
Molecular dynamics of surfactants at fluid-fluid interface.

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Outline

❖ INTRODUCTION AND MOTIVATION

Contextualization

Literature review

Surfactants

Phase diagrams of microemulsion

Highlight

❖ METHODOLOGY

Molecular Dynamics

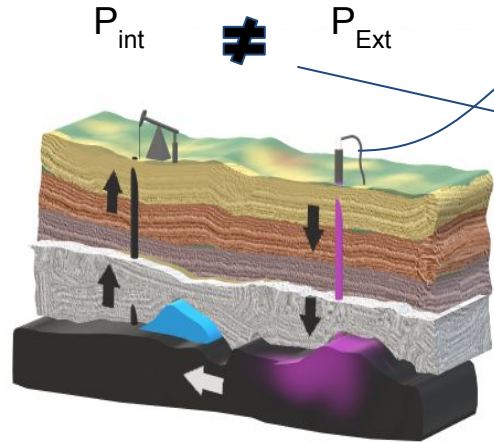
❖ PARTIAL RESULTS

One-Component Oil Interfaces with Surfactants

Multi-Component Oil Interfaces with Surfactants

❖ NEXT STEP

Contextualization



Secondary method

Primary method

EOR Method

Enhanced Oil Recovery

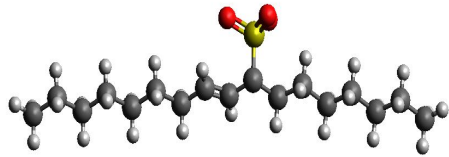
Thermal

Chemical

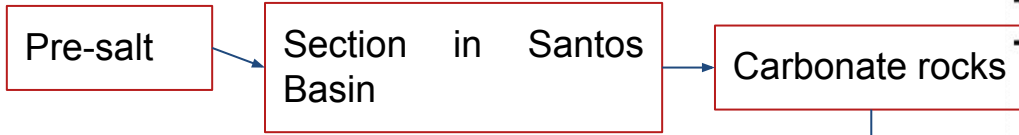
Gas

Surfactants

MD



LITERATURE REVIEW(PRE-SALT)


















calcite, dolomite and quartz.

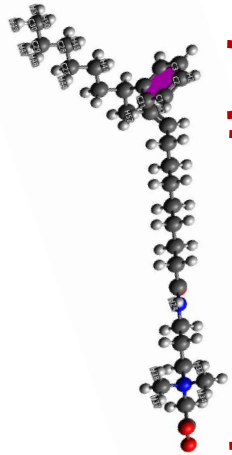
Diversity of pore geometries in the carbonates

- RESERVOIR**
- Pore geometry:
 - Geological mechanisms:
 - Pressure and Temperature:
 - Acid values (PH)

Direct influence on the fluid/fluid interface.

BASIC POROSITY TYPES					
FABRIC SELECTIVE			NOT FABRIC SELECTIVE		
	INTERPARTICLE	BP		FRACTURE FR	
	INTRAPARTICLE	WP		CHANNEL* CH	
	INTERCRYSTAL	BC		VUG* VUG	
	MOLDIC	MO		CAVERN* CV	
	FENESTRAL	FE			
	SHELTER	SH			
	GROWTH-FRAMEWORK	GF			
*Cavern applies to man-sized or larger pores of channel or vug shapes.					
FABRIC SELECTIVE OR NOT					
	BRECCIA BR		BORING BO		BURROW BU
					SHRINKAGE SK

Surfactants



Hydrophilic head

Hydrophobic tails

Surfactant Familie

- Anionic:
- Zwitterionic:
- Cationic:
- Non-ionic:

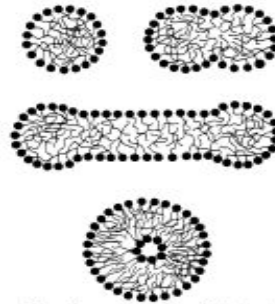
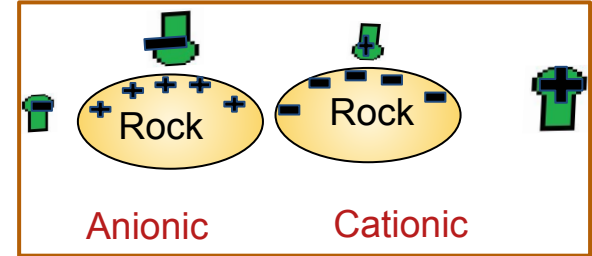


