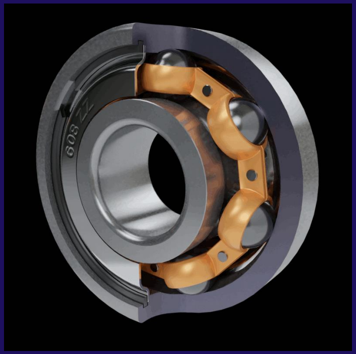
ESCOLA POLITÉCNICA DA UNIVERSIDADE DE SÃO PAULO

Elementos de Máquinas para Automação

PMR 3320 – A14

Mancais de elementos rolantes

2023.2

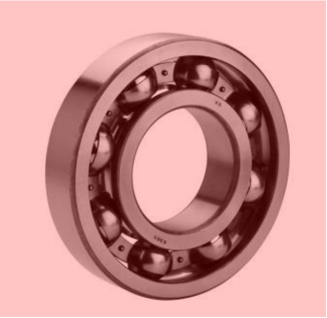


Mancais

classificação

- Escorregamento

- Rolamento



- Fluídicos
  - Hidrodinâmicos

  - Hidrostáticos

- Magnéticos

Mancais de rolamento

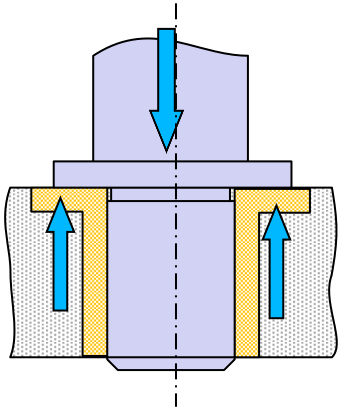
Exemplos

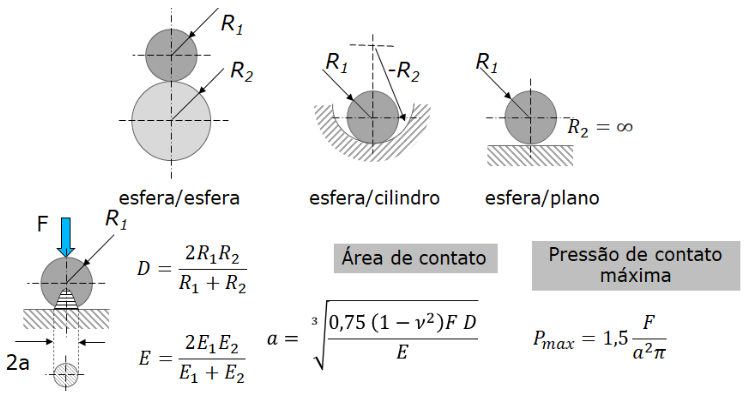
http://cento-kullager.se/om/

Introdução

Mancais de escorregamento

- Mecânica dos sólidos
- Contatos de Hertz
- Curva de Stribeck





$$D = \frac{2R_1R_2}{R_1+R_2}$$

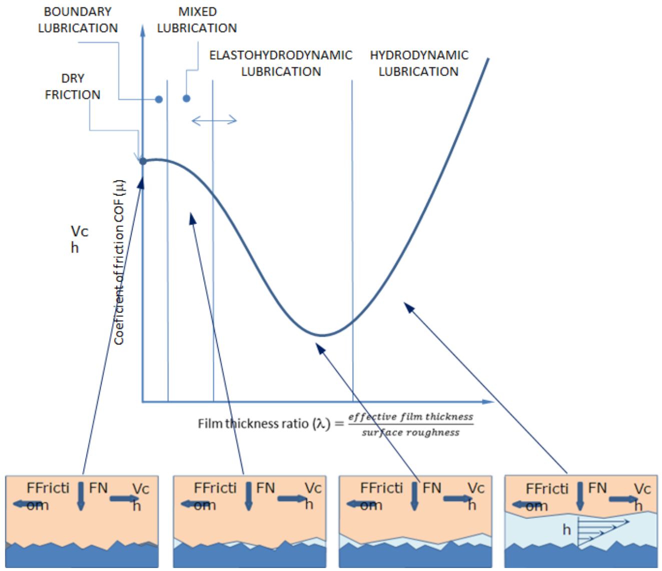
$$E = \frac{2E_1E_2}{E_1+E_2}$$

Área de contato

$$a = \sqrt[3]{\frac{0{,}75\,(1-\nu^2)F\,D}{E}}$$

Pressão de contato máxima

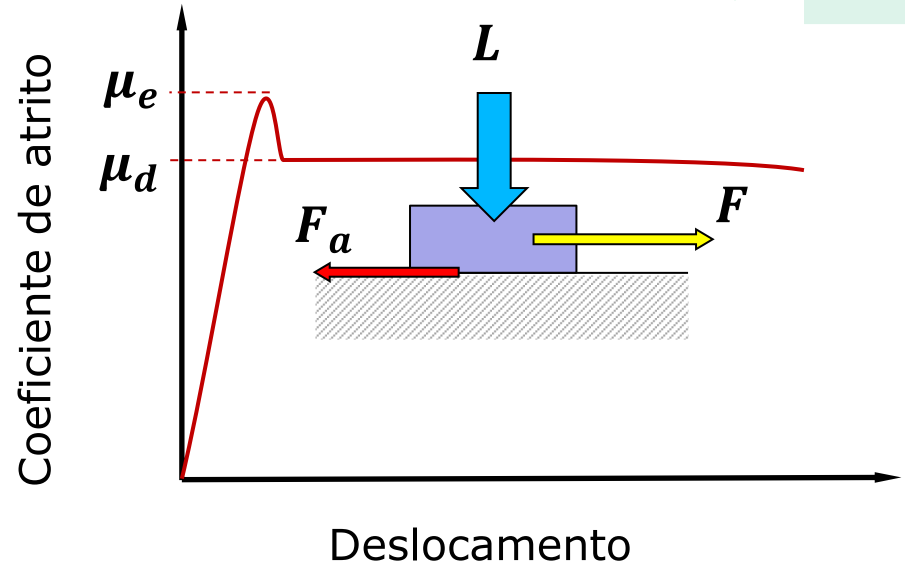
$$P_{max} = 1{,}5\,\frac{F}{a^2\pi}$$

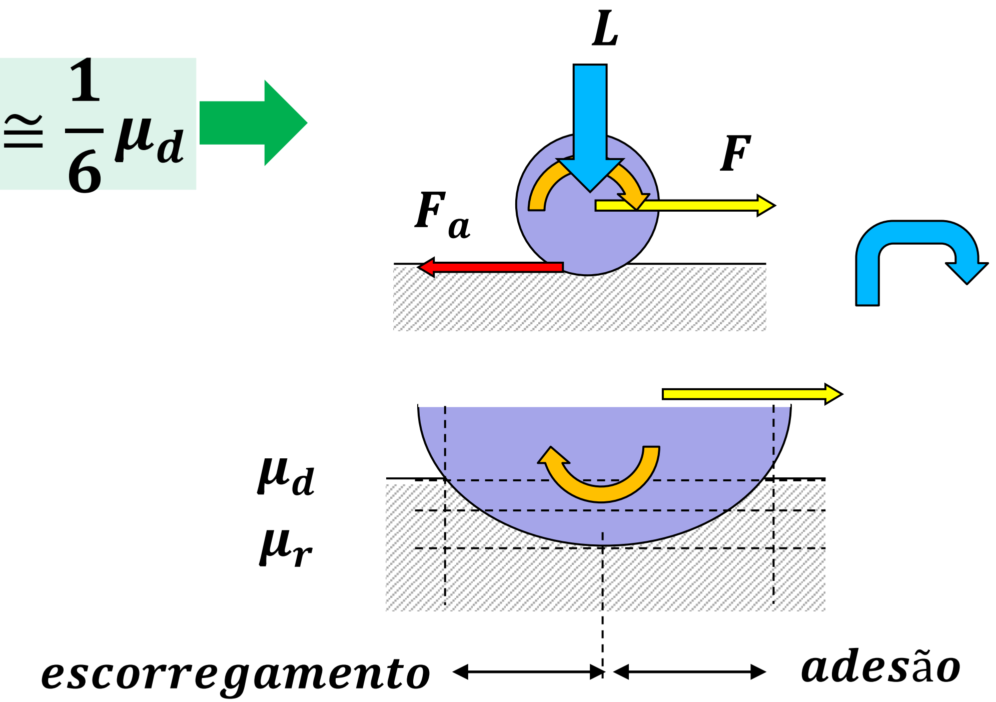


Introdução

- Atrito
  - Atrito de escorregamento
  - Atrito de rolamento

$$\mu_r \cong \frac{1}{6}\mu_d$$





Mancais de rolamento

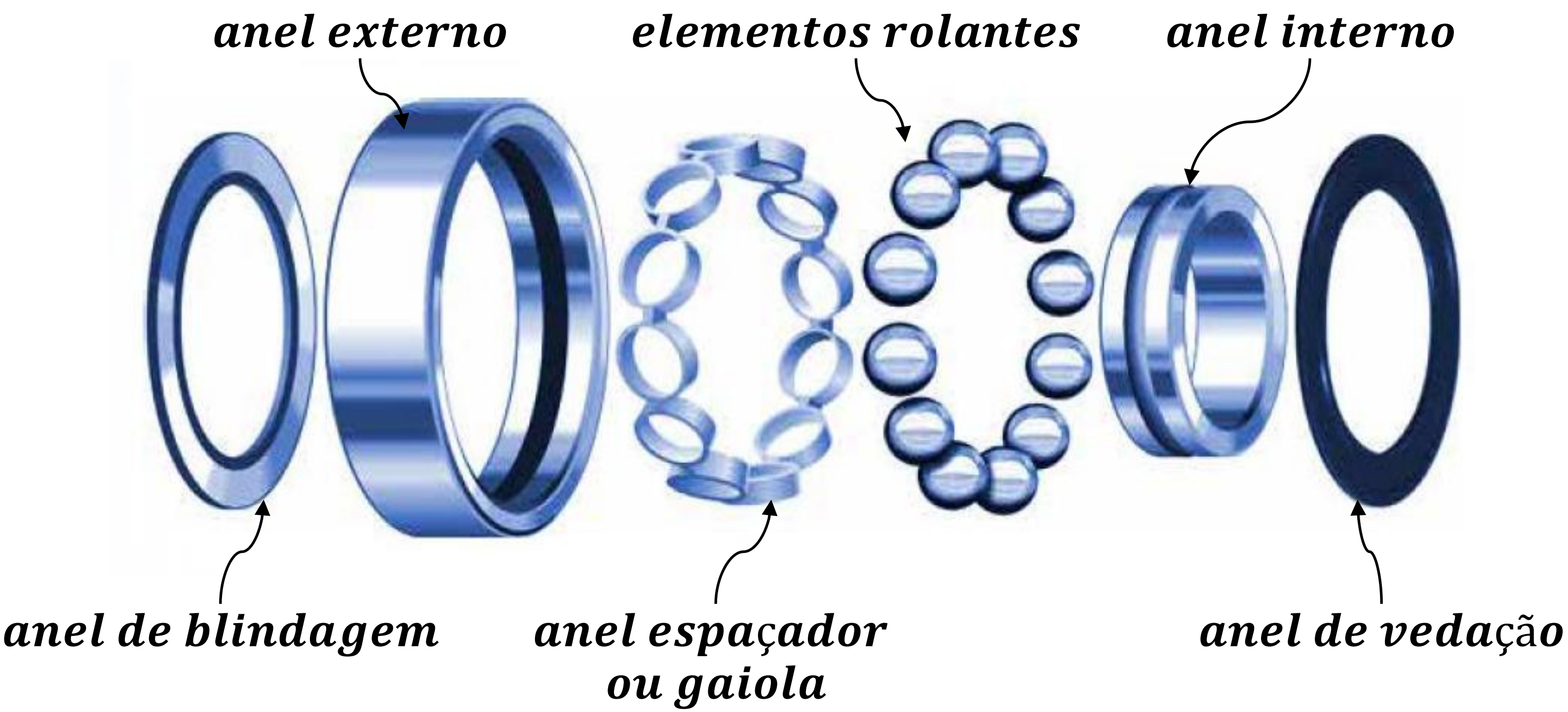
Introdução

São os tipos de mancais mais utilizados, e são caracterizados por:

- Fácil movimentação
- Baixo atrito
- Elevado nível de padronização
- Baixo custo relativo

