

Sistemas de Alta Sustentação

Tópicos:

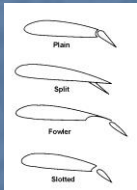
1. Aspectos históricos
2. Tipos
3. Características Aerodinâmicas
4. Ensaios Experimentais
5. Considerações Finais

Aspectos históricos origens do eslate (slat).



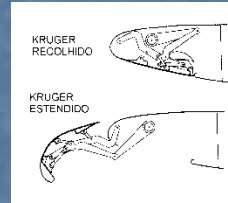
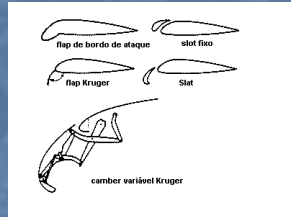
- Em 1917 Handley Page and Boswall realizam experimentos com uma asa com fendas (slots) e também com eslates (slats). Usando um aerofólio RAF15 conseguiram um aumento de 25% no CL. Mais tarde, chegaram a um aumento de 50% no CL com um aumento pequeno em CD.
- Handley Page patenteou a idéia (incluindo um sistema móvel operado pelo piloto) em 1920.
- Ao mesmo tempo, na Alemanha, G.V. Lachmann desenvolveu uma asa com aerofólios em cascata. Tentou uma patente em 1918 que foi recusada por falta de confirmação experimental convincente.
- Com auxílio de Prandtl, Lachmann realizou experimentos convincentes e a patente foi confirmada em 1921 retroativamente a 1918.
- Somente em 1972, A.M.O. Smith apresenta o artigo: “Aerodynamic of High lift Airfoil Systems” explicando definitivamente os princípios físicos dos slots e flaps.

Aspectos históricos origens do flape.

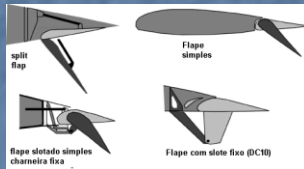


- Os flapes são derivados dos ailerons inventados no começo do século 20.
- Utilização começa em 1914.
- Split Flap foi desenvolvido em 1920
- Em 1920, Harland D. Fowler inventou o Fowler-flap, mas usado somente em 1937 pela Lockheed.
- Em 1937 são introduzidos os flapes com duplo e triplo eslots (Piaggio)

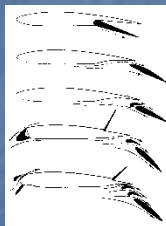
2- Tipos de sistemas de Alta Sustentação



- De bordo de ataque.



- De bordo de fuga.



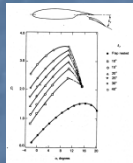
- Combinado.

3- Características Aerodinâmicas

- Análise do escoamento numa asa com sistemas de alta sustentação



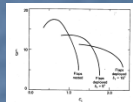
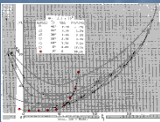
1. O perfil da asa é definido pelo formato da sua superfície superior e inferior. O formato da superfície superior é definido pelo formato da superfície inferior e pelo formato da superfície superior. O formato da superfície superior é definido pelo formato da superfície inferior e pelo formato da superfície superior. O formato da superfície superior é definido pelo formato da superfície inferior e pelo formato da superfície superior.



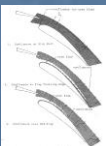
- Efeito em C_L ,

- C_D

- C_m e L/D .



- Efeito do tamanho da fenda (gap) e sobreposição (overlap)

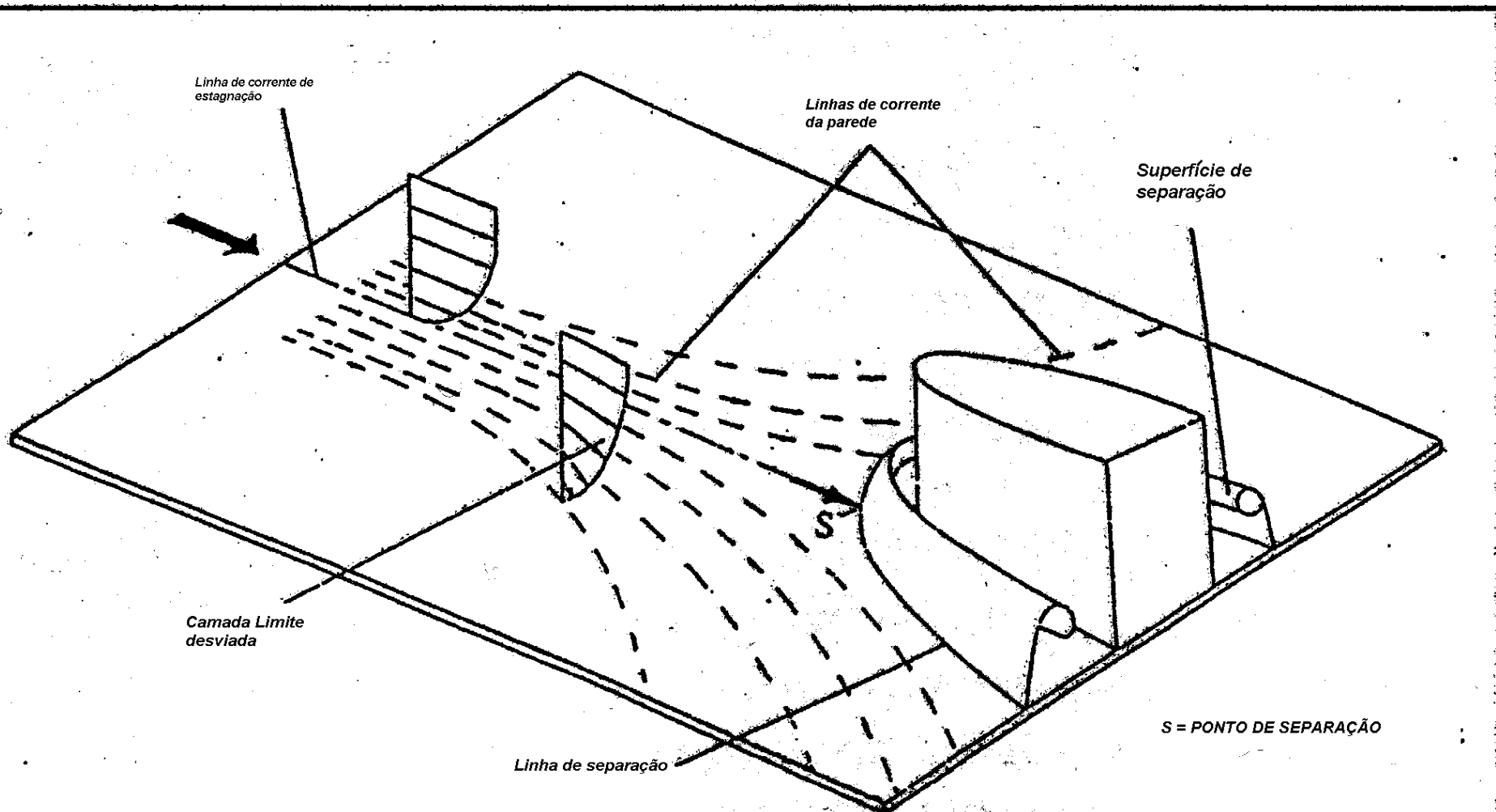


4- Ensaaios Experimentais

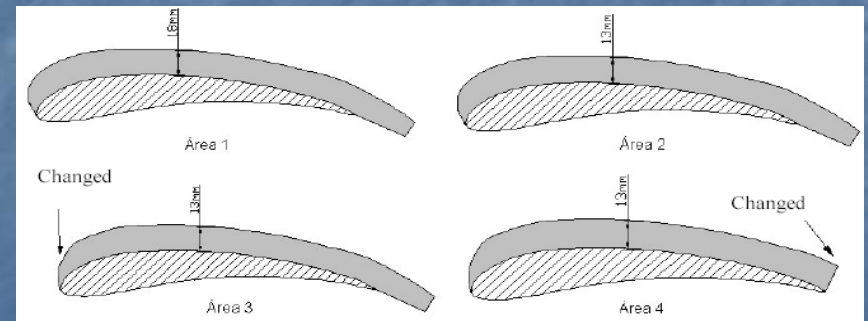
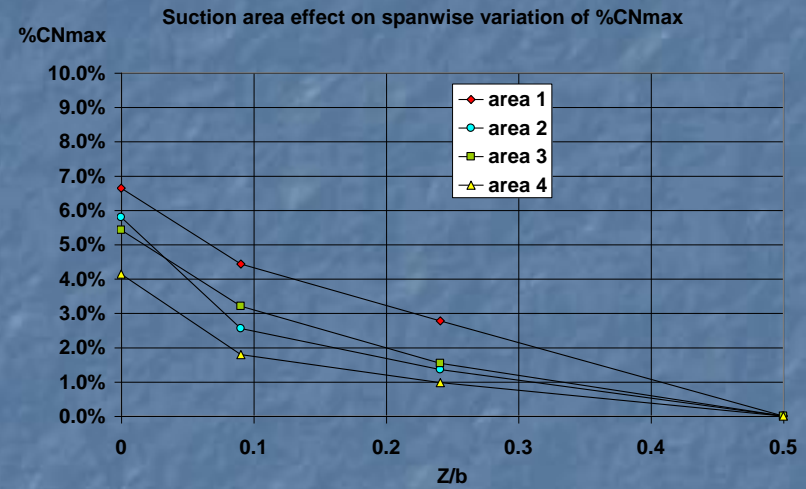
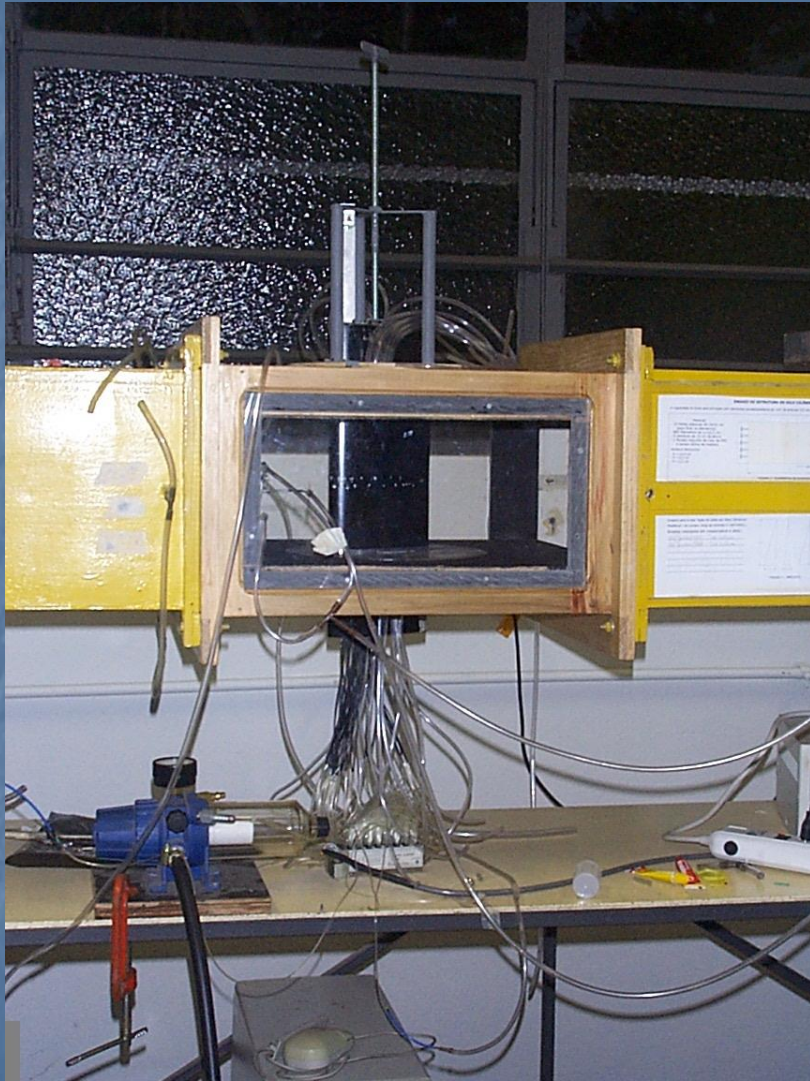
- Asa bi-dimensional com alta sustentação
 - Problemas
 - Soluções
- Ensaaios de ruído
 - Efeito do flape
 - Efeito do slat
- Alternativas

