4.3 – The Scattering Matrix

Reading Assignment: ***pp. 174-183***

Admittance and Impedance matrices use the quantities $I(z)$, $V(z)$, and $Z(z)$ (or $Y(z)$).

Q: *Is there an **equivalent** matrix for transmission line activity expressed in terms of $V^+(z)$, $V^-(z)$, and $\Gamma(z)$?*

A: Yes! Its called the **scattering matrix**.

HO: THE SCATTERING MATRIX

Q: *Can we likewise determine something **physical** about our device or network by simply **looking** at its scattering matrix?*

A: HO: MATCHED, RECIPROCAL, LOSSLESS

EXAMPLE: A LOSSLESS, RECIPROCAL DEVICE

Q: *Isn't all this linear algebra a bit **academic**? I mean, it can't help us design components, **can it?***

A: It sure can! An analysis of the scattering matrix can tell us if a certain device is **even possible** to construct, and if so, what the **form** of the device must be.

HO: THE MATCHED, LOSSLESS, RECIPROCAL 3-PORT NETWORK

HO: THE MATCHED, LOSSLESS, RECIPROCAL 4-PORT NETWORK

Q: *But how are scattering parameters **useful?** How do we use them to **solve or analyze** real microwave circuit problems?*

A: Study the **examples** provided below!

EXAMPLE: THE SCATTERING MATRIX

EXAMPLE: SCATTERING PARAMETERS

Q: *OK, but how can we **determine** the scattering matrix of a device?*

A: We must carefully apply our **transmission line theory**!

EXAMPLE: DETERMINING THE SCATTERING MATRIX

Q: *Determining the Scattering Matrix of a multi-port device would seem to be particularly laborious. Is there any way to simplify the process?*

A: Many (if not most) of the useful devices made by us humans exhibit a high degree of **symmetry**. This can greatly **simplify** circuit analysis—if we **know how** to exploit it!

HO: CIRCUIT SYMMETRY

EXAMPLE: USING SYMMETRY TO DETERMINING A SCATTERING MATRIX

Q: *Is there any* ***other*** *way to use circuit symmetry to our advantage?*

A: Absolutely! One of the most **powerful** tools in circuit analysis is **Odd-Even Mode** analysis.

HO: SYMMETRIC CIRCUIT ANALYSIS

HO: ODD-EVEN MODE ANALYSIS

EXAMPLE: ODD-EVEN MODE CIRCUIT ANALYSIS

Q: *Aren't you* ***finished*** *with this section yet?*

A: Just **one more** very important thing.

HO: GENERALIZED SCATTERING PARAMETERS

EXAMPLE: THE SCATTERING MATRIX OF A CONNECTOR

The Scattering Matrix

At **"low"** frequencies, we can completely characterize a **linear** device or network using an **impedance** matrix, which relates the currents and voltages at **each** device terminal to the currents and voltages at **all** other terminals.