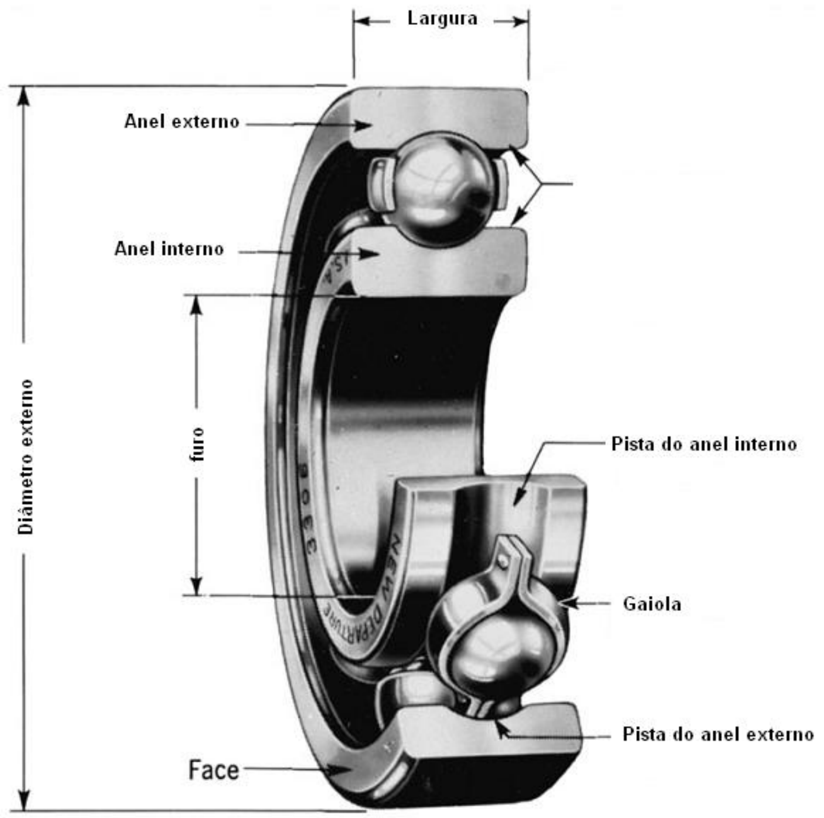
Mancais de rolamento

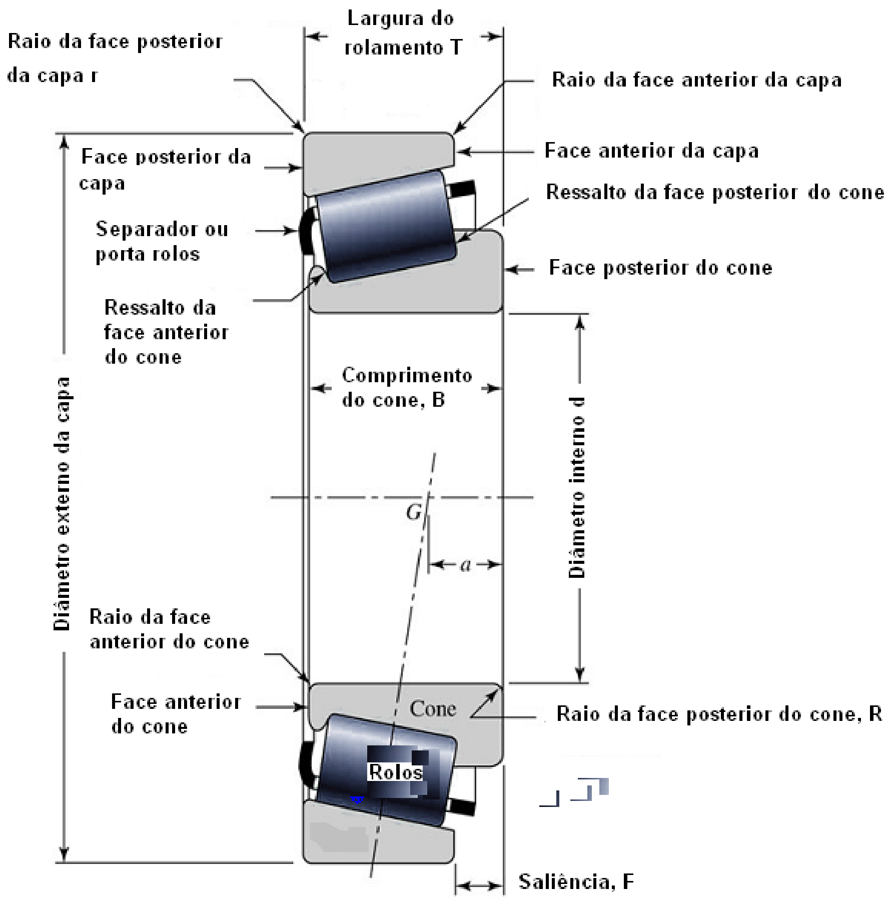
Constituintes



Mancais de rolamento

Nomenclatura

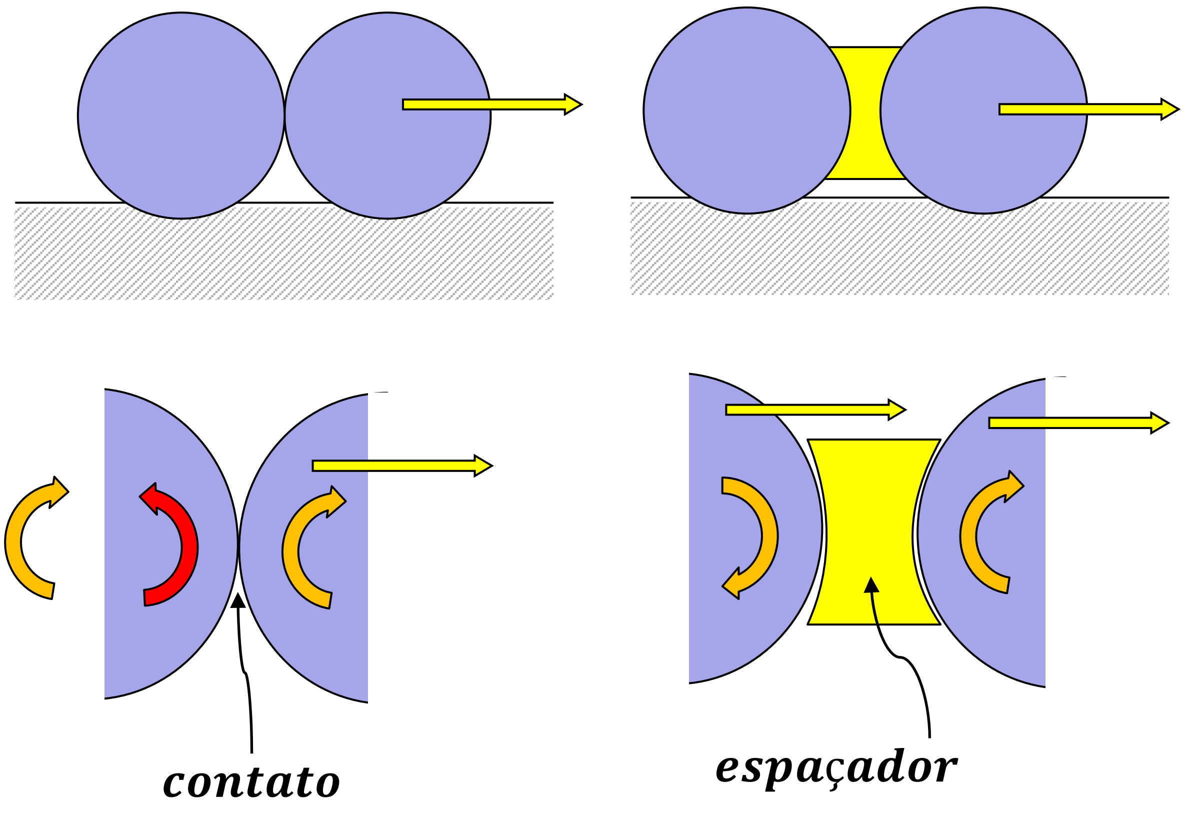




Mancais de rolamento

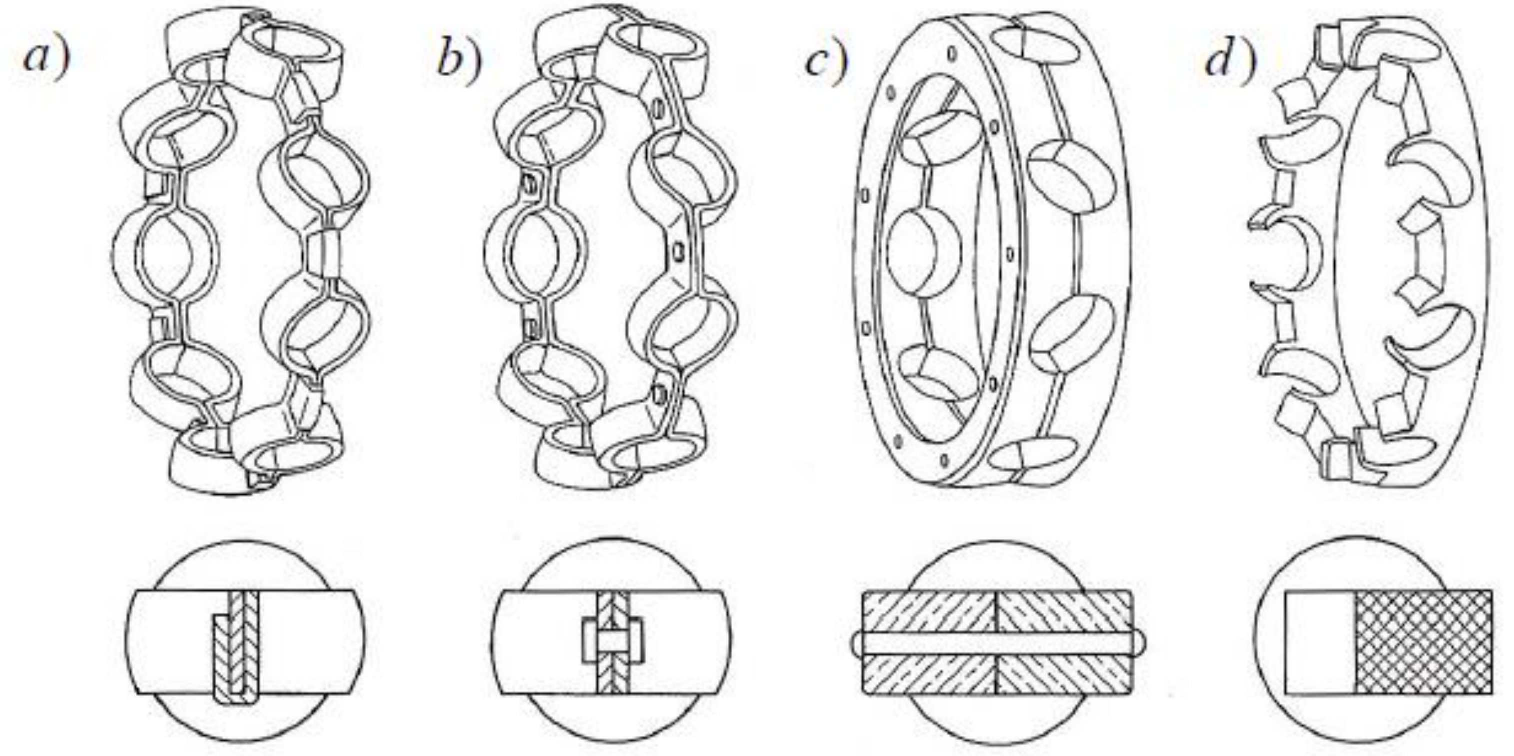
Espaçador

anel espaçador ou gaiola



Mancais de rolamento

Espaçador



gaiola costurada

gaiola rebitada

gaiola maciça

gaiola injetada

Mancais de rolamento

Carregamentos

Radiais

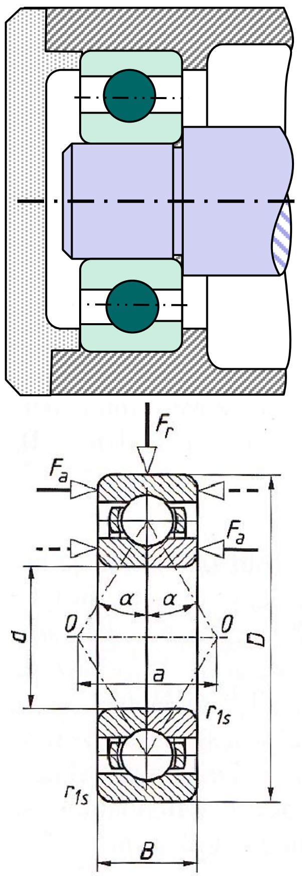
Radiais/Axiais

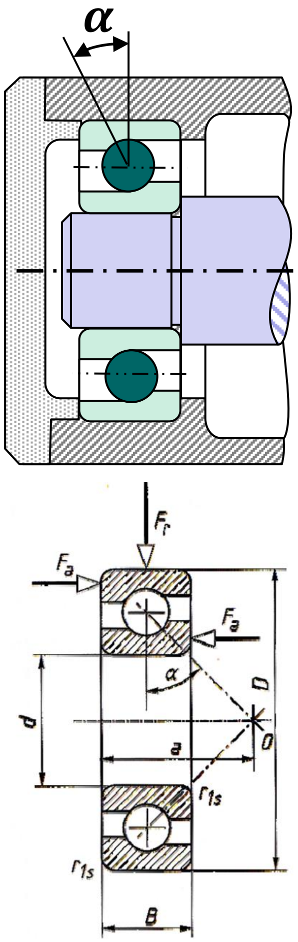
Axiais

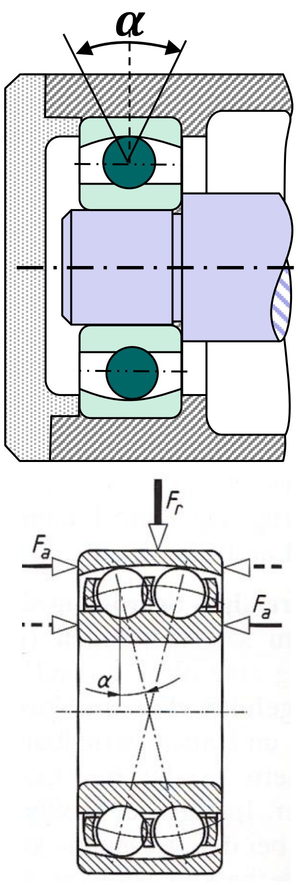
Mancais de rolamento

Radiais de esfera

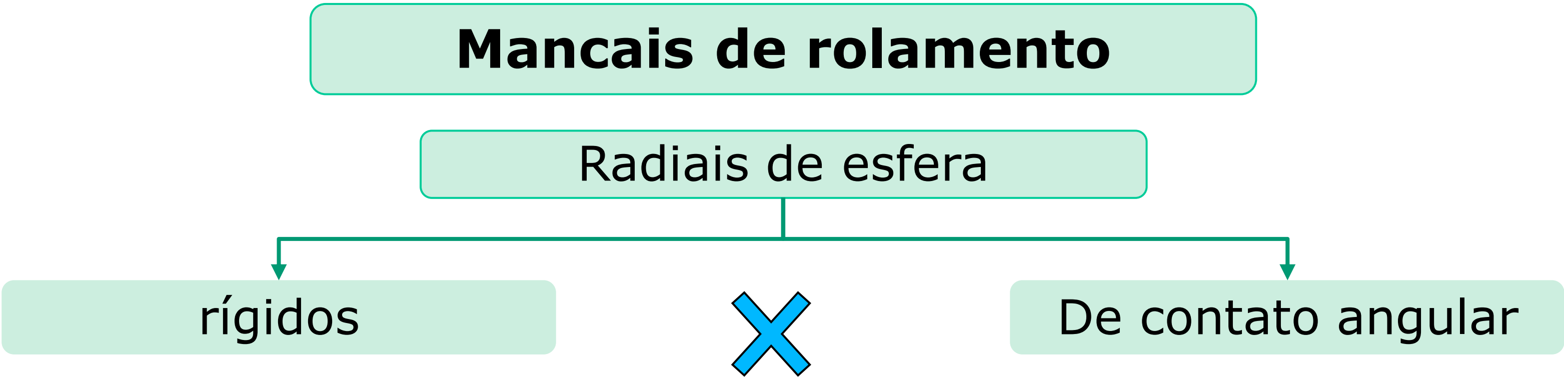
- rígidos
- De contato angular
- autocompensadores