Ensaio bidimensionais

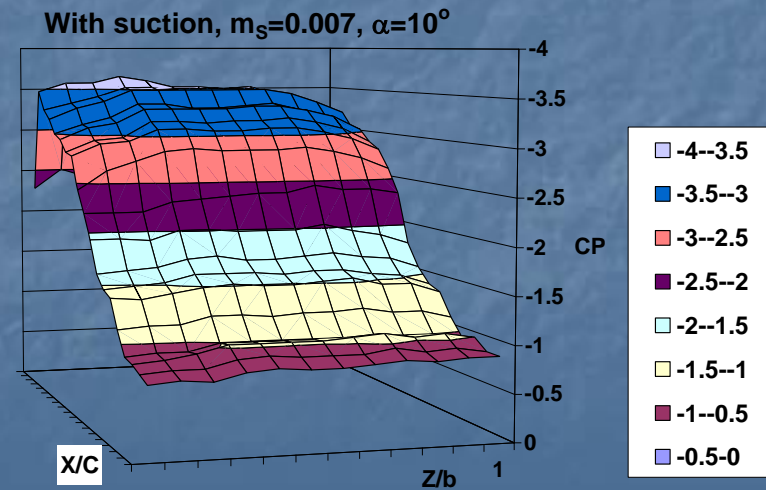
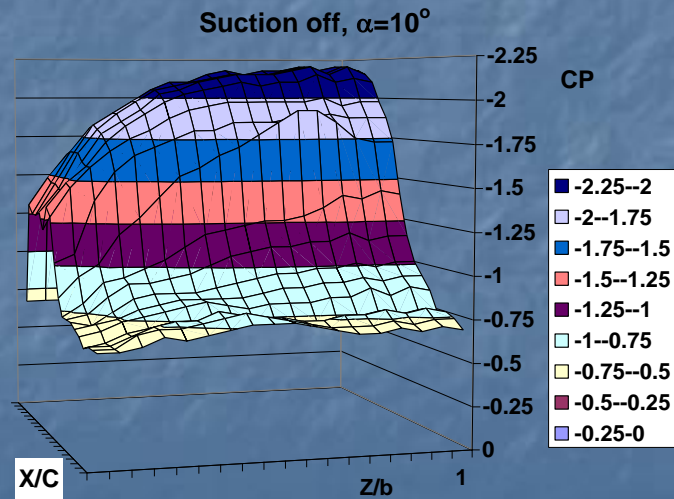
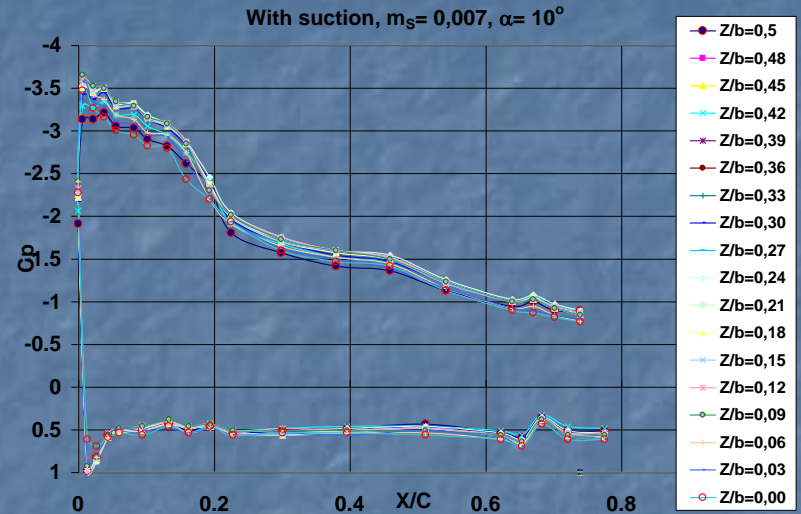
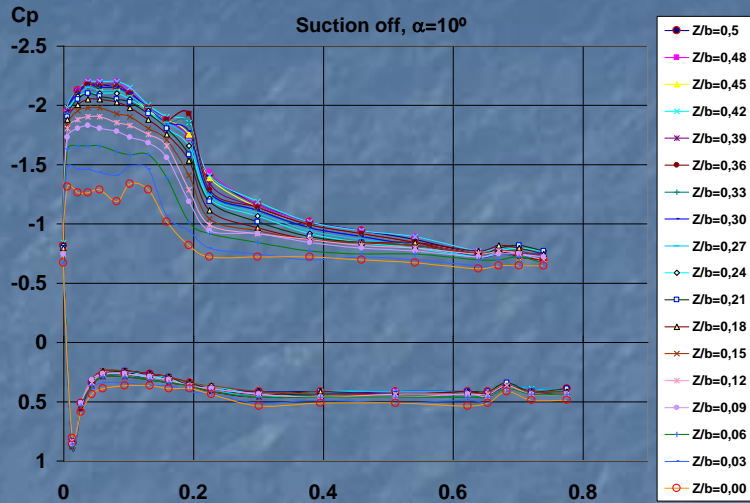
problemas



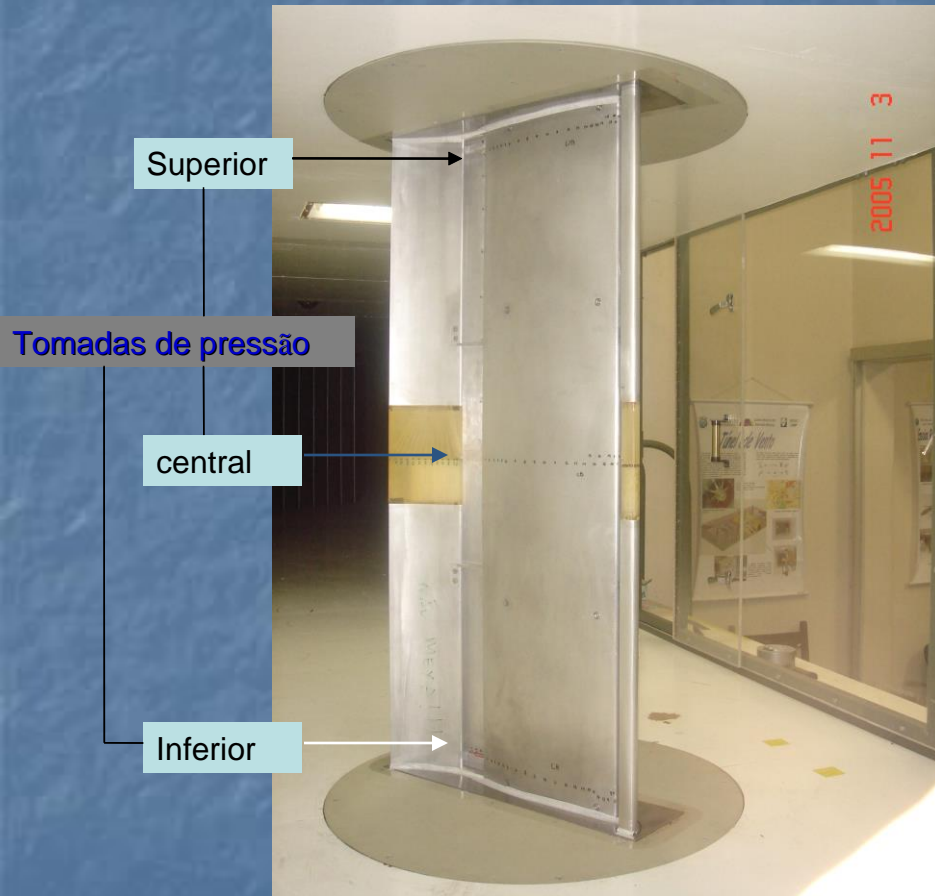
Investigação preliminar



Ensaaios bidimensionais

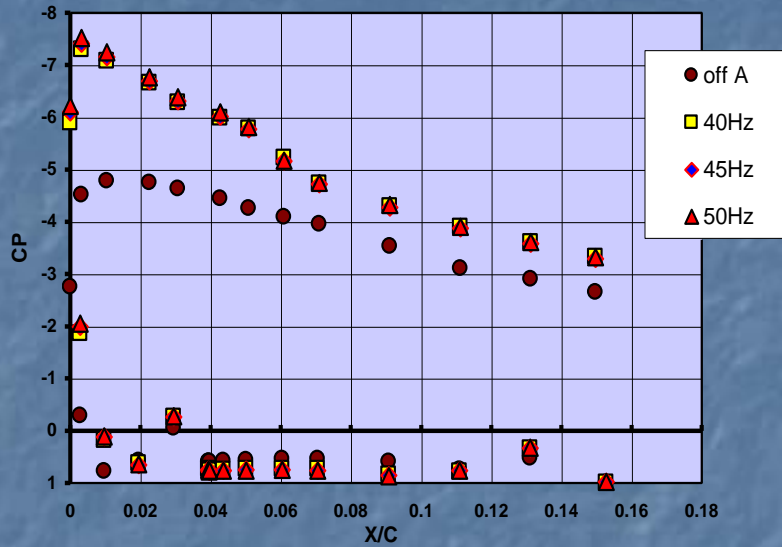


Ensaio bidimensionais com uma asa com flape e slat soluções:

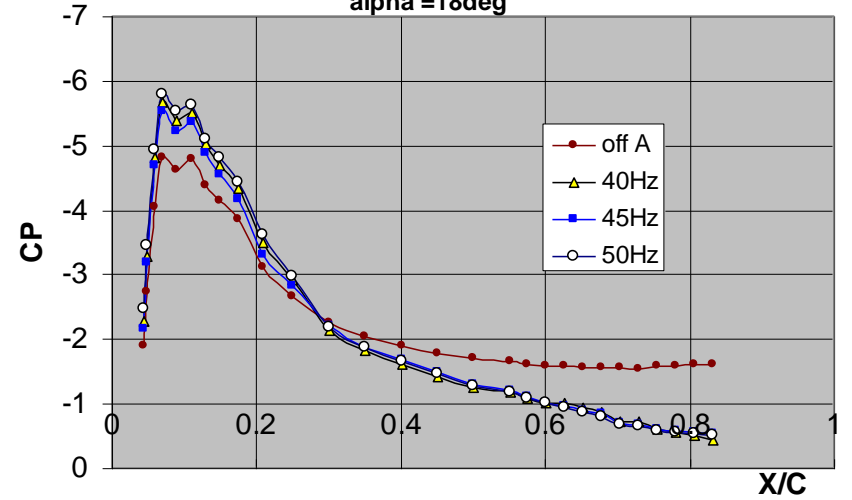


Ensaio bidimensionais com uma asa com flape e slat

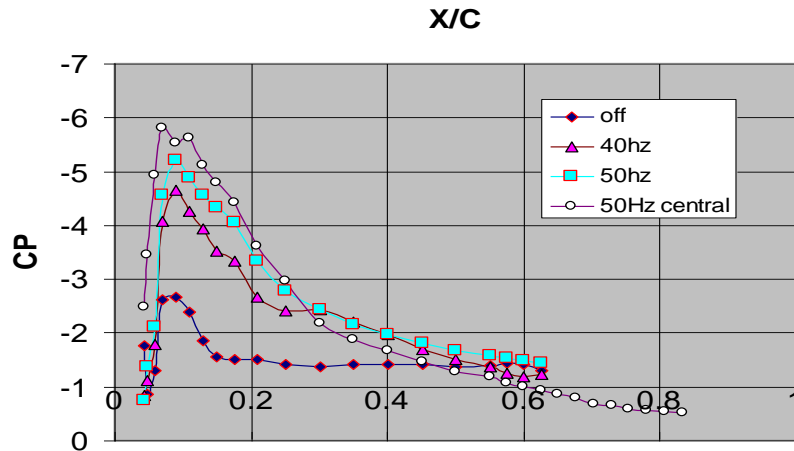
SUCTION MASS FLOW EFFECT ON SLAT CP AT CENTRE SECTION
 $\alpha=18$



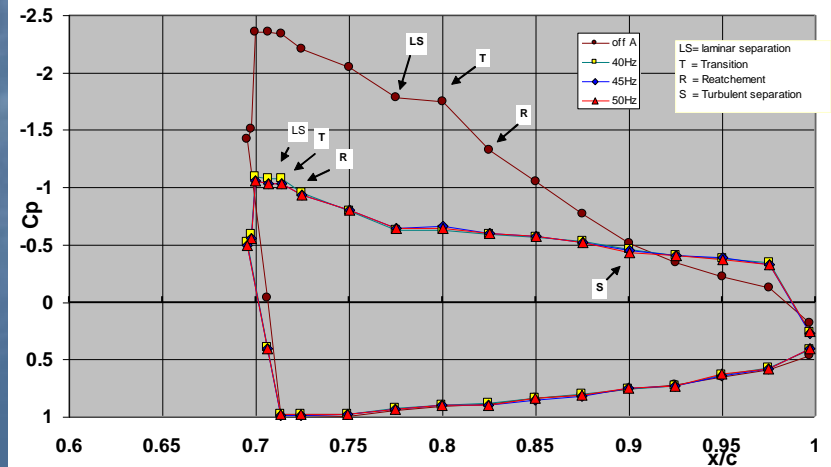
CP no centro da asa para varias vazões de sucção
 $\alpha = 18 \text{deg}$



