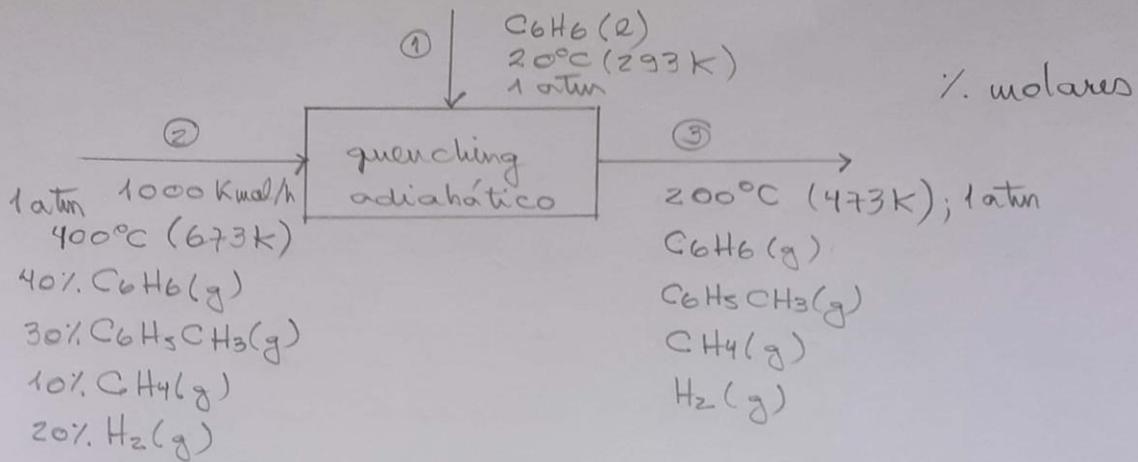


### exemplo 3 – quenching adiabático



hipóteses: estado estacionário;  $\Delta E_c = \Delta E_p = 0$ ;  $\dot{W}_\Delta = 0$ ;  
 dependência das entalpias c/a pressão é desprezado; gases ideais; mistura ideal.

a) Análise do N° GL:

	BM	BM+BE
NVI	3	$(3) + 3(T) + 2(\dot{Q}; \dot{W}_\Delta)$
NVEI	4	$(4) + 3(T_1; T_2; T_3) + 2(\dot{Q} = \dot{W}_\Delta = 0)$
NBI	4	$(4) + 1(BE)$
NRI	0	0
N° GL	1	0

O problema está subespecificado quanto ao BM, mas constantemente especificado como um todo (BM+BE). Dessa forma, o BM está acoplado ao BE, de modo que as equações correspondentes devem ser resolvidas simultaneamente. O BE será usado para calcular uma vazão que falta.

b) Com as hipóteses e simplificações acima, já adotando uma condição de referência, o balanço de energia em base molar para o sistema adiabático fica:

$$\sum_{\Delta=1}^S \left[ \sum_{j=1}^J F_{\Delta,j} \cdot (\tilde{H}_{\Delta,j} - \tilde{H}_{\Delta,ref}) - \sum_{k=1}^K F_{\Delta,k} \cdot (\tilde{H}_{\Delta,k} - \tilde{H}_{\Delta,ref}) \right] = 0$$

Para o problema, tem-se:

$$\begin{aligned} & F_{C_6H_6,1} \cdot (\tilde{H}_{C_6H_6,1} - \tilde{H}_{C_6H_6,ref}) + F_{C_6H_6,2} \cdot (\tilde{H}_{C_6H_6,2} - \tilde{H}_{C_6H_6,ref}) \\ & - F_{C_6H_6,3} \cdot (\tilde{H}_{C_6H_6,3} - \tilde{H}_{C_6H_6,ref}) \\ & + F_{C_6H_5CH_3,2} \cdot (\tilde{H}_{C_6H_5CH_3,2} - \tilde{H}_{C_6H_5CH_3,ref}) \\ & - F_{C_6H_5CH_3,3} \cdot (\tilde{H}_{C_6H_5CH_3,3} - \tilde{H}_{C_6H_5CH_3,ref}) \\ & + F_{CH_4,2} \cdot (\tilde{H}_{CH_4,2} - \tilde{H}_{CH_4,ref}) - F_{CH_4,3} \cdot (\tilde{H}_{CH_4,3} - \tilde{H}_{CH_4,ref}) \\ & + F_{H_2,2} \cdot (\tilde{H}_{H_2,2} - \tilde{H}_{H_2,ref}) - F_{H_2,3} \cdot (\tilde{H}_{H_2,3} - \tilde{H}_{H_2,ref}) = 0 \end{aligned}$$

