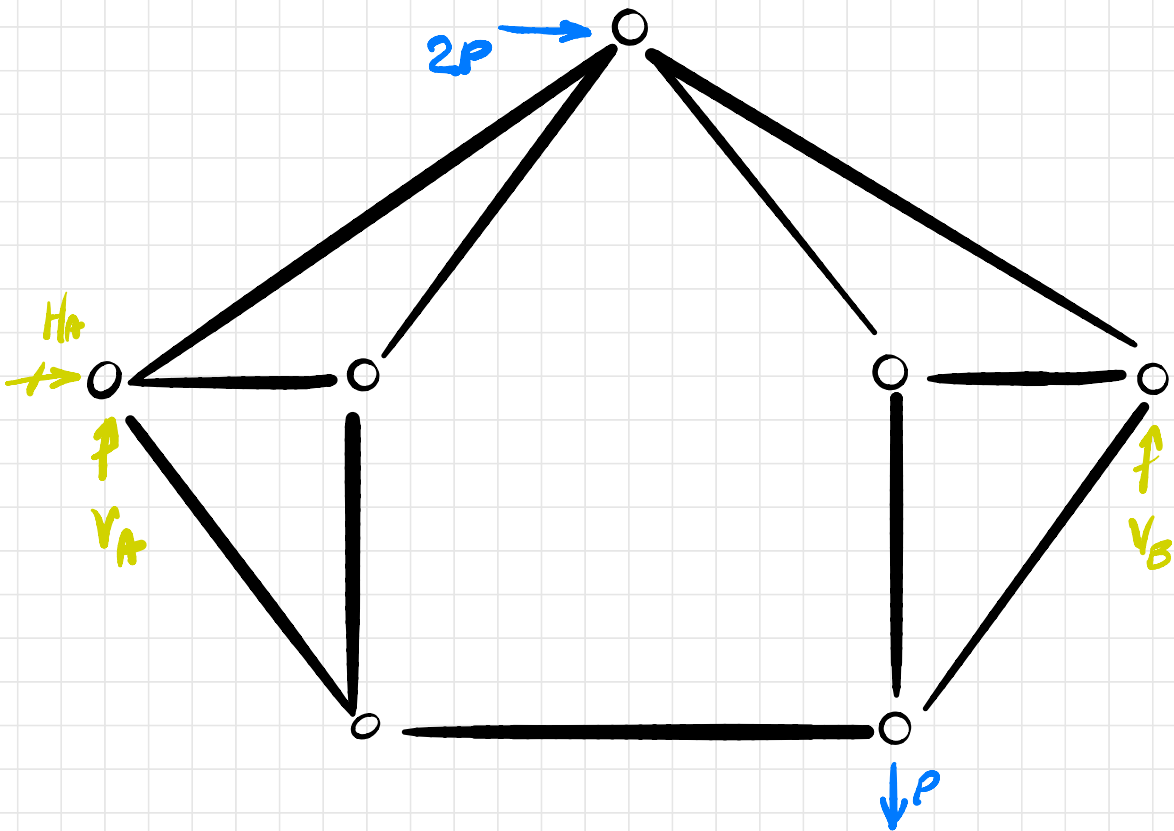


Determinar  $N_1$ ,  $N_2$  e  $N_6$ .

0,5 pontos por normal

total 1,5



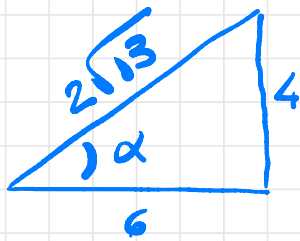
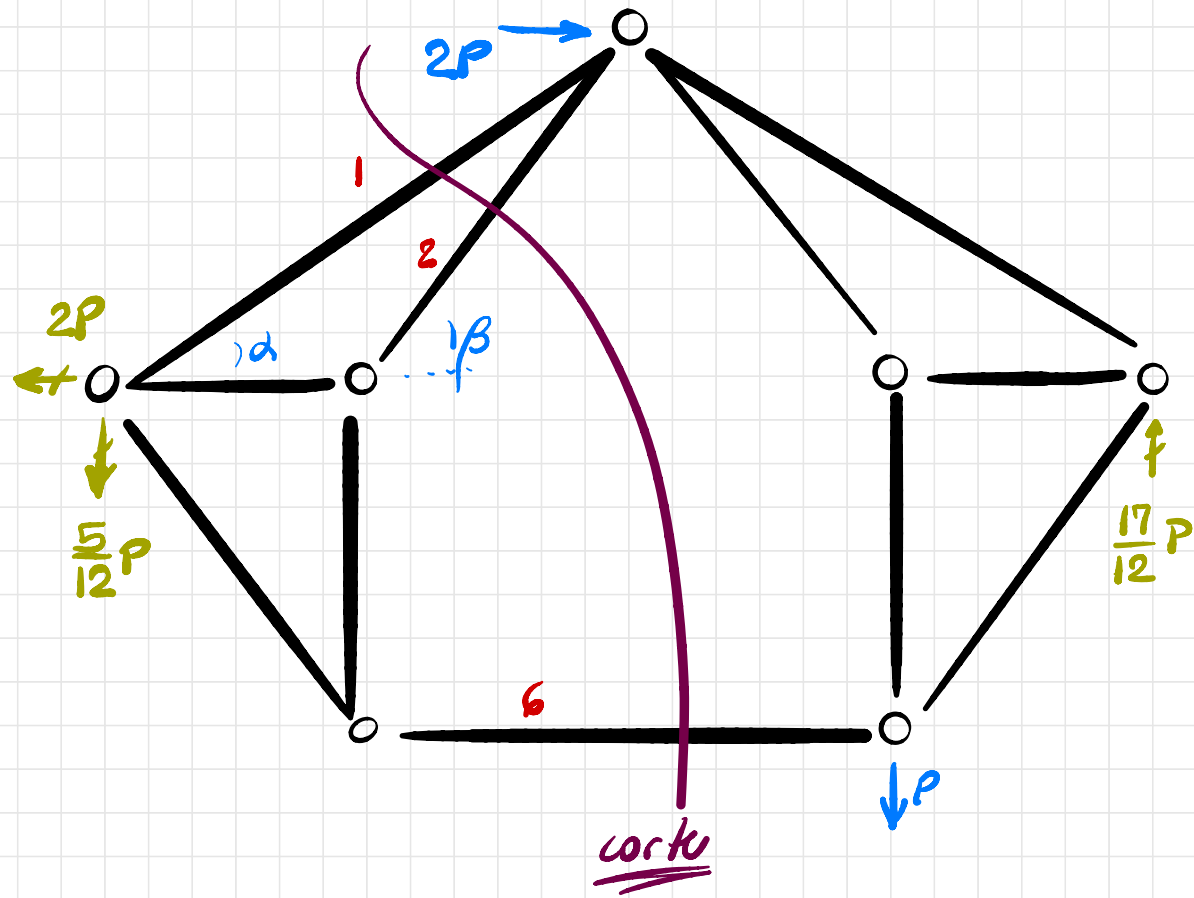
Equilibrio:

$$\sum F_H = 0: H_A + 2P = 0 \Rightarrow H_A = -2P$$

$$\sum F_V = 0: V_A + V_B - P = 0$$

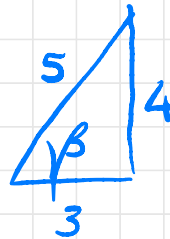
$$\odot \sum M_A = 0: -2P \cdot 4 - P \cdot 9 + V_B \cdot 12 = 0$$

$$V_B = \frac{17}{12}P \Rightarrow V_A = -\frac{5}{12}P$$



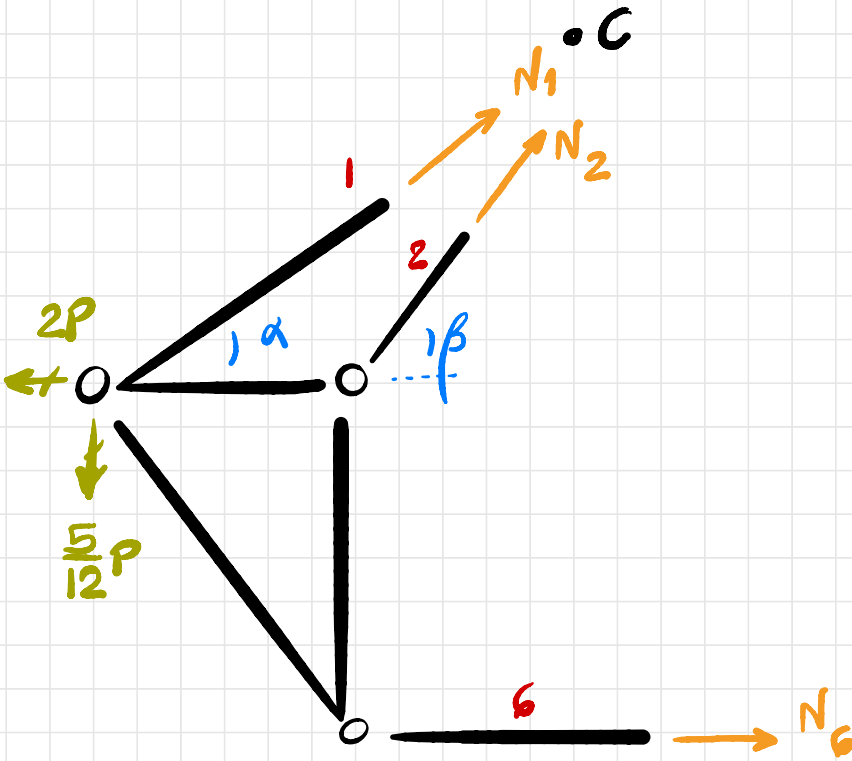
$$\sin \alpha = \frac{2}{\sqrt{13}}$$

$$\cos \alpha = \frac{3}{\sqrt{13}}$$



$$\sin \beta = \frac{4}{5}$$

$$\cos \beta = \frac{3}{5}$$



$$\sum F_H = 0: -2P + N_1 \cos \alpha + N_2 \cos \beta + N_6 = 0$$

$$\sum F_V = 0: -\frac{5}{12}P + N_1 \sin \alpha + N_2 \sin \beta = 0$$

$$\sqrt{\text{)}} \sum M_C = 0: N_6 \cdot 8 + \frac{5}{12}P \cdot 6 - 2P \cdot 4 = 0$$

$$8 \cdot N_6 = \frac{11}{2}P \Rightarrow N_6 = \frac{11}{16}P \quad 0,6875P$$

$$\begin{cases} N_1 \cos \alpha + N_2 \cos \beta = 2P - 11/16P = 21/16P \\ N_1 \sin \alpha + N_2 \sin \beta = 5/12P \end{cases}$$

$$\frac{3}{\sqrt{13}} N_1 + \frac{3}{5} N_2 = \frac{21}{16} P \Rightarrow \frac{N_1}{\sqrt{13}} + \frac{N_2}{5} = \frac{7}{16} P$$

$$\frac{2}{\sqrt{13}} N_1 + \frac{4}{5} N_2 = \frac{5}{12} P \Rightarrow \frac{N_1}{2\sqrt{13}} + \frac{N_2}{5} = \frac{5}{48} P$$

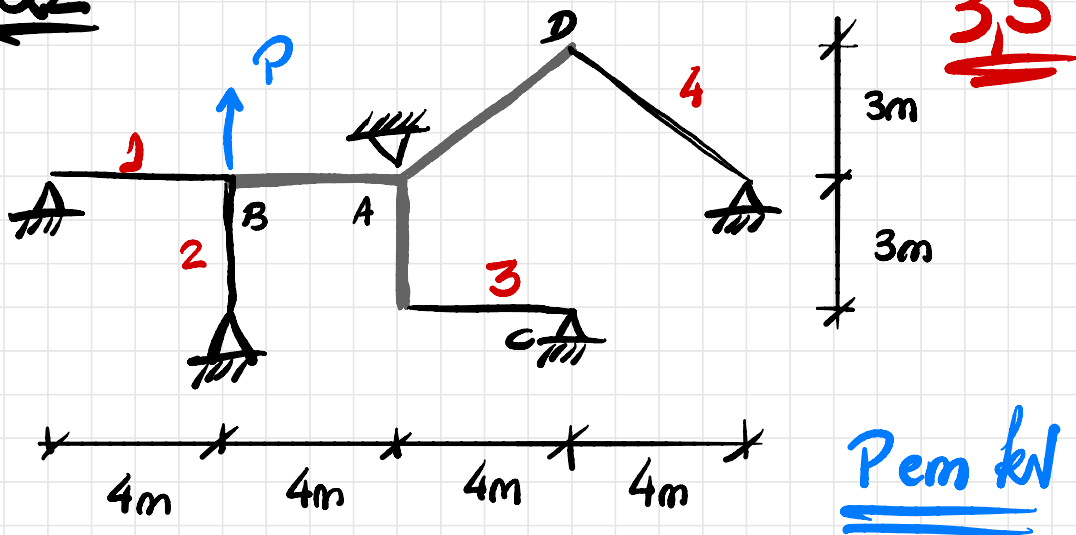
$$\frac{N_1}{\sqrt{13}} - \frac{N_1}{2\sqrt{13}} = \frac{7}{16} P - \frac{5}{48} P$$

$$\frac{N_1}{2\sqrt{13}} = \frac{P}{3} \Rightarrow N_1 = \frac{2\sqrt{13}}{3} P \quad 2404P$$

