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DETERMINAÇÃO DA MATRIZ S DE ELEMENTOS
DE CIRCUITOS

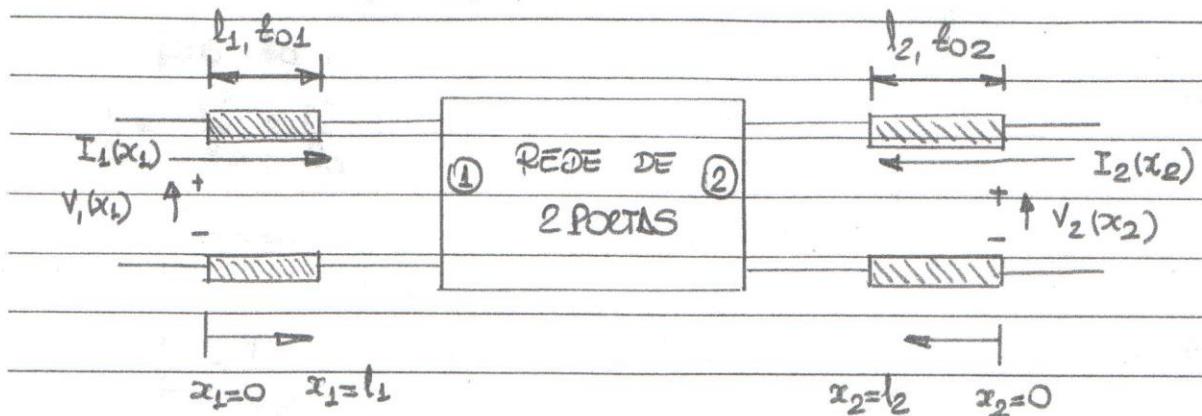


Fig.1. Rede de 2 portas conectada a 2 tratos de linha de transmissão sem fundo.

Linha 1: comprimento l_1 e impedância característica Z_{01} , fundo-mute real

Linha 2: idem, l_2 e Z_{02}

Tensões e correntes nos linhos l_1 e l_2 : $V_1(x_1)$; $I_1(x_1)$
 $V_2(x_2)$; $I_2(x_2)$

reunidas em notações únicas: $V_i(x_i)$; $I_i(x_i)$

para simplificar as notações ao longo dos de duíos, vamos utilizar as notações simplificadas:

$$V_i(x_i), V_i(x_2) \rightarrow V_i(x_L) \rightarrow V(x) \rightarrow V$$

$$I_i(x_i), I_i(x_2) \rightarrow I_i(x_i) \rightarrow I(x) \rightarrow I$$

Para uma linha de transmissão,

$$V = V^+ + V^- \quad (1)$$

$$I = I^+ - I^- \quad (2)$$

(+): Onda incidente

(-): Onda refletida

De (2):

$$I = I^+ - I^- = \frac{V^+}{Z_0} - \frac{V^-}{Z_0} \quad (3)$$

÷ por Z_0 :

$$\frac{V}{Z_0} = \frac{V^+}{Z_0} + \frac{V^-}{Z_0} \quad (4)$$

Assim, temos:

$$I = \frac{V^+}{Z_0} - \frac{V^-}{Z_0} \quad (5)$$

$$\frac{V}{Z_0} = \frac{V^+}{Z_0} + \frac{V^-}{Z_0} \quad (6)$$

Somando (5) e (6):

$$\frac{2V^+}{Z_0} = \frac{V}{Z_0} + I \quad (7)$$

× por Z_0 :

$$2V^+ = V + Z_0 I \quad \text{ou} \quad V^+ = \frac{1}{2}(V + Z_0 I)$$

÷ por $\sqrt{Z_0}$

$$\frac{V^+}{\sqrt{Z_0}} = \frac{1}{2\sqrt{Z_0}}(V + Z_0 I) \quad (8)$$

definindo:

$$a_i = \frac{V^+}{\sqrt{Z_0}} \quad \text{e} \quad a_i = \sqrt{Z_0} I^+ \quad (9)$$

