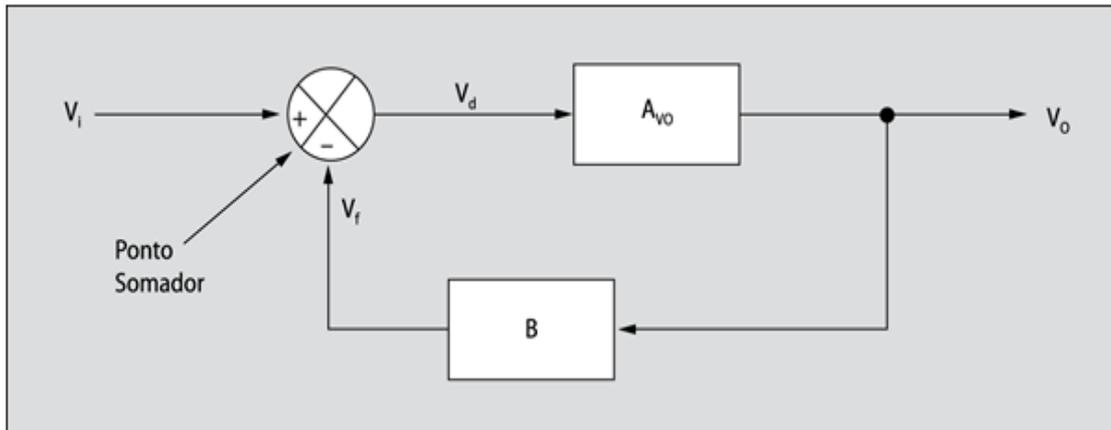
Osciladores

1

Two general classes of oscillators exist: sinusoidal and relaxation. Sinusoidal oscillators consist of amplifiers with RC or LC circuits that have adjustable oscillation frequencies, or crystals that have a fixed oscillation frequency. Relaxation oscillators generate triangular, sawtooth, square, pulse, or exponential waveforms, and they are not discussed here.

Op amp sine wave oscillators operate without an externally applied input signal. Some combination of positive and negative feedback is used to drive the op amp into an unstable state, causing the output to transition back and forth at a continuous rate. The amplitude and the oscillation frequency are set by the arrangement of passive and active components around a central op amp.

Realimentação



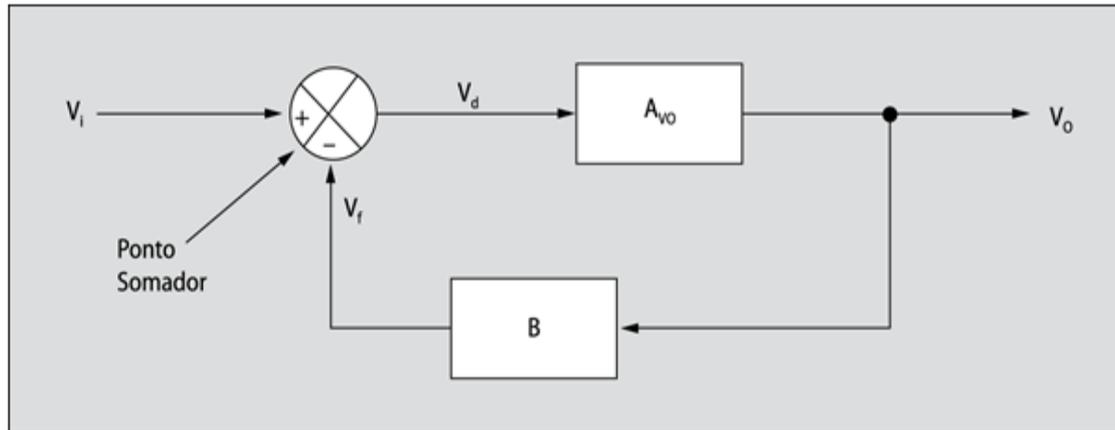
$$V_d = V_i - V_f \quad (2.1)$$

$$V_d = \frac{V_o}{A_{vo}} \quad (2.2)$$

$$V_f = B V_o \quad (2.3)$$

Substituindo (2.1) em (2.2)

$$\frac{V_o}{A_{vo}} = V_i - V_f \quad (2.4)$$



Substituindo (2.3) em (2.4)

$$\frac{V_o}{A_{vo}} = V_i - BV_o \quad (2.5)$$

Rearranjando (2.5)

$$A_{vf} = \frac{A_{vo}}{1 + BA_{vo}} \quad (\text{Equação de Black})$$

Se $A_{vo} \rightarrow \infty$, \rightarrow $A_{vf} = \frac{1}{B}$

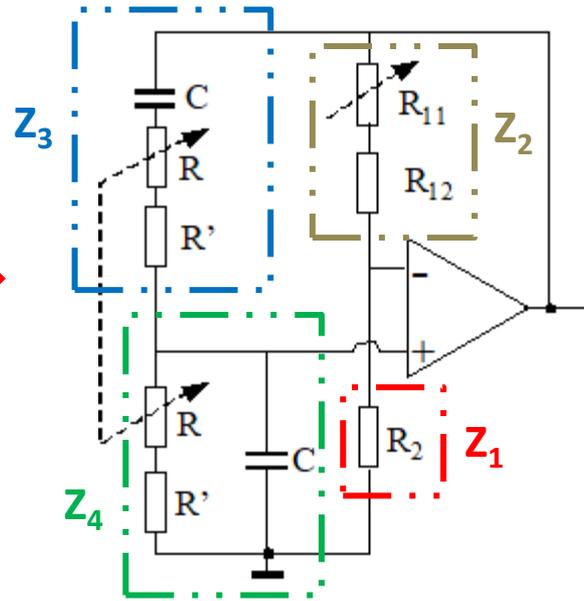
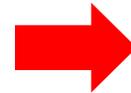
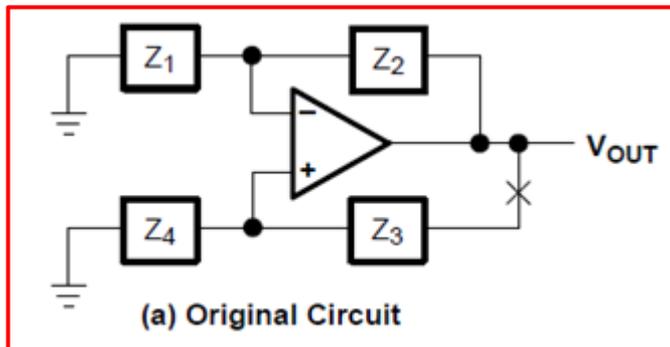
Oscillators do not require an externally applied input signal, but instead use some fraction of the output signal created by the feedback network as the input signal. It is the noise voltage that provides the initial boost signal to the circuit when positive feedback is employed. Over a period of time, the output builds up, oscillating at the frequency set by the circuit components.