Lembrando que:

$$\begin{aligned} \tilde{H}_{\Delta,j} &= \tilde{H}_{\Delta}(T_j, P_j, \Pi_j) \\ \tilde{H}_{\Delta,k} &= \tilde{H}_{\Delta}(T_k, P_k, \Pi_k) \\ \tilde{H}_{\Delta,ref} &= \tilde{H}_{\Delta}(T_{ref}, P_{ref}, \Pi_{ref}) \end{aligned}$$

Seja a condição de referência correspondente à condição da corrente 3:

$$\tilde{H}_{\Delta,ref} = \tilde{H}_{\Delta}(T_{ref}, P_{ref}, \Pi_{ref}) = \tilde{H}_{\Delta}(T_3, P_3, \Pi_3) = \tilde{H}_{\Delta,3}$$

espécies ←  
na condição da  
corrente 3

O BE fica:

$$\begin{aligned}
& F_{C_6H_6,1} \cdot (\tilde{H}_{C_6H_6,1} - \tilde{H}_{C_6H_6,3}) + F_{C_6H_6,2} \cdot (\tilde{H}_{C_6H_6,2} - \tilde{H}_{C_6H_6,3}) \\
& + F_{C_6H_5CH_3,2} \cdot (\tilde{H}_{C_6H_5CH_3,2} - \tilde{H}_{C_6H_5CH_3,3}) \\
& + F_{CH_4,2} \cdot (\tilde{H}_{CH_4,2} - \tilde{H}_{CH_4,3}) \\
& + F_{H_2,2} \cdot (\tilde{H}_{H_2,2} - \tilde{H}_{H_2,3}) = 0
\end{aligned}$$


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mas:  $\Pi_1 = \text{líqu}$ ;  $\Pi_2 = \Pi_3 = \text{gás}$   
 $P_1 = P_2 = P_3$

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$$\begin{aligned}
& F_{C_6H_6,1} \cdot [\tilde{H}_{C_6H_6}(T_1, \text{líqu}) - \tilde{H}_{C_6H_6}(T_3, \text{gás})] \\
& + F_{C_6H_6,2} \cdot [\tilde{H}_{C_6H_6}(T_2, \text{gás}) - \tilde{H}_{C_6H_6}(T_3, \text{gás})] \\
& + F_{C_6H_5CH_3,2} \cdot [\tilde{H}_{C_6H_5CH_3}(T_2, \text{gás}) - \tilde{H}_{C_6H_5CH_3}(T_3, \text{gás})] \\
& + F_{CH_4,2} \cdot [\tilde{H}_{CH_4}(T_2, \text{gás}) - \tilde{H}_{CH_4}(T_3, \text{gás})] \\
& + F_{H_2,2} \cdot [\tilde{H}_{H_2}(T_2, \text{gás}) - \tilde{H}_{H_2}(T_3, \text{gás})] = 0
\end{aligned}$$


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$$\begin{aligned}
& - F_{\text{C}_6\text{H}_6,1} \left[ \tilde{H}_{\text{C}_6\text{H}_6} (T_3, g_{\infty}) - \tilde{H}_{\text{C}_6\text{H}_6} (T_1, \text{liq}) \right] \\
& + F_{\text{C}_6\text{H}_6,2} \left[ \tilde{H}_{\text{C}_6\text{H}_6} (T_2, g_{\infty}) - \tilde{H}_{\text{C}_6\text{H}_6} (T_3, g_{\infty}) \right] \\
& + F_{\text{C}_6\text{H}_5\text{CH}_3,2} \left[ \tilde{H}_{\text{C}_6\text{H}_5\text{CH}_3} (T_2, g_{\infty}) - \tilde{H}_{\text{C}_6\text{H}_5\text{CH}_3} (T_3, g_{\infty}) \right] \\
& + F_{\text{CH}_4,2} \left[ \tilde{H}_{\text{CH}_4} (T_2, g_{\infty}) - \tilde{H}_{\text{CH}_4} (T_3, g_{\infty}) \right] \\
& + F_{\text{H}_2,2} \left[ \tilde{H}_{\text{H}_2} (T_2, g_{\infty}) - \tilde{H}_{\text{H}_2} (T_3, g_{\infty}) \right] = 0
\end{aligned}$$