(9) em (8):

$$a_i(x_i) = \sqrt{Z_{0i}} I_i^+(x_i) = \frac{1}{2\sqrt{Z_{0i}}} [V_i(x_i) + Z_{0i} I_i(x_i)] \quad (10)$$

subtraindo; (6) - (5):

$$\frac{V}{20} - I = 2 \frac{V}{20} \quad (11)$$

\times por $\frac{2}{20}$

$$V = \frac{1}{2} (V - \frac{2}{20} I)$$

\div por $\sqrt{20}$

$$\frac{V}{(20)^{1/2}} = \frac{1}{2\sqrt{20}} (V - \frac{2}{20} I)$$

definindo

$$b = \frac{V}{\sqrt{20}} \quad (12)$$

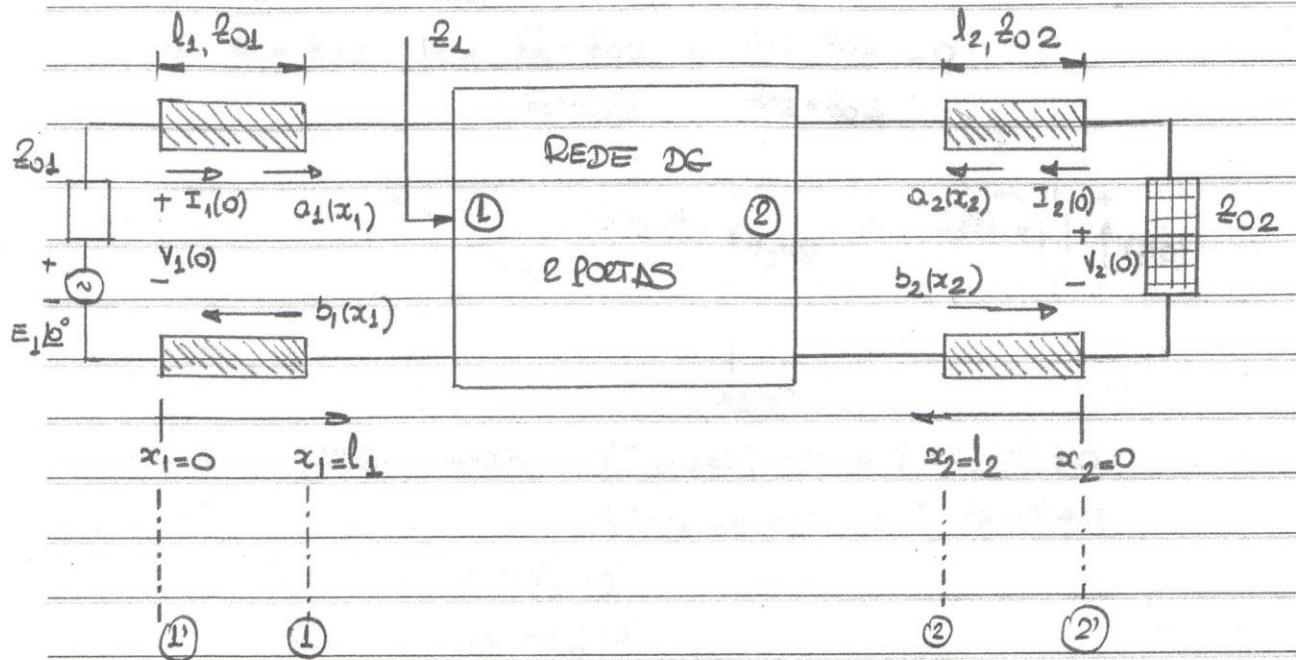
termos;

$$b_i(x_i) = \sqrt{20_i} I_i^-(x_i) = \frac{1}{2\sqrt{20_i}} [V_i(x_i) - \frac{2}{20_i} I_i(x_i)] \quad (13)$$

RESUMO:

$$a_i(x_i) = \sqrt{20_i} I_i^+(x_i) = \frac{1}{2\sqrt{20_i}} [V_i(x_i) + \frac{2}{20_i} I_i(x_i)] \quad (14)$$

$$b_i(x_i) = \sqrt{20_i} I_i^-(x_i) = \frac{1}{2\sqrt{20_i}} [V_i(x_i) - \frac{2}{20_i} I_i(x_i)] \quad (15)$$