Cp proximo à parede superior

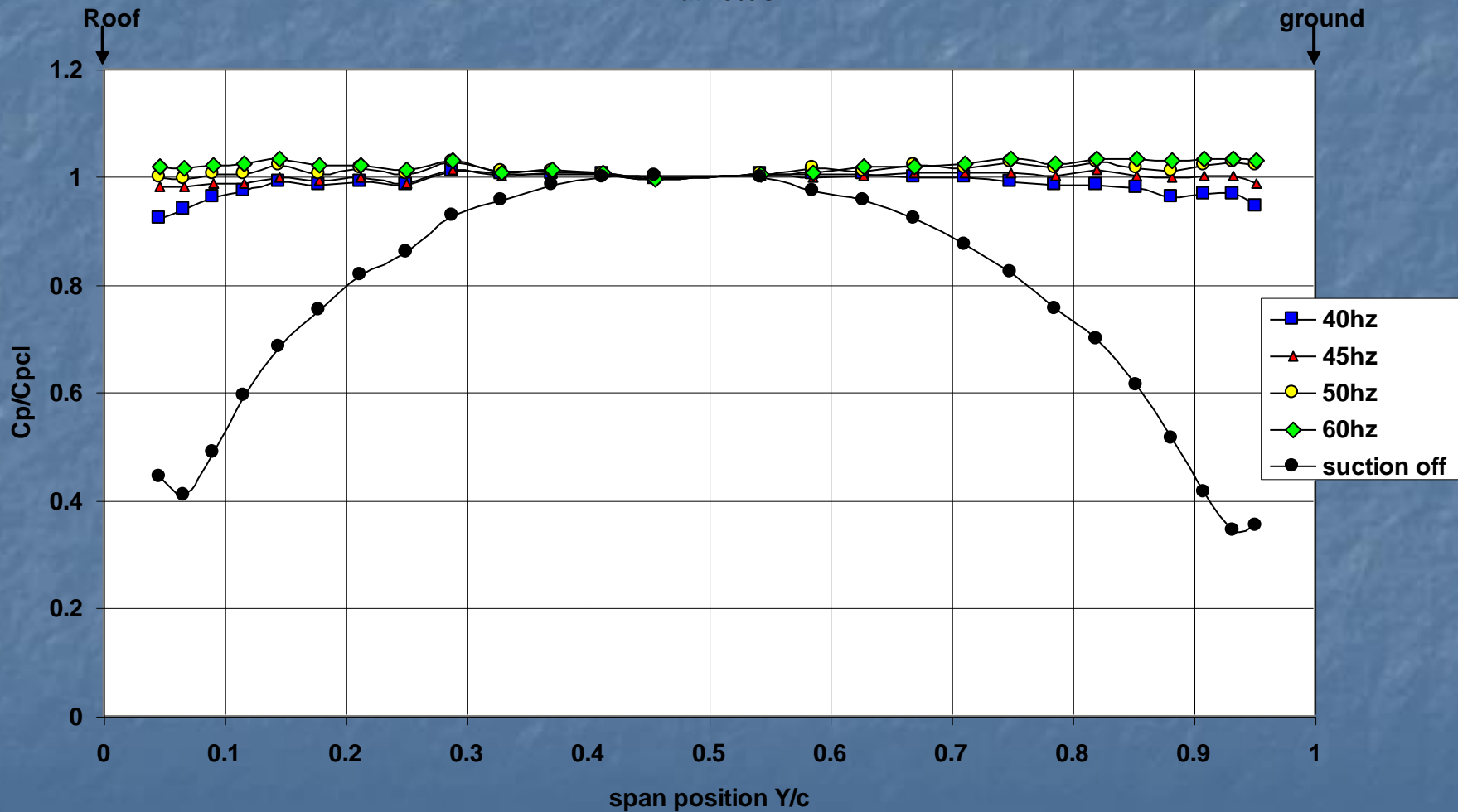


suction mass flow effect on flap Cp distribution at centre line, $\alpha=18$



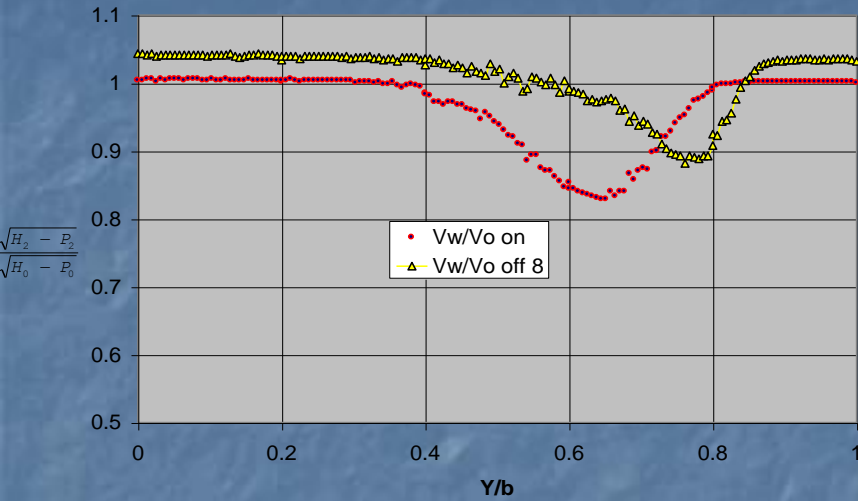
Ensaaios bidimensionais com uma asa com flape e slat

alpha=18deg, Spanwise Cp/Cpcl variation
at 25%C

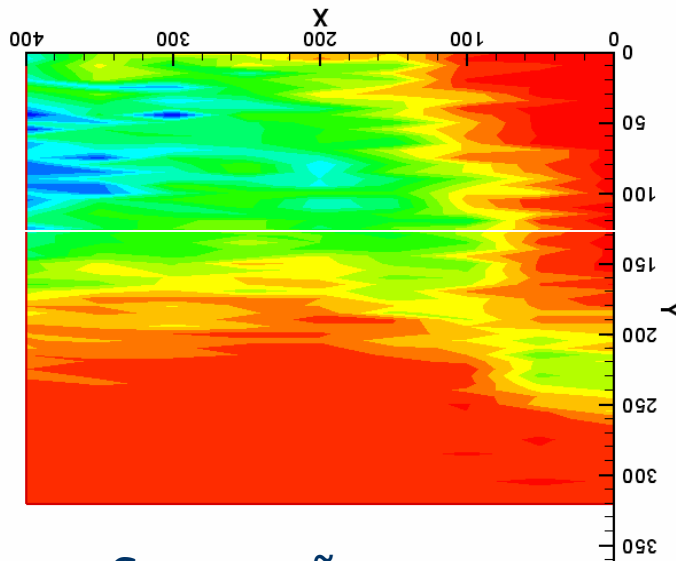
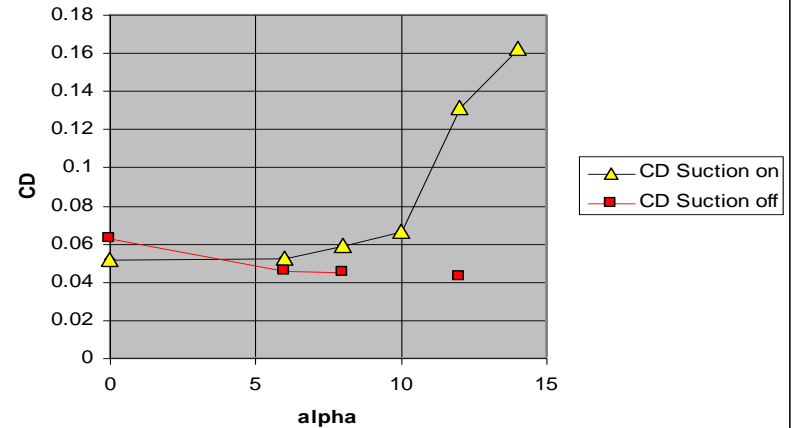


Ensaio bidimensionais com uma asa com flape e slat

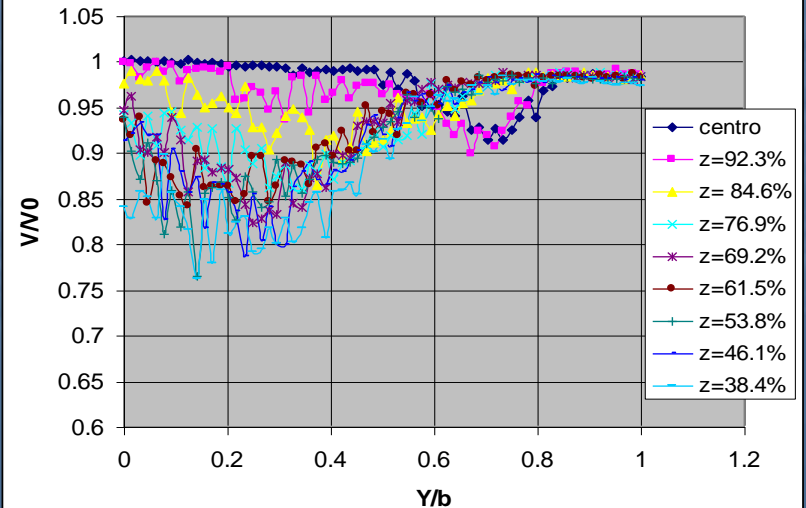
Esteira normalizada com e sem sucção
alpha=8deg



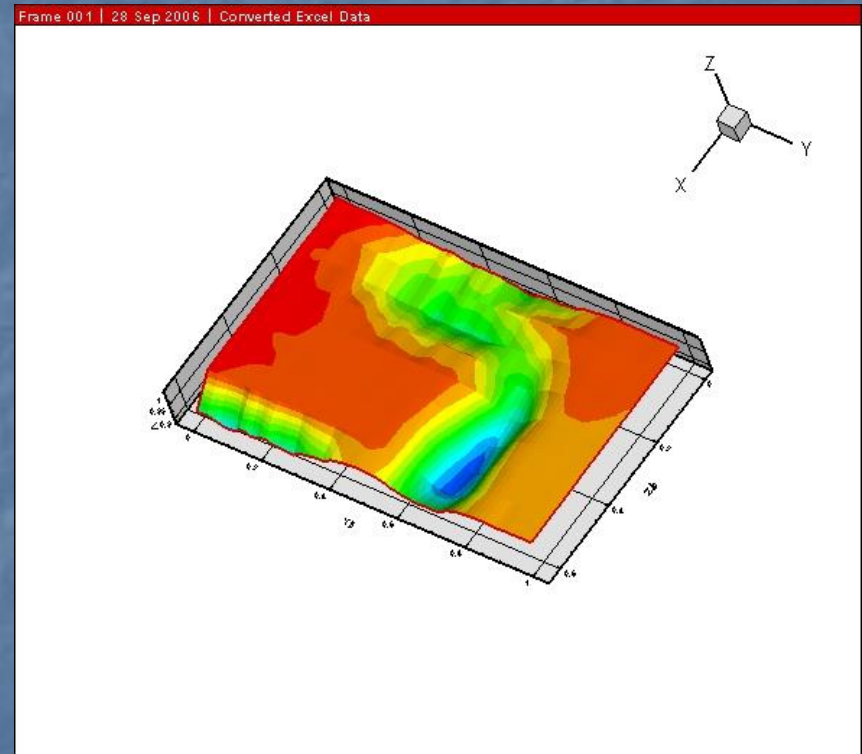
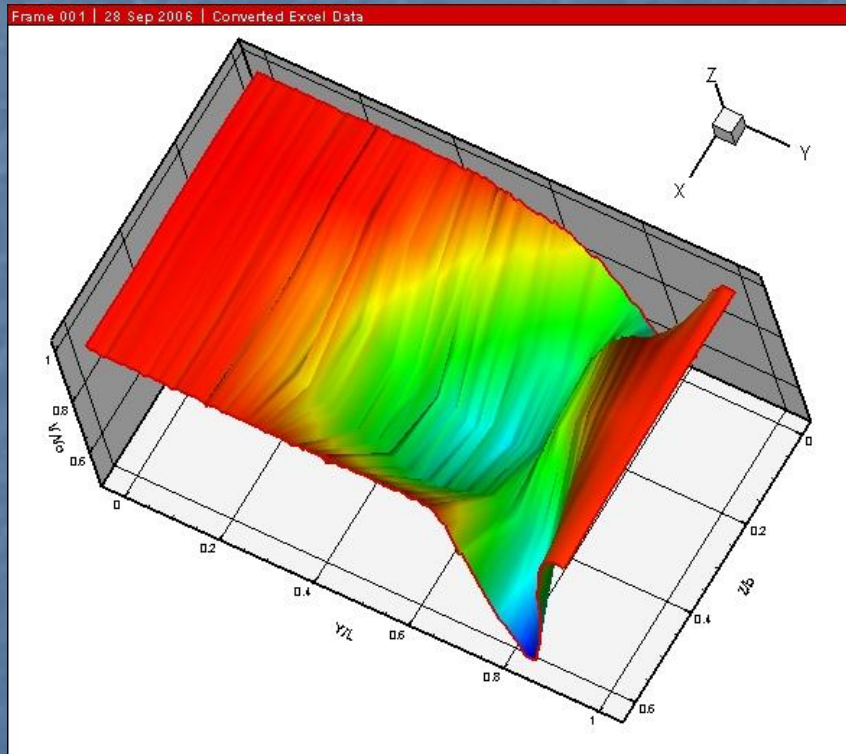
Calculo de CD por integração da distribuição de pressão na esteira.