$$\frac{N_2}{5} = \frac{7}{16} P - \frac{1}{\sqrt{13}} \left( \frac{2\sqrt{13}}{3} P \right) = \frac{7}{16} P - \frac{2}{3} P = -\frac{11}{48} P$$

$$N_2 = -\frac{55}{48} P \quad -1,146P$$

Q2

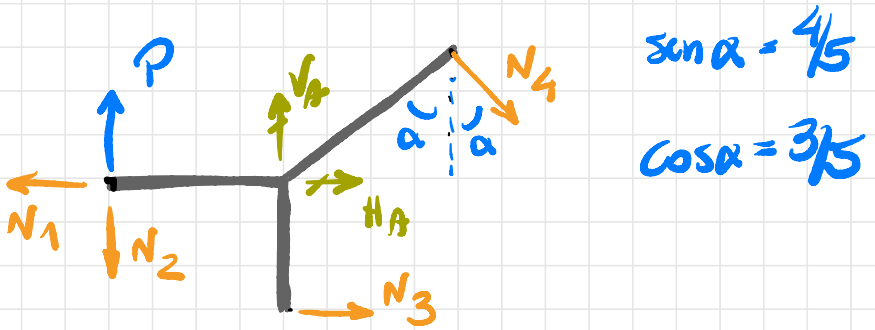


Determinar a área mínima, considerando que a barra ABCD é rígida e:

$$\left\{ \begin{array}{l} \bar{\sigma} = 160 \text{ MPa} \\ \bar{\varphi}_{AB} = 0,01 \text{ rad} \end{array} \right.$$

- considere que os fios são do mesmo material e têm a mesma área.

$$E = 200 \text{ GPa}$$



Equilibrio:

$$\sum F_H = 0: -N_1 + H_A + N_3 + N_4 \sin \alpha = 0$$

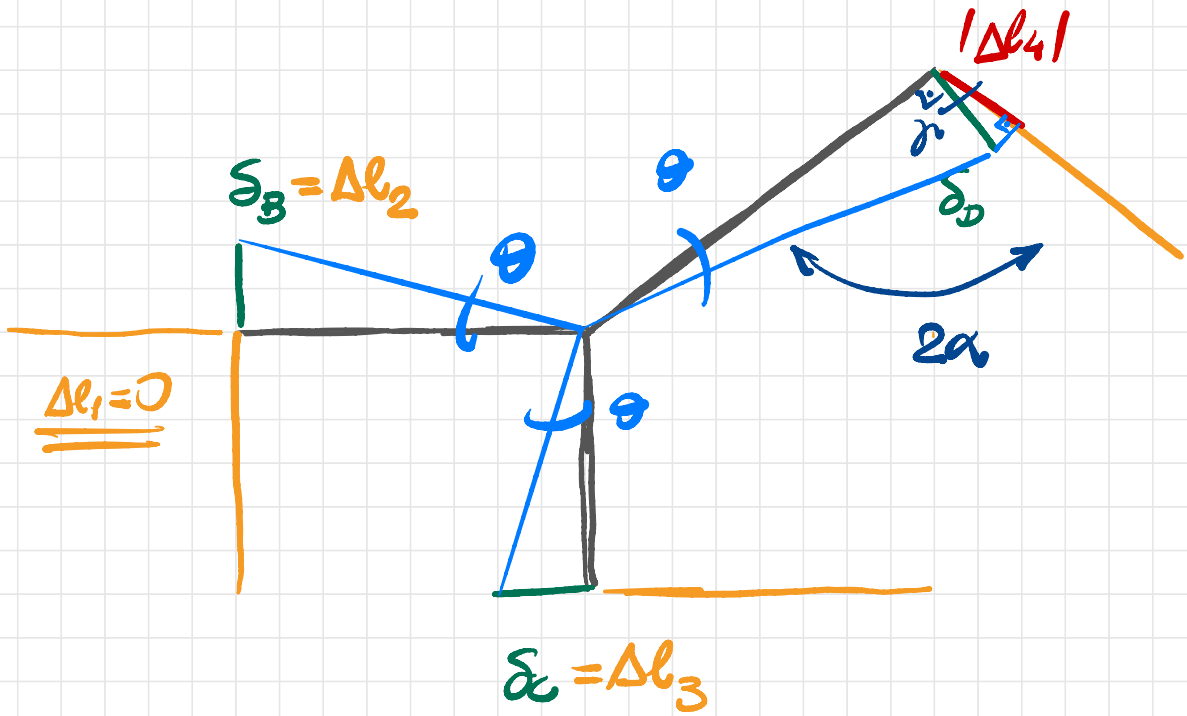
$$\sum F_V = 0: -N_2 + P + V_A - N_4 \cos \alpha = 0$$

$$\begin{aligned} \text{v)} \sum M_A = 0: & -P \cdot 4 + N_2 \cdot 4 + N_3 \cdot 3 - N_4 \cdot \cos \alpha \cdot 4 \\ & - N_4 \sin \alpha \cdot 3 = 0 \end{aligned}$$

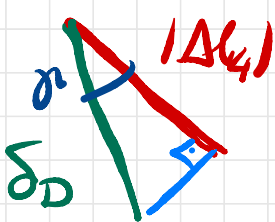
$$4N_2 + 3N_3 - \frac{24}{5}N_4 = 4P$$

$$20N_2 + 15N_3 - 24N_4 = 20P$$

# Diagrama de Williot:



$$\frac{\pi}{2} + \delta = 2\alpha \Rightarrow \delta = 2\alpha - \frac{\pi}{2}$$



$$\cos \delta = \frac{|\Delta l_4|}{\delta_D} \Rightarrow \delta_D = \frac{|\Delta l_4|}{\cos \delta}$$

$$\cos \delta = \cos(2\alpha - \frac{\pi}{2}) = \sin 2\alpha = 2\sin \alpha \cos \alpha = \frac{24}{25}$$



Resumiendo:

Más:

$$\Delta l_1 = 0$$

$$\delta_B = \Delta l_2$$

$$\delta_C = \Delta l_3$$

$$\delta_D = \frac{|\Delta l_4|}{\cos \theta}$$

$$\operatorname{tg} \theta = \frac{\delta_B}{4} = \frac{\delta_C}{3} = \frac{\delta_D}{5}$$

$\bar{E}$ :

$$\Delta l_i = \frac{N_i l_i}{EA} \rightarrow \text{memos } E \text{ e } A$$

$$\frac{\Delta l_2}{4} = \frac{\Delta l_3}{3} \Rightarrow \frac{N_2 l_2}{4EA} = \frac{N_3 l_3}{3EA}$$

$$\frac{N_2 \cdot 3}{4} = \frac{N_3 \cdot 4}{3} \Rightarrow N_2 = \frac{16}{9} N_3$$

$$\frac{\Delta l_2}{4} = \frac{|\Delta l_4|}{\frac{5 \cdot 24}{25}} \Rightarrow \frac{N_2 l_2}{4EA} = \frac{5 |N_4| l_4}{24 \cdot EA}$$

$$\frac{N_2 \cdot 3}{4} = \frac{|N_4| \cdot 25}{24} \Rightarrow N_2 = \frac{100}{72} |N_4|$$