Linhos de transmissão (referência, $x=0$, sobre a carga)

onda incidente: $V^+ e^{j\beta x}$

onda refletida: $V^- e^{-j\beta x}$

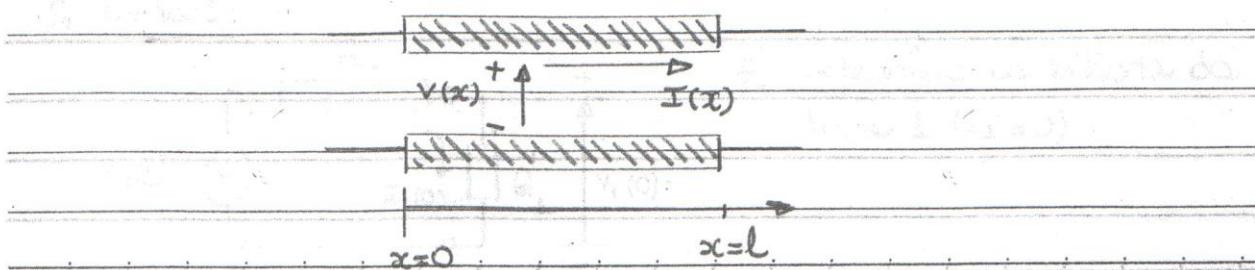
$$\text{coeficiente de reflexão: } \Gamma(x) = \frac{V^- e^{-j2\beta x}}{V^+} = \Gamma_c e^{-j2\beta x}$$

Tensão em qualquer ponto: $V(x) = V^+ e^{j\beta x} + V^- e^{-j\beta x}$

$$\text{corrente: } I(x) = \frac{1}{Z_0} (V^+ e^{j\beta x} - V^- e^{-j\beta x})$$

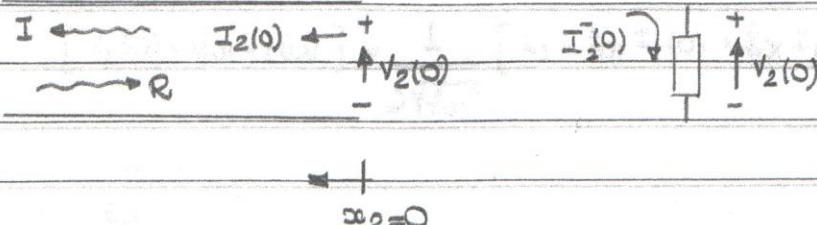
$$Z(x) = \frac{V}{I} = Z_0 \cdot \frac{1 + \Gamma(x)}{1 - \Gamma(x)} = Z_0 \cdot \frac{1 + \Gamma_c e^{j2\beta x}}{1 - \Gamma_c e^{-j2\beta x}}$$

$$\text{Se } \Gamma_c = 0 \rightarrow Z(x) = Z_0$$



1. Linha 2: $Z_L = Z_{02}$ (Linha casada)

$$\text{como } Z_L = Z_{02}, \Gamma_C = \frac{Z_C - Z_{02}}{Z_C + Z_{02}} = \frac{Z_{02} - Z_{02}}{Z_{02} + Z_{02}} = 0$$



sobre a carga casada: $V^+(x_2=0) = 0$ e $V^-(x_2=0) \neq 0$

$$I^+(x_2=0) = 0 \text{ e } I^-(x_2=0) \neq 0$$

$$\text{como } V_2(0) = V_2^+(0) + V_2^-(0)$$

$$I_2(0) = I_2^+(0) - I_2^-(0)$$

$$\therefore V_2(0) = I_2^-(0)$$

$$I_2(0) = -I_2^-(0)$$

mas, $V_2(0) = I_2^-(0) Z_{02}$: condições de contorno em $x_2=0$

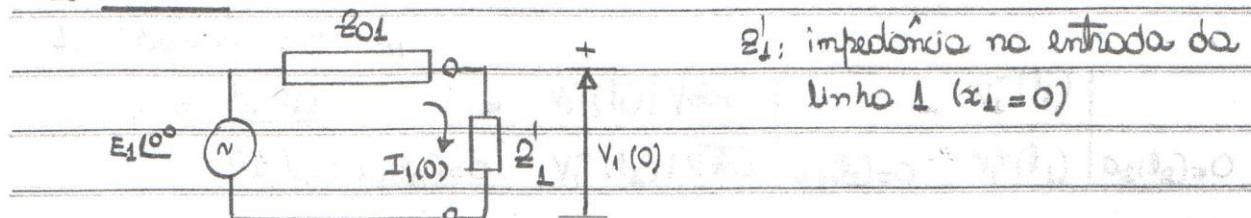
$$\therefore V_2(x_2=0) = -Z_{02} I_2(x_2=0) \quad (16)$$

de (14):

$$Q_2(0) = \frac{1}{2\sqrt{Z_{02}}} [V_2(0) + Z_{02} I_2(0)] = \frac{1}{2\sqrt{Z_{02}}} [-Z_{02} I_2(0) + Z_{02} I_2(0)]$$

$$\therefore Q_2(x_2=0) = 0 \quad (17)$$

2. Linha 1:



Do circuito temos que:

$$V_L(0) = E_L - Z_0 L I_L(0) \quad (18)$$

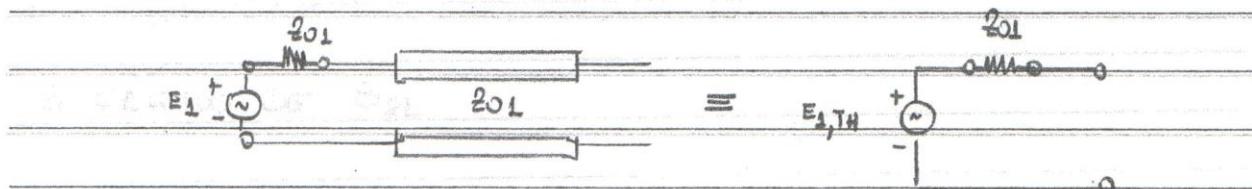
De (14):

$$Q_L(x_L=0) = \frac{1}{Z_0} [V_L(0) + Z_0 I_L(0)] = \frac{1}{Z_0} [E_L - Z_0 I_L(0) + Z_0 I_L(0)]$$

$$\therefore Q_L(x_L=0) = \frac{E_L}{Z_0} \quad (19)$$

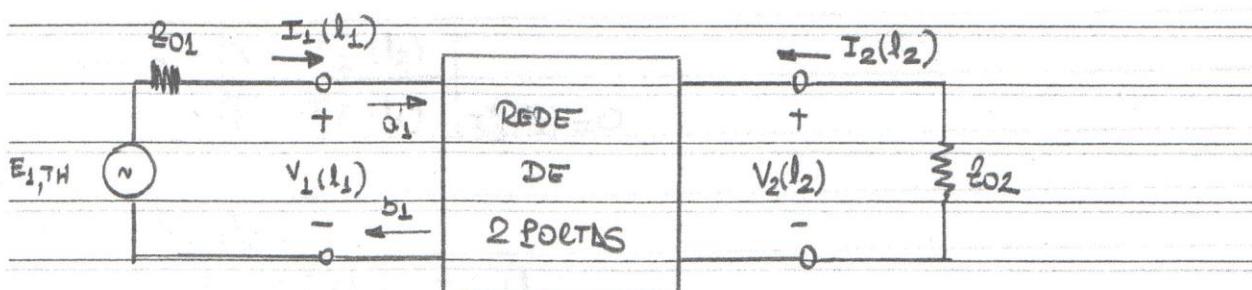
CÁLCULO DOS PARÂMETROS S NAS PORTAS 1 e 2

equivalente de Thévenin referente à fonte e linha de transmissão L



fonte de Tensão: curto-circuito

fonte de corrente: circuito aberto

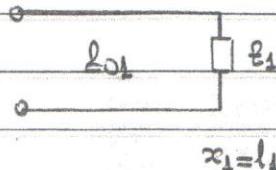


1. Cálculo de S_{11}

$$S_{11} = \frac{b_{11}(I_1)}{a_{11}(I_1) \mid a_{21}(I_2)=0} = \frac{V_{11}^-(I_1) / \sqrt{Z_0}}{V_{11}^+(I_1) / \sqrt{Z_0}} \mid a_{21}(I_2)=0 = \frac{V_{11}^-(I_1)}{V_{11}^+(I_1)} \mid a_{21}(I_2)=0$$

$$\text{mos, } V_1^-(l_1) / V_1^+(l_1) = \Gamma(x=l_1)$$

Síntese:



Z_1 : impedância vista no introdo de 1 de rede de 2 portas

$$x_1 = l_1$$

$$\therefore V_1^-(l_1) / V_1^+(l_1) = \Gamma(x=l_1) = \frac{Z_1 - Z_{01}}{Z_1 + Z_{01}}$$

Assim,

$$S_{11} = \frac{Z_1 - Z_{01}}{Z_1 + Z_{01}} \quad (20)$$

S_{11} : coeficiente de reflexão na fonte 1 com a linha 2 cerrada
($a_2(l_2) = 0$)