$$\begin{aligned}
& - F_{\text{C}_6\text{H}_6,1} \left[ \int_{T_1}^{T_b} \tilde{C}_{p,\text{C}_6\text{H}_6(\text{l})} dT + \Delta \tilde{H}_{\text{lv},\text{C}_6\text{H}_6}(T_b) + \int_{T_b}^{T_3} \tilde{C}_{p,\text{C}_6\text{H}_6(\text{g})} dT \right] \\
& + F_{\text{C}_6\text{H}_6,2} \int_{T_3}^{T_2} \tilde{C}_{p,\text{C}_6\text{H}_6(\text{g})} dT + F_{\text{C}_6\text{H}_5\text{CH}_3,2} \int_{T_3}^{T_2} \tilde{C}_{p,\text{C}_6\text{H}_5\text{CH}_3(\text{g})} dT \\
& + F_{\text{CH}_4,2} \int_{T_3}^{T_2} \tilde{C}_{p,\text{CH}_4(\text{g})} dT + F_{\text{H}_2,2} \int_{T_3}^{T_2} \tilde{C}_{p,\text{H}_2(\text{g})} dT = 0
\end{aligned}$$

obs:  $T_b$  é a temperatura de saturação do  $\text{C}_6\text{H}_6$  à pressão normal (NBP). Da tab. 2, p.637:

$$T_b \cong 353,3 \text{ K } (80,1^\circ\text{C}) \text{ @ } 1 \text{ atm}$$

$$\Delta \tilde{H}_{\text{lv}}(T_b) = 30763,4 \frac{\text{KJ}}{\text{kmol}}$$

$$\begin{aligned}
& - F_{\text{C}_6\text{H}_6, 1} \cdot \left[ a_{\text{C}_6\text{H}_6(l)} \cdot (T_b - T_1) + b_{\text{C}_6\text{H}_6(l)} \cdot \frac{(T_b^2 - T_1^2)}{2} + \right. \\
& + c_{\text{C}_6\text{H}_6(l)} \cdot \frac{(T_b^3 - T_1^3)}{3} + d_{\text{C}_6\text{H}_6(l)} \cdot \frac{(T_b^4 - T_1^4)}{4} + \Delta \tilde{H}_{\text{LV}, \text{C}_6\text{H}_6}(T_b) + \\
& + a_{\text{C}_6\text{H}_6(g)} \cdot (T_3 - T_b) + b_{\text{C}_6\text{H}_6(g)} \cdot \frac{(T_3^2 - T_b^2)}{2} + c_{\text{C}_6\text{H}_6(g)} \cdot \frac{(T_3^3 - T_b^3)}{3} + \\
& \left. + d_{\text{C}_6\text{H}_6(g)} \cdot \frac{(T_3^4 - T_b^4)}{4} + e_{\text{C}_6\text{H}_6(g)} \cdot \frac{(T_3^5 - T_b^5)}{5} \right] + \\
& + \left( \sum F_{\lambda, 2} \cdot a_{\lambda}(g) \right) \cdot (T_2 - T_3) + \left( \sum F_{\lambda, 2} \cdot b_{\lambda}(g) \right) \cdot \frac{(T_2^2 - T_3^2)}{2} + \\
& + \left( \sum F_{\lambda, 2} \cdot c_{\lambda}(g) \right) \cdot \frac{(T_2^3 - T_3^3)}{3} + \left( \sum F_{\lambda, 2} \cdot d_{\lambda}(g) \right) \cdot \frac{(T_2^4 - T_3^4)}{4} + \\
& + \left( \sum F_{\lambda, 2} \cdot e_{\lambda}(g) \right) \cdot \frac{(T_2^5 - T_3^5)}{5} = 0
\end{aligned}$$

$$\tilde{C}_{p,\Delta}(g) = a_{\Delta} + b_{\Delta}T + c_{\Delta}T^2 + d_{\Delta}T^3 + e_{\Delta}T^4 \quad (\text{tab. 3})$$

$\Delta$	$a_{\Delta}$	$b_{\Delta}$	$c_{\Delta}$	$d_{\Delta}$	$e_{\Delta}$
$C_6H_6$	18,5868	$-1,17439 \cdot 10^{-2}$	$1,27514 \cdot 10^{-3}$	$-2,07984 \cdot 10^{-6}$	$1,05329 \cdot 10^{-9}$
$C_6H_5CH_3$	31,8200	$-1,61654 \cdot 10^{-2}$	$1,44465 \cdot 10^{-3}$	$-2,28948 \cdot 10^{-6}$	$1,13573 \cdot 10^{-9}$
$CH_4$	38,3870	$-7,36639 \cdot 10^{-2}$	$2,90981 \cdot 10^{-4}$	$-2,63849 \cdot 10^{-7}$	$8,00679 \cdot 10^{-11}$
$H_2$	17,6386	$6,70055 \cdot 10^{-2}$	$-1,31485 \cdot 10^{-4}$	$1,25883 \cdot 10^{-7}$	$-2,91803 \cdot 10^{-11}$

$$\tilde{C}_{p,C_6H_6}(l) = -7,27329 + 7,70541 \cdot 10^{-4}T - 1,64818 \cdot 10^{-3}T^2 + 1,89794 \cdot 10^{-6}T^3$$