Mapeamento de esteira sem sucção alpha =8

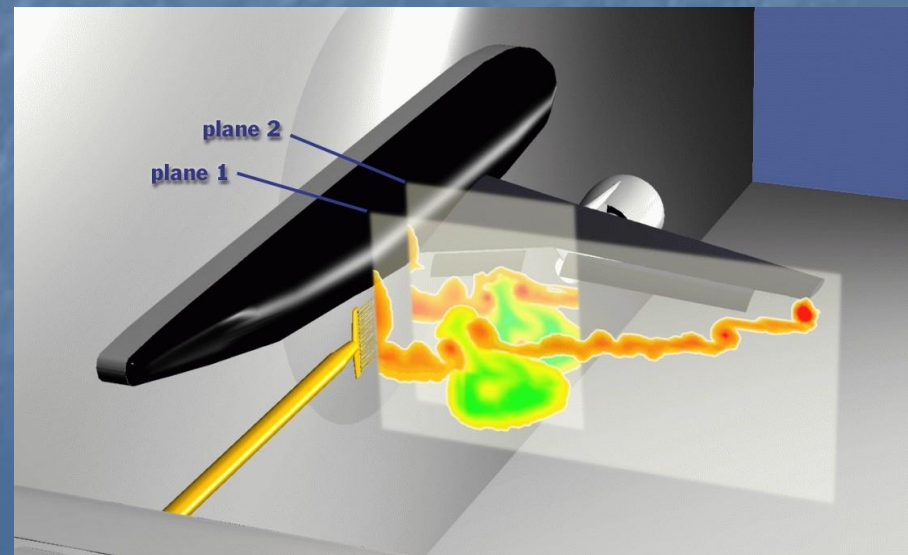


Ensaio bidimensionais com uma asa com flape e slat

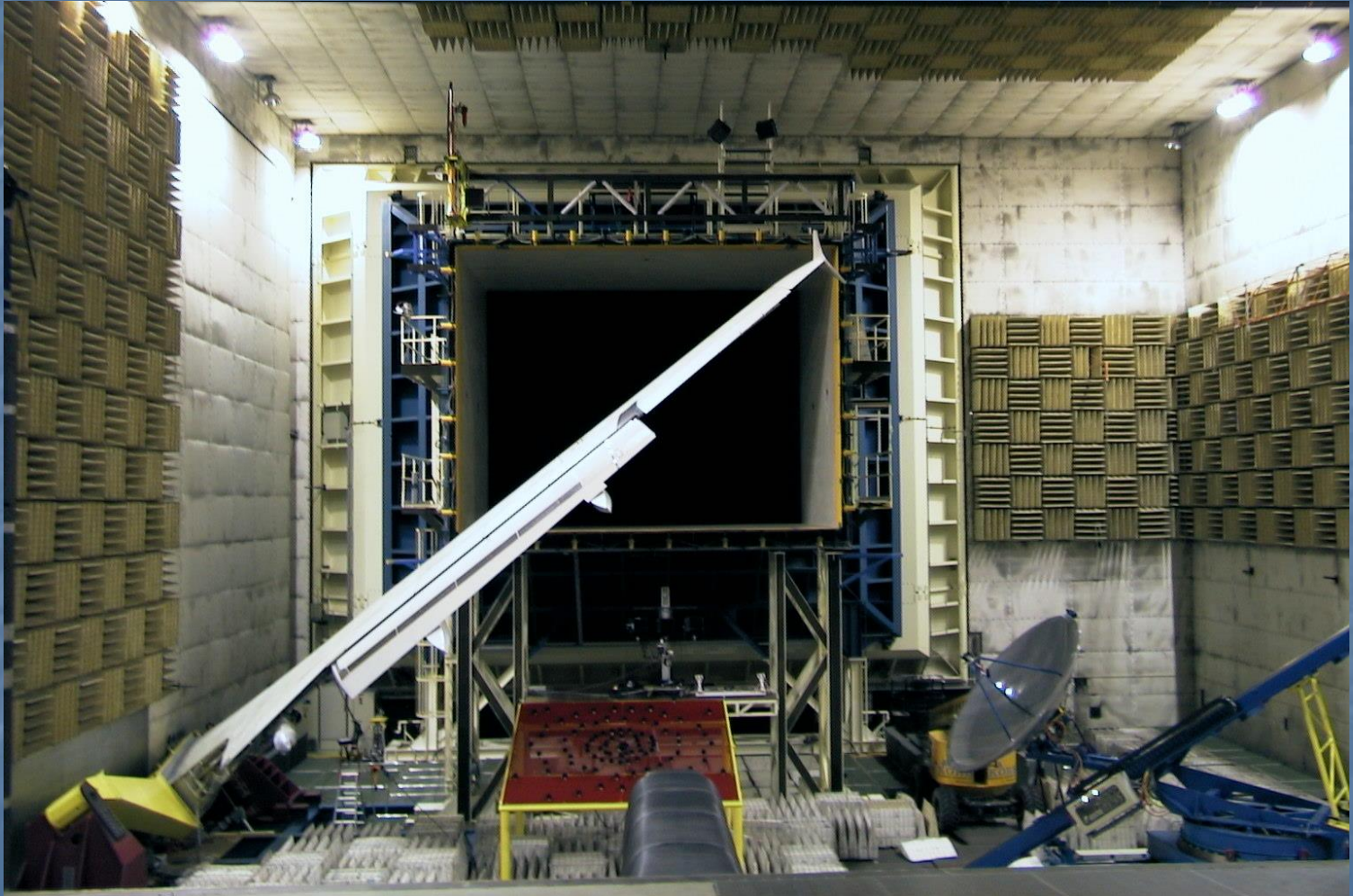




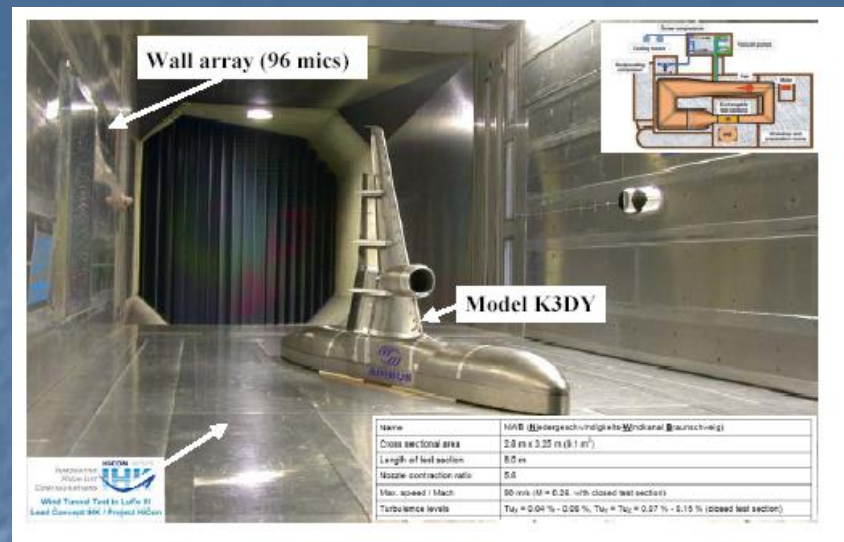
Ensaaios tridimensionais



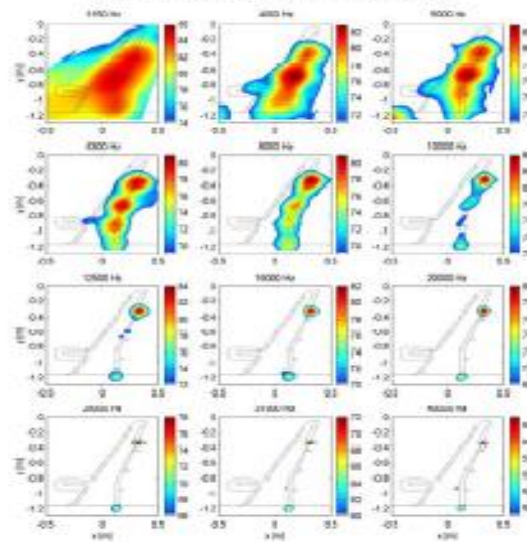
Ensaaios de ruído



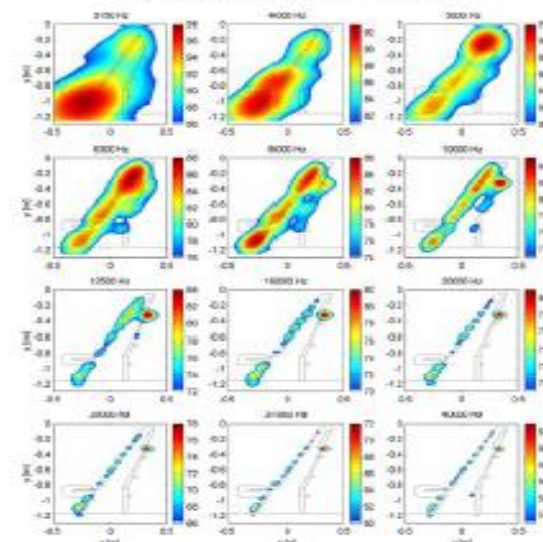
Ensaaios de ruído



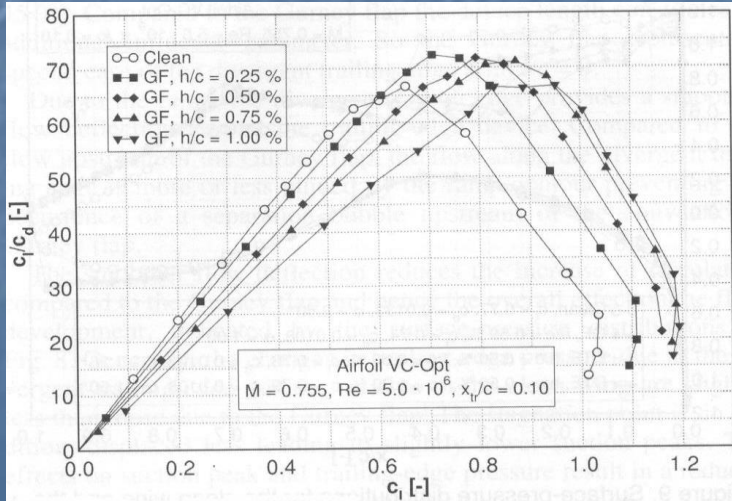
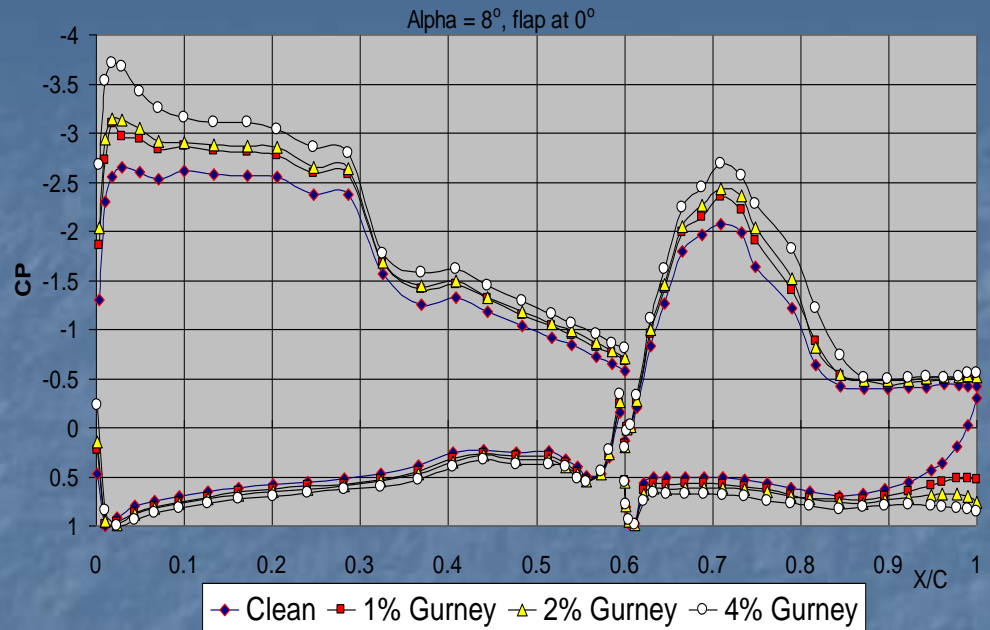
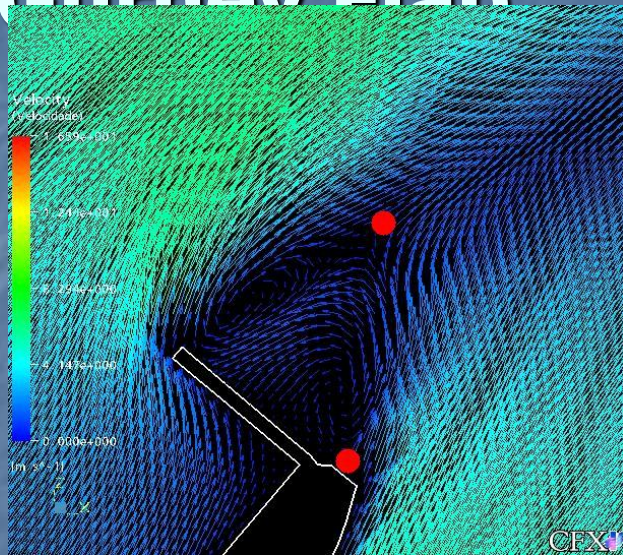
a) A321 with slatless leading edge (landing configuration)



b) A321 standard leading edge (landing configuration)



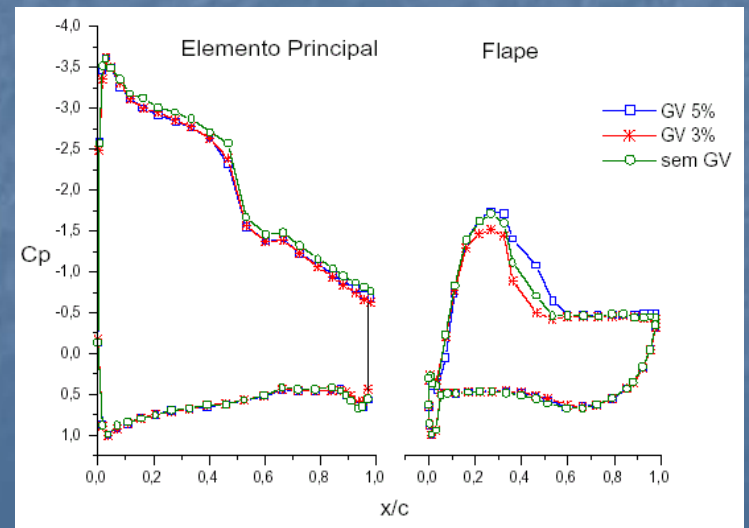
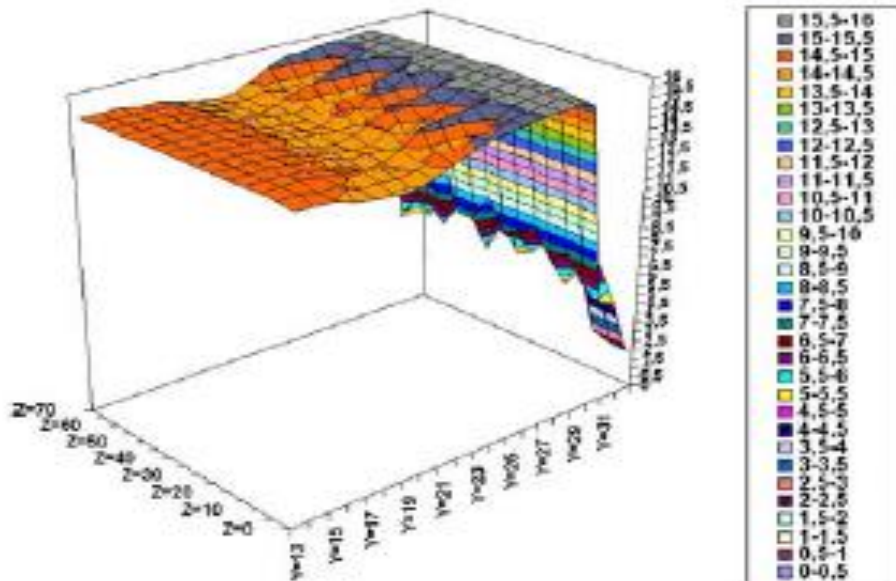
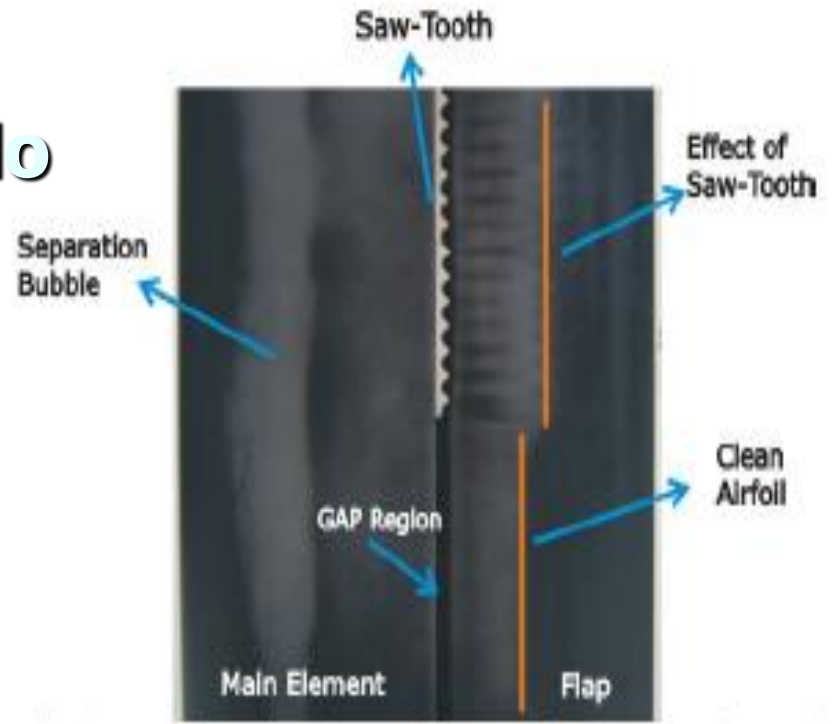
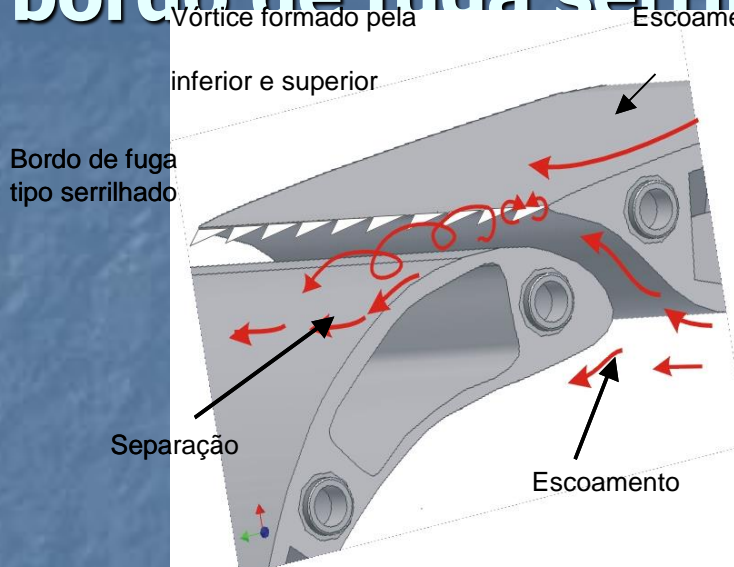
Alternativas: Gurney Flap