2. cálculo de S_{21}

$$S_{21} = \frac{b_2(l_2)}{a_1(l_1) \quad | \quad a_2(l_2) = 0}$$

$$S_{21} = \frac{\sqrt{Z_{02}} \quad I_2^-(l_2)}{\sqrt{Z_{01}} \quad I_1^+(l_1) \quad | \quad I_2^+(l_2) = 0}$$

$$\text{em } x_2 = l_2 :$$

$$I_2(l_2) = I_2^+(l_2) - I_2^-(l_2)$$

$$\text{como } a_2(l_2) = 0 \rightarrow I_2^+(l_2) = 0 \quad \& \quad I_2^-(l_2) = -I_2(l_2)$$

$$S_{21} = - \frac{\sqrt{Z_{02}} \quad I_2(l_2)}{\sqrt{Z_{01}} \quad I_1^+(l_1) \quad | \quad I_2^+(l_2) = 0} \quad (21)$$

$$\rightarrow (16): V_2(l_2) = -Z_{02} I_2(l_2) \rightarrow I_2(l_2) = -\frac{V_2(l_2)}{Z_{02}} \quad (22)$$

(22) um (21):

$$S_{21} = -\frac{\sqrt{Z_{02}} I_2(l_2)}{\sqrt{Z_{01}} I_1^+(l_1)} = -\frac{\sqrt{Z_{02}}}{\sqrt{Z_{01}}} \cdot \left[-\frac{V_2(l_2)}{Z_{02}} \right] \frac{1}{I_1^+(l_1)}$$

$$S_{21} = \frac{\sqrt{Z_{02}} V_2(l_2)}{\sqrt{Z_{01}} Z_{02} I_1^+(l_1)} \Big|_{I_2^+(l_2)=0} \quad (23)$$

Determinações de $I_1^+(l_1)$:

De (10) temos que

$$a_i(x_i) = \sqrt{Z_{0i}} I_i^+(x_i) = \frac{1}{2\sqrt{Z_{0i}}} [V_i(x_i) + Z_{0i} I_i(x_i)]$$

$$\text{e} \\ \sqrt{Z_{01}} I_1^+(l_1) = \frac{1}{2\sqrt{Z_{01}}} [V_1(l_1) + Z_{01} I_1(l_1)]$$

ou

$$I_1^+(l_1) = \frac{1}{2\sqrt{Z_{01}}} \left[\frac{\sqrt{Z_{01}} I_1(l_1)}{\sqrt{Z_{01}}} + \frac{V_1(l_1)}{\sqrt{Z_{01}}} \right] \quad (24)$$

do circuito equivalente,

$$E_{1,TH} = V_1(l_1) + Z_{01} I_1(l_1)$$

$$\text{e} \\ I_1(l_1) = \frac{E_{1,TH}}{Z_{01}} - \frac{V_1(l_1)}{Z_{01}} \quad (25)$$

(25) um (24),

$$I_1^+(l_1) = \frac{1}{2\sqrt{Z_{01}}} \left[\frac{\sqrt{Z_{01}} E_{1,TH}}{Z_{01}} - \frac{\sqrt{Z_{01}} V_1(l_1)}{Z_{01}} + \frac{V_1(l_1)}{\sqrt{Z_{01}}} \right]$$

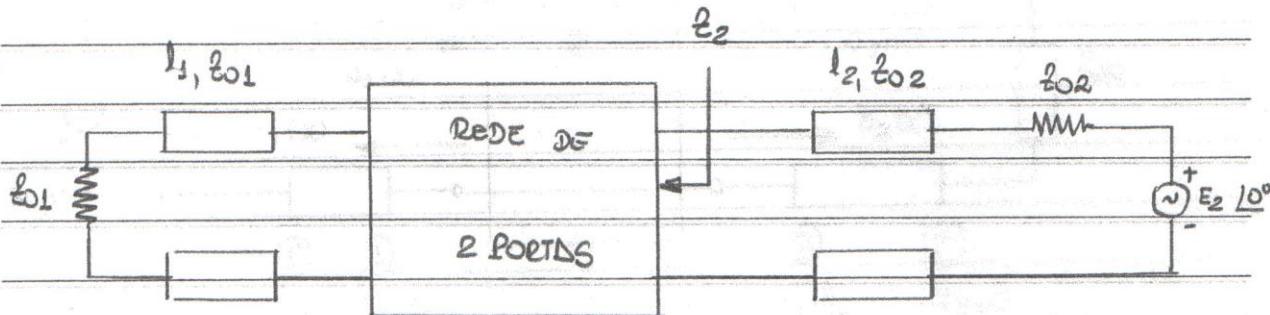
$$I_1^+(l_1) = \frac{1}{2\sqrt{2}0_1} \left[\sqrt{2}0_1 \frac{E_{1,TH}}{Z_0_1} - V_1(l_1) + \frac{V_1(l_1)}{\sqrt{2}0_1} \right] = \frac{E_{1,TH}}{2Z_0_1} \quad (26)$$