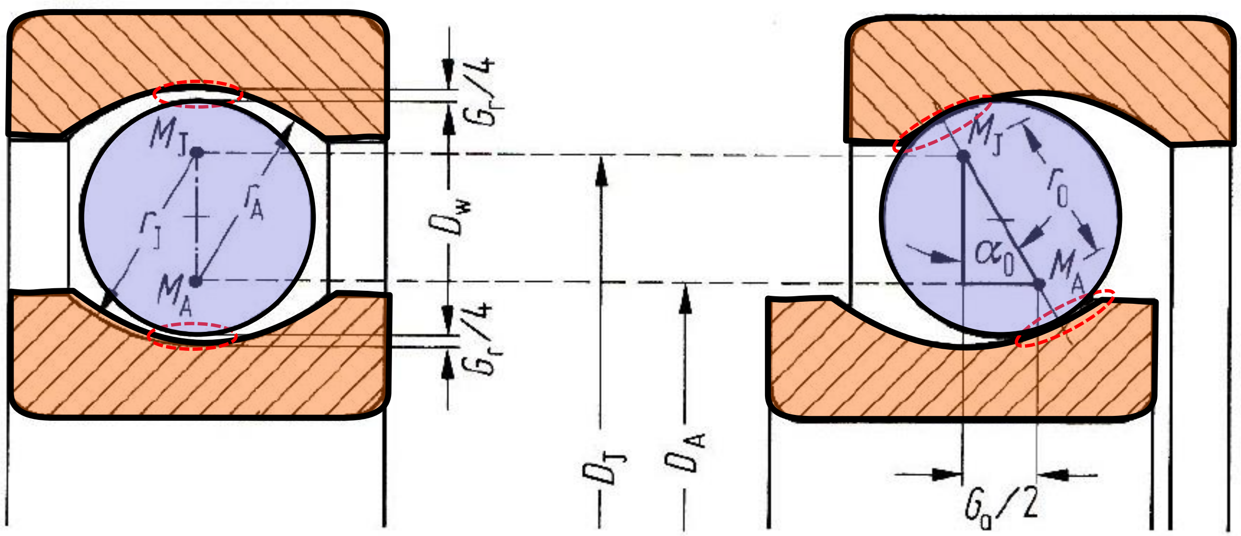
Mancais de rolamento



Radiais de esfera

rígidos

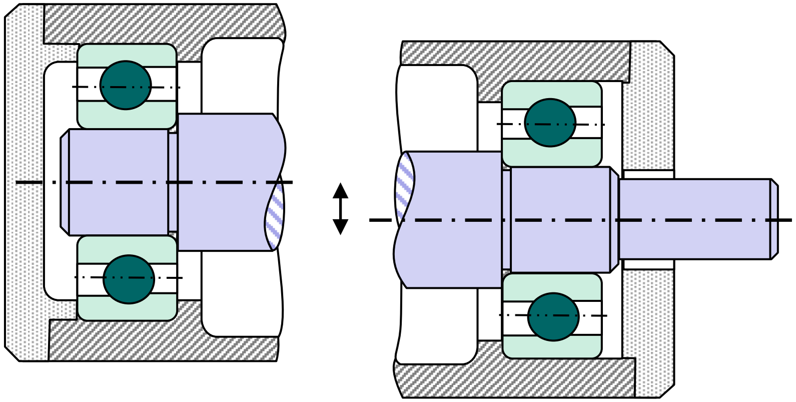
De contato angular



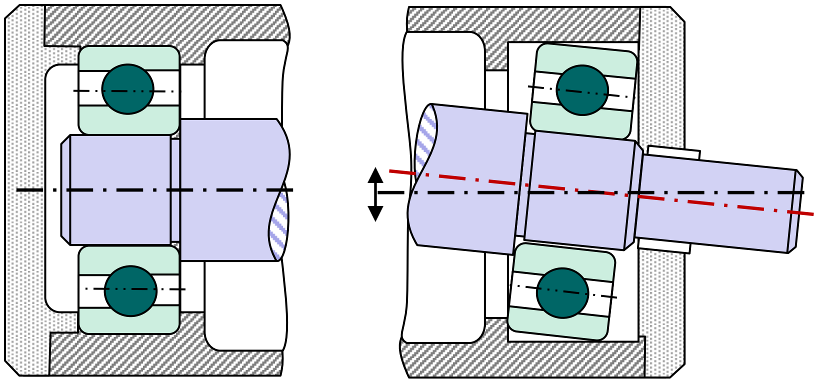
Mancais de rolamento

Quando usar mancais autocompensadores

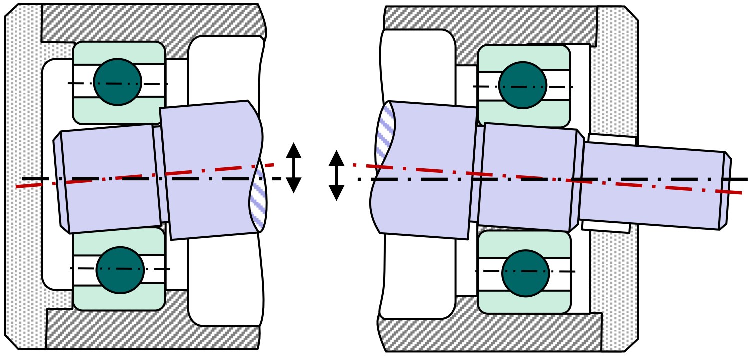
Desalinhamento



Montagem errada



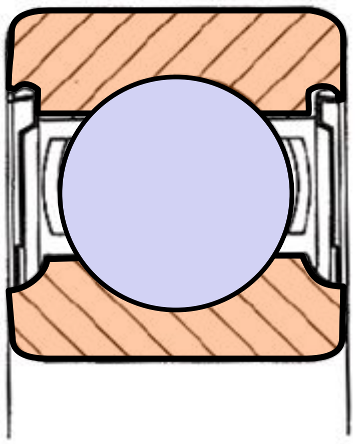
Flexão dos eixos

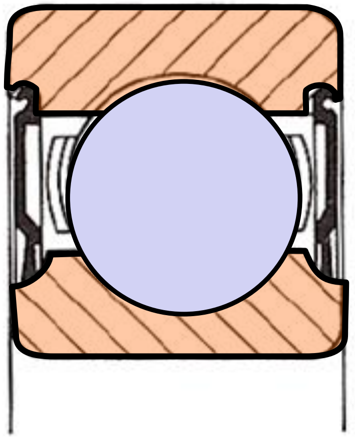


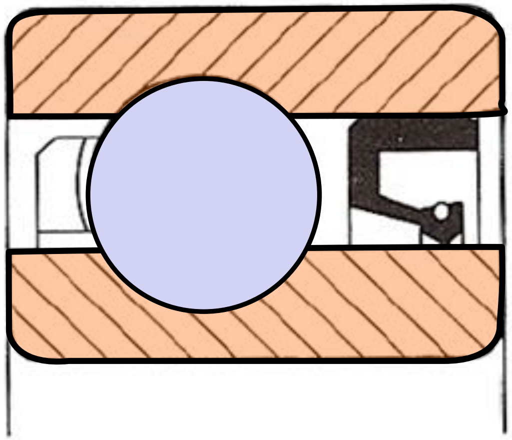
Mancais de rolamento

proteção

- vedados
- blindados
- selados

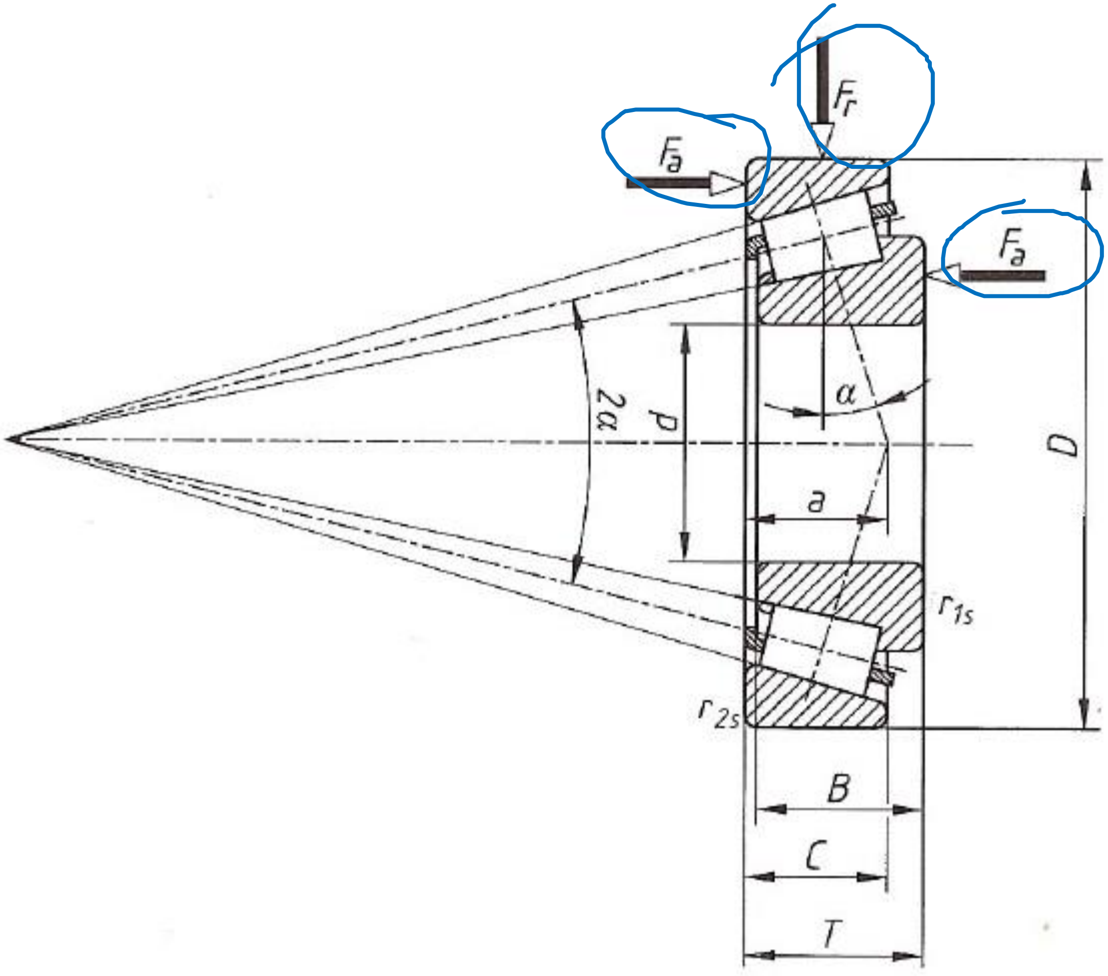






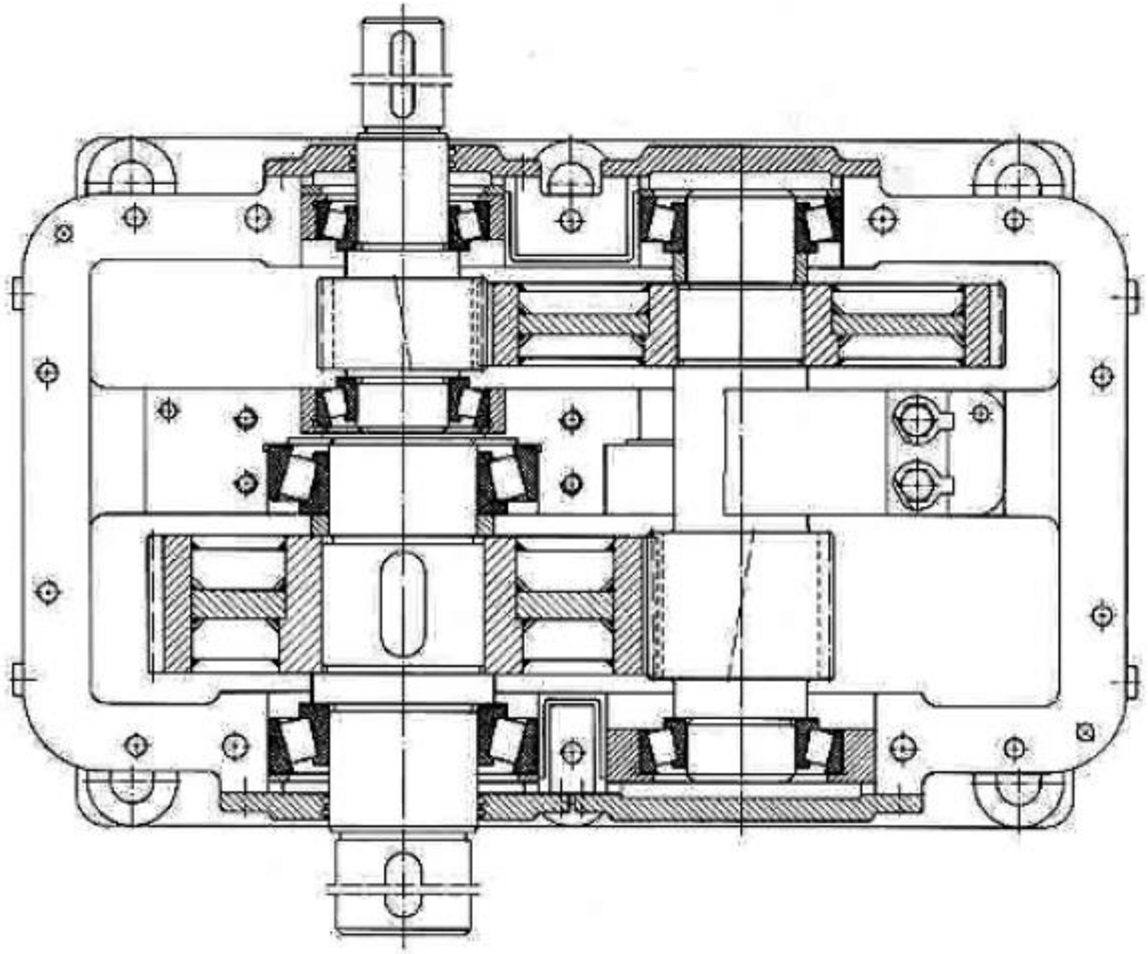
Mancais de rolamento

Rolos cônicos



Mancais de rolamento

Exemplo do uso de mancais de rolo cônicos

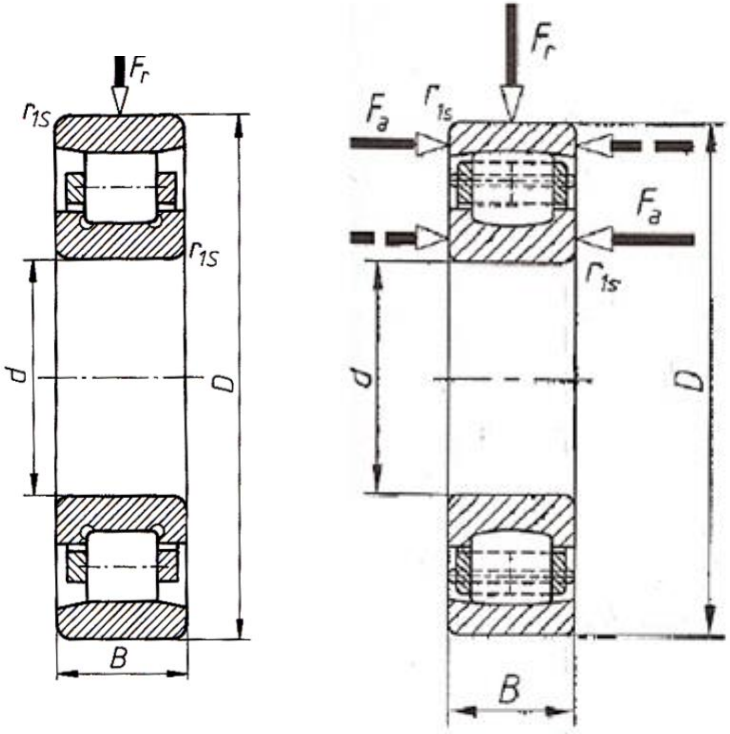


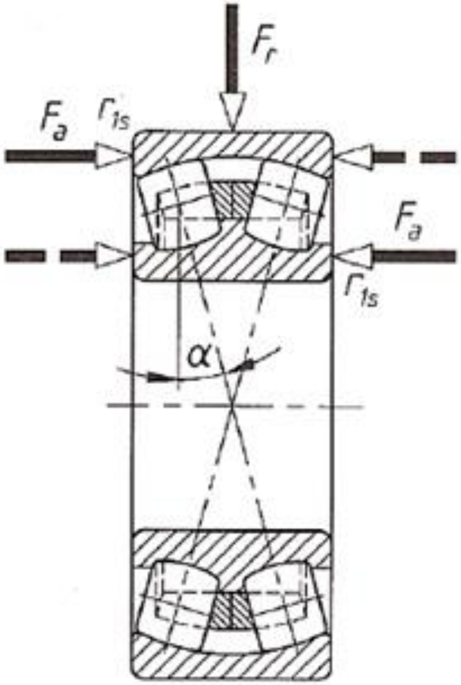
Mancais de rolamento

de rolo radiais

rígidos

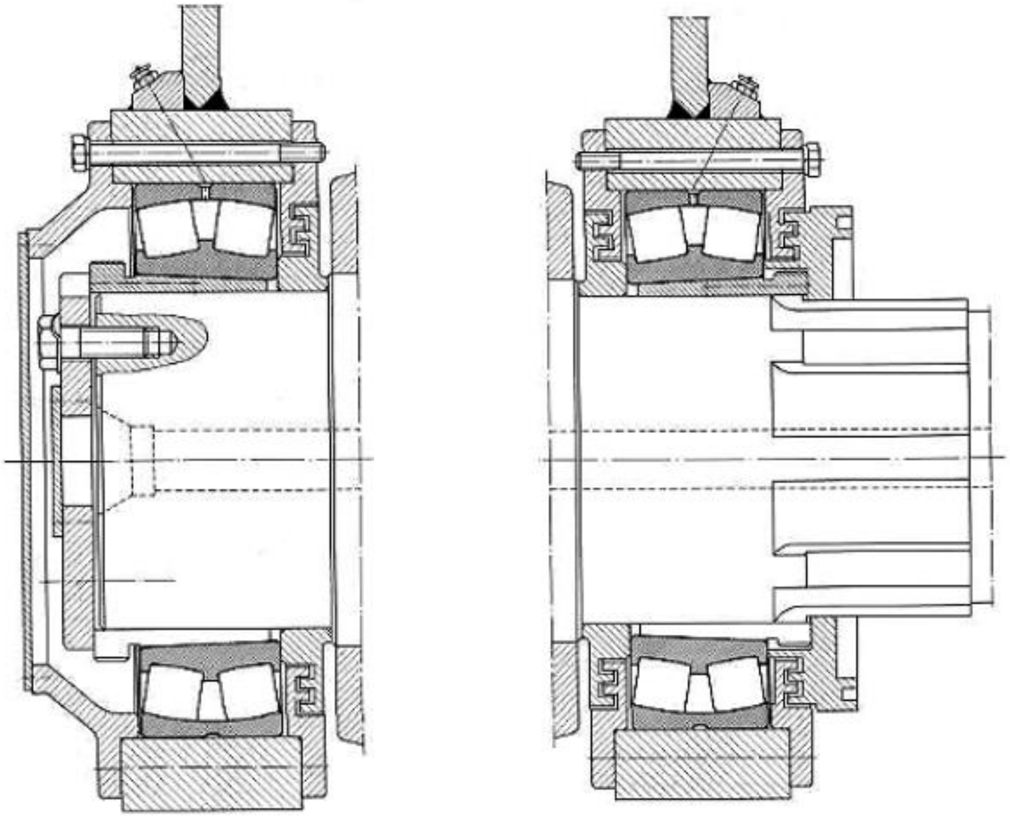
autocompensadores





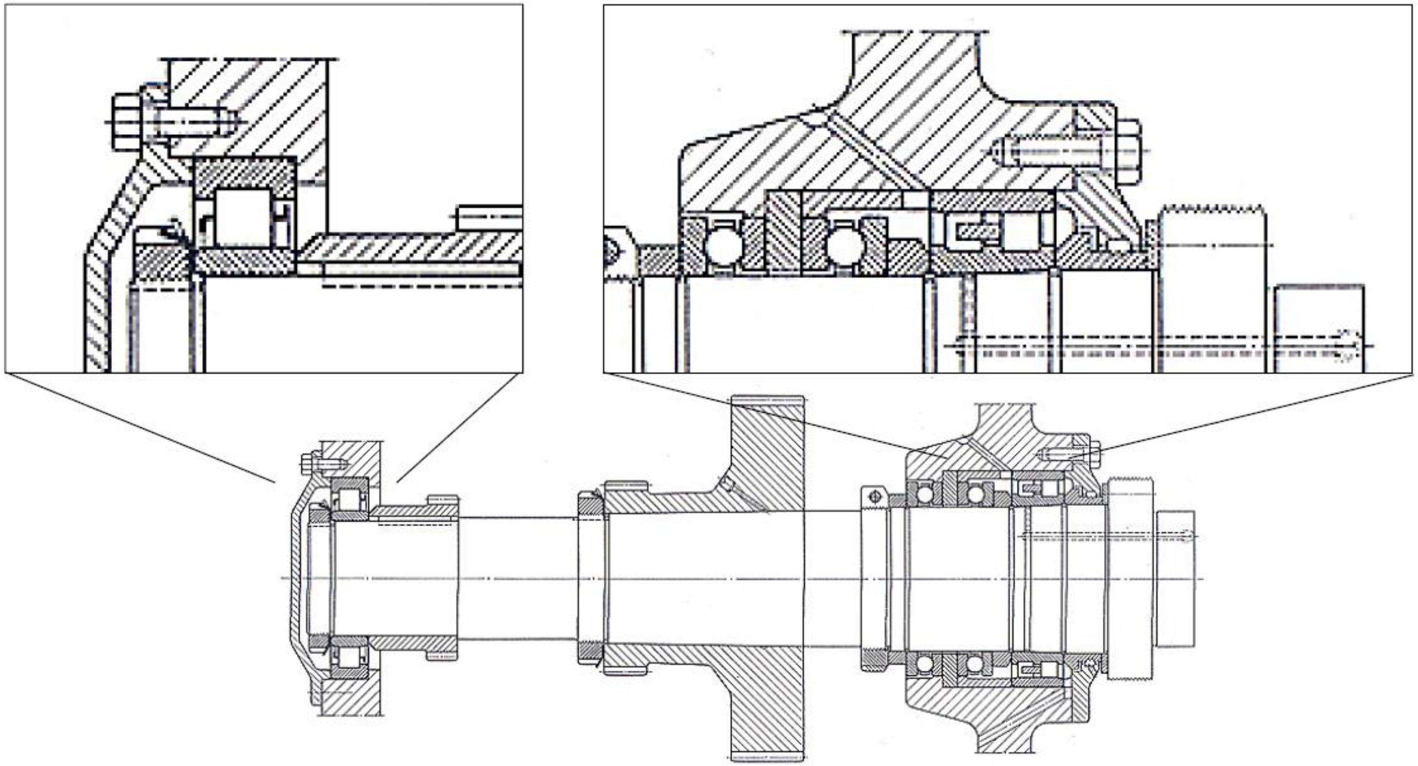
Mancais de rolamento

Exemplo do uso de mancais de rolo radiais autocompensadores



Mancais de rolamento

Exemplo do uso de mancais radiais de rolo e de esfera