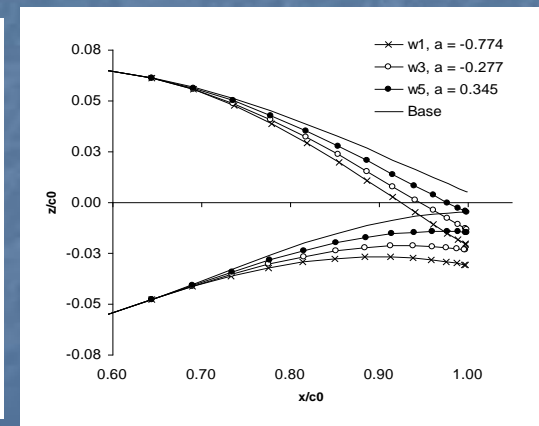
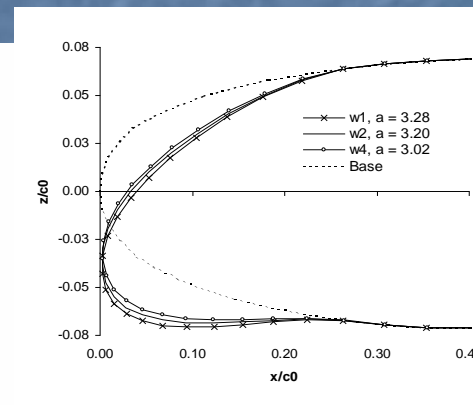
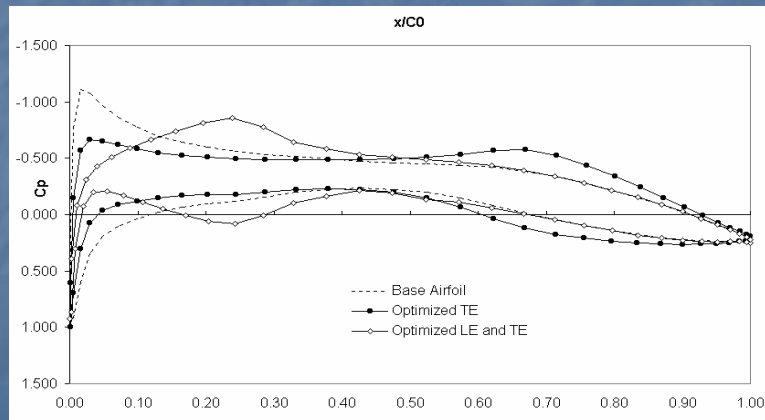
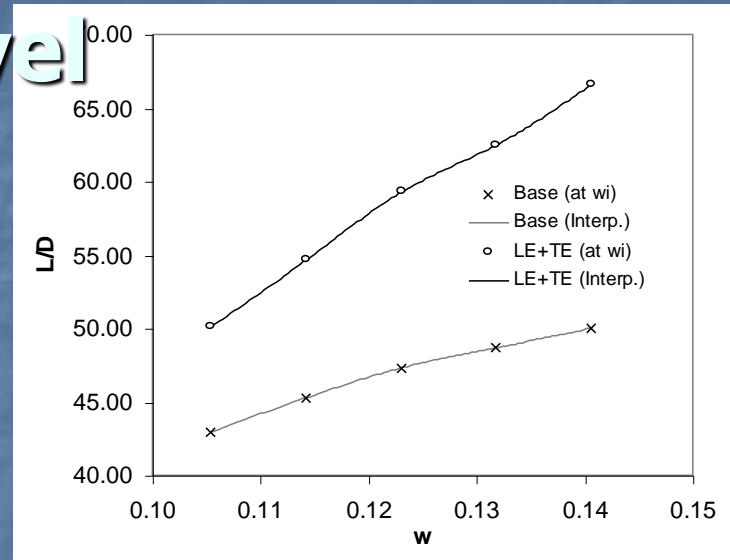
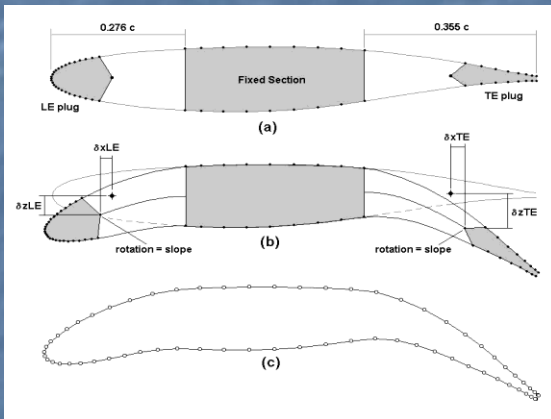
Lift-to-drag ratio of the clean wing and the Gurney-flap configurations tested at M = 0.755.



Alternativas: bordo de fuga serrilhado



Alternativas: Asa com câamber variável



Considerações finais

- O projeto aerodinâmico e mecânico de sistemas de alta sustentação é um processo de compromisso entre:
 - Otimização Aerodinâmica
 - Ruído
 - Complexidade estrutural e mecânica.
 - custos

1- Aspectos históricos

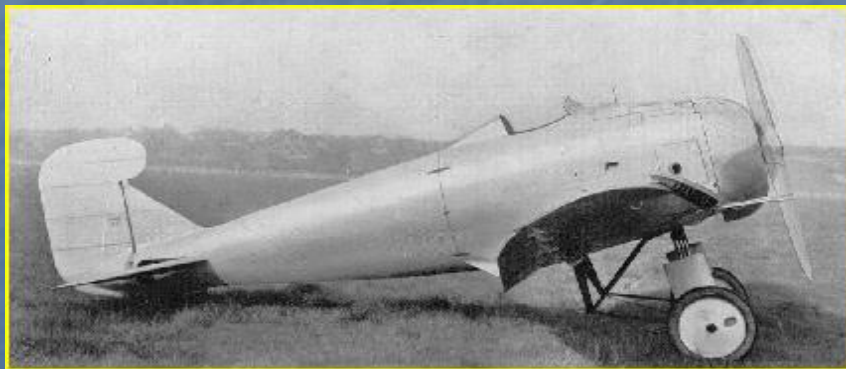
- Atualmente, o desenvolvimento de um sistema de alta sustentação eficiente equivale de 5% a 11% do custo total de desenvolvimento de uma aeronave.
- Aumento de 1% no L/D de decolagem significa um aumento de 1.3 ton na carga paga, ou 280Km a mais de alcance.
- Combinando com um aumento de 1,5% no CL_{max} de aterrissagem pode adicionar mais 3t na carga paga.
- A partir de 2020 custos de desenvolvimento e de construção deverão ser reduzidos em 35% e a eficiência aerodinâmica aumentada em 20%! . Ruído deverá diminuir em 10dB

Aeronaves Handley Page com eslotes

1919



1921

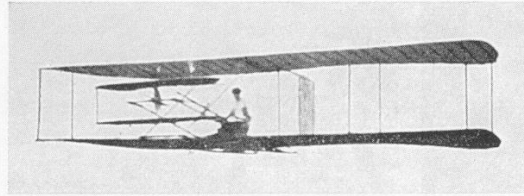


1922

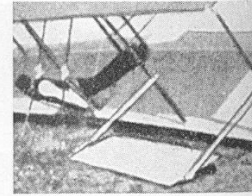


1929

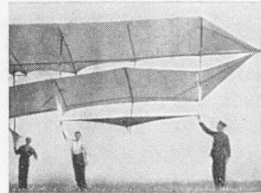
ailerons



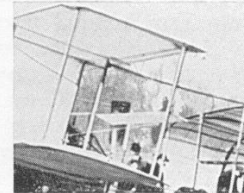
a Wing-warping in action: a British-built Wright glider of 1909, showing the Wrights' system, invented in 1899



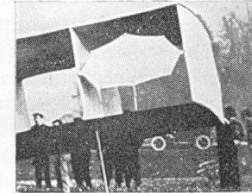
b The first use of ailerons: Esnault-Pelterie's glider: 1904



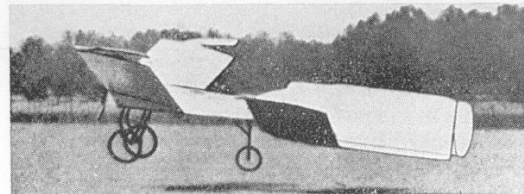
c Cody's kite-glider: 1905



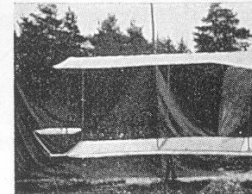
d Blériot *No. IV* biplane: 1906



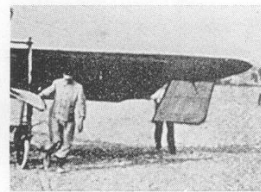
e Santos-Dumont *14-bis* biplane: 1906



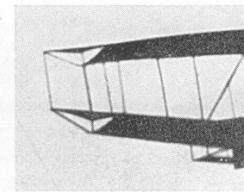
f Blériot *No. VI* tandem-wing *Libellule*: 1907 (showing the pivoting wing-tip elevons)



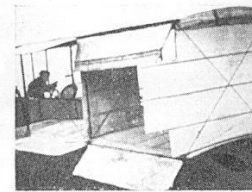
g Cody *British Army Aeroplane No. 1*: 1908



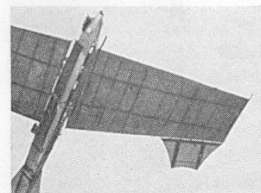
h Blériot *No. VIII-bis* monoplane: 1908



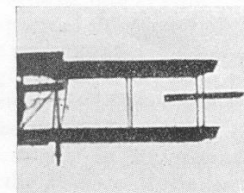
i A.E.A. (Curtiss) *June Bug* biplane: 1908