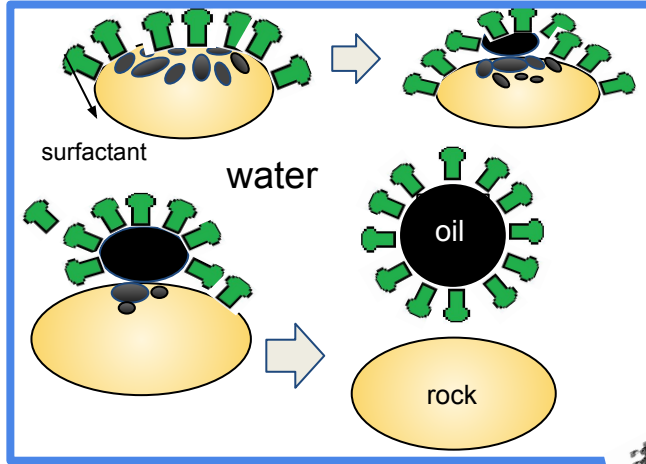
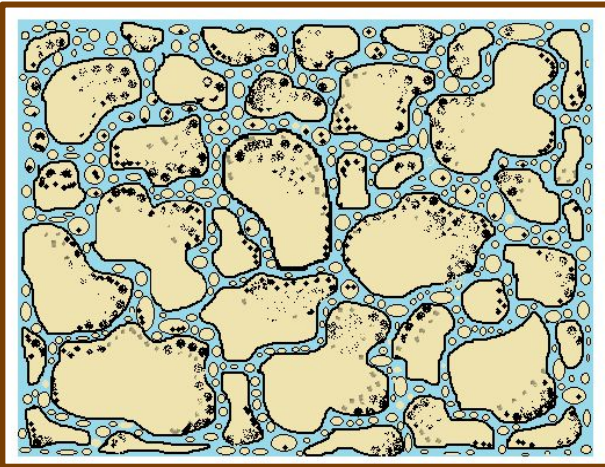
Figure 1. Schematic representation of the structures of surfactant aggregates in dilute aqueous solutions. Shown are aggregates that are spherical, rod-like, and bilayer vesicles.

DODECYL TRIMETHYL AMMONIUM BROMIDE (DTAB)



Exploring phase diagrams of microemulsion systems

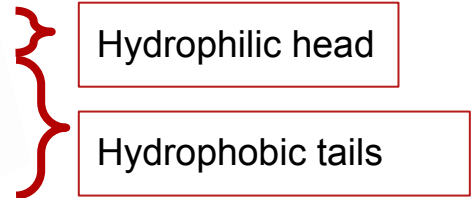
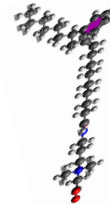
- Transition of Winsor:



Solubilization,
Emulsification, and
Roll-up



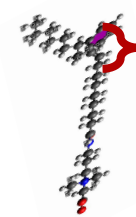
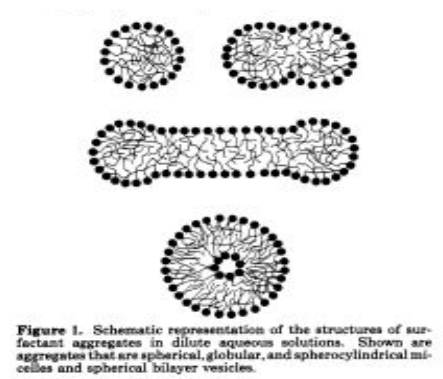
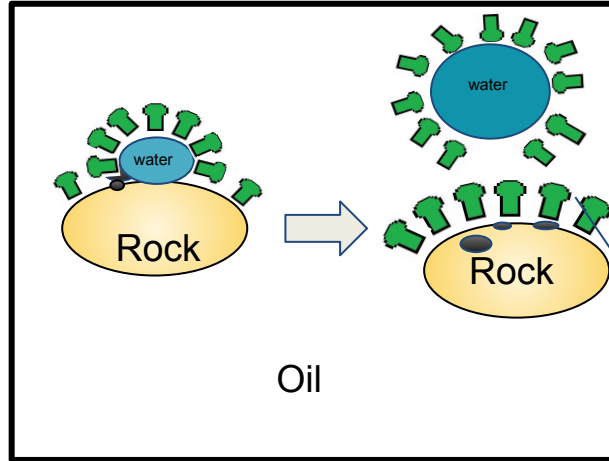
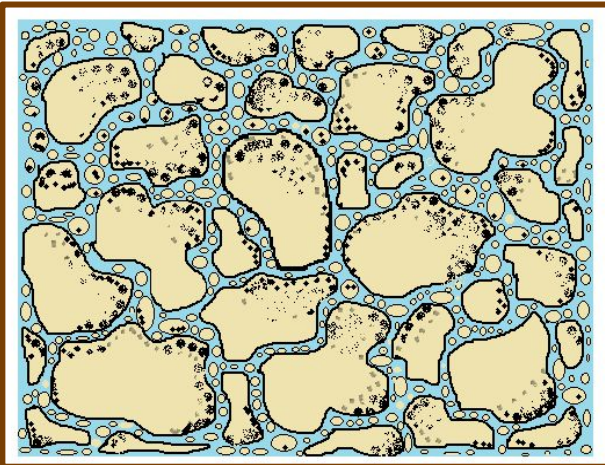
Oil/water microemulsion