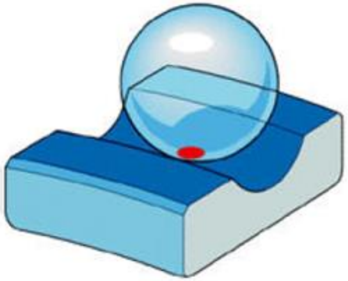


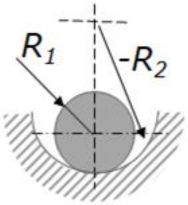
Mancais de rolamento

Classificação quanto a forma do elemento rolante

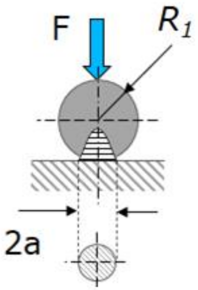
esféricos

Cilíndricos/cônicos





esfera/cilindro



$$D = \frac{2R_1R_2}{R_1 + R_2}$$

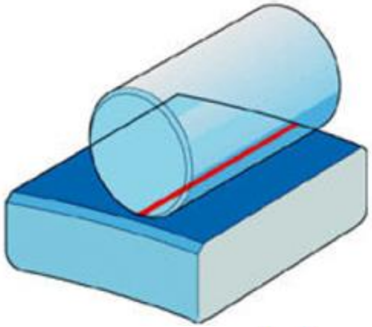
$$E = \frac{2E_1E_2}{E_1 + E_2}$$

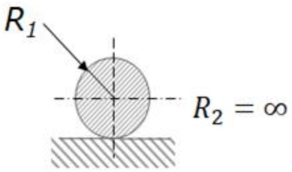
Área de contato

$$a = \sqrt[3]{\frac{0{,}75\,(1-\nu^2)F\,D}{E}}$$

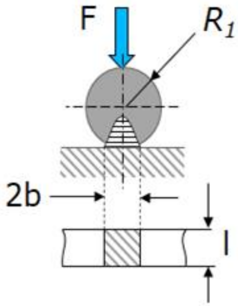
Pressão de contato máxima

$$P_{max} = 1{,}5\,\frac{F}{a^2\pi}$$





cilindro/plano



$$E = \frac{2E_1E_2}{E_1 + E_2}$$

$$D = \frac{2R_1R_2}{R_1 + R_2}$$

Área de contato

$$b = \sqrt[2]{\frac{4\,F\,D(1-\nu^2)}{\pi\,E\,l}}$$

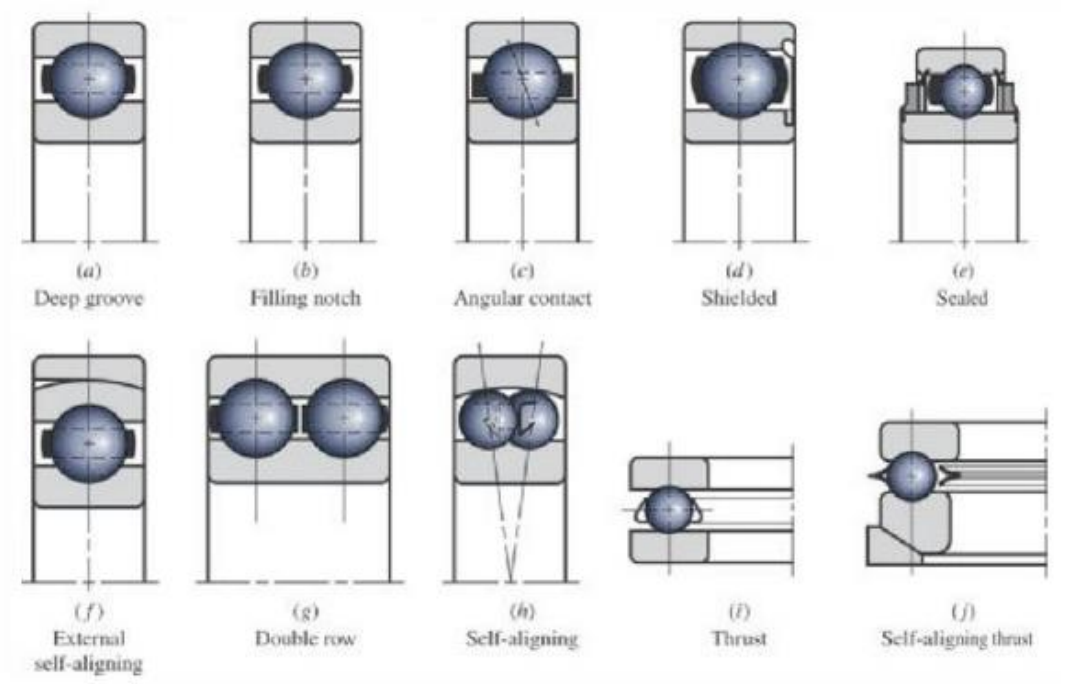
Pressão de contato máxima

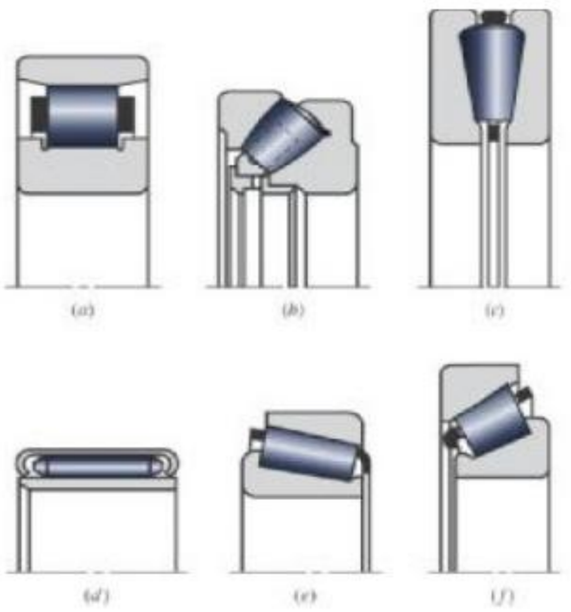
$$P_{max} = \frac{2F}{\pi\,b\,l}$$

Mancais de rolamento

Tipos de elementos rolante

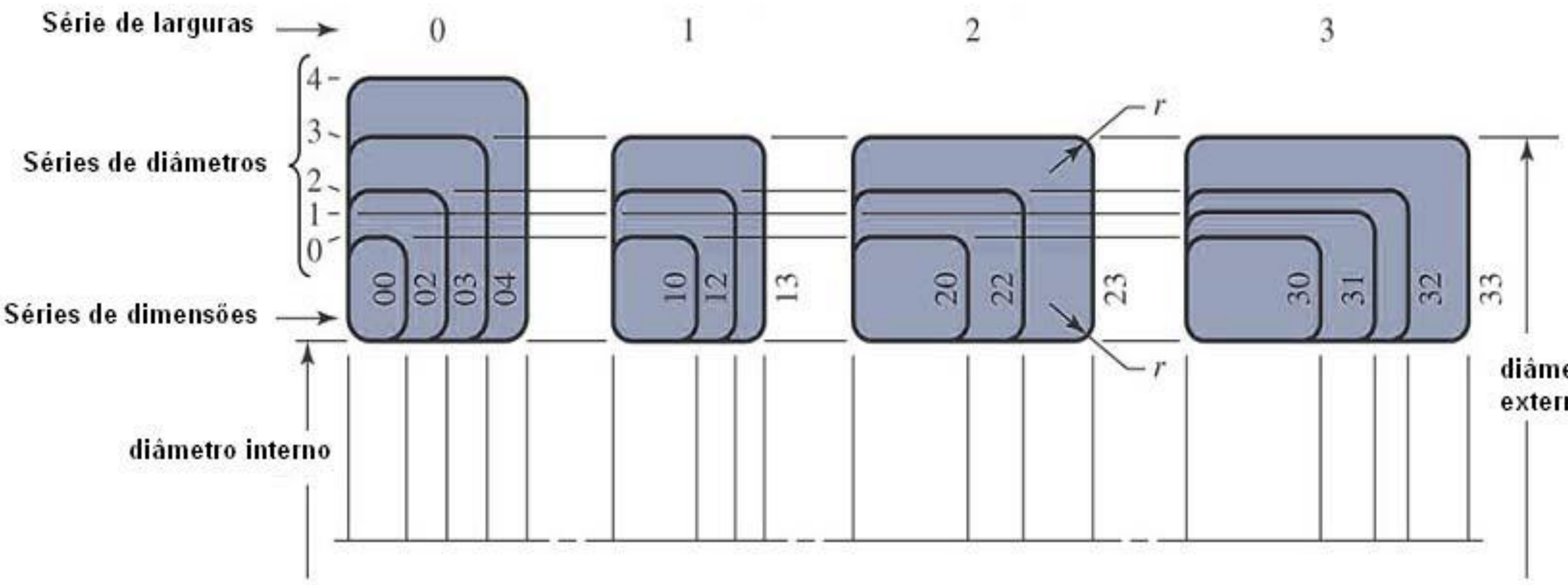
- esféricos
- Cilíndricos/cônicos





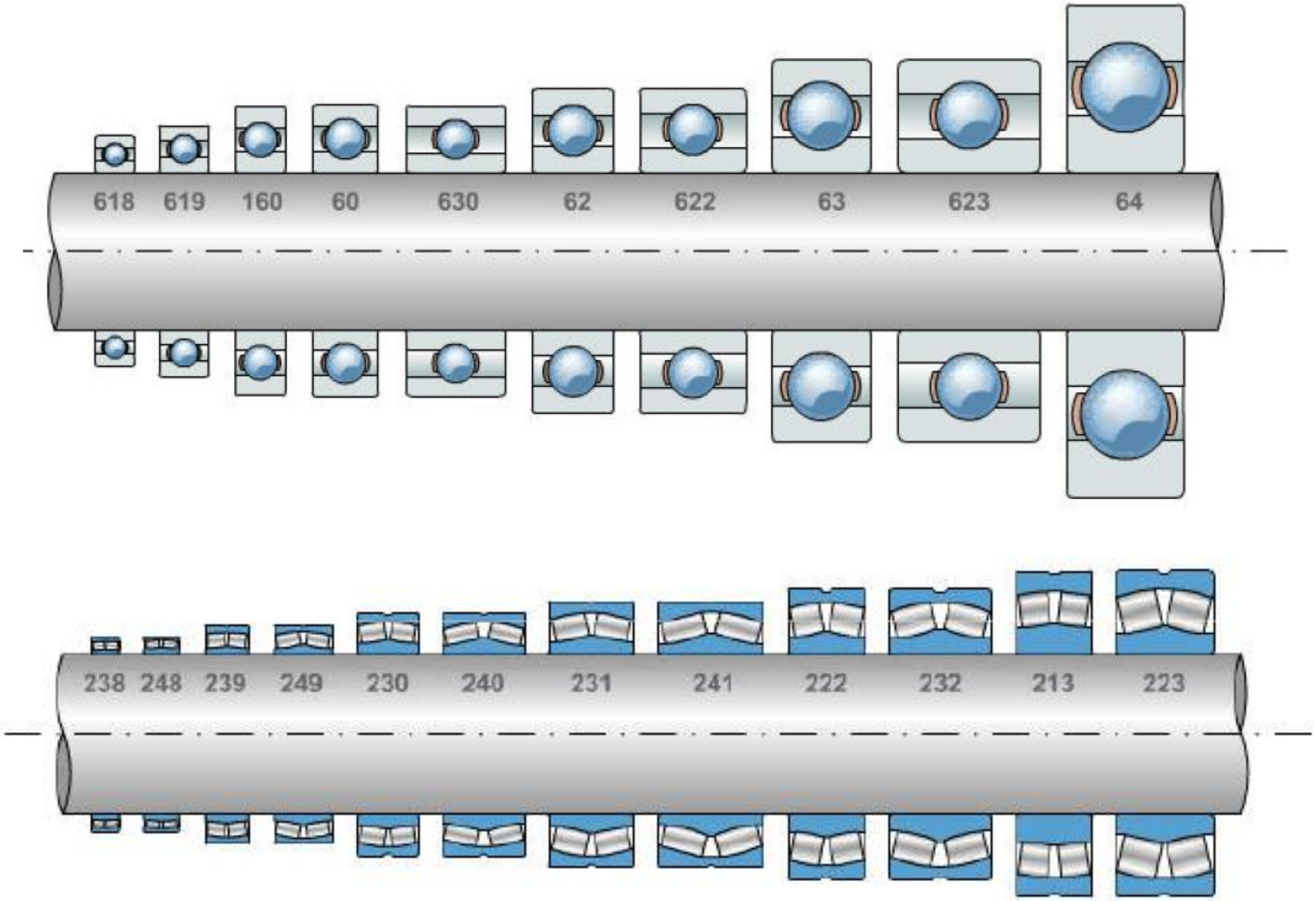
Mancais de rolamento

Classes de dimensões