Assim:

$$N_1 = 0; N_3 = \frac{9}{16} N_2; N_4 = -\frac{18}{25} N_2$$

Voltando ao equilíbrio:

$$20N_2 + 15\left(\frac{9}{16}N_2\right) - 24\left(-\frac{18}{25}N_2\right) = 20P$$

$$\left(20 + \frac{135}{16} + \frac{432}{25}\right)N_2 = 20P$$

$$\frac{18287}{400}N_2 = 20P$$

$$N_1 = 0$$

$$N_2 = 0,437P$$

$$N_3 = 0,246P$$

$$N_4 = -0,315P$$

Dimensionando: ① tensão:

Como  $|N_2| > |N_3|$  e  $|N_2| > |N_4|$

$$\max(|\sigma_2|, |\sigma_3|, |\sigma_4|) = |\sigma_2|$$

$$|\sigma_2| \leq \bar{\sigma}$$

$$\frac{N_2}{A} \leq \bar{\sigma} \Rightarrow A \geq \frac{N_2}{\bar{\sigma}} = \frac{0,437P \cdot 10^3}{160 \cdot 10^6}$$

em N

em Pa

$$A \geq 2,73 \cdot 10^{-6} P \text{ [m}^2\text{]}$$

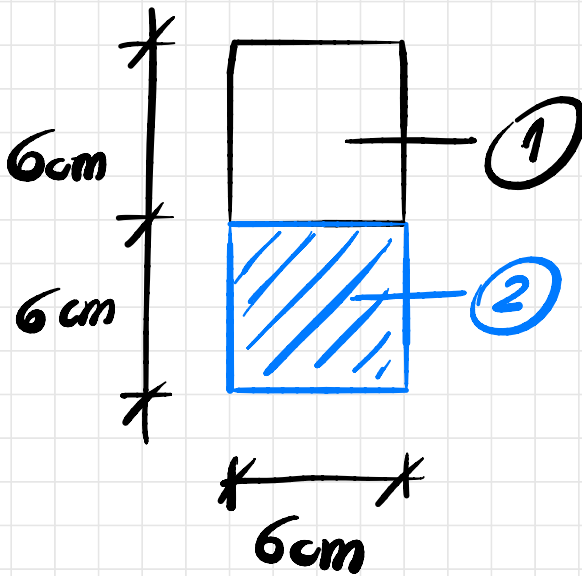
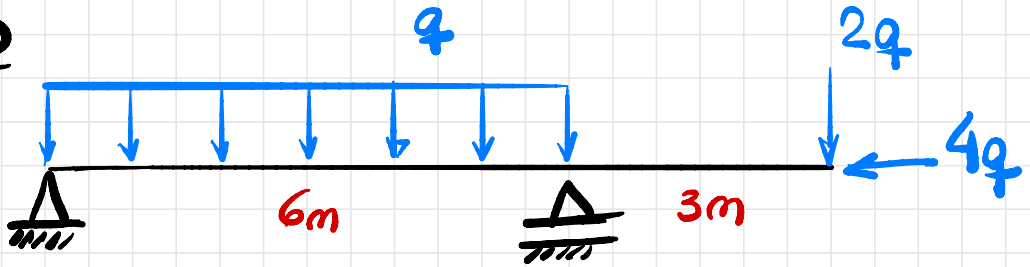
② giro máximo:

$$\varphi \approx \theta \approx \frac{\delta_B}{4} = \frac{N_2 l_2}{4EA} \leq \bar{\varphi}$$

$$A \geq \frac{N_2 l_2}{4E\bar{\varphi}} = \frac{0,437P \cdot 10^3 \cdot 3}{4 \cdot 200 \cdot 10^9 \cdot 0,01} = 1,63 \cdot 10^{-7} P \text{ [m}^2\text{]}$$

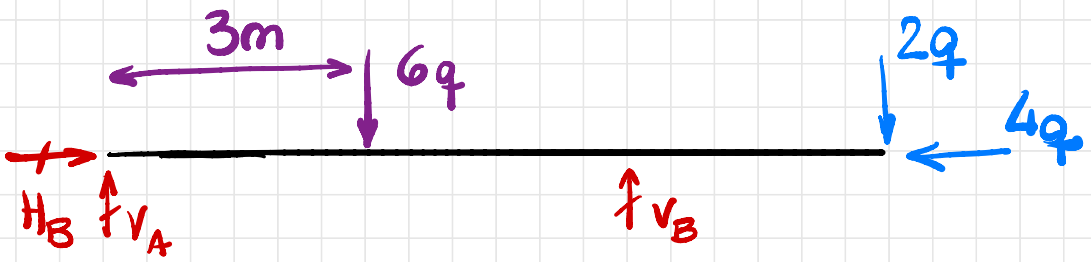
$$\text{Logo } A_{\min} = 2,73 \cdot 10^{-6} P \text{ [m}^2\text{]}$$