positive curvature

Exploring phase diagrams of microemulsion systems

- Transition of Winsor:



Hydrophilic head

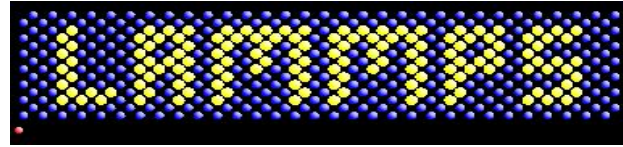
Hydrophobic tails

negative curvature

Methodology

Molecular Dynamics

- ❖ Surfactants Dodecyl box



- ❖ CGenFF CHARMM General Force Field and SPCE.

INTERFACES

- ❖ Surfactant/Water
- ❖ Surfactant/Brine
- ❖ Surfactant-Brine/Heptane
- ❖ Surfactant-Brine/Toluene
- ❖ Surfactant-Brine/Heptol

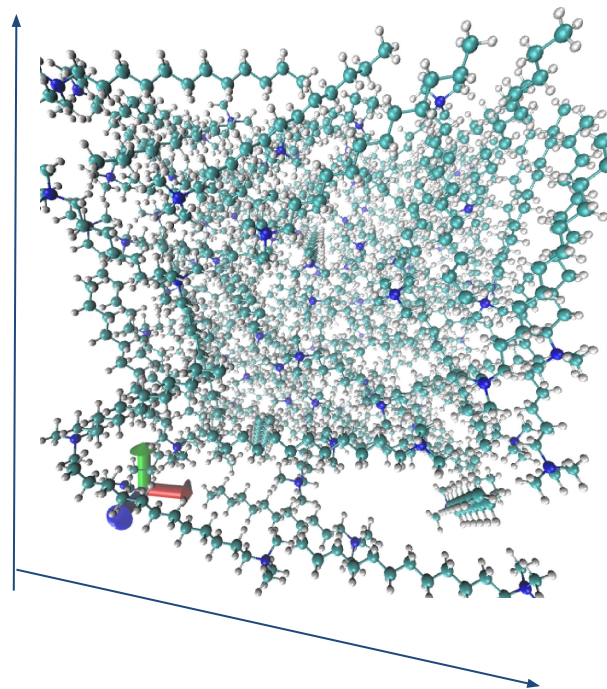
$$U = \sum_{\text{bonds}} k_b (b - b_0)^2 + \sum_{\text{angles}} k_\theta (\theta - \theta_0)^2 + \sum_{\text{dihedrals}} k_\phi [1 + \cos(n\phi - \delta)] \\ + \sum_{\text{impropers}} k_\omega (\omega - \omega_0)^2 + \sum_{\text{Urey-Bradley}} k_u (u - u_0)^2 \\ + \sum_{\text{nonbonded}} \epsilon \left[\left(\frac{R_{\text{min}_{ij}}}{r_{ij}} \right)^{12} - \left(\frac{R_{\text{min}_{ij}}}{r_{ij}} \right)^6 \right] + \frac{q_i q_j}{\epsilon r_{ij}}$$

$$\mathbf{F}_i = -\nabla U(\mathbf{r}) = - \sum_{j \neq i}^N \frac{\partial u(r_{ij})}{\partial r_{ij}} \hat{\mathbf{r}}_{ij}$$