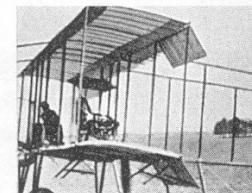
j Henri Farman's modified Voisin biplane: 1908



k Levavasseurs *Antoinette IV*: 1909



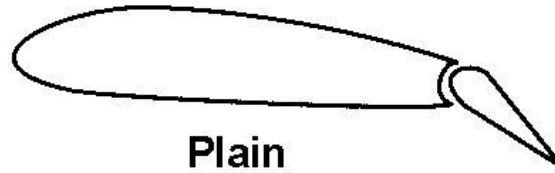
l Curtiss Reims biplane: 1909



m Henry Farman *III* biplane: 1909

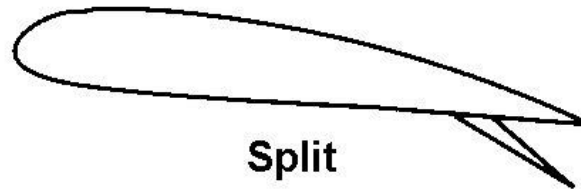
Evolução do flape

Derivado dos
ailerons



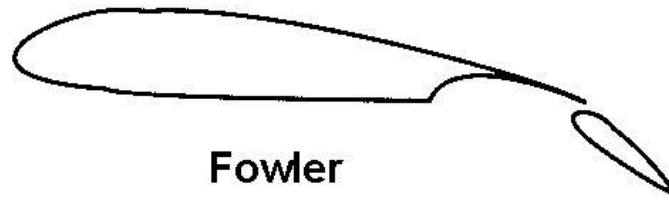
Plain

1920



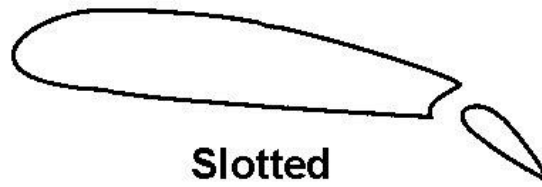
Split

Fowler 1920,
aplicado em 1937



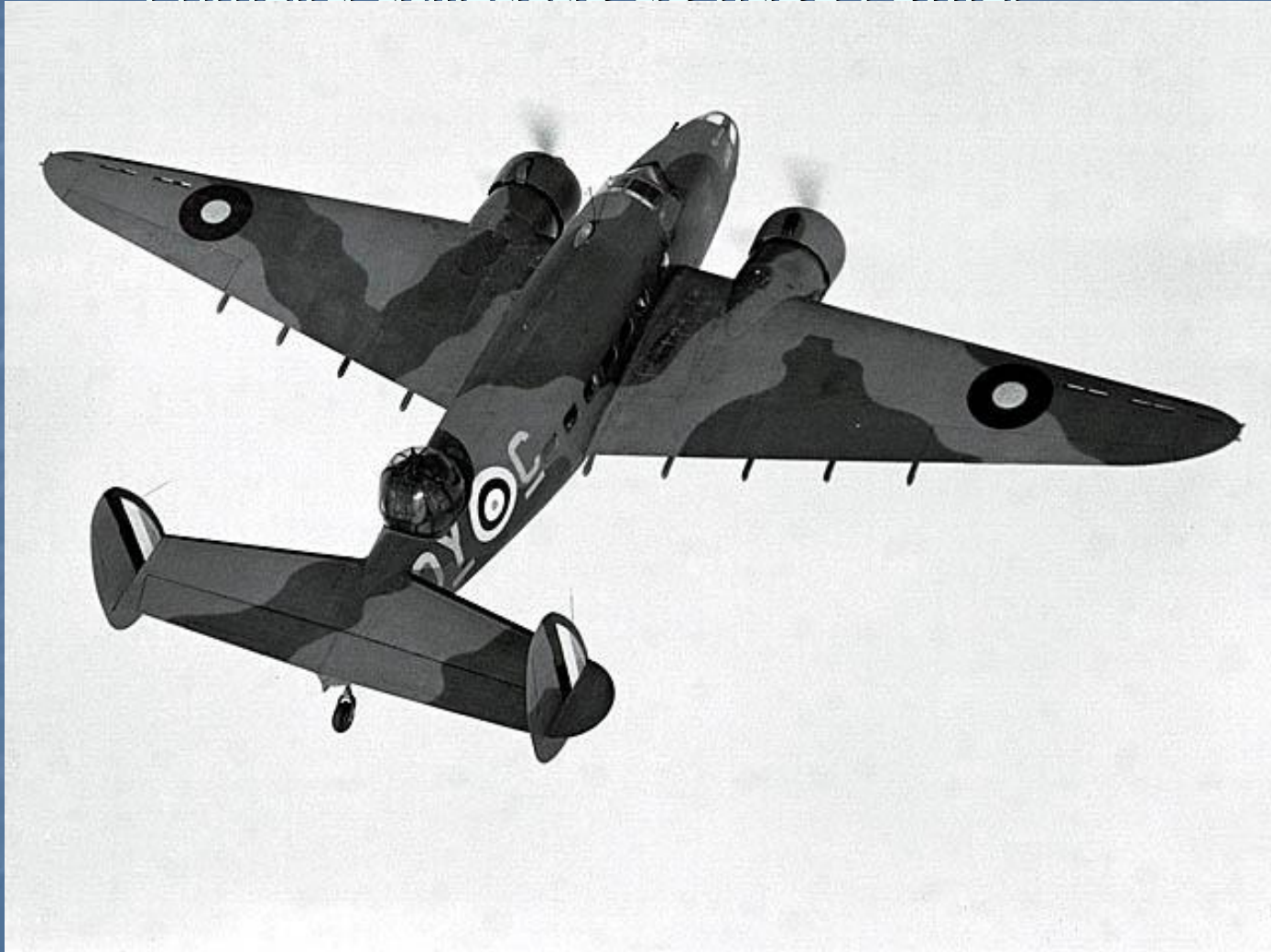
Fowler

1937 Derivado dos
estudos de Handley
Page;Lachmann

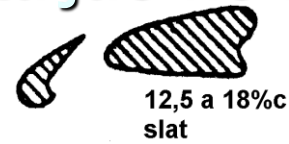


Slotted

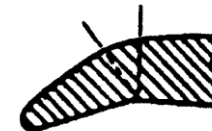
Primeira utilização do flape Fowler



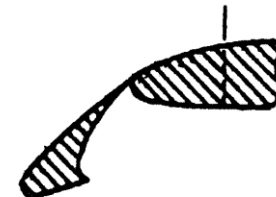
Tipos de elementos de alta sustentação no bordo de ataque:



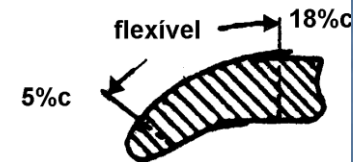
12,5 a 18%c
slat



15%c BA Flape
simples

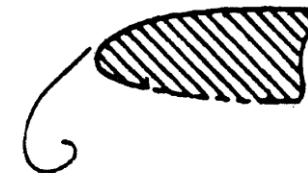


12 a 18%c flape de bordo
de ataque

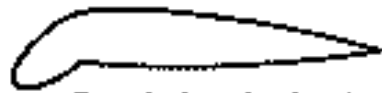


5%c

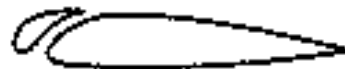
18%c RAEVAN



Flape Kruger Fexível
18%c



flap de bordo de ataque



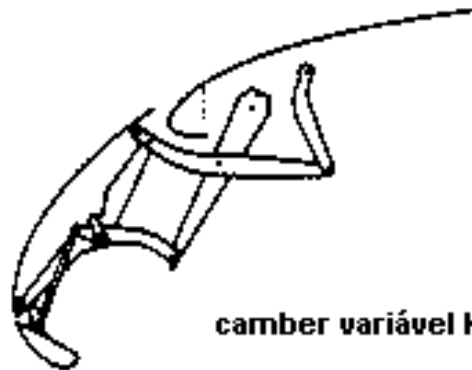
slot fixo



flap Kruger

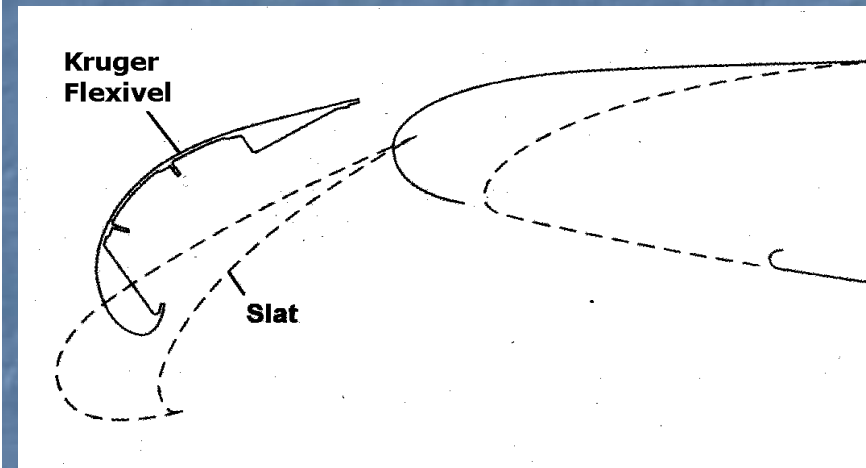
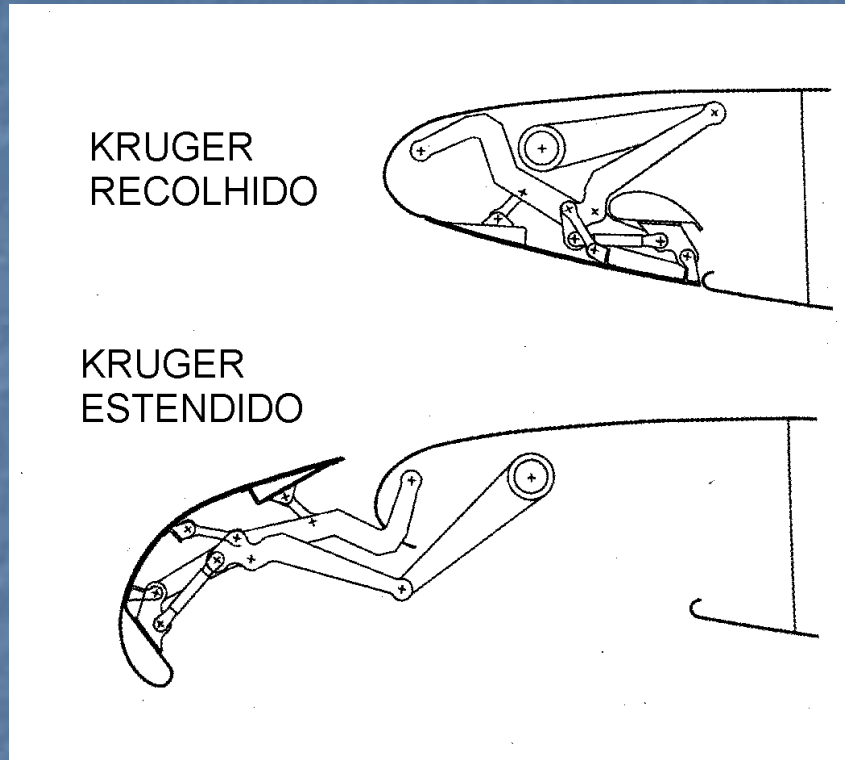


Slat



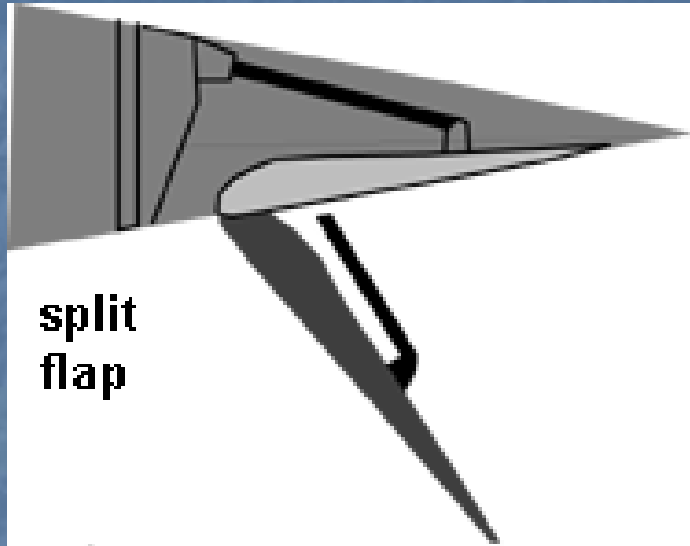
camber variável Kruger

Tipos de elementos de alta sustentação no bordo de ataque:

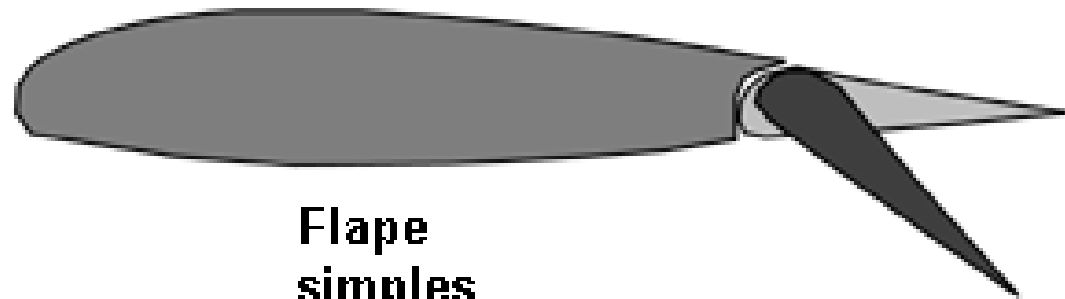


O slat flexível Kruger produz um CL_{max} um pouco maior que o slat convencional, dando um aumento na ordem de 1,5% no carregamento da asa na decolagem. Porém, seu maior peso reduz essa vantagem para apenas 0,75%. Seu impacto estrutural também é maior (maior área aberta na asa).