(tab. 6, p. 657)

Novas equações:  $\tilde{C}_{p,\Delta}$  (KJ/kmol.K)  
T (K)

$$F_{C_6H_6,2} = 0,4 \cdot 1000 = 400 \text{ kmol/h}$$

$$F_{C_6H_5CH_3,2} = 0,3 \cdot 1000 = 300 \text{ kmol/h}$$

$$F_{CH_4,2} = 0,1 \cdot 1000 = 100 \text{ kmol/h}$$

$$F_{H_2,2} = 0,2 \cdot 1000 = 200 \text{ kmol/h}$$

$$\sum F_{\Delta,2} \cdot a_{\Delta} = 2,434714 \cdot 10^4$$

$$\sum F_{\Delta,2} \cdot b_{\Delta} = -3,51247$$

$$\sum F_{\Delta,2} \cdot c_{\Delta} = 0,94625$$

$$\sum F_{\Delta,2} \cdot d_{\Delta} = -1,524 \cdot 10^{-3}$$

$$\sum F_{\Delta,2} \cdot e_{\Delta} = 7,6421 \cdot 10^{-7}$$

$$\begin{aligned}
& - F_{C_6H_6,1} \left[ -7,27329 \cdot (353,3 - 299) + 7,70541 \cdot 10^{-4} \cdot \frac{(353,3^2 - 299^2)}{2} + \right. \\
& - 1,64818 \cdot 10^{-3} \cdot \frac{(353,3^3 - 299^3)}{3} + 1,89794 \cdot 10^{-6} \cdot \frac{(353,3^4 - 299^4)}{4} + \\
& + 30763,4 + 18,9868 \cdot (473 - 353,3) - 1,17439 \cdot 10^{-2} \cdot \frac{(473^2 - 353,3^2)}{2} + \\
& \left. + 1,27519 \cdot 10^{-3} \cdot \frac{(473^3 - 353,3^3)}{3} - 2,07984 \cdot 10^{-6} \cdot \frac{(473^4 - 353,3^4)}{4} + 1,05929 \cdot 10^{-3} \cdot \frac{(473^5 - 353,3^5)}{5} \right] \\
& + (2,439714 \cdot 10^4) \cdot (673 - 473) + (-3,71247) \cdot \frac{(673^2 - 473^2)}{2} + \\
& + (0,94625) \cdot \frac{(673^3 - 473^3)}{3} + (-1,529 \cdot 10^9) \cdot \frac{(673^4 - 473^4)}{4} + \\
& + (7,6921 \cdot 10^{-7}) \cdot \frac{(673^5 - 473^5)}{5} = 0
\end{aligned}$$

$$\begin{aligned}
& \swarrow \text{Kcal/h} \qquad \qquad \qquad \nwarrow \text{KJ/Kcal} \\
& - F_{C_6H_6,1} \left[ 8065,35 + 30763,4 + 13782,51 \right] + \\
& + 25627764 = 0 \\
& \qquad \qquad \qquad \swarrow \text{KJ/h}
\end{aligned}$$

$$F_{C_6H_6,1} = \frac{25627764}{52609,08} \cong 487,1 \text{ kcal/h} = F_1$$

c) Como não há reações químicas, o balanço molar total fica:

$$F_1 + F_2 - F_3 = 0$$

$$487,1 + 1000 - F_3 = 0 \rightarrow F_3 = 1487,1 \text{ kmol/h}$$

BM  $C_6H_6$ :  $F_{C_6H_6,1} + F_{C_6H_6,2} - F_{C_6H_6,3} = 0$

$$487,1 + 400 - F_{C_6H_6,3} = 0$$

$$F_{C_6H_6,3} = 887,1 \text{ kmol/h}$$

BM  $C_6H_5CH_3$ :  $F_{C_6H_5CH_3,2} - F_{C_6H_5CH_3,3} = 0$

$$300 - F_{C_6H_5CH_3,3} = 0$$

$$F_{C_6H_5CH_3,3} = 300 \text{ kmol/h}$$

De modo análogo:  $F_{CH_4,3} = 100 \text{ kmol/h}$

$$F_{H_2,3} = 200 \text{ kmol/h}$$

Composição molar da corrente 3:

$$y_{C_6H_6,3} = \frac{887,1}{1487,1} = 0,5965 \quad (\sim 59,7\%)$$

$$y_{C_6H_5CH_3,3} = \frac{300}{1487,1} = 0,2017 \quad (\sim 20,2\%)$$

$$y_{CH_4,3} = \frac{100}{1487,1} = 0,0673 \quad (\sim 6,7\%)$$

$$y_{H_2,3} = \frac{200}{1487,1} = 0,1345 \quad (\sim 13,5\%)$$