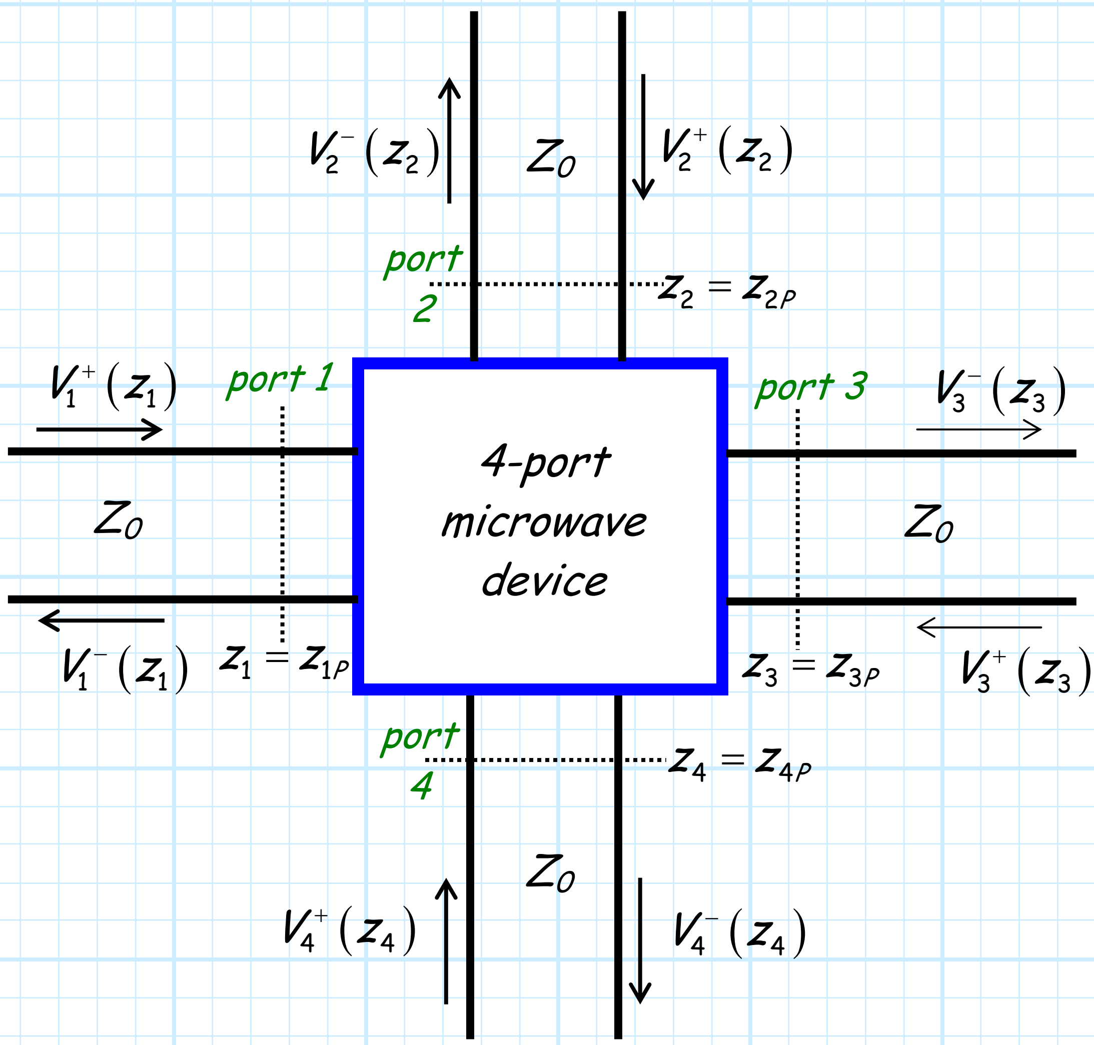
But, at microwave frequencies, it is **difficult** to measure total currents and voltages!

* Instead, we can measure the **magnitude** and **phase** of each of the two transmission line **waves** $V^+(z)$ and $V^-(z)$.

* In other words, we can determine the relationship between the incident and reflected wave at **each** device terminal to the incident and reflected waves at **all** other terminals.

These relationships are completely represented by the **scattering matrix**. It **completely** describes the behavior of a linear, multi-port device at a **given frequency** ω, and a given line impedance Z_0.

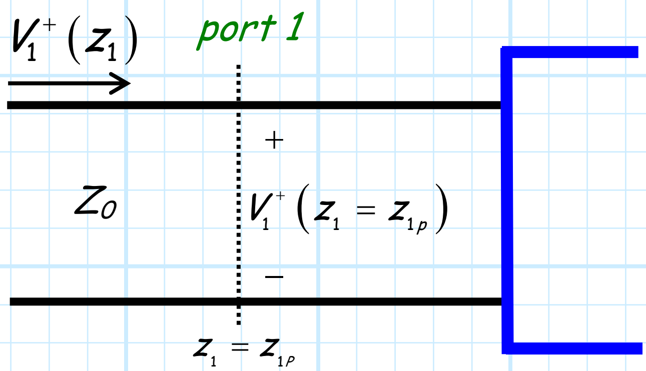
Consider now the **4-port** microwave device shown below:



Note that we have now characterized transmission line activity in terms of incident and "reflected" waves. Note the negative going "reflected" waves can be viewed as the waves **exiting** the multi-port network or device.