Oscillation results when the feedback system is not able to find a stable state because its transfer function can not be satisfied. The system becomes unstable when the denominator in Equation below is 0. When $(1 + A\beta) = 0$, $A\beta = -1$. The key to designing an oscillator, then, is to ensure that $A\beta = -1$. This is called the Barkhausen criterion. This constraint requires the magnitude of the loop gain be 1 with a corresponding phase shift of 180° as indicated by the minus sign. An equivalent expression using complex math is $A\beta = 1 \angle -180^\circ$ for a negative feedback system.

$$A_{vf} = \frac{A_{vo}}{1 + BA_{vo}}$$

(Equação de Black)

Oscilador de Wien sem CAG

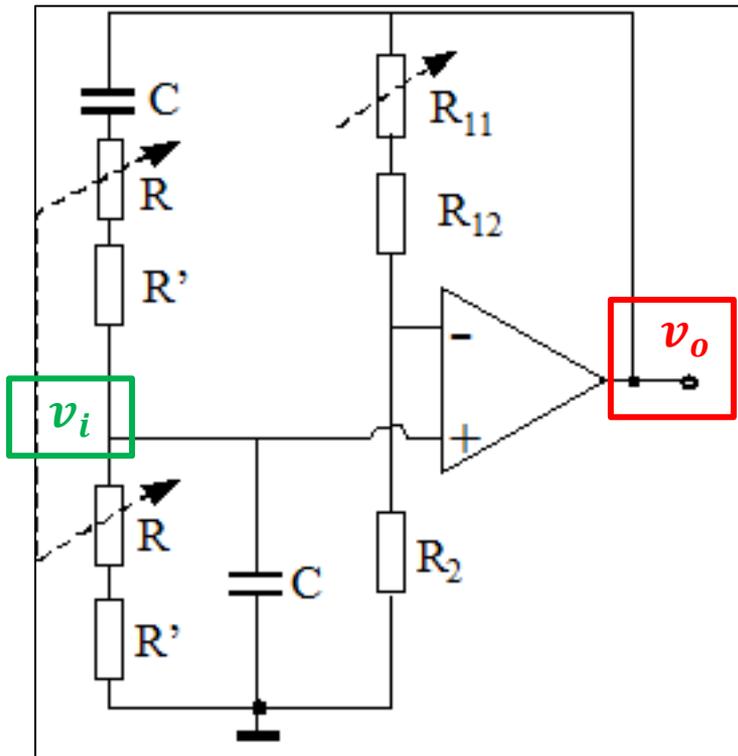


$$\omega_0 = \frac{1}{(R+R')C}$$

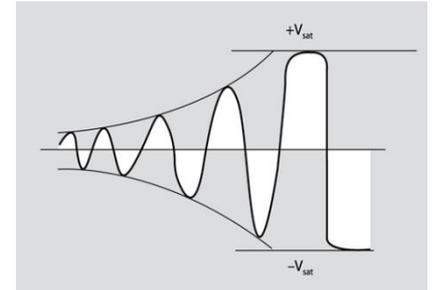
$$\frac{R_{11} + R_{12}}{R_2} = 2$$

A implementação do **circuito sem CAG** não é possível devido à dificuldade de se manter um **ganho constante igual a 3** no **amplificador não inversor** !