Partial Results

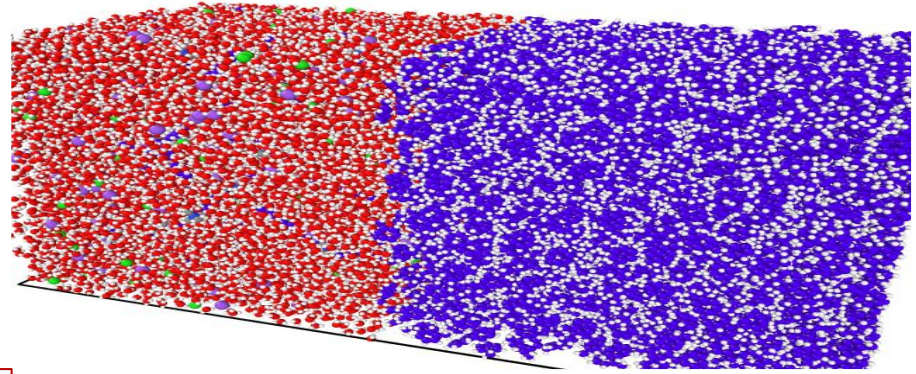
Computational Details

- Thermostat: Nosé-Hoover
 - LJ cutoff : 8,5Å e 10,0Å
 - Integrator: 0.5 fs time step
 - PPPM 10,0Å
 - Ensemble: NVT, NPT
 - T = 300K and P = 1atm
 - 100 molecules of the DTAB (N=1, H=34 E C=15)
 - Tolerance 2.0
- 50 ps NVT
 - 1 ns NVT
 - 1 ns NPT
 - 1 ns NPT

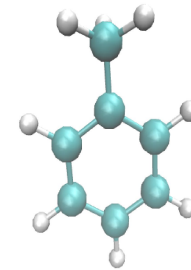
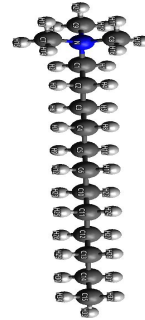


One-Component Oil Interfaces with Surfactants

- 70 x 140 x 70 Å
- 5 τ % NaCl
- Toluene/Surfactant-Brine
→ number 2.901 / 17.118



- 50 ps NVT
- 2 ns NPT
- 2 ns NVT structural property and dynamics
- 2 ns NPT to calculate IFT



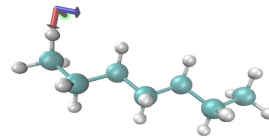
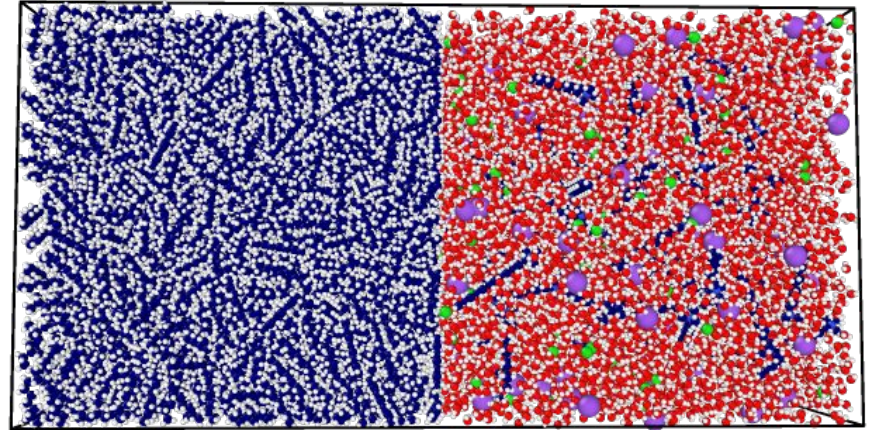
DTAB

$\rho = 0,8623 \text{ g/cm}^3$

One-Component Oil Interfaces with Surfactants

- 70 x 140 x 70 Å
- 5 τ % NaCl
- Heptane/Surfactant-Brine
→ number 2.089 / 11.468

- 50 ps NVT
- 2 ns NPT
- 2 ns NVT structural property and dynamics
- 2 ns NPT to calculated IFT