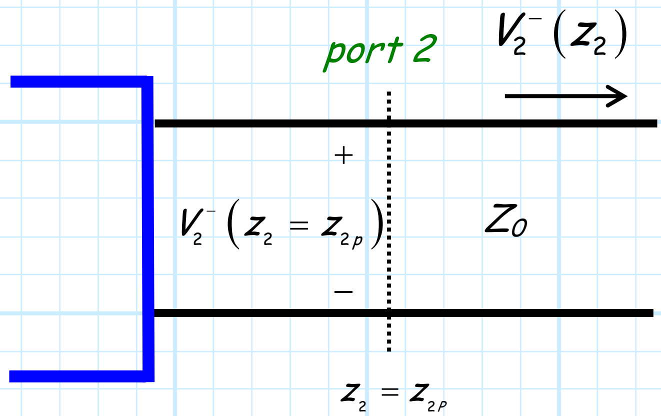
→ Viewing transmission line activity this way, we can fully characterize a multi-port device by its **scattering parameters**!

Say there exists an **incident** wave on **port 1** (i.e., $V_1^+(z_1) \neq 0$), while the incident waves on all other ports are known to be **zero** (i.e., $V_2^+(z_2) = V_3^+(z_3) = V_4^+(z_4) = 0$).



Say we measure/determine the voltage of the wave flowing **into port 1**, at the port 1 **plane** (i.e., determine $V_1^+(z_1 = z_{1P})$).

Say we then measure/determine the voltage of the wave flowing **out** of **port 2**, at the port 2 plane (i.e., determine $V_2^-(z_2 = z_{2P})$).



The complex ratio between $V_1^+(z_1 = z_{1P})$ and $V_2^-(z_2 = z_{2P})$ is know as the **scattering parameter** S_{21}:

$$S_{21} = \frac{V_2^-(z_2 = z_{2P})}{V_1^+(z_1 = z_{1P})} = \frac{V_{02}^- \, e^{+j\beta z_{2P}}}{V_{01}^+ \, e^{-j\beta z_{1P}}} = \frac{V_{02}^-}{V_{01}^+} \; e^{+j\beta(z_{2P}+z_{1P})}$$

Likewise, the scattering parameters S_{31} and S_{41} are:

$$S_{31} = \frac{V_3^-(z_3 = z_{3P})}{V_1^+(z_1 = z_{1P})} \qquad \text{and} \qquad S_{41} = \frac{V_4^-(z_4 = z_{4P})}{V_1^+(z_1 = z_{1P})}$$

We of course could **also** define, say, scattering parameter S_{34} as the ratio between the complex values $V_4^+(z_4 = z_{4P})$ (the wave **into** port 4) and $V_3^-(z_3 = z_{3P})$ (the wave **out of** port 3), given that the input to all other ports (1,2, and 3) are zero.

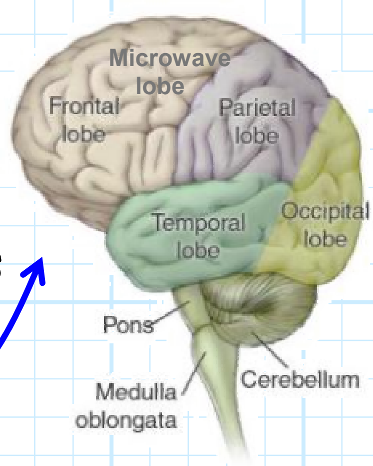
Thus, more **generally**, the ratio of the wave incident on port n to the wave emerging from port m is:

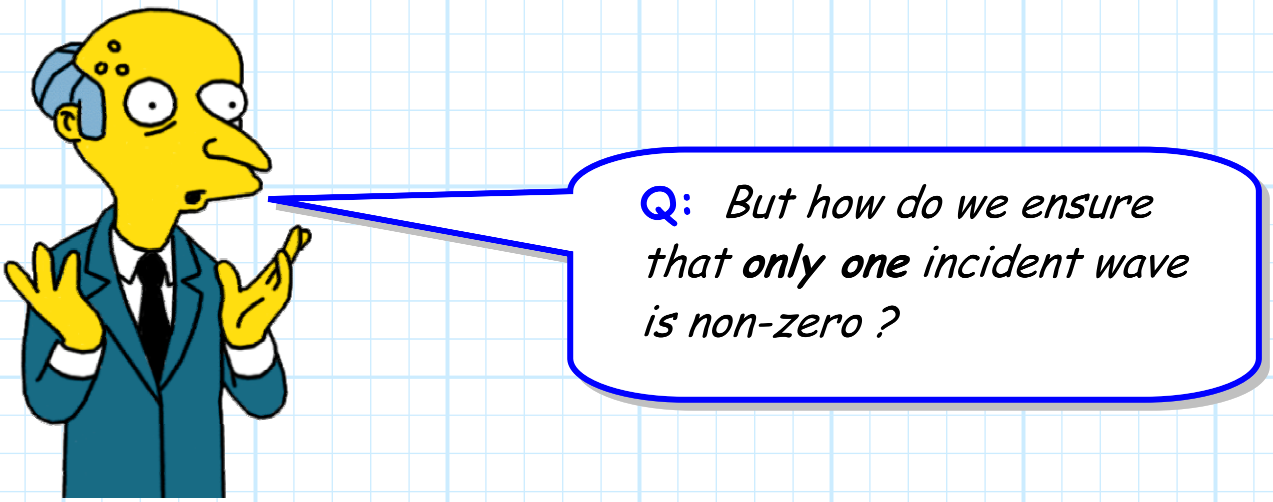
$$S_{mn} = \frac{V_m^-(z_m = z_{mP})}{V_n^+(z_n = z_{nP})} \qquad \text{(given that} \quad V_k^+(z_k) = 0 \ \text{ for all } k \neq n)$$

Note that frequently the port positions are assigned a **zero** value (e.g., $z_{1P} = 0$, $z_{2P} = 0$). This of course **simplifies** the scattering parameter calculation:

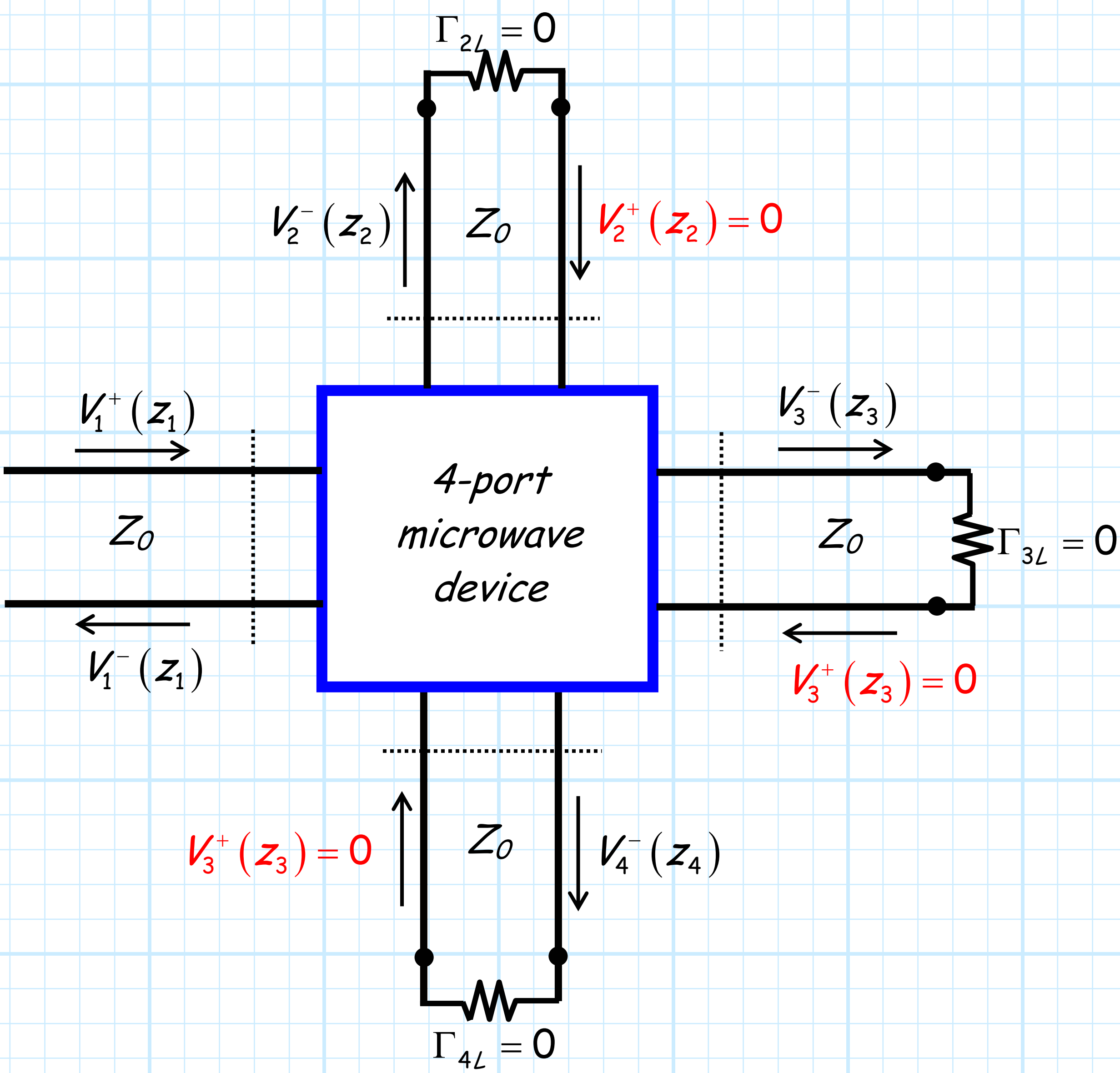
$$S_{mn} = \frac{V_m^-(z_m = 0)}{V_n^+(z_n = 0)} = \frac{V_{0m}^- \, e^{+j\beta 0}}{V_{0n}^+ \, e^{-j\beta 0}} = \frac{V_{0m}^-}{V_{0n}^+}$$