Q3



$$E_1 = 20 \text{ GPa}$$
$$E_2 = 70 \text{ GPa}$$

35



$$\sum F_H = 0: H_B - 4q = 0 \Rightarrow \boxed{H_B = 4q}$$

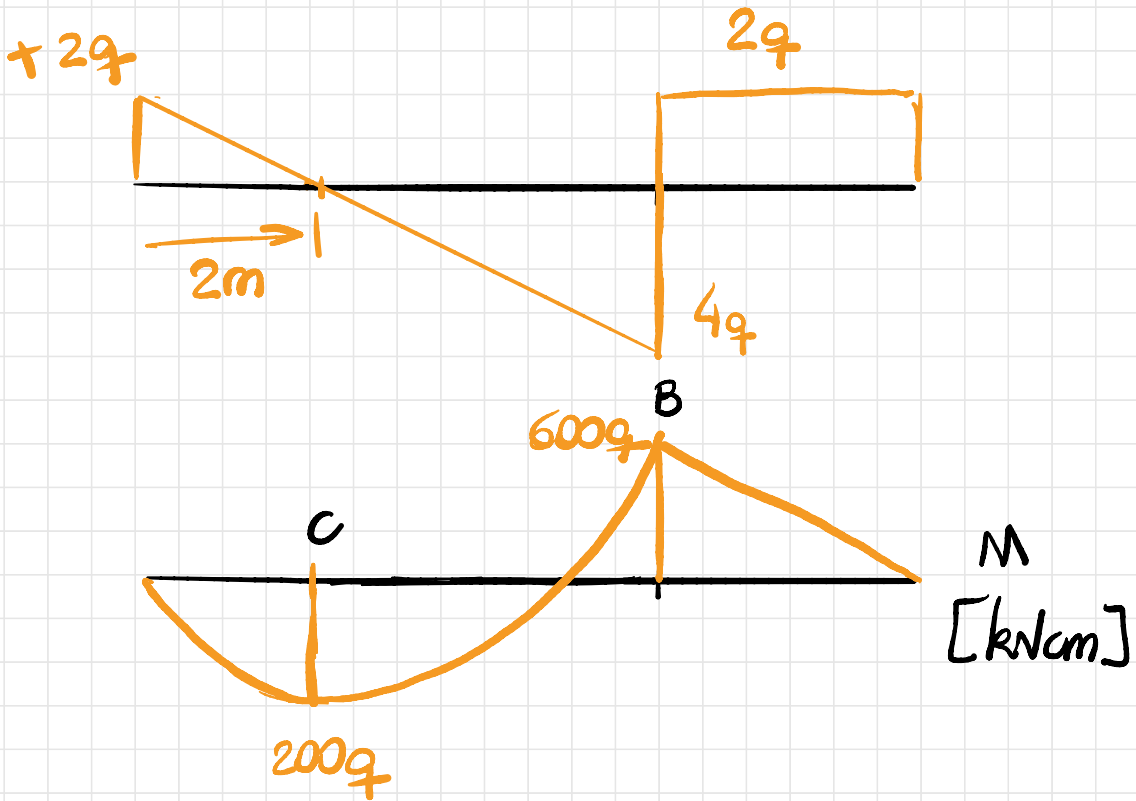
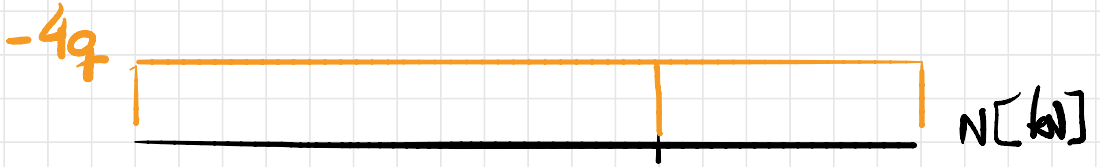
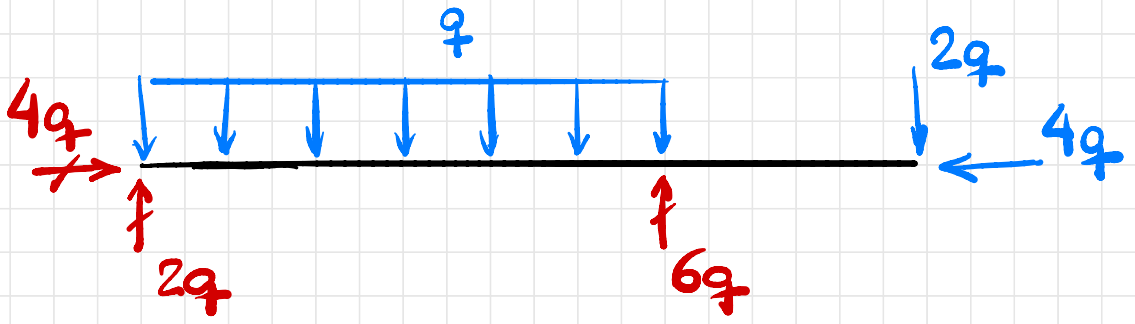
$$\sum F_V = 0: V_A - 6q + V_B - 2q = 0 \Rightarrow V_A + V_B = 8q$$

$$\textcircled{+}) \sum M_A = 0: -6q \cdot 3 + V_B \cdot 6 - 9 \cdot 2q = 0$$

$$6V_B = 18q + 18q$$

$$\boxed{V_B = 6q}$$

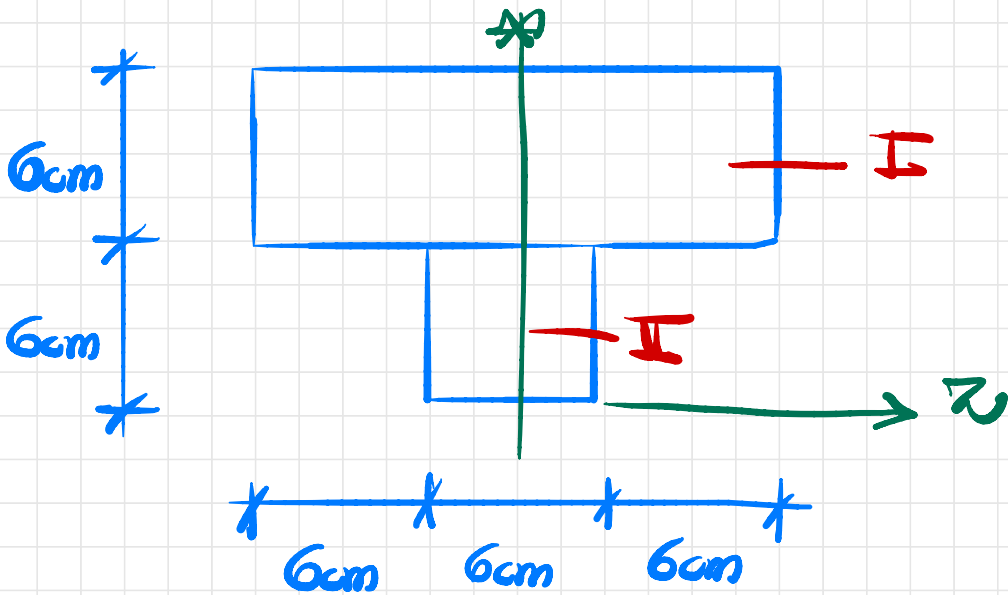
$$V_A = 8q - 6q \Rightarrow \boxed{V_A = 2q}$$



# Propriedades da seção transversal:

- escolhendo ② como base:

$$b_{eq} = \frac{E_1}{E_2} b = \frac{210}{70} b = 3 \cdot 6 = 18 \text{ cm}$$



	$y_a$	$A$	$d$	$d^2 A$	$I_w$
I	9	108	1,5	243	324
II	3	36	4,5	729	108

$$y_G = \frac{9 \cdot 108 + 3 \cdot 36}{108 + 36} = \frac{1080}{144} = 7,5 \text{ cm}$$