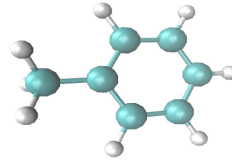
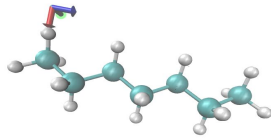
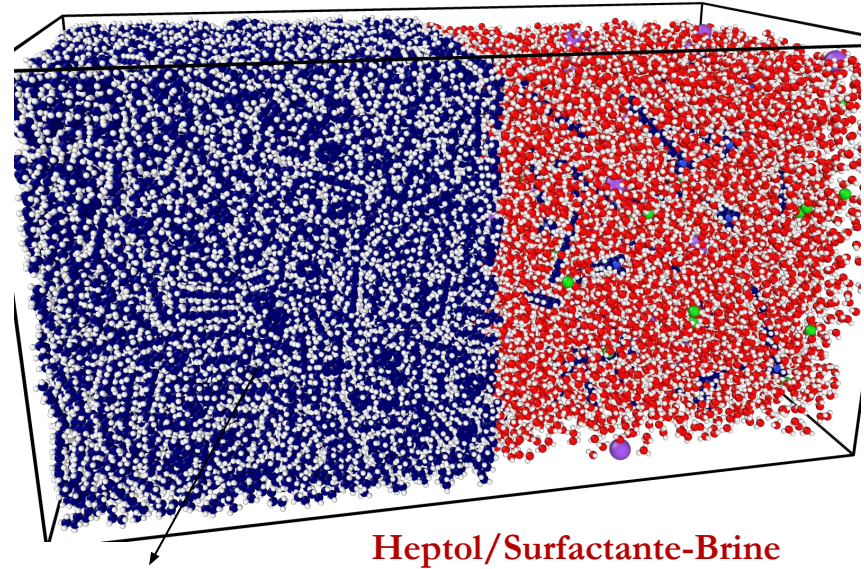
$$\rho = 0,6795 \text{ g/cm}^3$$



Multi-Component Oil Interfaces with Surfactants

- 50 ps NVT
- 2 ns NPT
- 2 ns NVT structural property and dynamics
- 2 ns NPT to calced IFT

- HEPTOL: 50% Heptane and 50% Toluene



$$\rho = 0,6795 \text{ g/cm}^3$$

$$\rho = 0,8623 \text{ g/cm}^3$$

Next step

- Calculate the Tilt and Rotation Angle of Chain Molecules. (Surfactant Bilayers: Temperature-dependent tilt)
- Interfaces between multi-component oil and brine/surfactant.
- Oil model 8 and 36 components.
- CMC

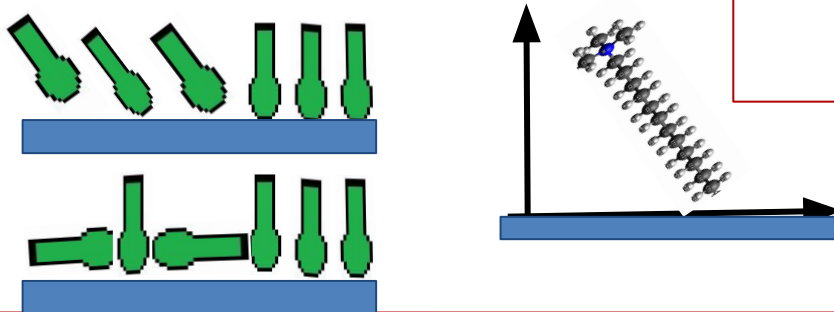


Tabela 6.3.1 – Valores de IFT das interfaces entre os modelos de cloretos e cada tipo de óleo, incluindo a água do mar. O erro padrão é de 0,2 mN/m

Salmoura	$\tau\%$	Médio	Leve	HepTol	Tolueno	Heptano
CaCl ₂	1,0	49,7	50,2	45,3	41,4	51,7
	3,5	51,3	49,6	46,8	42,1	52,6
	5,0	51,5	51,2	45,5	42,7	51,2
MgCl ₂	1,0	50,1	49,5	44,4	40,7	51,8
	3,5	51,0	49,3	45,1	41,2	51,5
	5,0	52,7	48,7	47,1	43,8	52,4
NaCl	1,0	49,3	49,9	44,3	41,9	51,8
	3,5	50,3	50,3	45,3	42,2	51,3
	5,0	50,3	50,7	45,9	41,6	51,5
KCl	1,0	50,5	48,6	43,4	40,9	51,5
	3,5	50,4	48,4	44,2	42,7	52,3
	5,0	50,2	48,9	45,6	41,1	51,5
Água do Mar	3,5	50,8	49,9	45,6	42,4	51,7

Components Oil models

Tabela 4.0.1 – Composição das moléculas para o modelo de óleo proposto neste trabalho.