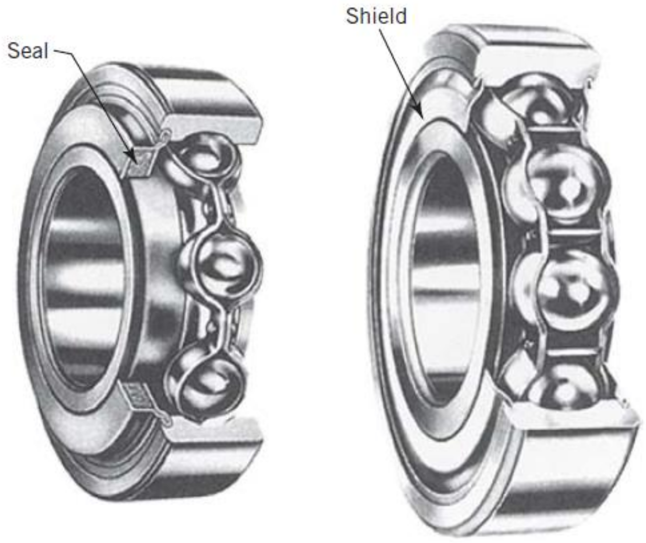
Mancais de rolamento

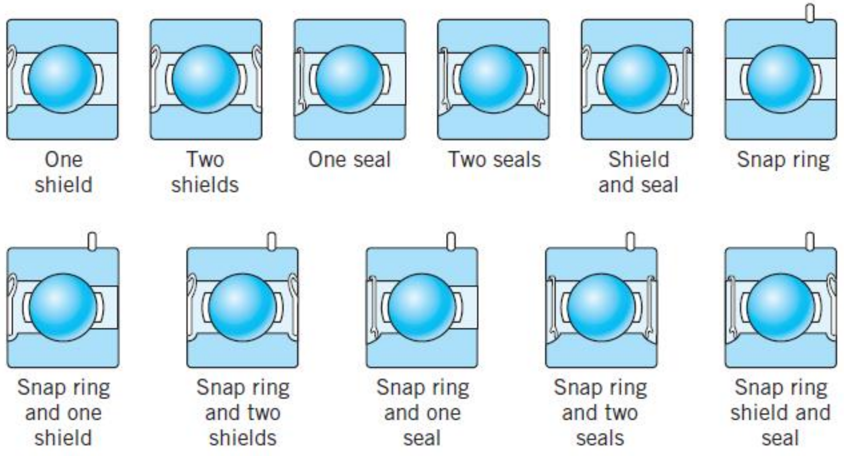
Classes de dimensões



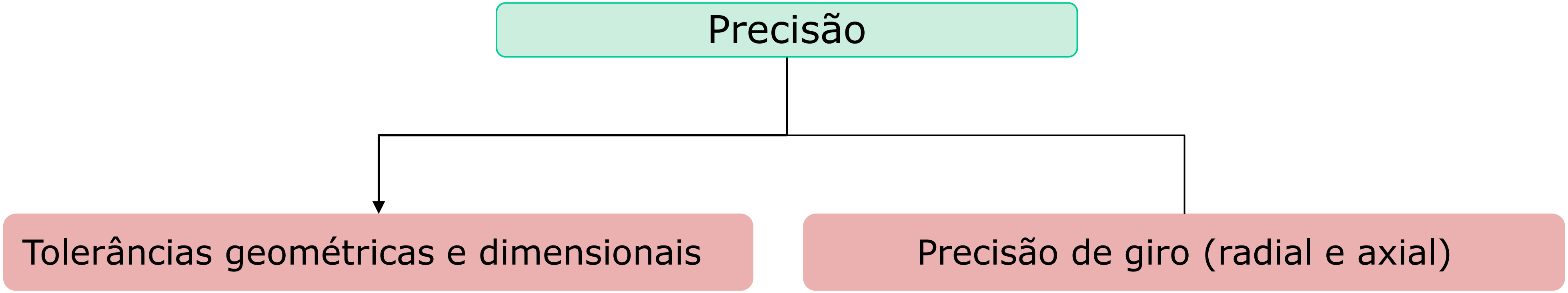
Mancais de rolamento

Classes de dimensões



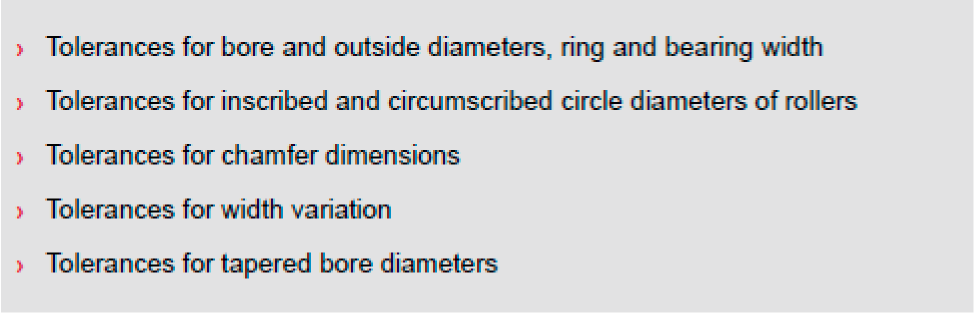


Mancais de rolamento



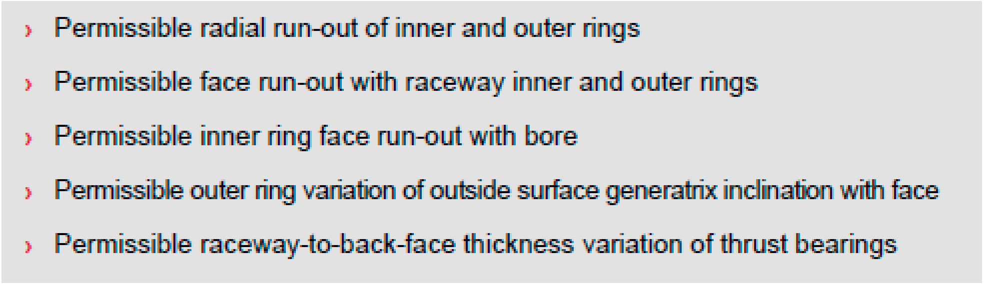
Precisão

Tolerâncias geométricas e dimensionais



- Tolerances for bore and outside diameters, ring and bearing width
- Tolerances for inscribed and circumscribed circle diameters of rollers
- Tolerances for chamfer dimensions
- Tolerances for width variation
- Tolerances for tapered bore diameters

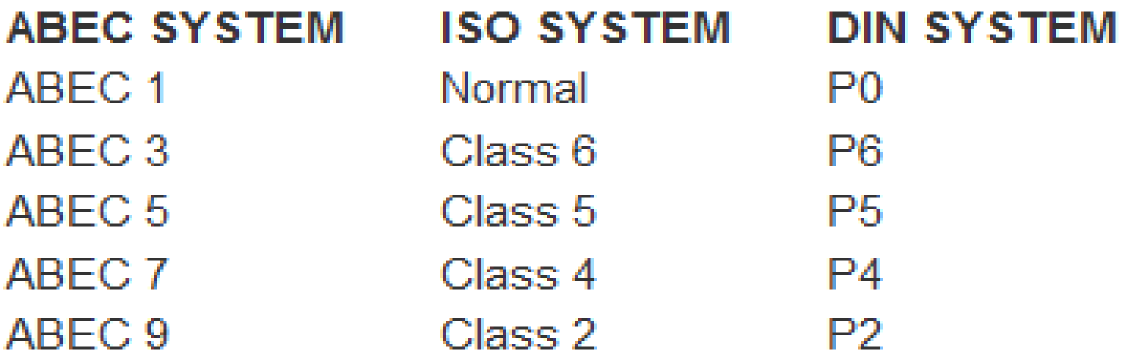
Precisão de giro (radial e axial)



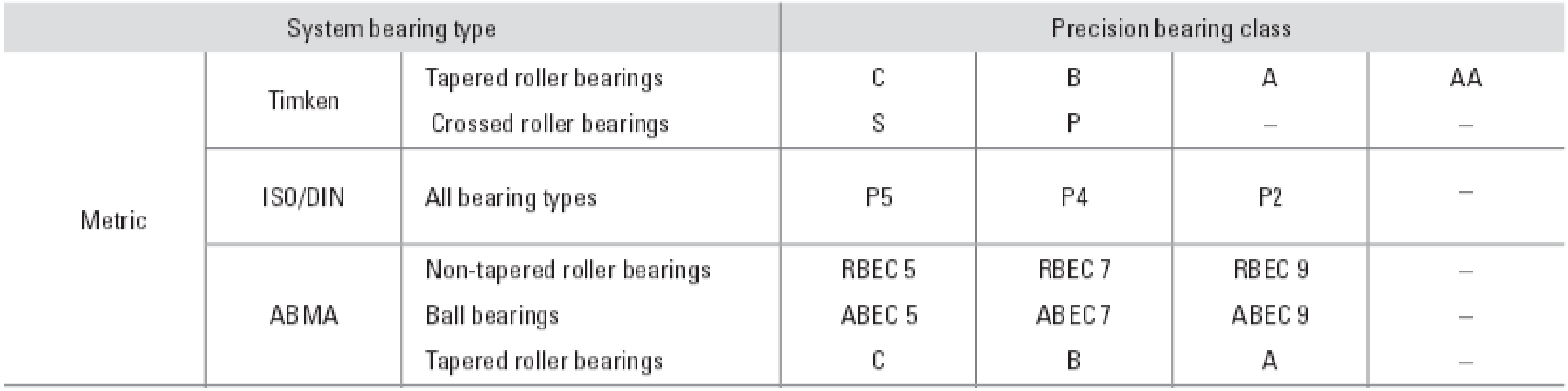
- Permissible radial run-out of inner and outer rings
- Permissible face run-out with raceway inner and outer rings
- Permissible inner ring face run-out with bore
- Permissible outer ring variation of outside surface generatrix inclination with face
- Permissible raceway-to-back-face thickness variation of thrust bearings

Mancais de rolamento

Classes de tolerâncias