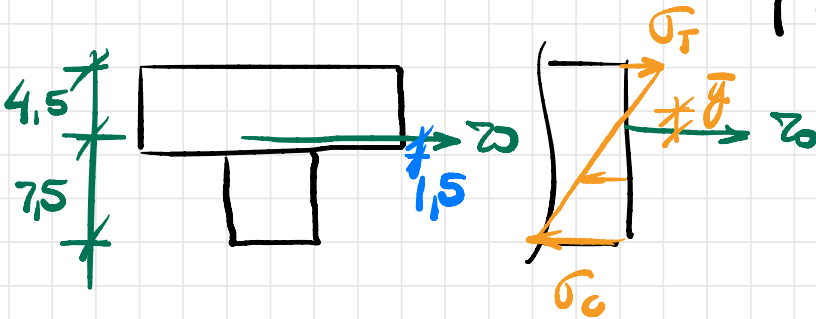
$$A = 144 \text{ cm}^2$$

$$I_z = (324 + 243) + (108 + 729)$$

$$I_z = 1404 \text{ cm}^4$$

Cálculo das tensões em B

$$\left\{ \begin{array}{l} M = -600q \text{ [kNm]} \\ N = -4q \text{ [kN]} \end{array} \right.$$



$$\sigma = -\frac{4q}{144} - \frac{600q}{1404} y$$

$$y \text{ [cm]}$$

$$\sigma \text{ [kN/cm}^2\text{]}$$

linha neutra:  $\sigma = 0$ .

$$-\frac{4q}{144} = \frac{600q}{1404} \bar{y} \Rightarrow \bar{y} = -0,065 \text{ cm}$$



$$\sigma_T = -\frac{4q}{144} - \frac{600q}{1404} \cdot (-4,5) = 1,895q$$

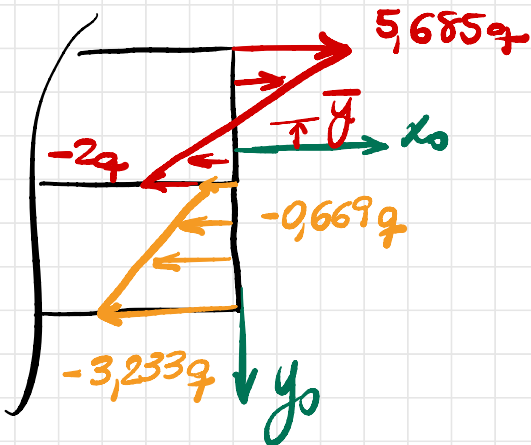
$$\sigma_C = -\frac{4q}{144} - \frac{600q}{1404} \cdot 7,5 = -3,233q$$

$$\sigma_I = -\frac{4q}{144} - \frac{600q}{1404} \cdot 1,5 = -0,669q$$

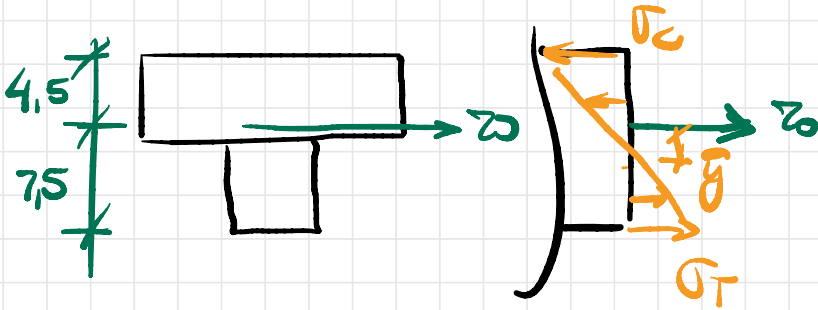
no material ①:

$$\sigma_T^{\text{①}} = 3\sigma_T = 5,685q$$

$$\sigma_T^{\text{②}} = 3\sigma_T = -2q \quad (\approx 2,007q)$$



Cálculo das tensões em C  $\left\{ \begin{array}{l} M = 200q \\ N = -4q \end{array} \right.$



$$\sigma = -\frac{4q}{144} + \frac{200q}{1404}y$$

linha neutra:  $\sigma = 0$

$$\frac{4q}{144} = \frac{200q}{1404}\bar{y} \Rightarrow \bar{y} = 0,195\text{cm}$$

$$\sigma_T = -\frac{4q}{144} + \frac{200q}{1404} \cdot 7,5 = 1,04q$$

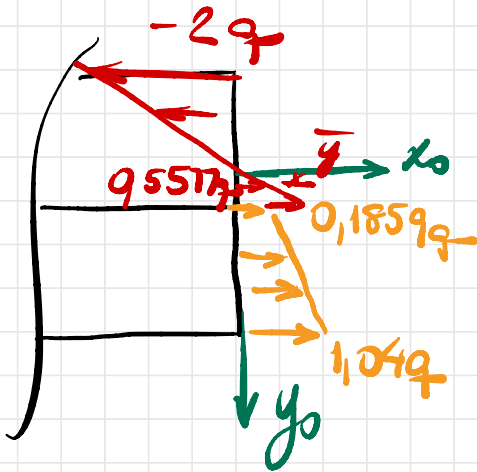
$$\sigma_C = -\frac{4q}{144} + \frac{200q}{1404} \cdot (-4,5) = -0,669q$$

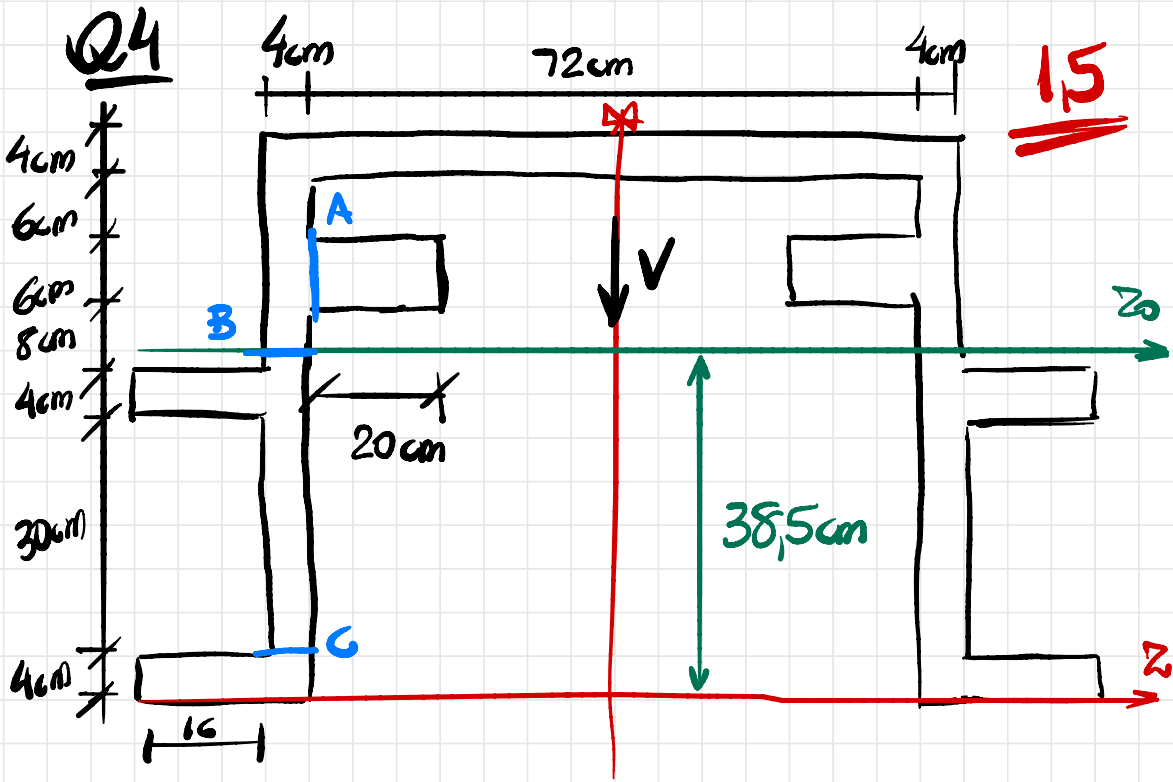
$$\sigma_I = \frac{-4q}{144} + \frac{200q}{1404} \cdot 1,5 = 0,1859q$$