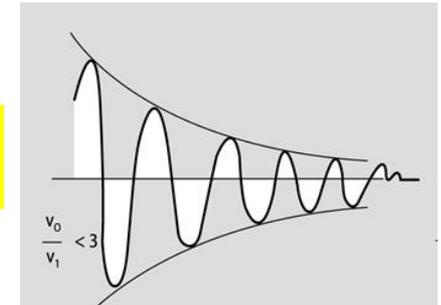
Oscilador de Wien sem CAG



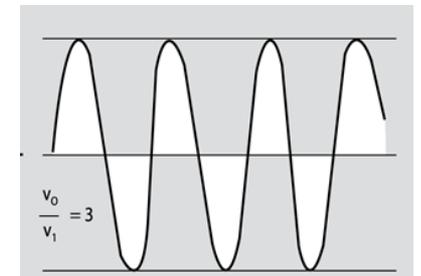
$$G = \frac{v_o}{v_1} > 3$$



$$G = \frac{v_o}{v_1} < 3$$



$$G = \frac{v_o}{v_1} = 3$$

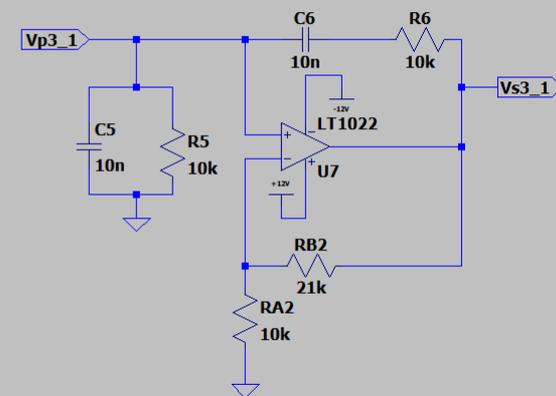
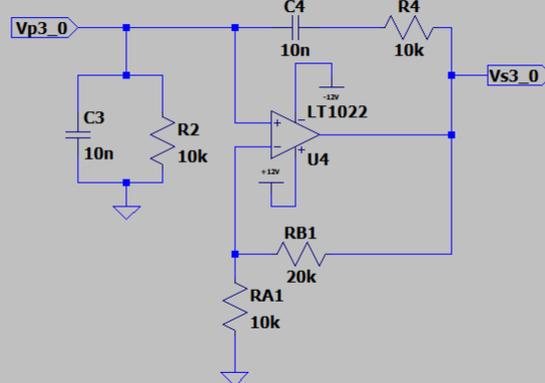
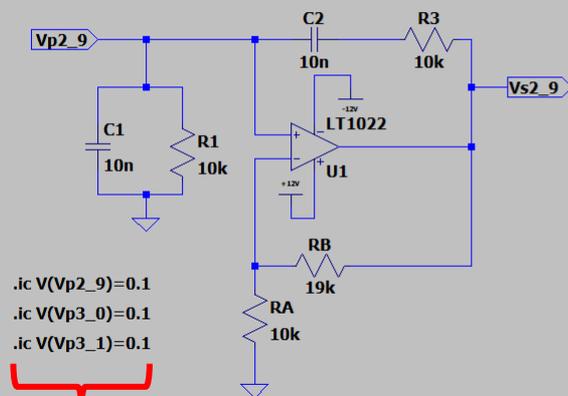


Oscilador de Wien sem CAG

G=2.9

G=3.0

G=3.1



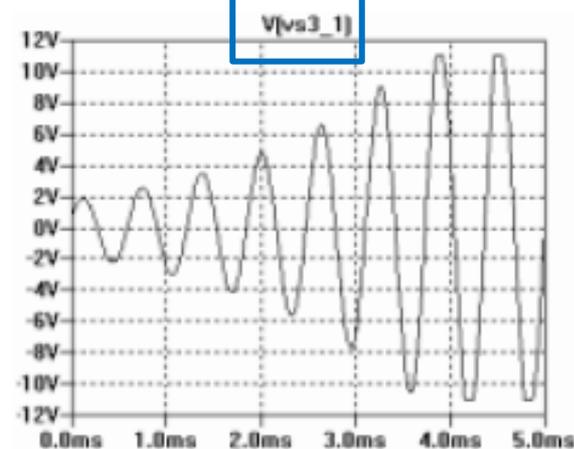
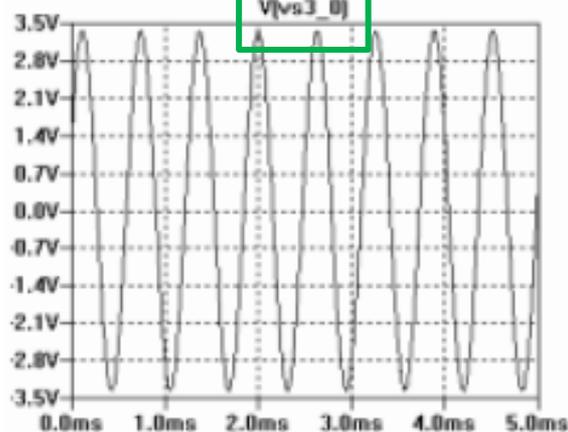
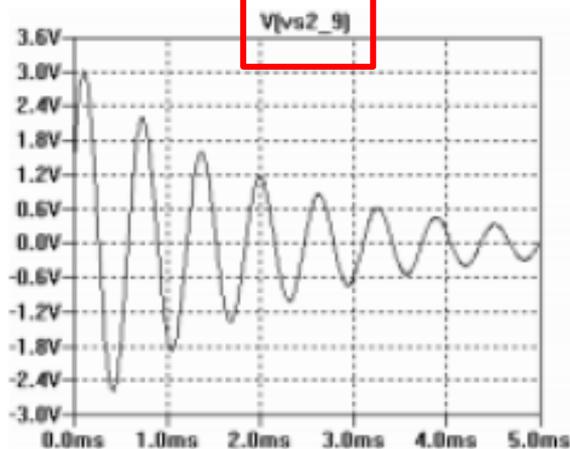
.tran 5ms
.ic V(Vp2_9)=0.1
.ic V(Vp3_0)=0.1
.ic V(Vp3_1)=0.1

(comandos para iniciar a oscilação, simulam a energização inicial de um circuito quando é LIGADO)

Oscilação Amortecida

Oscilação

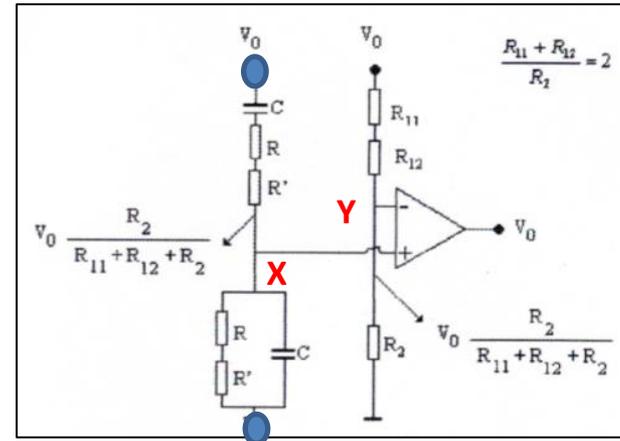
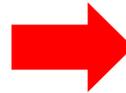
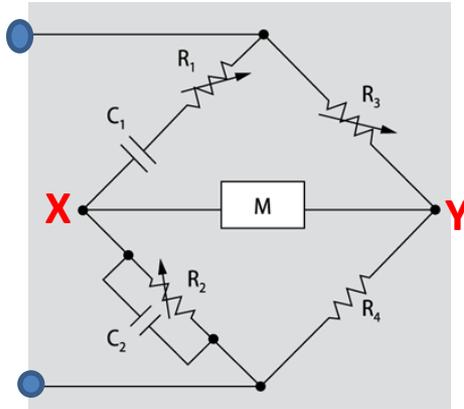
Oscilação com Aumento de Amplitude