ABEC SYSTEM	ISO SYSTEM	DIN SYSTEM
ABEC 1	Normal	P0
ABEC 3	Class 6	P6
ABEC 5	Class 5	P5
ABEC 7	Class 4	P4
ABEC 9	Class 2	P2

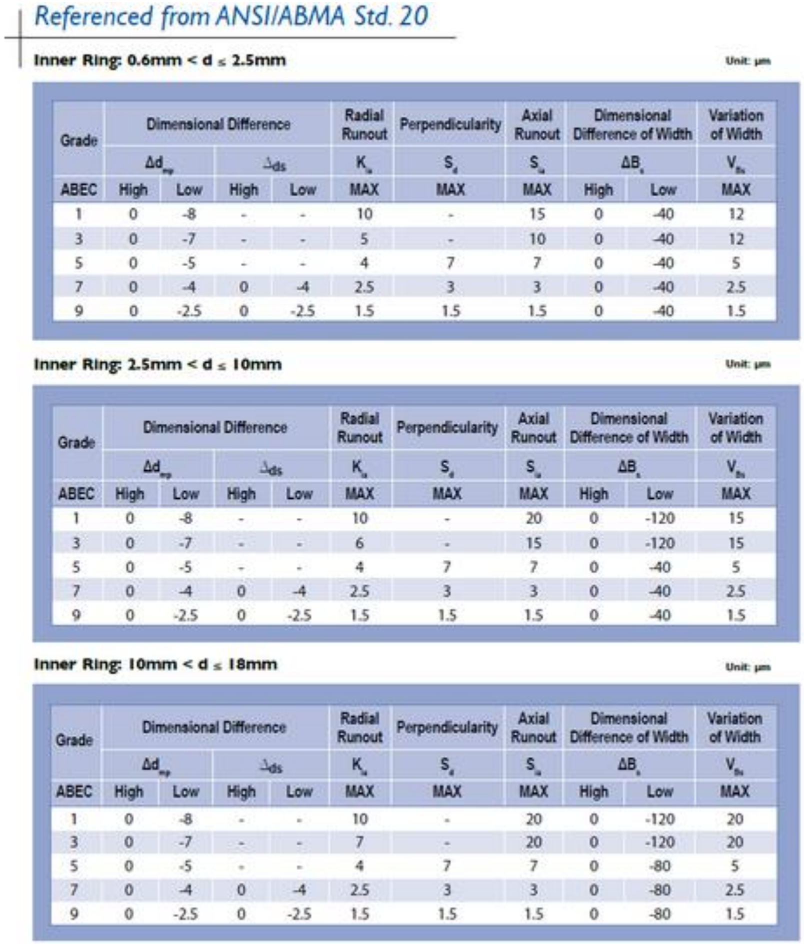


System bearing type			Precision bearing class			
Metric	Timken	Tapered roller bearings	C	B	A	AA
		Crossed roller bearings	S	P	–	–
	ISO/DIN	All bearing types	P5	P4	P2	–
	ABMA	Non-tapered roller bearings	RBEC 5	RBEC 7	RBEC 9	–
		Ball bearings	ABEC 5	ABEC 7	ABEC 9	–
		Tapered roller bearings	C	B	A	–

http://www.timken.com/pt-br/products/Documents/Super-Precision-Bearings-for-Machine-Tool-Applications-Catalog.pdf

Mancais de rolamento

Classes de tolerâncias



Referenced from ANSI/ABMA Std. 20

Inner Ring: 0.6mm < d ≤ 2.5mm Unit: µm

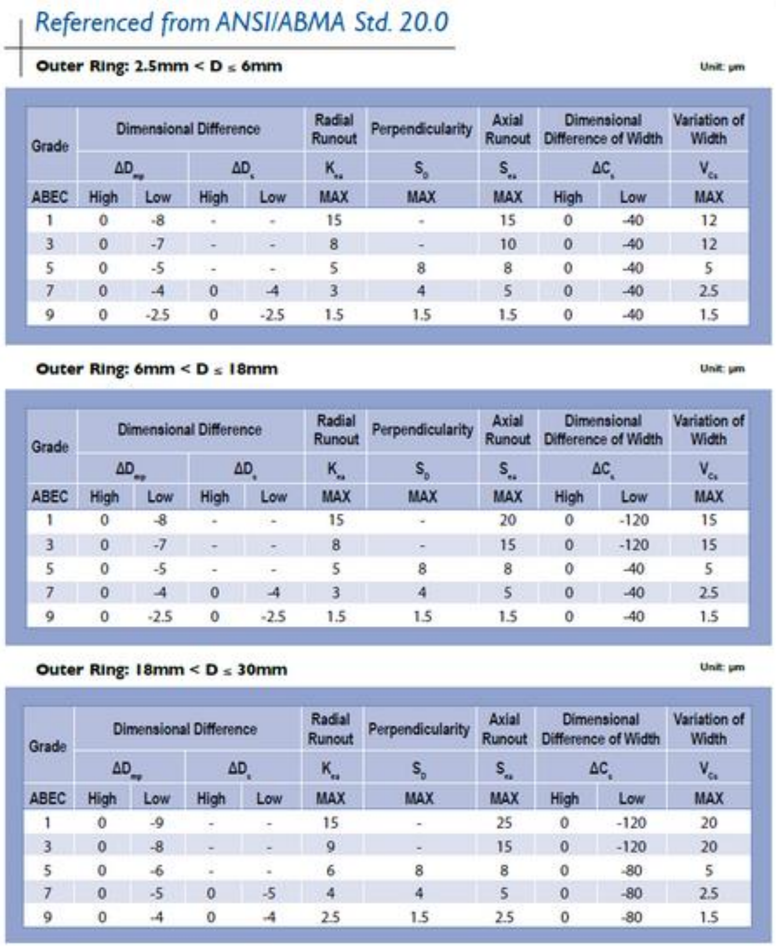
Grade	Dimensional Difference				Radial Runout	Perpendicularity	Axial Runout	Dimensional Difference of Width		Variation of Width
	Δd_{mp}		Δ_{ds}		K_{ia}	S_d	S_{ia}	ΔB_s		V_{Bs}
ABEC	High	Low	High	Low	MAX	MAX	MAX	High	Low	MAX
1	0	-8	-	-	10	-	15	0	-40	12
3	0	-7	-	-	5	-	10	0	-40	12
5	0	-5	-	-	4	7	7	0	-40	5
7	0	-4	0	-4	2.5	3	3	0	-40	2.5
9	0	-2.5	0	-2.5	1.5	1.5	1.5	0	-40	1.5