We will **generally assume** that the port locations are defined as $z_{nP} = 0$, and thus use the **above** notation. But **remember** where this expression came from!





A: **Terminate** all other ports with a **matched load**!



Note that **if** the ports are terminated in a **matched load** (i.e., $Z_L = Z_0$), then $\Gamma_{nL} = 0$ and therefore:

$$V_n^+(z_n) = 0$$

In other words, terminating a port ensures that there will be **no signal** incident on that port!

Q: *Just between you and me, I think you've messed this up! **In all** previous handouts you said that if $\Gamma_L = 0$, the wave in the **minus** direction would be zero:*

$$V^-(z) = 0 \quad \text{if} \quad \Gamma_L = 0$$

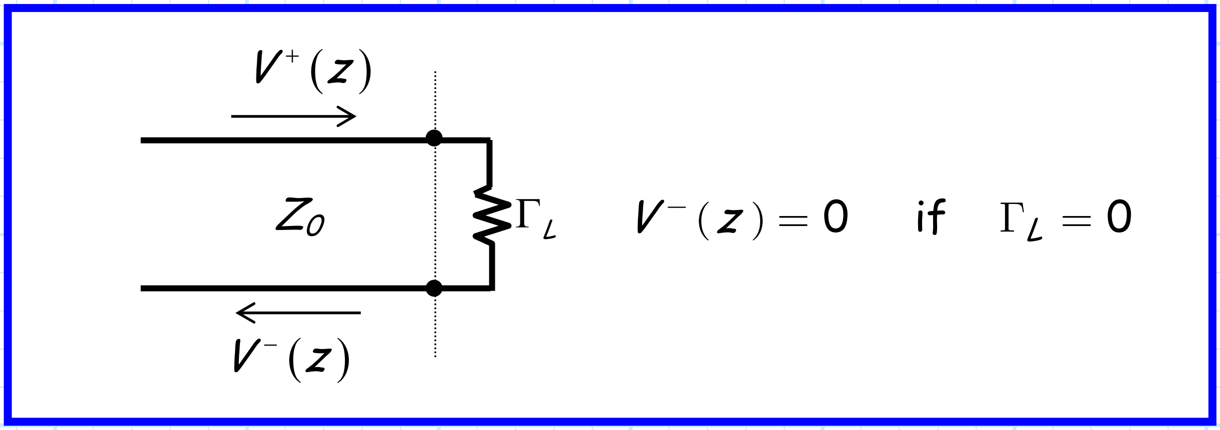
*but just **now** you said that the wave in the **positive** direction would be zero:*