Oscilador com Ponte de Wien

Fundamentos Teóricos

1 Seja o circuito do oscilador com Ponte de Wien:



Determinando-se a corrente no ramo esquerdo, tem-se que:

$$\frac{V_0 - V_0 \frac{R_2}{R_{11} + R_{12} + R_2}}{(R + R') + \frac{1}{sC}} = \frac{V_0 \frac{R_2}{R_{11} + R_{12} + R_2} - 0}{(R + R') \frac{1}{sC}}$$

Considerando que $(R_{11} + R_{12}) = 2R_2$ e simplificando:

$$2s(R + R')C = [1 + s(R + R')C]^2$$

As raízes desta equação são:

$$s_1 = \frac{i}{(R+R')C}$$

$$s_2 = -\frac{i}{(R+R')C}$$

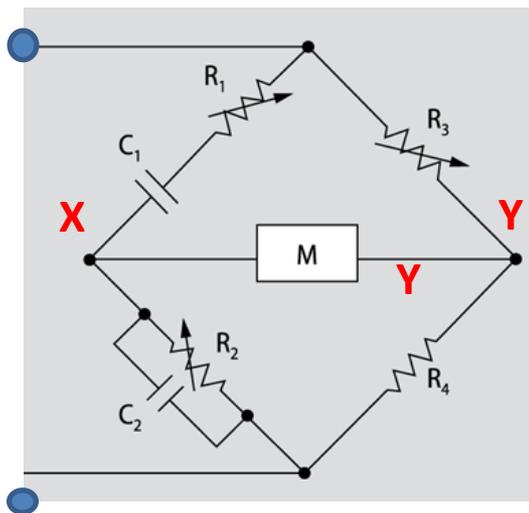


$$w = \frac{1}{(R+R')C}$$

$$f = \frac{1}{2\pi(R+R')C}$$

2

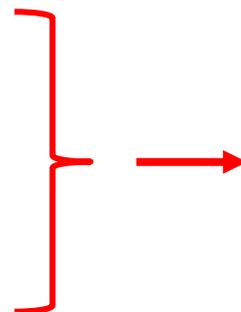
Seja a Ponte de Wien da figura. No equilíbrio:



$$V_x = V_y$$

$$R_1 R_2 C_1 C_2 = 1$$

$$R_3 \left[\frac{\frac{R_2}{sC_2}}{R_2 + \frac{1}{sC_2}} \right] = R_4 + \frac{1}{sC_1}$$



$$\rightarrow \frac{R_3}{R_4} = \frac{R_1 R_2 C_1 C_2 s^2 + (R_2 C_2 + R_1 C_1) s + 1}{R_2 C_1 s}$$

$$\rightarrow \frac{R_3}{R_4} = \frac{1}{R_1 R_2 C_1^2} + \frac{1}{R_2^2 C_2 C_1} + j \left[\frac{\omega}{R_2 C_1} - \frac{1}{\omega R_1 R_2^2 C_1^2 C_2} \right]$$

A parte imaginária da equação anterior deve ser nula :

$$\rightarrow \boxed{\omega = \left(\frac{1}{R_1 R_2 C_1 C_2} \right)^{1/2}} \quad \xrightarrow[C_1 = C_2]{R_1 = R_2 = R + R'} \quad \boxed{f = \frac{1}{2\pi(R+R')C}}$$

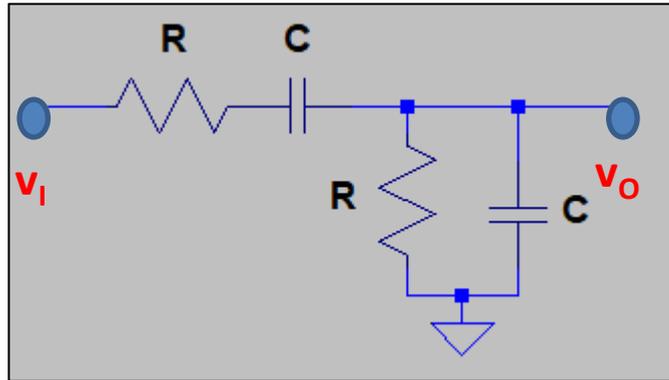
3 Parte real:

$$\frac{R_3}{R_4} = \frac{1}{R_1 R_2 C_1^2} + \frac{1}{R_2^2 C_2 C_1} = \frac{R_1 R_2 C_1 C_2}{R_1 R_2 C_1^2} + \frac{R_1 R_2 C_1 C_2}{R_2^2 C_2 C_1} \rightarrow$$

$$\rightarrow \frac{R_3}{R_4} = \frac{C_2}{C_1} + \frac{R_1}{R_2}$$

Se $R_1 = R_2$ e $C_1 = C_2$ \rightarrow $\frac{R_3}{R_4} = 2$

4 Seja o circuito da figura abaixo:

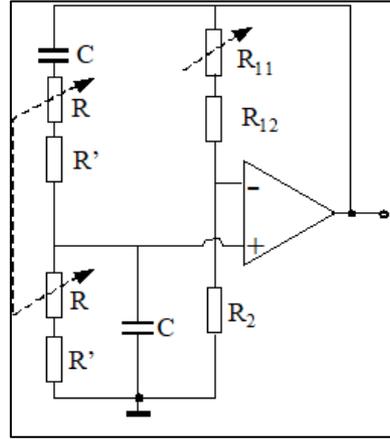


$$v_i = I Z_{total} = I \left[R + \frac{1}{sC} + \frac{R/sC}{R + \frac{1}{sC}} \right]$$