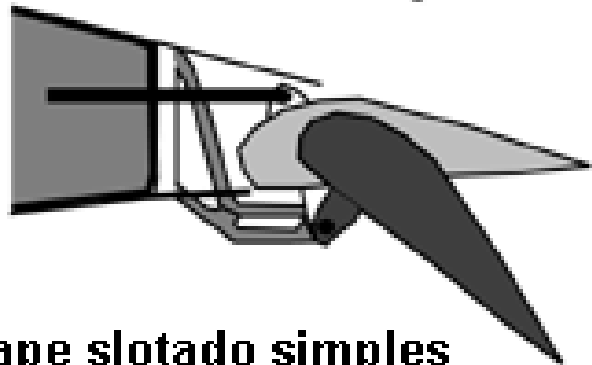
Tipos de elementos de alta sustentação no bordo de fuga:



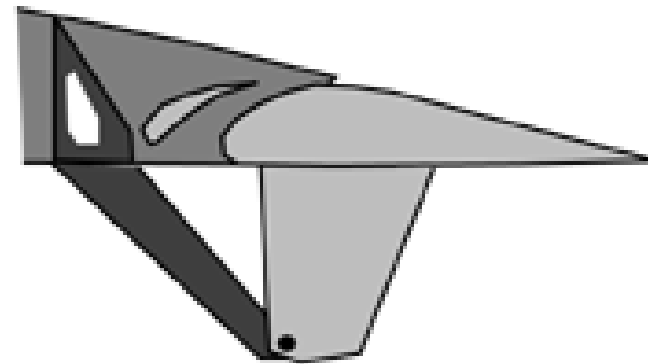
**split
flap**



**Flape
simples**

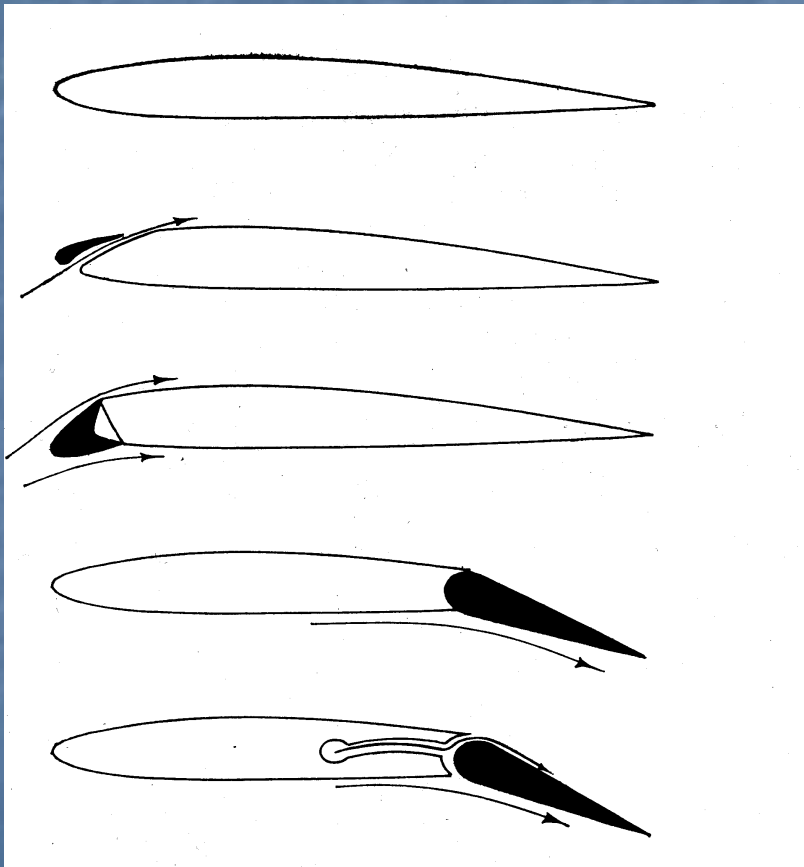


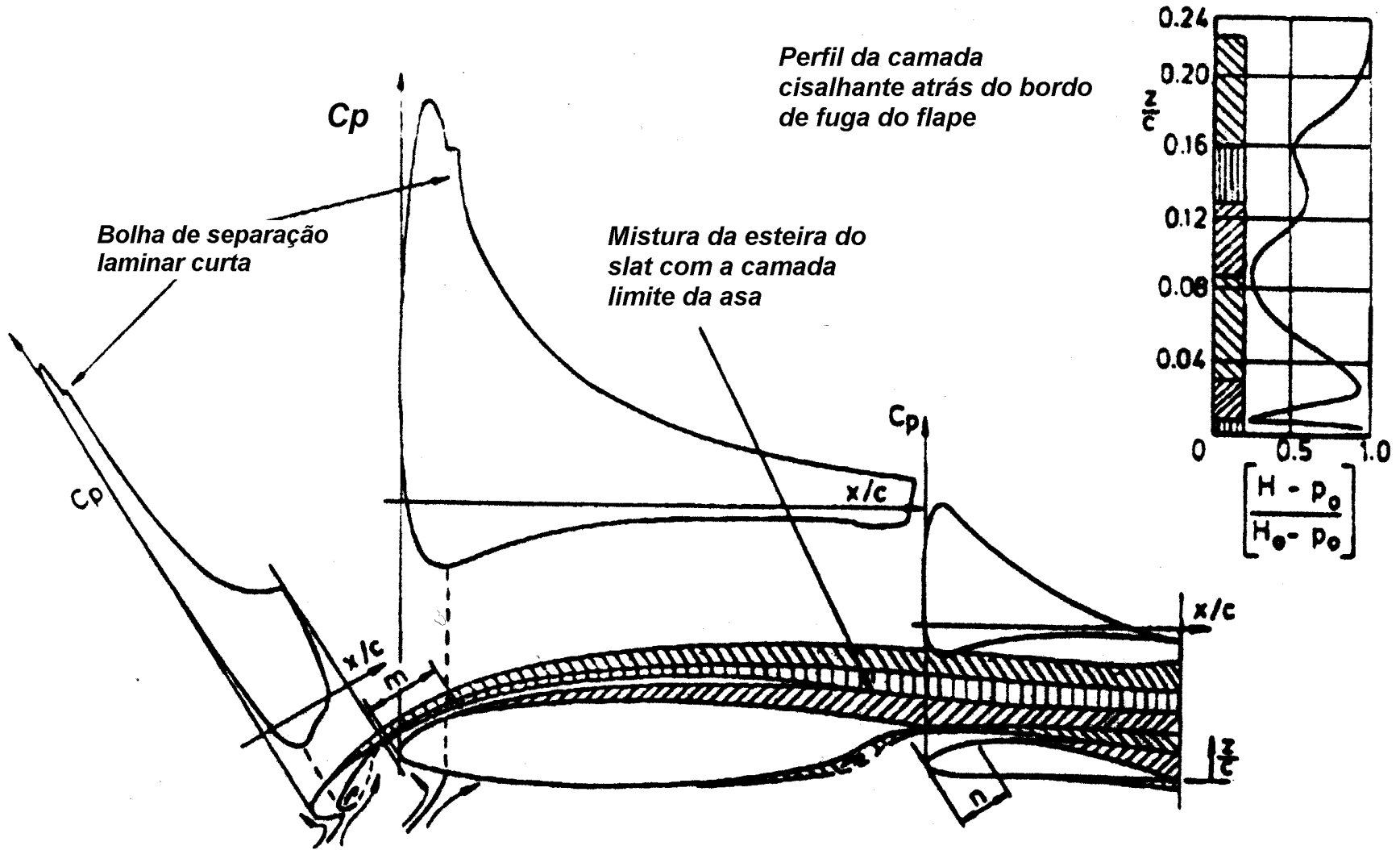
**flape slotado simples
charneira fixa**



Flape com slote fixo (DC10)

Tipos de sistemas de alta sustentação

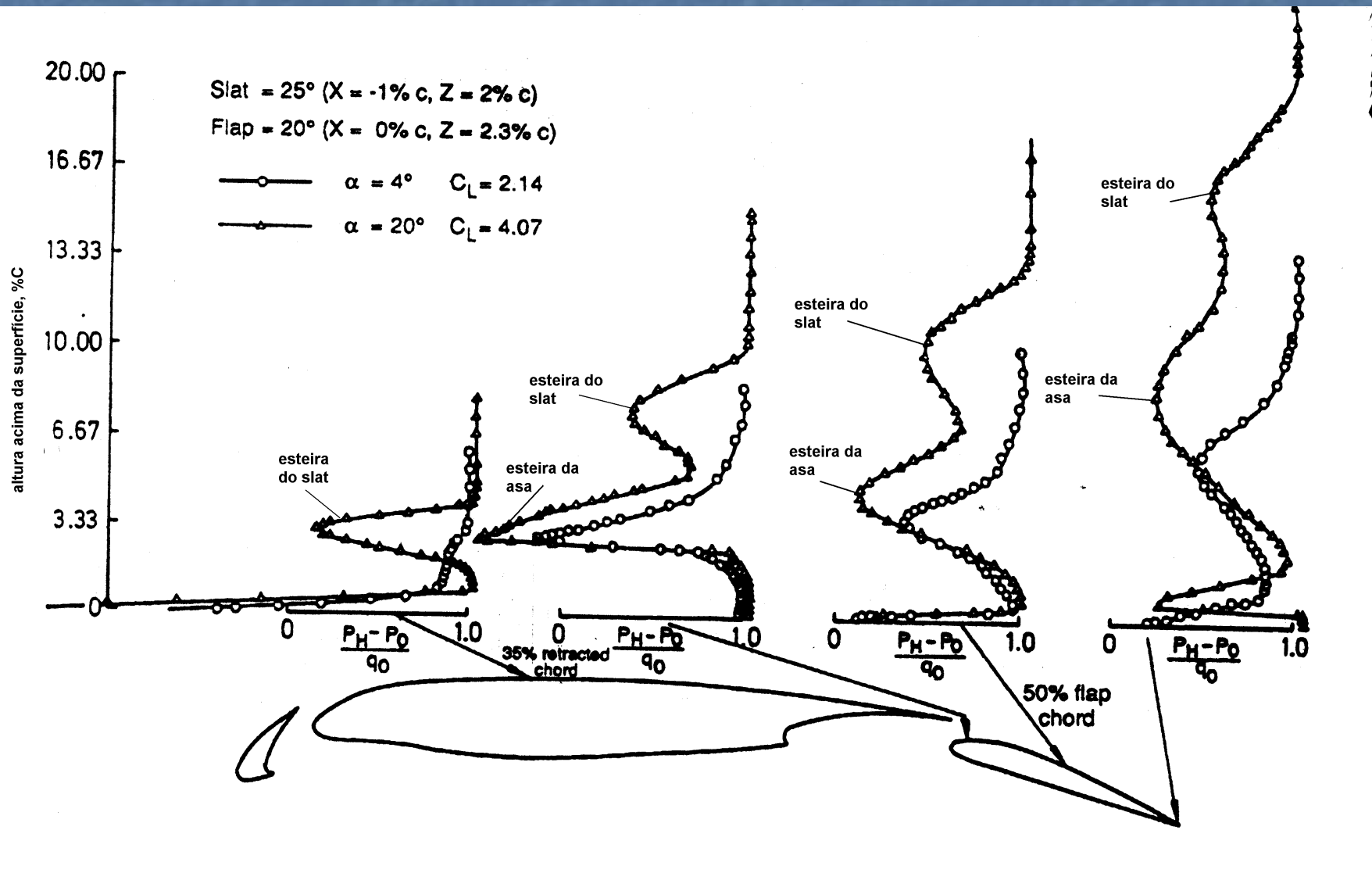




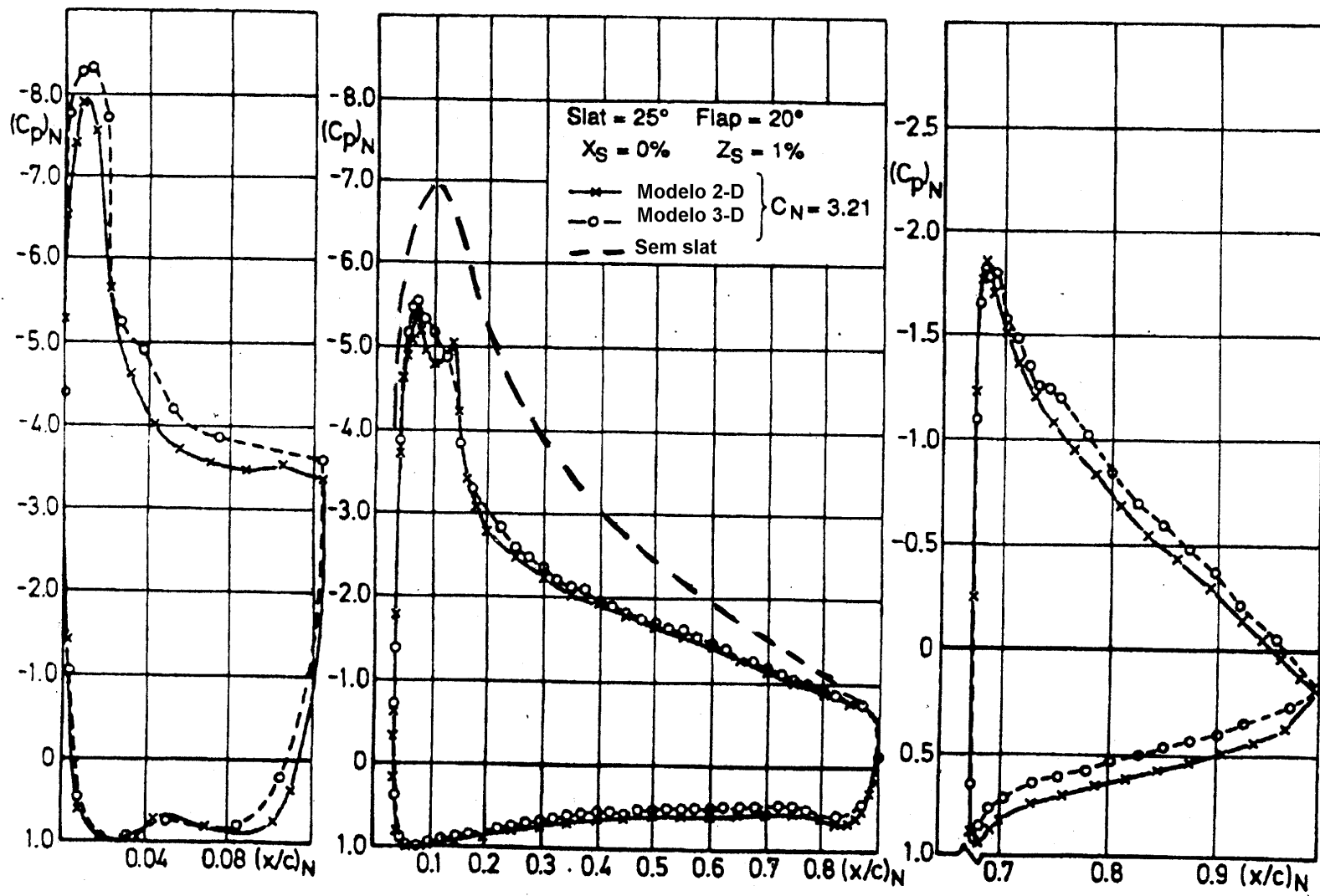
Sumário

- Sistemas de alta sustentação (SAS) não são sistemas de controle da camada limite. SAS agem na distribuição de pressão fora da camada limite.
- O bordo de fuga do slat fica numa região da alta velocidade o que diminui a pressão na sua parte traseira, para satisfazer a condição de Kutta o slat produz mais circulação (mais CL!). Esse ajuste se dá com uma diminuição da velocidade no bordo de ataque da asa.
- A incidência do escoamento na parte dianteira da asa é modificada pelo “downwash” do slat produzindo um pico de sucção menor. O mesmo acontece no flape.
- O mesmo acontece na região do bordo de fuga do elemento principal devido ao escoamento na parte dianteira do flap.
- Como uma resultado global, o aumento de pressão em toda a asa é dividido em vários aumentos de pressão pequenos.
- A mistura da esteira do elemento ‘a frente com a camada limite do próximo elemento induz uma aumento da espessura da camada limite, isso implica num aumento dos efeitos viscosos adesivos.
- Esse efeito é, em parte compensado pela “nova” camada limite de cada elemento.