no material ①:

$$\sigma_T^{\text{①}} = 3\sigma_T = -2q \quad (\approx -2,007q)$$

$$\sigma_L^{\text{①}} = 3\sigma_L = 0,5577q$$





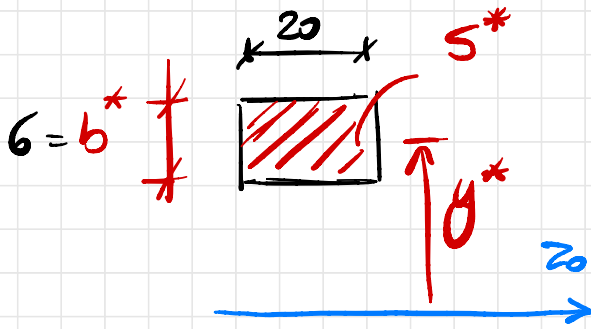
Esboçar o diagrama de fluxo de cisalhamento e calcular as tensões em A, B e C.

São dados:  $y_G = 38,5 \text{ cm}$  (na figura) e  $I_{G0} = 5,2 \cdot 10^5 \text{ cm}^4$ .

$$\underline{V = 156 \text{ P} \text{ [kN]}}$$

0,3 por tensões  
0,6 no esboço

## Tensões em A:



$$b^* = 6 \text{ cm}$$

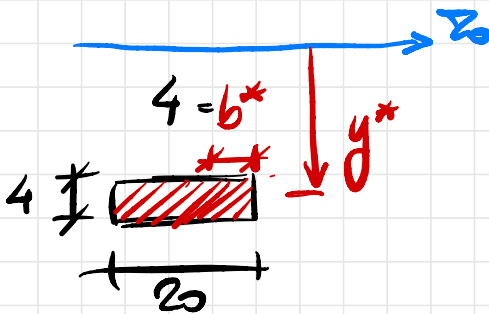
$$S^* = 120 \text{ cm}$$

$$y^* = 49 - 38,5 = 10,5 \text{ cm}$$

$$M_S^* = 1260 \text{ cm}^3$$

$$\sigma_A = \frac{156P \cdot 1260}{6 \cdot 5 \cdot 2 \cdot 10^5} = 0,063P \text{ kN/cm}^2 = 0,63P \text{ MPa}$$

## Tensões em C:



$$b^* = 4 \text{ cm}$$

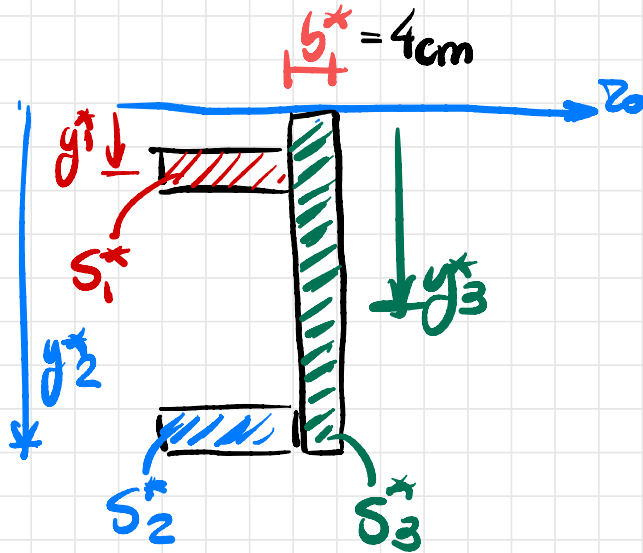
$$S^* = 80 \text{ cm}^2$$

$$y^* = 38,5 - 2 = 36,5 \text{ cm}$$

$$M_S^* = 2920 \text{ cm}^3$$

$$\sigma_C = \frac{156P \cdot 2920}{4 \cdot 5 \cdot 2 \cdot 10^5} = 0,219P \text{ kN/cm}^2 = 2,19P \text{ MPa}$$