$$V^+(z) = 0 \quad \text{if} \quad \Gamma_L = 0$$

*Of course, there is **no way** that **both** statements can be correct!*

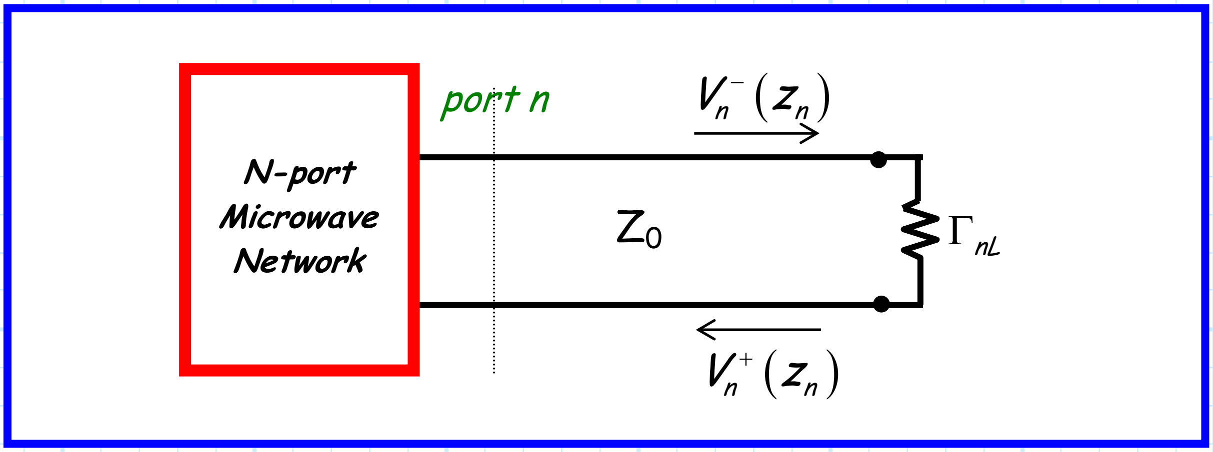
A: Actually, **both** statements are correct! You must be careful to understand the **physical definitions** of the plus and minus directions—in other words, the propagation directions of waves $V_n^+(z_n)$ and $V_n^-(z_n)$!

For example, we **originally** analyzed this case:



In this original case, the wave **incident** on the load is $V^+(z)$ (**plus** direction), while the **reflected** wave is $V^-(z)$ (**minus** direction).

Contrast this with the case we are **now** considering:

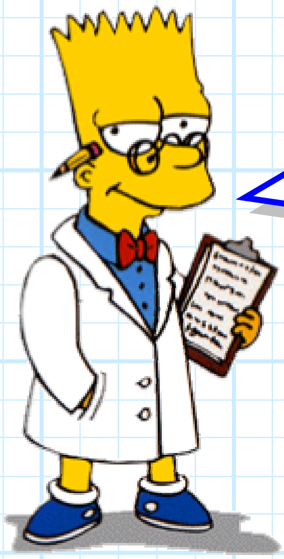


For this current case, the situation is **reversed**. The wave incident on the load is **now** denoted as $V_n^-(z_n)$ (coming **out** of port n), while the wave reflected off the load is **now** denoted as $V_n^+(z_n)$ (going **into** port n).

As a result, $V_n^+(z_n)=0$ when $\Gamma_{nL}=0$!

Perhaps we could more **generally** state that for some load Γ_L:

$$V^{reflected}(z = z_L) = \Gamma_L \; V^{incident}(z = z_L)$$



*For each case, **you** must be able to correctly identify the mathematical statement describing the wave **incident** on, and **reflected** from, some passive load.*

*Like most equations in engineering, the **variable names** can **change**, but the **physics** described by the mathematics will **not**!*

Now, **back** to our discussion of **S-parameters**. We found that **if** $z_{nP} = 0$ for all ports n, the scattering parameters could be directly written in terms of wave **amplitudes** V_{0n}^{+} and V_{0m}^{-}.

$$S_{mn} = \frac{V_{0m}^{-}}{V_{0n}^{+}} \qquad \text{(when } V_k^{+}(z_k) = 0 \text{ for all } k \neq n\text{)}$$

Which we can now **equivalently** state as:

$$S_{mn} = \frac{V_{0m}^{-}}{V_{0n}^{+}} \qquad \text{(when all ports, except port } n\text{, are terminated in } \textbf{matched loads}\text{)}$$

One more **important** note—notice that for the ports terminated in matched loads (i.e., those ports with **no** incident wave), the voltage of the exiting **wave** is also the **total** voltage!