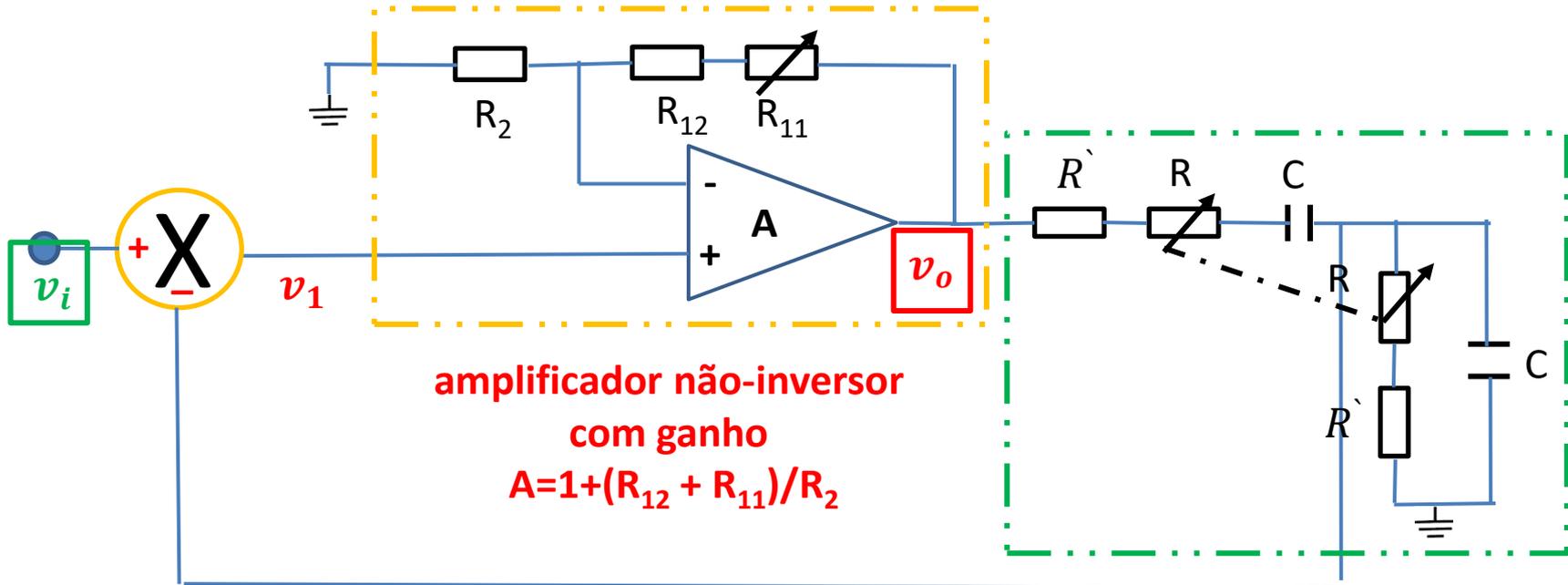
$$v_o = I \frac{R}{RCs + 1}$$

$$\rightarrow G = \frac{v_o}{v_i} = \frac{sW_o}{s^2 + 3W_o s + W_o^2}$$

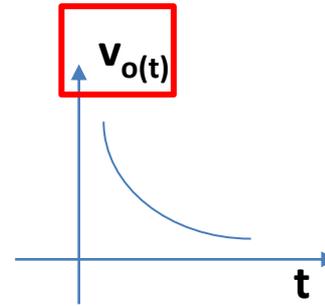
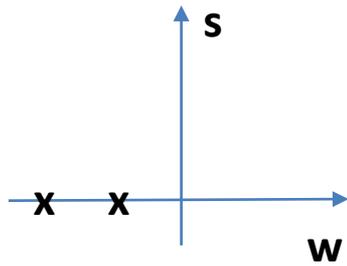
7) Seja o oscilador com ponte de Wien abaixo:



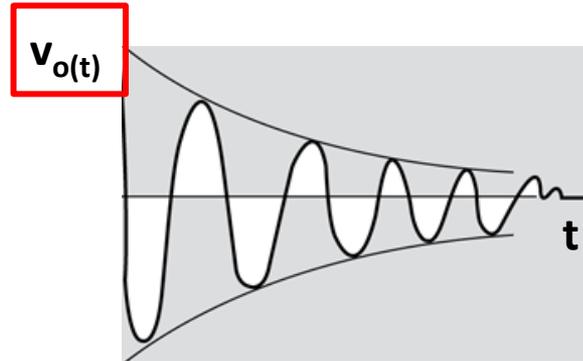
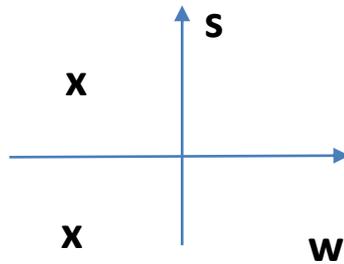
O oscilador com ponte de Wien pode ser visualizado como um amplificador com realimentação:



9 Se $G < 1$ os pólos são reais e negativos.

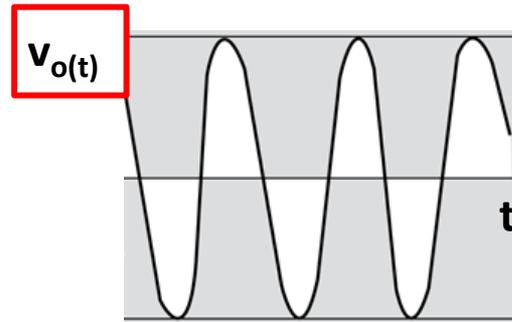
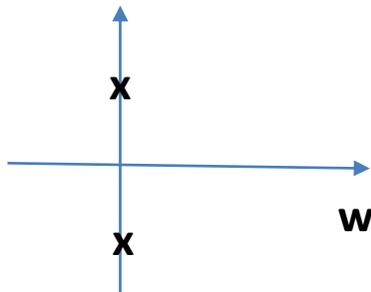