Classe	Porcentagem (%)	Componentes
C ₃	0,61	Propano
NC ₄	0,32	Butano
IC ₄	1,07	Isopropano
NC ₅	0,82	Pentano
IC ₅	1,46	Isobutano
C ₆	3,17	Hexano, ciclohexano
C ₇	5,78	Heptano, benzeno, cicloheptano, tolueno
C ₈	7,45	Octano, ciclooctano, o-xileno, m-xileno, p-xileno
C ₉	6,59	Nonano, 1,2,3-Trimetilbenzeno, 1,2,4-trimetilbenzeno, 1,3,5-trimetilbenzeno
C ₁₀	6,03	Decano, naftaleno
C ₁₁	4,94	Undecano
C ₁₂	4,43	Dodecano
C ₁₃	4,51	Tridecano
C ₁₄	3,80	Tetradecano, antraceno, fenantreno
C ₁₅	3,74	Pentadecano
C ₁₆	2,86	Hexadecano, pireno
C ₁₇	2,50	Heptadecano
C ₁₈	2,67	Octadecano
C ₁₉	2,38	Nonadecano
C ₂₀₊	34,88	Eicosano, benzopireno

Componente	Número de moléculas	$\rho_{calculado}$	ρ_{expt}^{131}	Erro (%)
Hexano	2343	0,6436	0,6549	1,7
Heptano	2105	0,6704	0,6795	1,3
Octano	1885	0,6912	0,6984	1,0
Nonano	1718	0,7075	0,7142	0,9
Decano	1582	0,7226	0,7300	1,0
Undecano	1460	0,7328	0,7402	1,0
Dodecano	1357	0,7421	0,7495	1,0
Benzeno	3450	0,8513	0,8738	2,6
Tolueno	2902	0,8505	0,8623	1,4

Gibbs free energy model

$$G_f = N_w \mu_w^o + N_{sA} \mu_{1A}^o + N_{sB} \mu_{1B}^o + \sum_{g=2}^{\infty} N_g g \Delta \mu_g^o$$

$$g \Delta \mu_g^o = \mu_g^o - g_A \mu_{1A}^o - g_B \mu_{1B}^o.$$

$$G_m = kT \left[N_w \ln X_w + N_{1A} \ln X_{1A} + N_{1B} \ln X_{1B} + \sum_{g=2}^{\infty} N_g \ln X_g \right]$$

$$\begin{aligned} G' &= G - N_w \mu_w^o - N_{sA} \mu_{1A}^o - N_{sB} \mu_{1B}^o \\ &= \sum_{g=2}^{\infty} N_g g \Delta \mu_g^o + kT \left[N_w \ln X_w + N_{1A} \ln X_{1A} + N_{1B} \ln X_{1B} + \sum_{g=2}^{\infty} N_g \ln X_g \right] \end{aligned}$$

$$\frac{G'}{kT} = \sum_{g=2}^{\infty} N_g g \frac{\Delta \mu_g^o}{kT} + N_w \ln X_w + N_{1A} \ln X_{1A} + N_{1B} \ln X_{1B} + \sum_{g=2}^{\infty} N_g \ln X_g$$

Free energy of formation of the aggregate-water core interface.

$$\left(\frac{\Delta\mu_g^0}{kT} \right)_{\text{int}} = \frac{\sigma_{\text{agg}}}{kT} (a - \alpha_{gA} a_{oA} - \alpha_{gB} a_{oB})$$

Aggregate-water core interfacial tension.

$$\sigma_{\text{tail}} = 35,0 - 325M^{-2/3} - 0,098(T - 298)$$

$$\sigma_w = 72,0 - 0,16(T - 298)$$

$$\sigma_{\text{agg}} = \sigma_{\text{tail}} + \sigma_w - 2\sqrt{\sigma_{\text{tail}}\sigma_w}$$

Hydrocarbon surface tension

Acknowledgments

Cluster
Josephson



sampa



**Thank you for your
attention**