# Tensão em B:



$$b^* = 4\text{ cm}$$

$$y_1^* = 38,5 - 36 = 2,5\text{ cm}$$

$$S_1^* = 4 \cdot 16 = 64\text{ cm}^2$$

$$y_2^* = 38,5 - 2 = 36,5\text{ cm}$$

$$S_2^* = 4 \cdot 16 = 64\text{ cm}^2$$

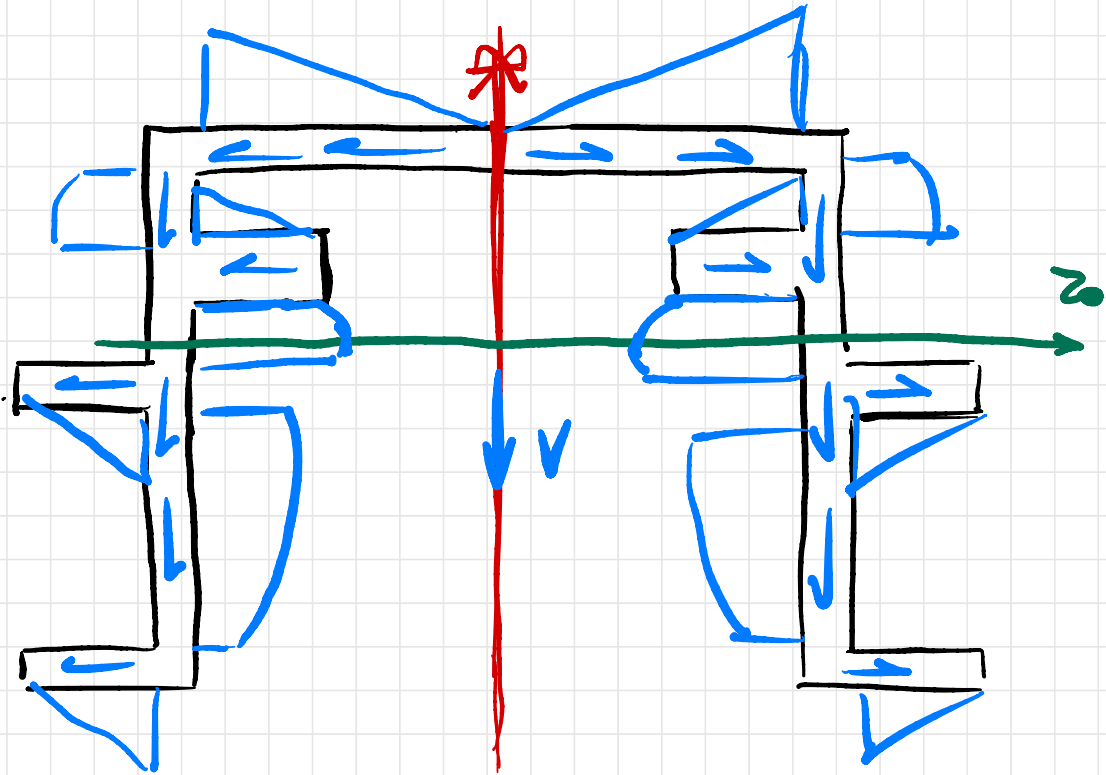
$$y_3^* = 38,5/2 = 19,25\text{ cm}$$

$$S_3^* = 154\text{ cm}^2$$

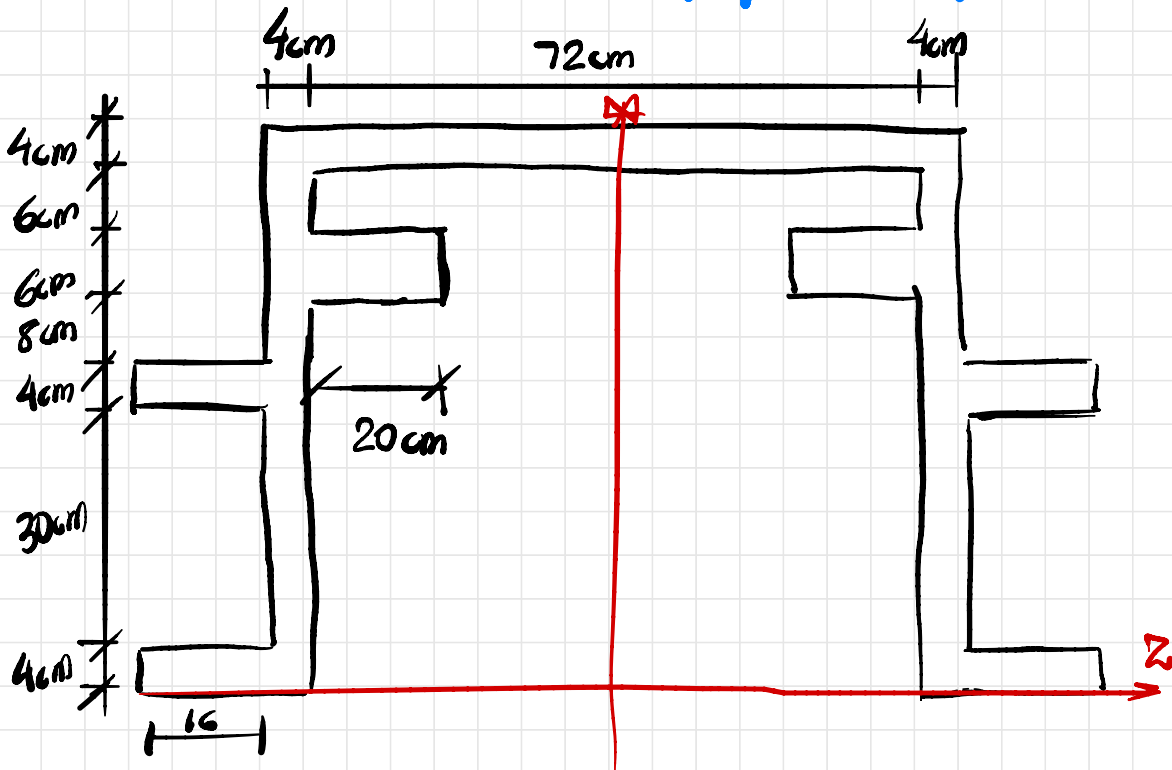
$$M_S^* = 2,5 \cdot 64 + 36,5 \cdot 64 + 19,25 \cdot 154 = 5460,5\text{ cm}^3$$

$$\tau_B = \frac{156 P \cdot 5460,5}{4 \cdot 52 \cdot 10^5} = 0,41 P \text{ kN/cm}^2 = 4,1 P \text{ MPa}$$

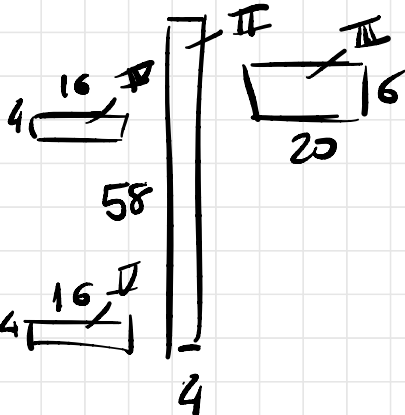
# Esboço das tensões



# Cálculos auxiliares (Propriedades)



Propriedades:



usando a simetria, tem-se  
que  $I_{Z0} = 2 I_{Z0}^{1/2}$

←  $\left(\frac{1}{2}\right)$



	$y_G$	$A$	$d$	$d^2 A$	$I_{\text{to}}$
I	60	160	21,5	73.960	$640/3$
II	29	232	9,5	20.938	$195112/3$
III	49	120	10,5	13.230	360
IV	36	64	2,5	400	$256/3$
V	2	64	36,5	85.264	$256/3$

$$y_G = \frac{60 \cdot 160 + 29 \cdot 232 + 49 \cdot 120 + 36 \cdot 64 + 2 \cdot 64}{160 + 232 + 120 + 64 + 64}$$

$$y_G = \frac{24640}{640} = \underline{\underline{38,5 \text{ cm}}}$$

$$I_{\text{to}}^{1/2} = \sum (I_{\text{to}}^i + d_i^2 A_i)$$

$$I_{\text{to}}^{1/2} = 2,6 \cdot 10^5 \text{ cm}^4$$

$$I_{\text{to}} = 2 I_{\text{to}}^{1/2} = \underline{\underline{5,2 \cdot 10^5 \text{ cm}^4}}$$