$$\begin{aligned} V_m(z_m) &= V_{0m}^{+}\, e^{-j\beta z_n} + V_{0m}^{-}\, e^{+j\beta z_n} \\ &= 0 + V_{0m}^{-}\, e^{+j\beta z_m} \\ &= V_{0m}^{-}\, e^{+j\beta z_m} \qquad \text{(for all terminated ports)} \end{aligned}$$

Thus, the value of the exiting wave **at** each terminated **port** is likewise the value of the total voltage **at** those ports:

$$\begin{aligned} V_m(0) &= V_{0m}^{+} + V_{0m}^{-} \\ &= 0 + V_{0m}^{-} \\ &= V_{0m}^{-} \qquad \text{(for all terminated ports)} \end{aligned}$$

And so, we can express **some** of the scattering parameters equivalently as:

$$\boxed{S_{mn} = \frac{V_m(0)}{V_{0n}^{+}} \qquad \text{(for \textbf{terminated} port } m\text{, } i.e.\text{, for } m \neq n)}$$

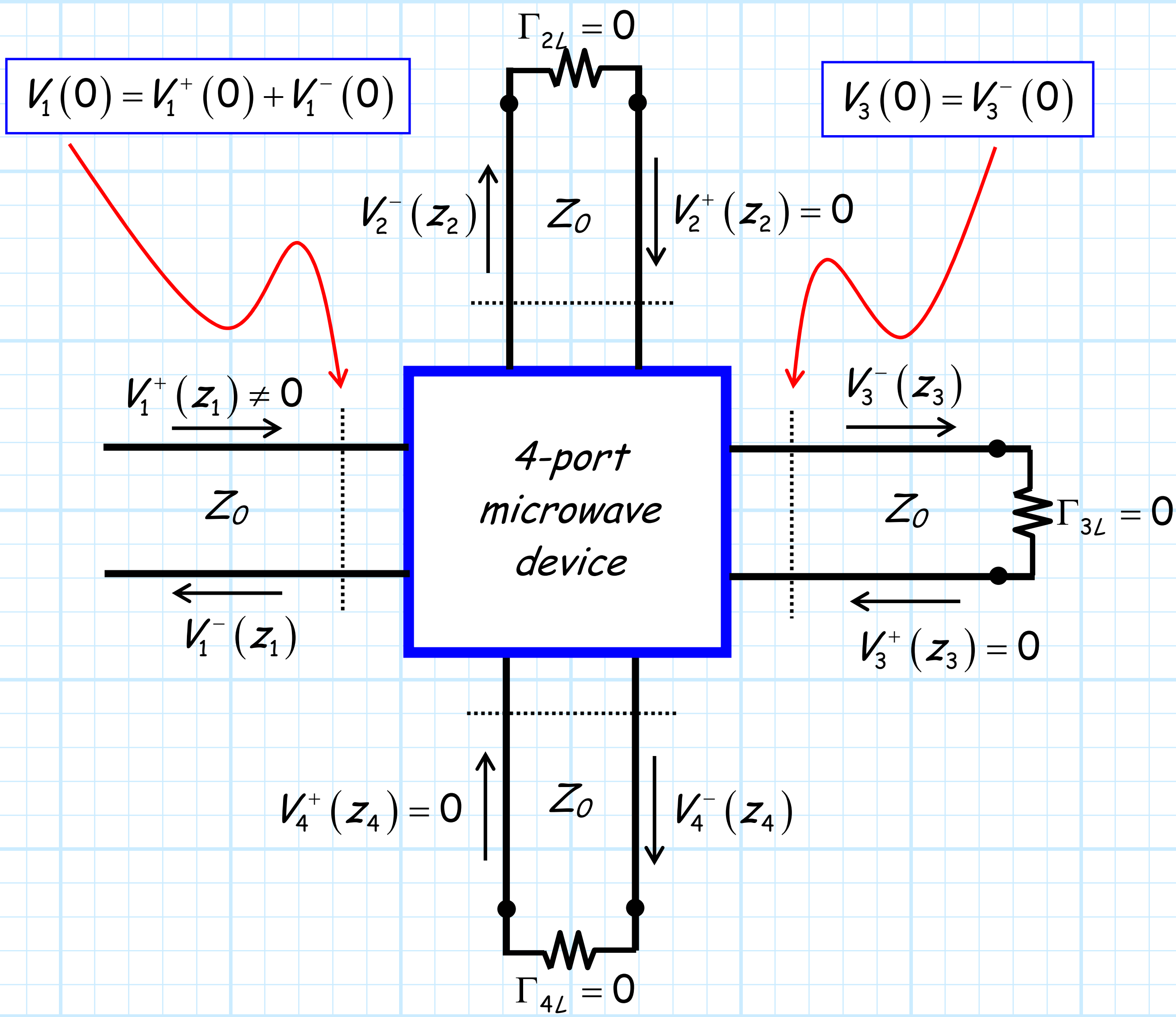
You might find this result **helpful** if attempting to determine scattering parameters where $m \neq n$ (e.g., S_{21}, S_{43}, S_{13}), as we can often use traditional **circuit theory** to easily determine the **total** port voltage $V_m(0)$.