Camada limite confluyente



Distribuição de pressão

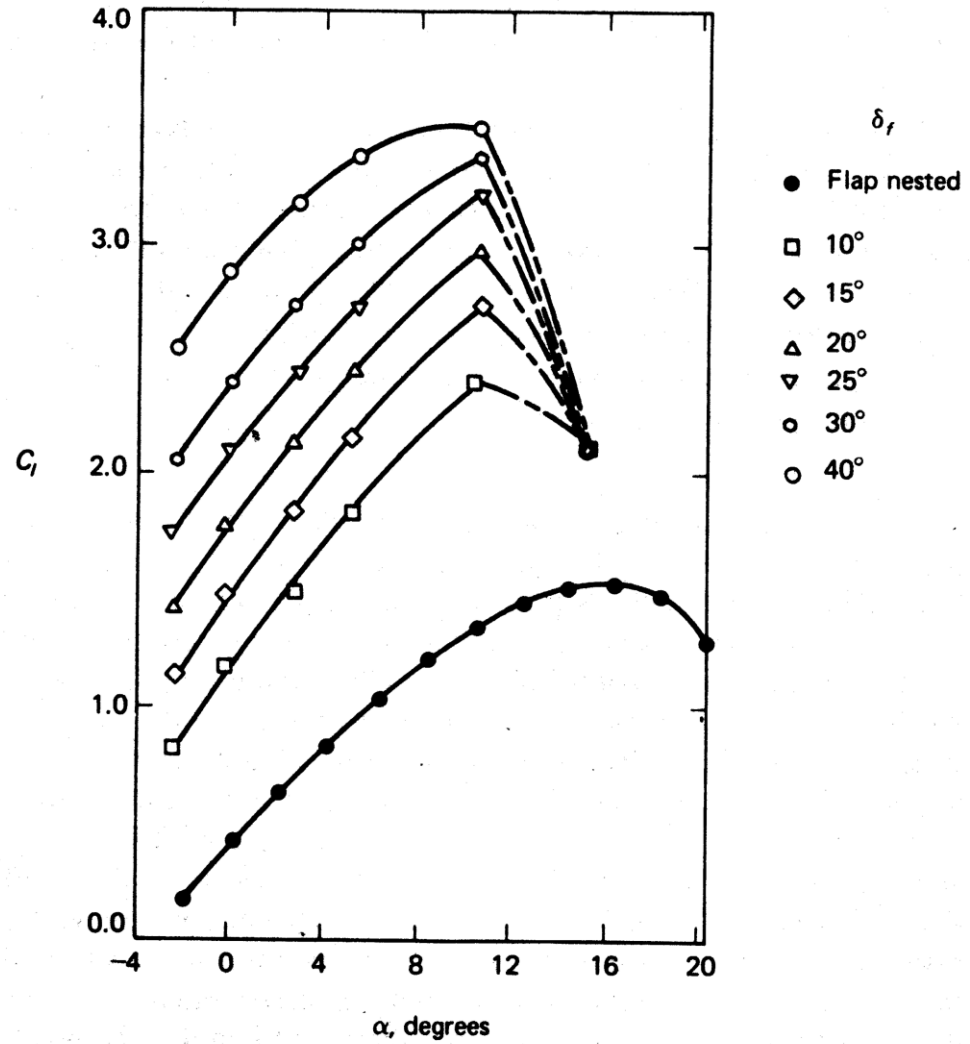
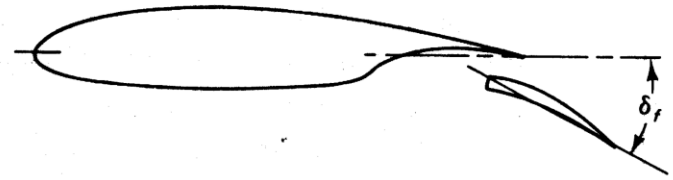
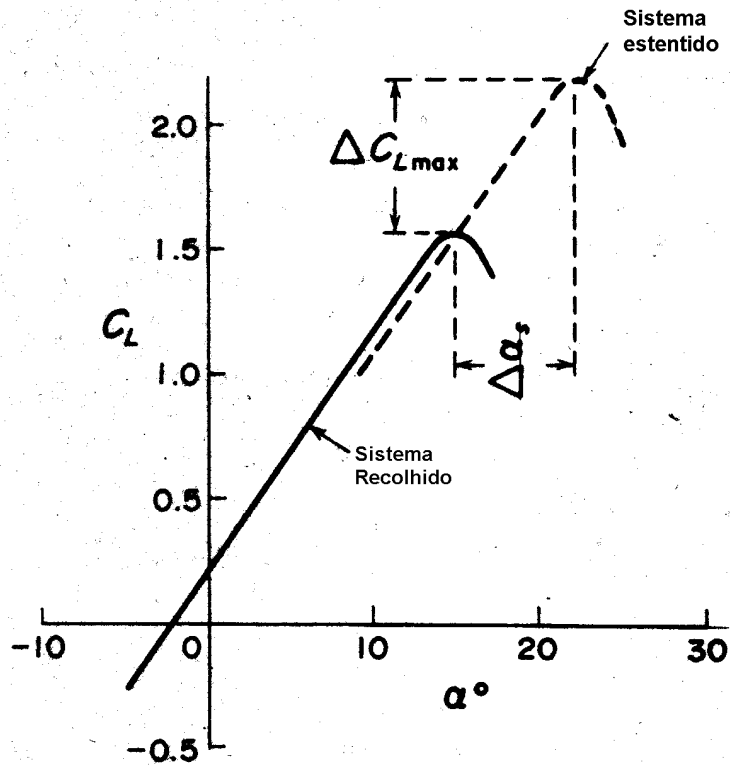


Efeito em C_L

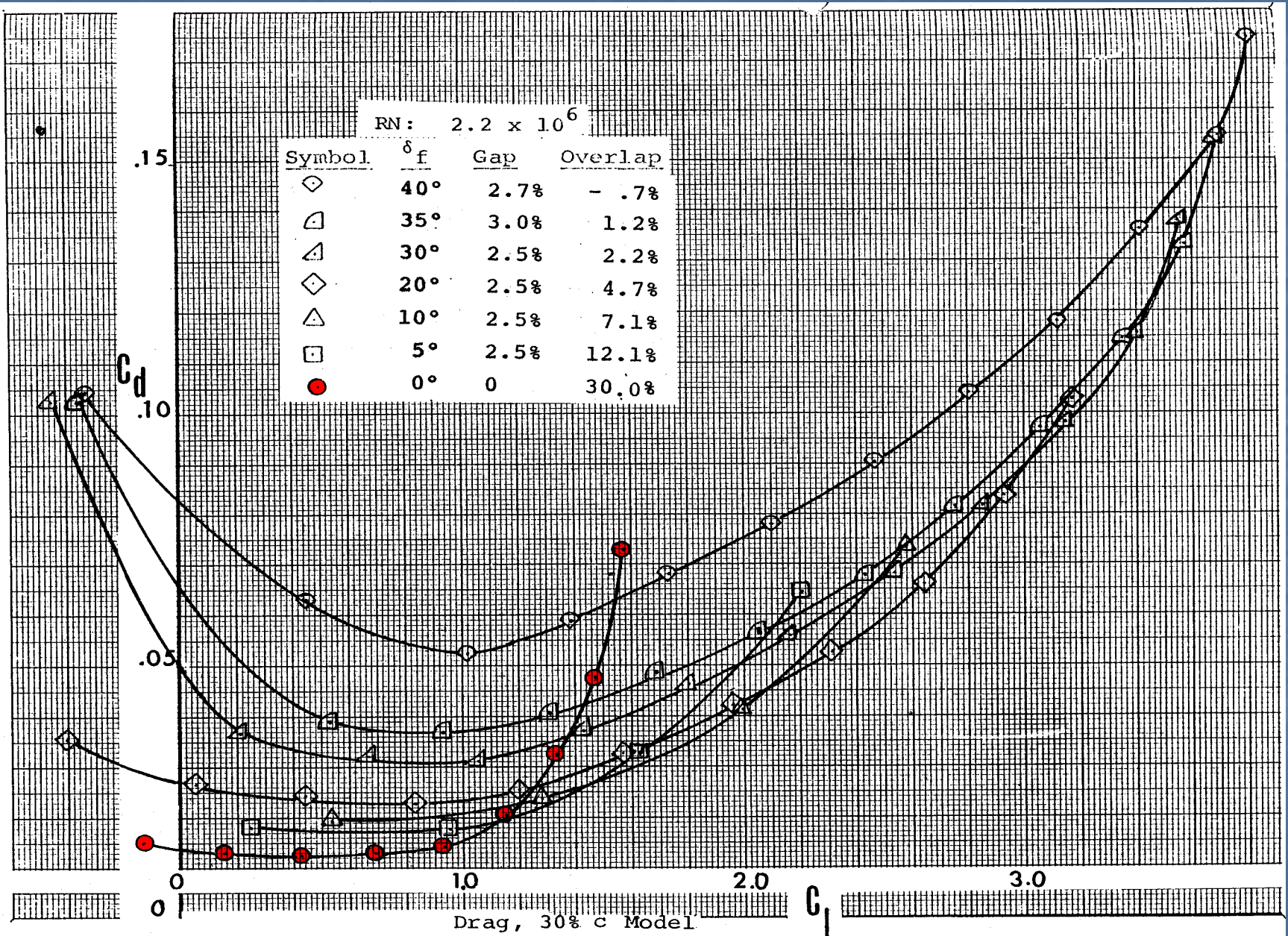
L.E. slat 

L.E. droop 

Kruger flap 



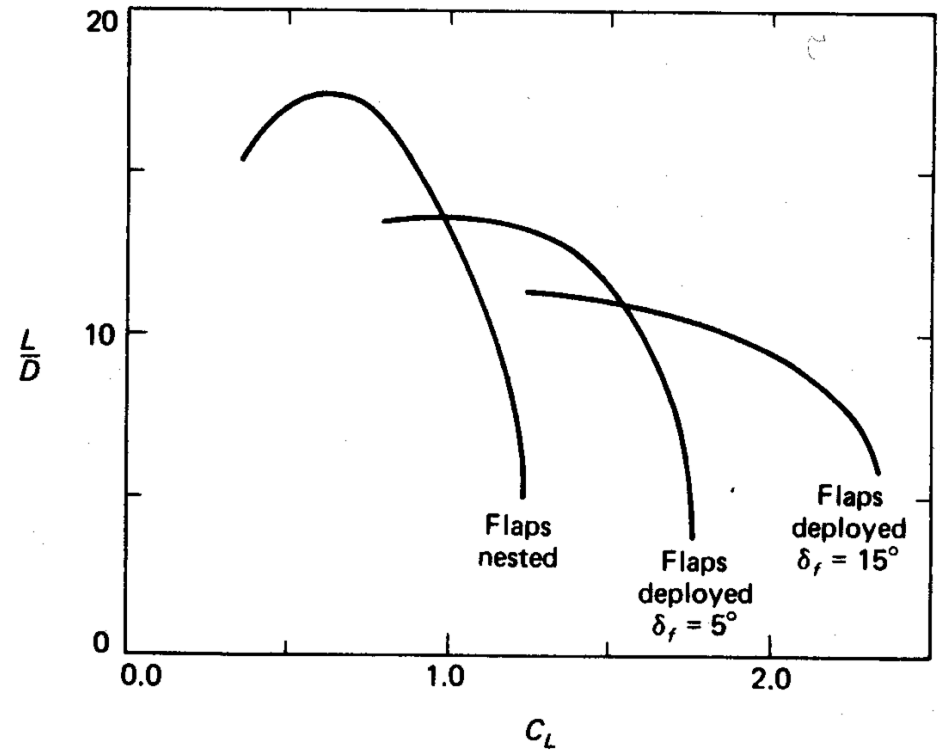
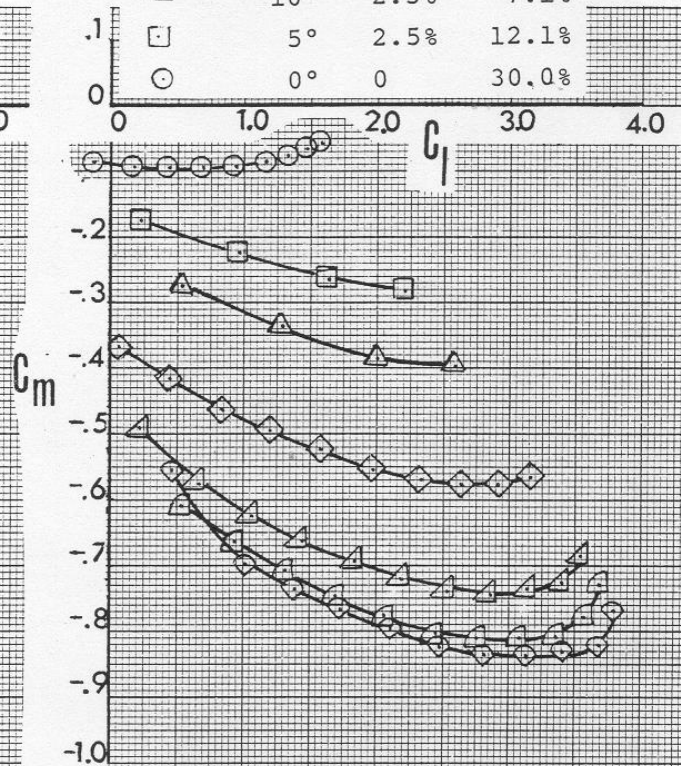
Efeito no CD



Efeito no C_m e L/D

RN: 2.2×10^6

Symbol	δ_f	Gap	Overlap
◇	40°	2.7%	- .7%
◐	35°	3.0%	1.2%
◑	30°	2.5%	2.2%
◒	20°	2.5%	4.7%
◓	10°	2.5%	7.1%
◔	5°	2.5%	12.1%
○	0°	0	30.0%



Gap e overlap