Inner Ring: 2.5mm < d ≤ 10mm Unit: µm

Grade	Dimensional Difference				Radial Runout	Perpendicularity	Axial Runout	Dimensional Difference of Width		Variation of Width
	Δd_{mp}		Δ_{ds}		K_{ia}	S_d	S_{ia}	ΔB_s		V_{Bs}
ABEC	High	Low	High	Low	MAX	MAX	MAX	High	Low	MAX
1	0	-8	-	-	10	-	20	0	-120	15
3	0	-7	-	-	6	-	15	0	-120	15
5	0	-5	-	-	4	7	7	0	-40	5
7	0	-4	0	-4	2.5	3	3	0	-40	2.5
9	0	-2.5	0	-2.5	1.5	1.5	1.5	0	-40	1.5

Inner Ring: 10mm < d ≤ 18mm Unit: µm

Grade	Dimensional Difference				Radial Runout	Perpendicularity	Axial Runout	Dimensional Difference of Width		Variation of Width
	Δd_{mp}		Δ_{ds}		K_{ia}	S_d	S_{ia}	ΔB_s		V_{Bs}
ABEC	High	Low	High	Low	MAX	MAX	MAX	High	Low	MAX
1	0	-8	-	-	10	-	20	0	-120	20
3	0	-7	-	-	7	-	20	0	-120	20
5	0	-5	-	-	4	7	7	0	-80	5
7	0	-4	0	-4	2.5	3	3	0	-80	2.5
9	0	-2.5	0	-2.5	1.5	1.5	1.5	0	-80	1.5



Referenced from ANSI/ABMA Std. 20.0

Outer Ring: 2.5mm < D ≤ 6mm Unit: µm

Grade	Dimensional Difference				Radial Runout	Perpendicularity	Axial Runout	Dimensional Difference of Width		Variation of Width
	ΔD_{mp}		ΔD_s		K_{ea}	S_D	S_{ea}	ΔC_s		V_{Cs}
ABEC	High	Low	High	Low	MAX	MAX	MAX	High	Low	MAX
1	0	-8	-	-	15	-	15	0	-40	12
3	0	-7	-	-	8	-	10	0	-40	12
5	0	-5	-	-	5	8	8	0	-40	5
7	0	-4	0	-4	3	4	5	0	-40	2.5
9	0	-2.5	0	-2.5	1.5	1.5	1.5	0	-40	1.5

Outer Ring: 6mm < D ≤ 18mm Unit: µm

Grade	Dimensional Difference				Radial Runout	Perpendicularity	Axial Runout	Dimensional Difference of Width		Variation of Width
	ΔD_{mp}		ΔD_s		K_{ea}	S_D	S_{ea}	ΔC_s		V_{Cs}
ABEC	High	Low	High	Low	MAX	MAX	MAX	High	Low	MAX
1	0	-8	-	-	15	-	20	0	-120	15
3	0	-7	-	-	8	-	15	0	-120	15
5	0	-5	-	-	5	8	8	0	-40	5
7	0	-4	0	-4	3	4	5	0	-40	2.5
9	0	-2.5	0	-2.5	1.5	1.5	1.5	0	-40	1.5

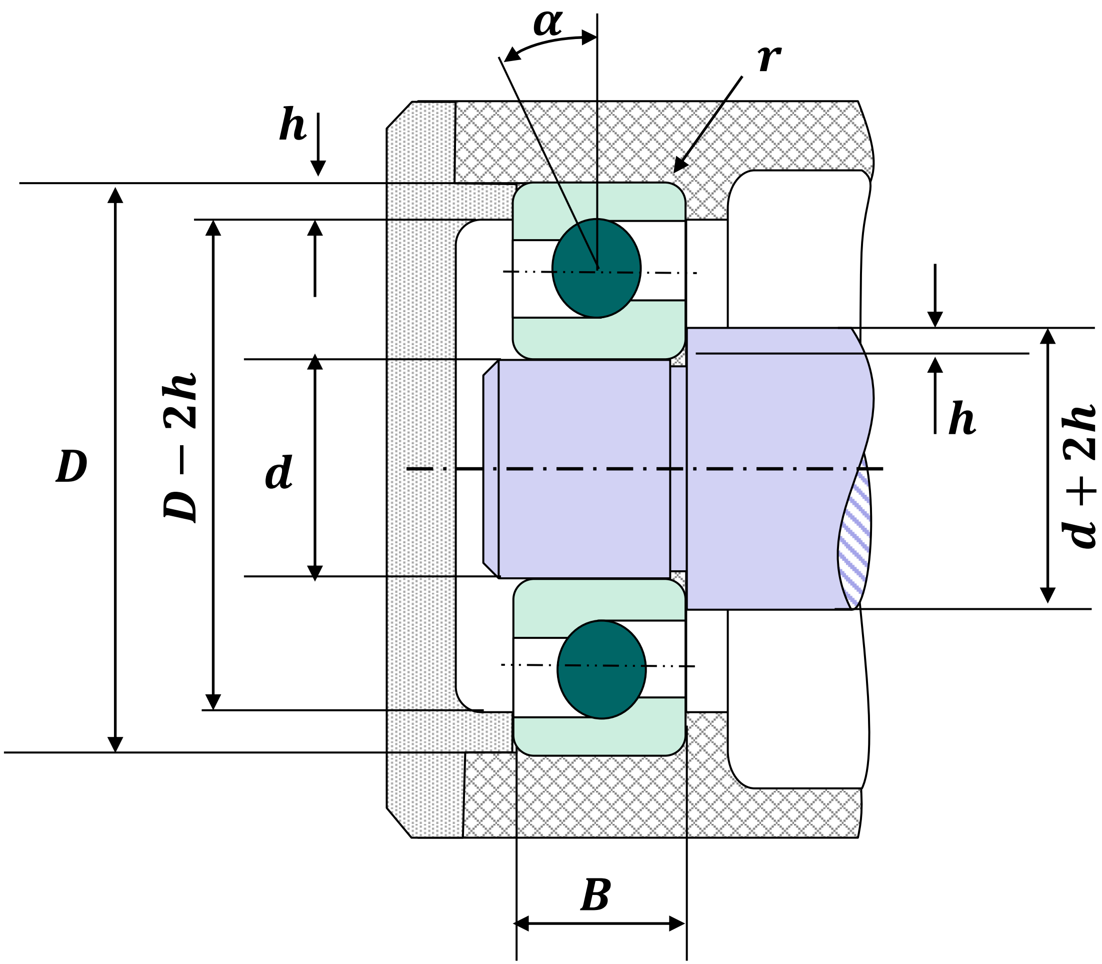
Outer Ring: 18mm < D ≤ 30mm Unit: µm

Grade	Dimensional Difference				Radial Runout	Perpendicularity	Axial Runout	Dimensional Difference of Width		Variation of Width
	ΔD_{mp}		ΔD_s		K_{ea}	S_D	S_{ea}	ΔC_s		V_{Cs}
ABEC	High	Low	High	Low	MAX	MAX	MAX	High	Low	MAX
1	0	-9	-	-	15	-	25	0	-120	20
3	0	-8	-	-	9	-	15	0	-120	20
5	0	-6	-	-	6	8	8	0	-80	5
7	0	-5	0	-5	4	4	5	0	-80	2.5
9	0	-4	0	-4	2.5	1.5	2.5	0	-80	1.5

http://www.nmbtc.com/bearings/engineering/accuracy/

Mancais de rolamento

Dimensionamento



Mancais de rolamento

Dimensionamento

$capacidade\ nominal$

$$\boldsymbol{L = L_R\left(\frac{C}{F_r}\right)^{3,33}}$$

$Vida\ correspondente\ a\ 9X10^6 rotações$

$Vida\ correspondente\ ao\ carregamento\ radial\ F_r$

$$\boldsymbol{C_{req} = F_R\left(\frac{L}{L_r}\right)^{0,3}}$$

$Capacidade\ nominal\ corrigida\ em\ função\ da\ aplicação$

Mancais de rolamento

Dimensionamento

Bearing Rated Capacities, C, for $L_R = 90 \times 10^6$
Revolution Life with 90 Percent Reliability

	Radial Ball, $\alpha = 0°$			Angular Ball, $\alpha = 25°$			Roller		
Bore (mm)	L00 Xlt (kN)	200 lt (kN)	300 med (kN)	L00 Xlt (kN)	200 lt (kN)	300 med (kN)	1000 Xlt (kN)	1200 lt (kN)	1300 med (kN)
10	1.02	1.42	1.90	1.02	1.10	1.88			
12	1.12	1.42	2.46	1.10	1.54	2.05			
15	1.22	1.56	3.05	1.28	1.66	2.85			
17	1.32	2.70	3.75	1.36	2.20	3.55	2.12	3.80	4.90
20	2.25	3.35	5.30	2.20	3.05	5.80	3.30	4.40	6.20
25	2.45	3.65	5.90	2.65	3.25	7.20	3.70	5.50	8.50
30	3.35	5.40	8.80	3.60	6.00	8.80	2.40[a]	8.30	10.0
35	4.20	8.50	10.6	4.75	8.20	11.0	3.10[a]	9.30	13.1
40	4.50	9.40	12.6	4.95	9.90	13.2	7.20	11.1	16.5
45	5.80	9.10	14.8	6.30	10.4	16.4	7.40	12.2	20.9
50	6.10	9.70	15.8	6.60	11.0	19.2	5.10[a]	12.5	24.5
55	8.20	12.0	18.0	9.00	13.6	21.5	11.3	14.9	27.1
60	8.70	13.6	20.0	9.70	16.4	24.0	12.0	18.9	32.5
65	9.10	16.0	22.0	10.2	19.2	26.5	12.2	21.1	38.3
70	11.6	17.0	24.5	13.4	19.2	29.5		23.6	44.0
75	12.2	17.0	25.5	13.8	20.0	32.5		23.6	45.4
80	14.2	18.4	28.0	16.6	22.5	35.5	17.3	26.2	51.6
85	15.0	22.5	30.0	17.2	26.5	38.5	18.0	30.7	55.2
90	17.2	25.0	32.5	20.0	28.0	41.5		37.4	65.8
95	18.0	27.5	38.0	21.0	31.0	45.5		44.0	65.8
100	18.0	30.5	40.5	21.5	34.5		20.9	48.0	72.9
105	21.0	32.0	43.5	24.5	37.5			49.8	84.5
110	23.5	35.0	46.0	27.5	41.0	55.0	29.4	54.3	85.4
120	24.5	37.5		28.5	44.5			61.4	100.1
130	29.5	41.0		33.5	48.0	71.0	48.9	69.4	120.1
140	30.5	47.5		35.0	56.0			77.4	131.2
150	34.5			39.0	62.0		58.7	83.6	
160								113.4	
180	47.0			54.0			97.9	140.1	
200								162.4	
220								211.3	
240								258.0	

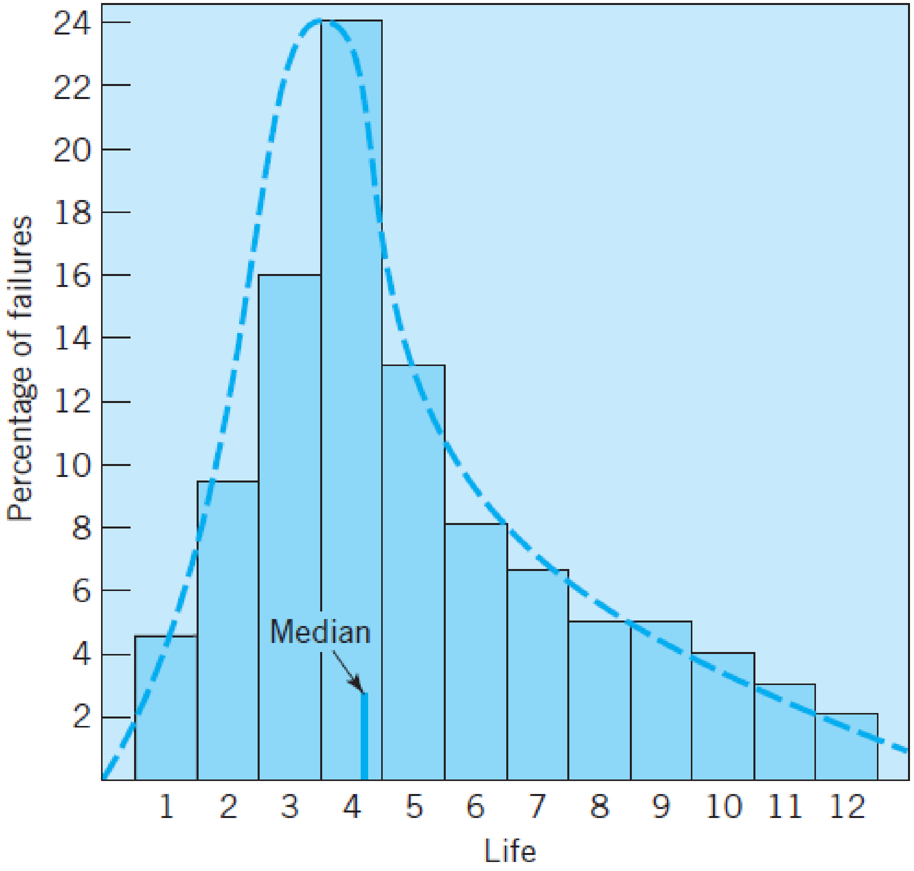
Mancais de rolamento

Dimensionamento

- A vida padrão é comumente designada como a vida L_{10}.
- A vida L_{10} corresponde a uma probabilidade de falha de 10%, isso representa que 90% dos rolamentos não falharam quando essa vida é atingida, correspondendo a 90% de confiabilidade
- Os testes mostram que a vida média de rolamentos (rolamentos de esferas em particular) é cerca de cinco vezes a vida de fadiga padrão para L_{10}
- Muitos projetos exigem mais de 90% de confiabilidade
- A probabilidade de falha de mancais de elementos rolantes não segue uma distribuiçã gaussiana, mas sim um distribuição de Weibull
- Isso leva a necessidade do ajuste da curva de vida por meio do fator de confiabilidade Kr