10 Se $1 < G < 3$ os pólos são complexos com parte real negativa.



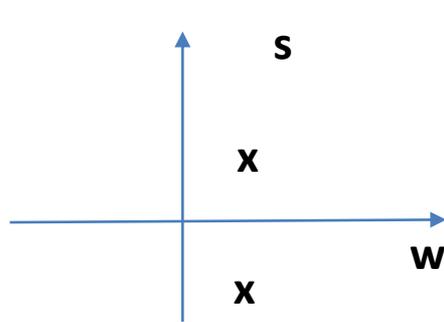
$$G = \frac{v_o}{v_i} = \frac{s\omega_0}{s^2 + 3\omega_0 s + \omega_0^2}$$

11 Se $G = 3$ os pólos são imaginários puros.

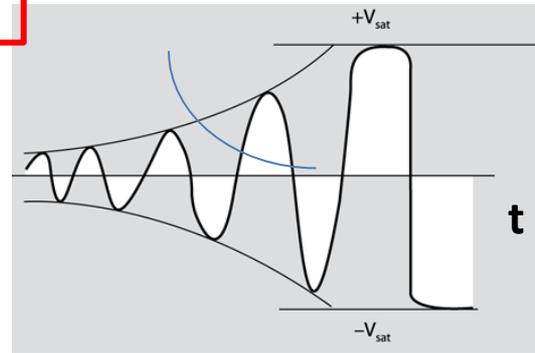


12

Se $3 < G < 5$ os pólos são complexos com parte real positiva.

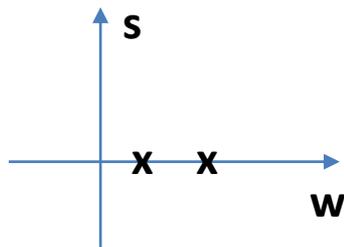


$V_o(t)$

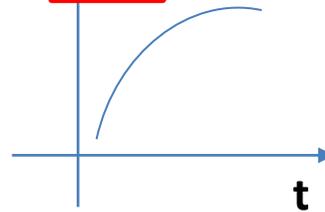


13

Se $G \geq 5$ os pólos são reais positivos.