However, we **cannot** use the expression above to determine the scattering parameters when $m = n$ (e.g., S_{11}, S_{22}, S_{33}).

Think about this! The scattering parameters for these cases are:

$$S_{nn} = \frac{V_{0n}^-}{V_{0n}^+}$$

Therefore, port n is a port where there actually **is** some incident wave V_{0n}^+ (port n is **not** terminated in a matched load!). And thus, the total voltage is **not** simply the value of the exiting wave, as **both** an incident wave and exiting wave exists at port n.



Typically, it is **much** more difficult to determine/measure the scattering parameters of the form S_{nn}, as opposed to scattering parameters of the form S_{mn} (where $m \neq n$) where there is **only** an **exiting** wave from port m!

We can use the scattering matrix to determine the solution for a more **general** circuit—one where the ports are **not** terminated in matched loads!

Q: *I'm not understanding the importance scattering parameters. How are they useful to us* ***microwave engineers?***

A: Since the device is **linear**, we can apply **superposition**. The output at any port due to **all** the incident waves is simply the coherent **sum** of the output at that port due to **each** wave!

For example, the **output** wave at port 3 can be determined by (assuming $z_{nP} = 0$):

$$V_{03}^{-} = S_{34}\, V_{04}^{+} + S_{33}\, V_{03}^{+} + S_{32}\, V_{02}^{+} + S_{31}\, V_{01}^{+}$$

More **generally**, the output at port m of an N-port device is:

$$\boxed{V_{0m}^{-} = \sum_{n=1}^{N} S_{mn}\, V_{0n}^{+} \qquad (z_{nP} = 0)}$$

This expression can be written in **matrix** form as:

$$\mathbf{V}^- = \mathcal{S}\ \mathbf{V}^+$$

Where $\mathbf{V}^-$ is the **vector**:

$$\mathbf{V}^- = \left[V_{01}^-, V_{02}^-, V_{03}^-, \ldots, V_{0N}^-\right]^T$$

and $\mathbf{V}^+$ is the vector:

$$\mathbf{V}^+ = \left[V_{01}^+, V_{02}^+, V_{03}^+, \ldots, V_{0N}^+\right]^T$$

Therefore $\mathcal{S}$ is the **scattering matrix**:

$$\mathcal{S} = \begin{bmatrix} \mathcal{S}_{11} & \cdots & \mathcal{S}_{1n} \\ \vdots & \ddots & \vdots \\ \mathcal{S}_{m1} & \cdots & \mathcal{S}_{mn} \end{bmatrix}$$

The scattering matrix is a N by N matrix that **completely characterizes** a linear, N-port device. Effectively, the scattering matrix describes a multi-port device the way that Γ_L describes a single-port device (e.g., a load)!

But **beware**! The values of the scattering matrix for a particular device or network, just like Γ_L, are **frequency dependent**! Thus, it may be more instructive to **explicitly** write:

$$\mathcal{S}(\omega) = \begin{bmatrix} S_{11}(\omega) & \cdots & S_{1n}(\omega) \\ \vdots & \ddots & \vdots \\ S_{m1}(\omega) & \cdots & S_{mn}(\omega) \end{bmatrix}$$

Also realize that—also just like Γ_L—the scattering matrix is dependent on **both** the **device/network** and the Z_0 value of the **transmission lines connected** to it.

Thus, a device connected to transmission lines with $Z_0 = 50\Omega$ will have a **completely different scattering matrix** than that same device connected to transmission lines with $Z_0 = 100\Omega$!!!