(26) em (23):

$$S_{21} = \frac{\sqrt{2}0_2}{\sqrt{2}0_1} \frac{1}{2} \frac{V_2(l_2)}{E_{1,TH}} \cdot 2Z_0_1 = \frac{2\sqrt{2}0_2}{\sqrt{2}0_1} \frac{\sqrt{2}0_1}{\sqrt{2}0_2} \frac{\sqrt{2}0_1}{\sqrt{2}0_2} \frac{V_2(l_2)}{E_{1,TH}}$$

$$S_{21} = \frac{2\sqrt{2}0_1}{\sqrt{2}0_2} \frac{V_2(l_2)}{E_{1,TH}} \quad (27)$$

FONTE NO LADO 2

3. cálculo de S_{22}

$$S_{22} = \frac{b_2(l_2)}{a_2(l_2)} = \frac{Z_2 - Z_02}{Z_2 + Z_02} \quad (28)$$

$$S_{12} = \frac{b_1(l_1)}{a_2(l_2)} = \frac{2\sqrt{2}0_2}{\sqrt{2}0_1} \frac{V_1(l_1)}{E_{2,TH}} \quad (29)$$

RESUMO

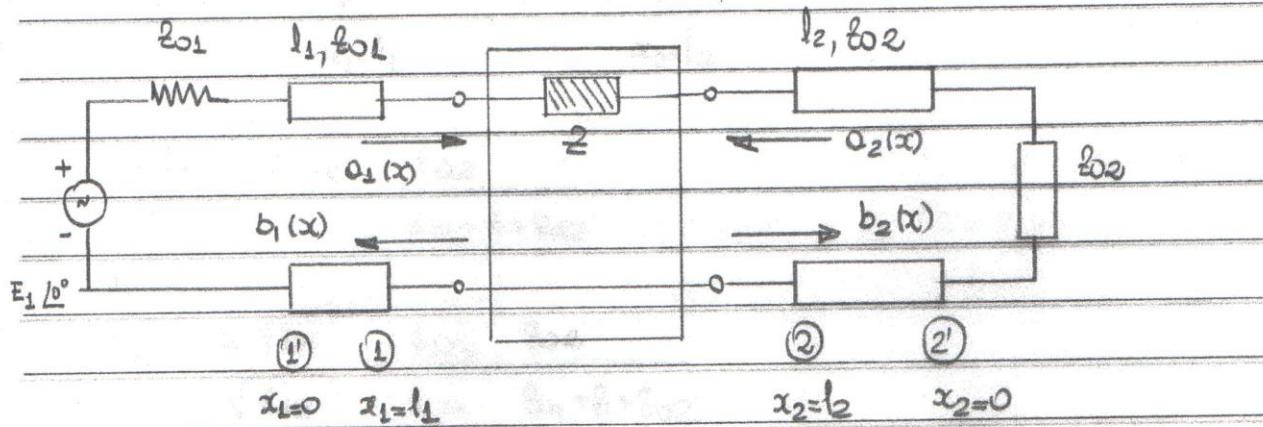
$$S_{11} = \frac{Z_1 - Z_{01}}{Z_1 + Z_{01}}$$

$$S_{12} = \frac{2 \sqrt{Z_{02}}}{\sqrt{Z_{01}}} \frac{V_2(l_1)}{E_{2,TH}}$$

$$S_{21} = \frac{2 \sqrt{Z_{01}}}{\sqrt{Z_{02}}} \frac{V_1(l_2)}{E_{1,TH}}$$

$$S_{22} = \frac{Z_2 - Z_{02}}{Z_2 + Z_{02}}$$

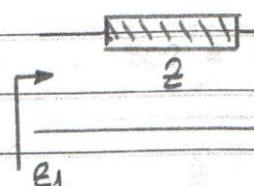
EXEMPLO L: Determinar os parâmetros S de uma impedância em série.



1. cálculo de S_{11}

$$S_{11} = \left| \frac{b_1}{a_1} \right|_{a_2=0} ; \quad a_2=0 \rightarrow \text{I.t. 2 terminado por } Z_{02} + \frac{Z}{x_2-l_2} = Z_{02}$$

$$S_{11} = \frac{Z_1 - Z_{01}}{Z_1 + Z_{01}}$$



$$S_{11} = \frac{Z + Z_{02} - Z_{01}}{Z + Z_{02} + Z_{01}}$$