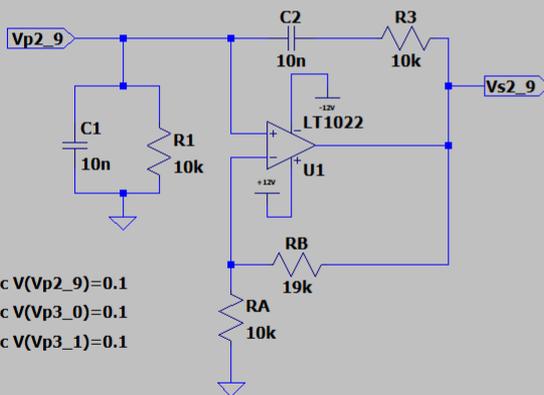


$V_o(t)$

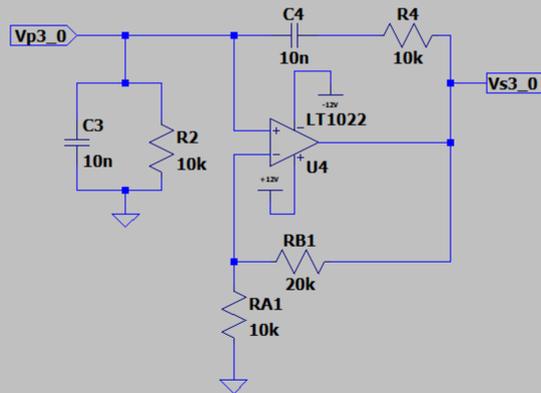


**Resultado de
Simulação
(sem CAG)**

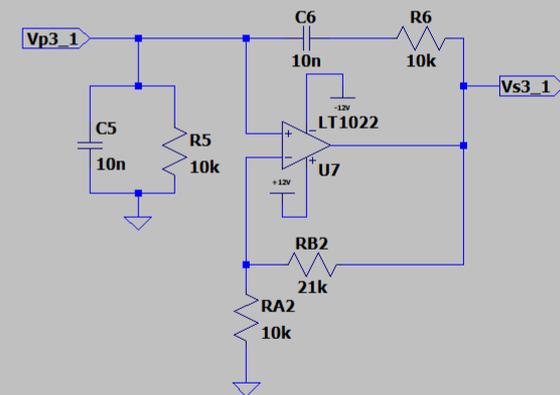
G=2.9



G=3.0



G=3.1



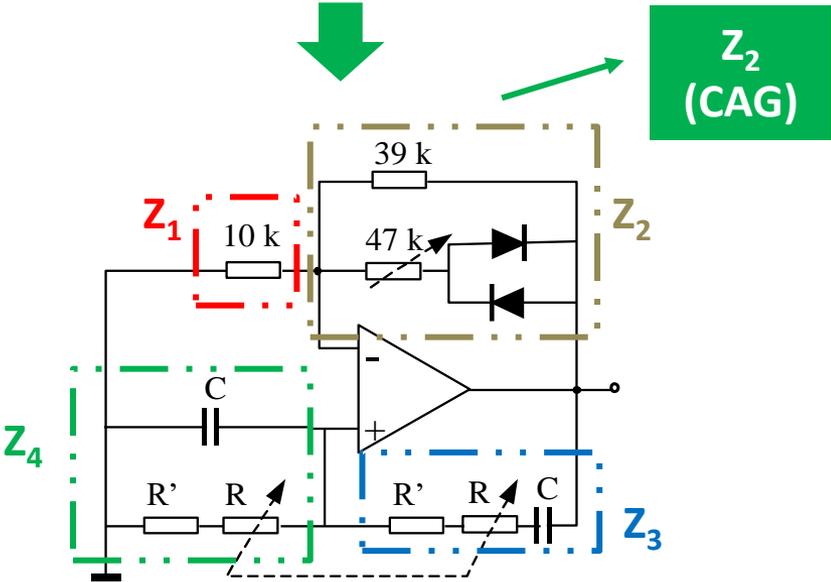
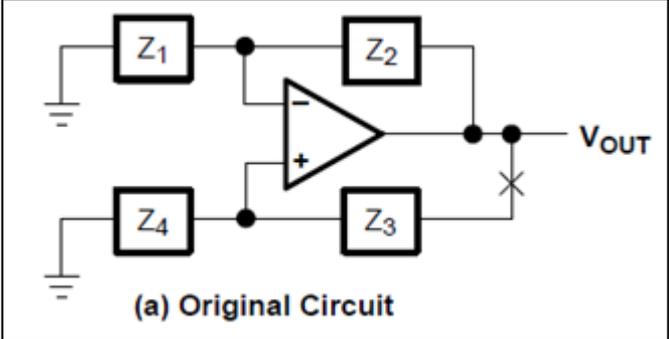
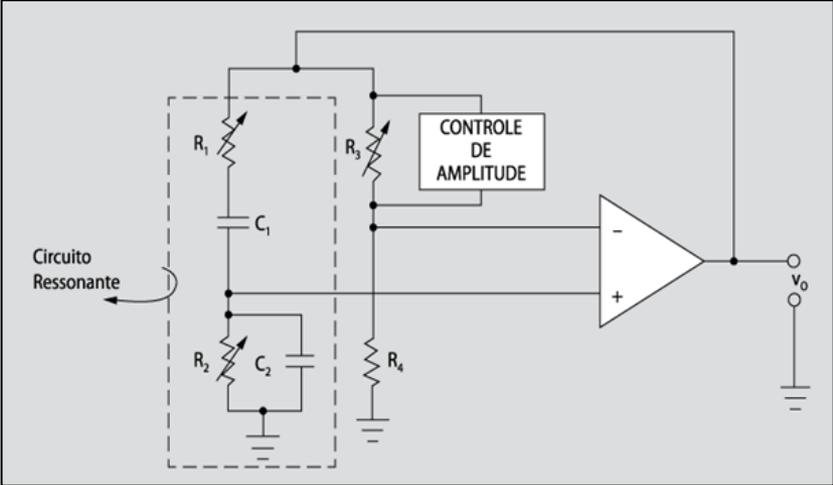
.tran 5ms
 .ic V(Vp2_9)=0.1
 .ic V(Vp3_0)=0.1
 .ic V(Vp3_1)=0.1

$$G = 1 + \frac{R_B}{R_A}$$

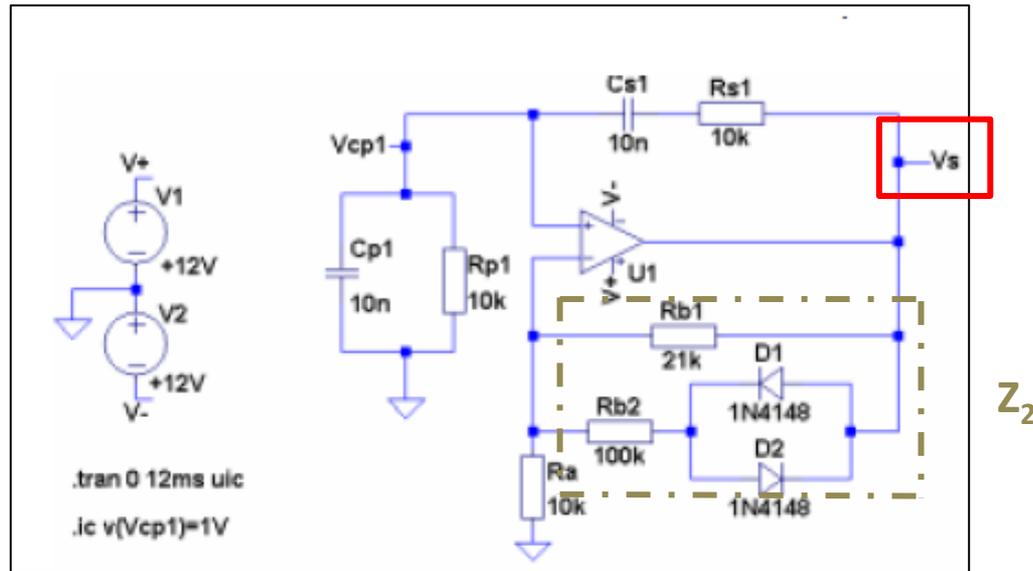
**Resultado de
Simulação
(com CAG)**

Oscilador de Wien com CAG

A introdução de um controle de ganho com diodos (Z_2) é uma das soluções !



Oscilador de Wien com CAG

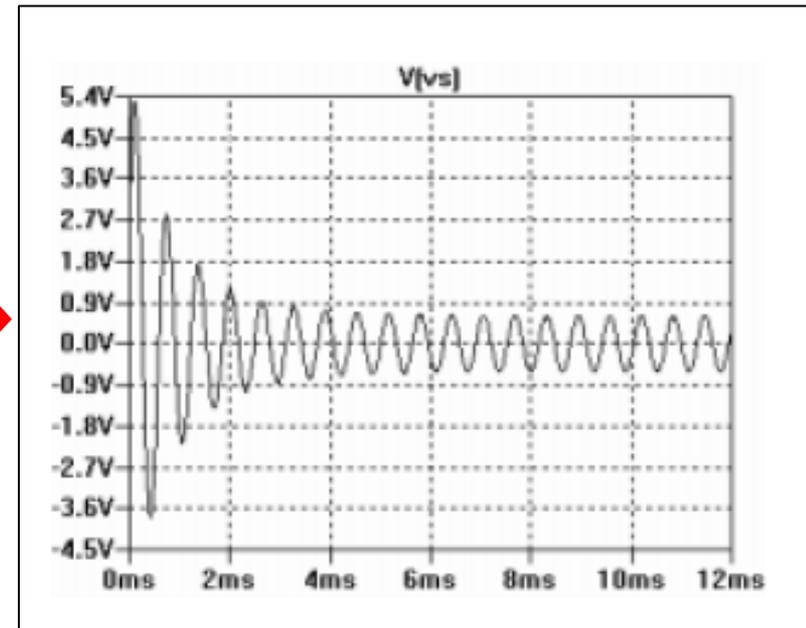
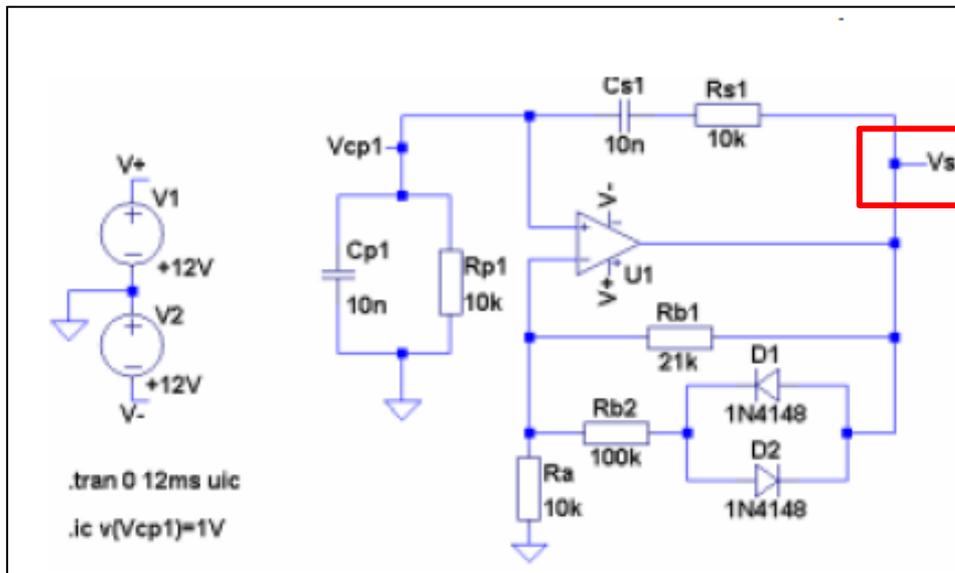


A resistência Z_2 do circuito consiste de um par de diodos e duas resistências, R_{b1} e R_{b2} . Supondo um dos diodos cortado, $R_b = R_{b1} // R_{b2}$ e o ganho do circuito é igual a $A = 1 + (R_b/R_a) = 1 + (21k/10k) = 3,1$.

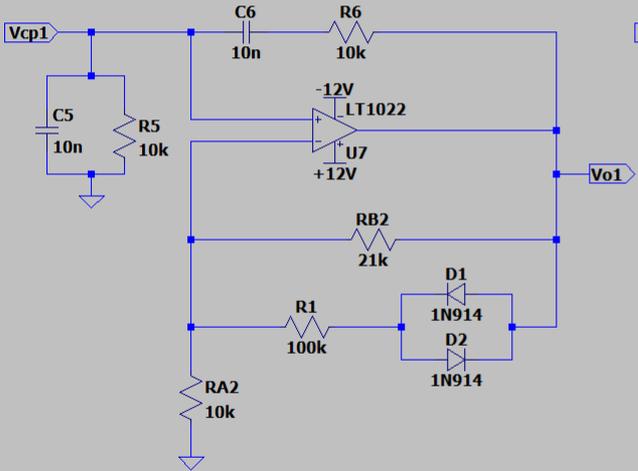
Para este valor de ganho a amplitude do sinal em V_s tende a aumentar levando os diodos gradualmente, e alternadamente, para a condução.

Com a condução dos diodos, o valor de R_b diminui devido a presença de R_{b2} em paralelo com R_{b1} e o circuito tende a se estabilizar em um nível de condução dos diodos tal que o ganho fique igual à 3.

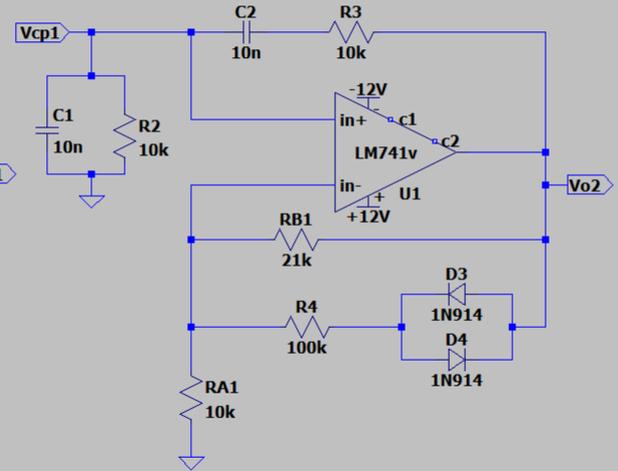
Oscilador de Wien com CAG



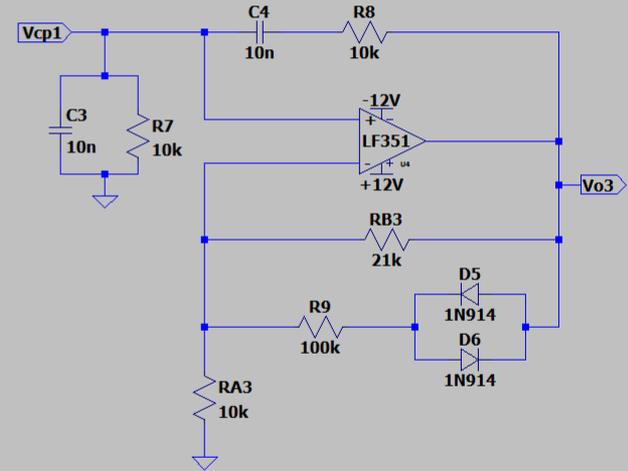
LT1022



LM741



LF351



.ic V(Vcp1)=0.1
.tran 12m