Mancais de rolamento

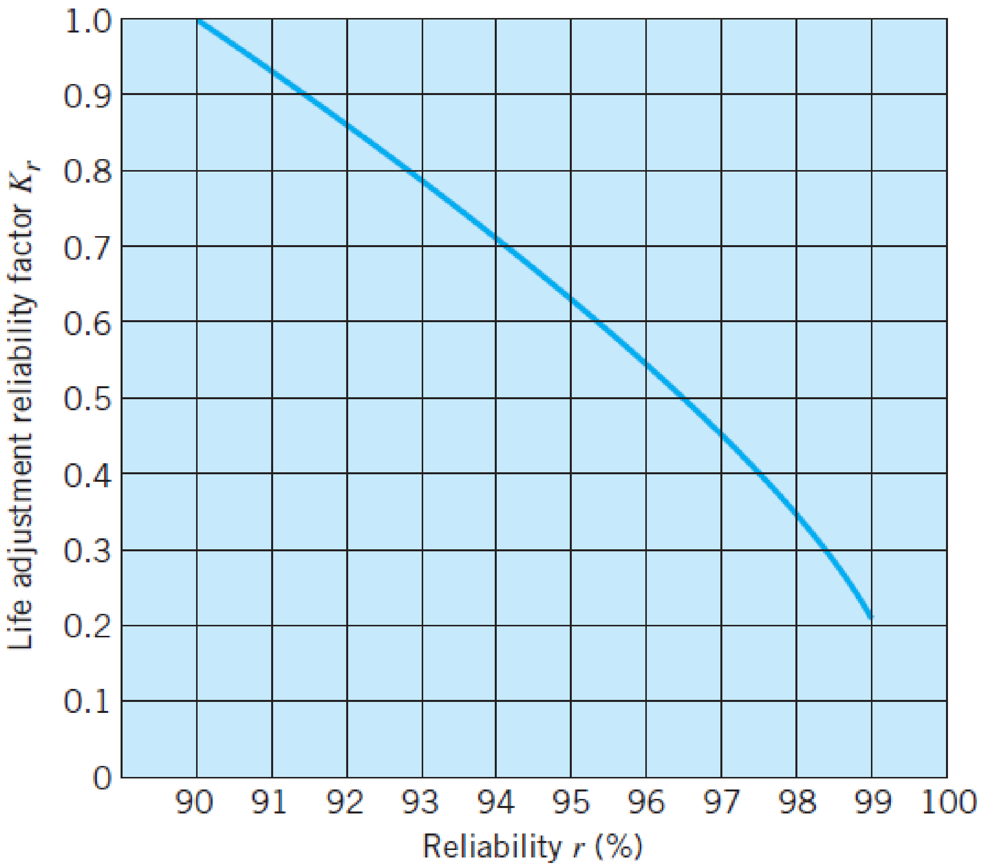
Dimensionamento



Distribuição de Weibull para vida em fadiga de mancais de elementos rolantes

Mancais de rolamento

Dimensionamento



Fator de confiabilidade Kr

Mancais de rolamento

Dimensionamento

$\boldsymbol{corrigindo\ L_r\ e\ C_{req}\ em\ termos\ de\ K_r, temos\ \Rightarrow}$

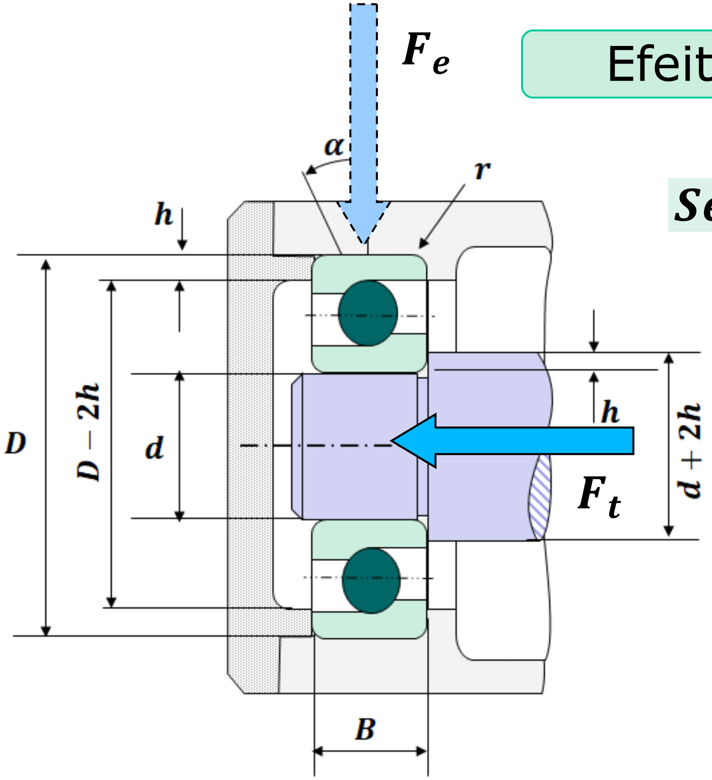
$$L = L_R\left(\frac{C}{F_r}\right)^{3{,}33} \longrightarrow L = K_r L_R\left(\frac{C}{F_r}\right)^{3{,}33}$$

$$C_{req} = F_R\left(\frac{L}{L_r}\right)^{0{,}3} \longrightarrow C_{req} = F_R\left(\frac{L}{K_r . L_r}\right)^{0{,}3}$$

Mancais de rolamento

Dimensionamento

Efeito do carregamento axial



Sendo F_e o carregamento radial equivalente

para mancais rígidos de esfera ⇒ $\alpha = 0°$

para: $0 < F_t/F_r < 0.35, \quad F_e = F_r$

para: $0.35 < F_t/F_r < 10, \quad F_e = F_r\left[1 + 1.115\left(\dfrac{F_t}{F_r} - 0.35\right)\right]$

para: $F_t/F_r > 10, \quad F_e = 1.176F_t$

para mancais de contato angular ⇒ $\alpha = 25°$

para: $0 < F_t/F_r < 0.68, \quad F_e = F_r$

para: $0.68 < F_t/F_r < 10, \quad F_e = F_r\left[1 + 0.870\left(\dfrac{F_t}{F_r} - 0.68\right)\right]$

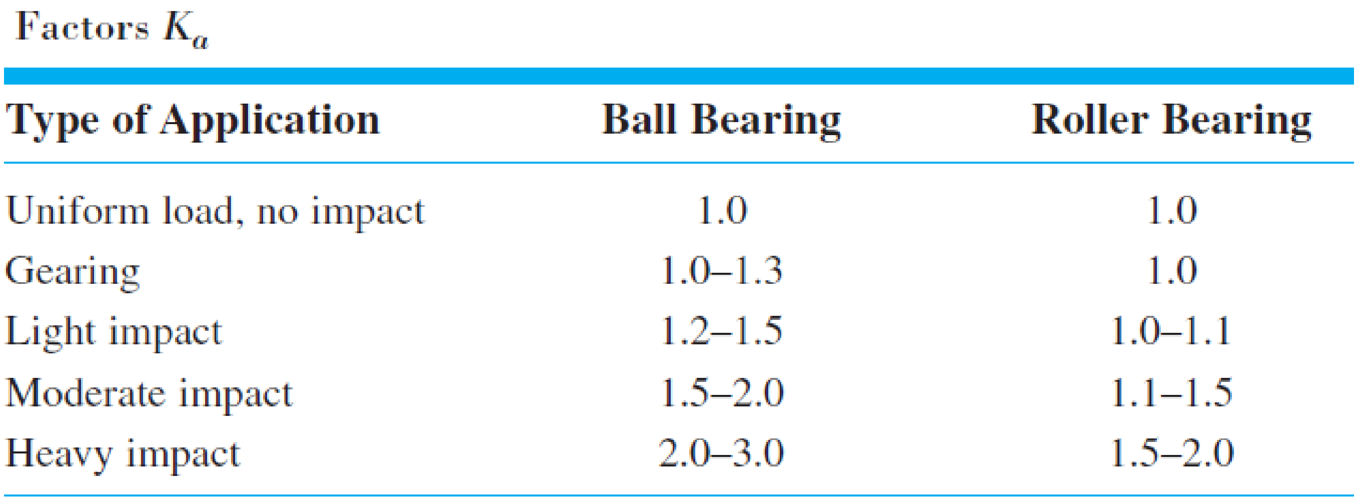
para: $F_t/F_r > 10, \quad F_e = 0.911F_t$

Mancais de rolamento

Dimensionamento

Efeito de choques e impactos

- O dimensionamento de mancais de elementos rolantes em geral é feito para condições de carregamento uniforme.
- Na presença de choques ou impactos, o fator Ka deve ser aplicado para corrigir a vida



Factors K_a

Type of Application	Ball Bearing	Roller Bearing
Uniform load, no impact	1.0	1.0
Gearing	1.0–1.3	1.0
Light impact	1.2–1.5	1.0–1.1
Moderate impact	1.5–2.0	1.1–1.5
Heavy impact	2.0–3.0	1.5–2.0

Mancais de rolamento

Dimensionamento

corrigindo L_r em termos de K_a,

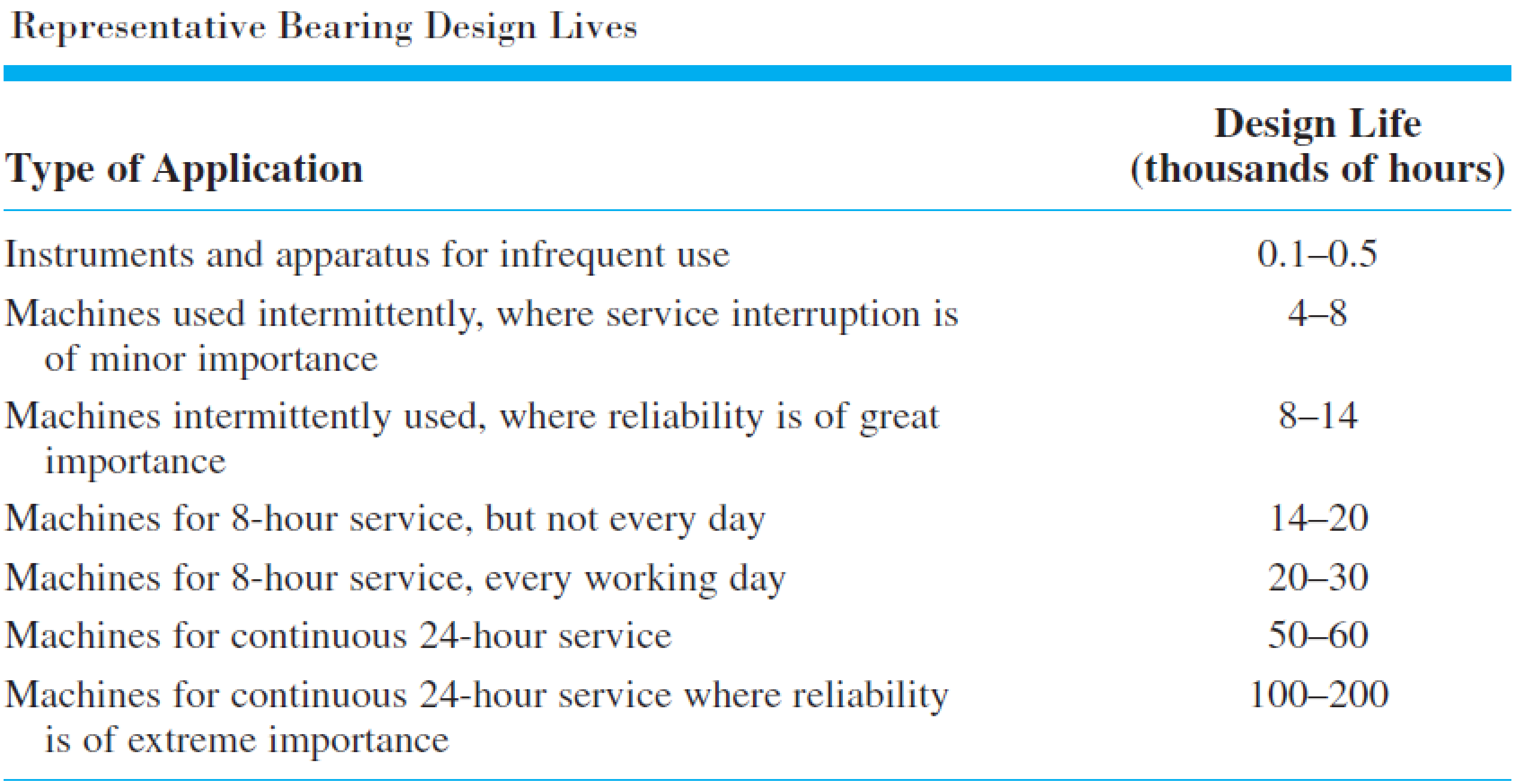
e espressando o carregamento em termos de $F_e$temos ⇒

$$L = K_r L_R \left(\frac{C}{F_r}\right)^{3,33} \longrightarrow L = K_r L_R \left(\frac{C}{K_a . F_e}\right)^{3,33}$$

$$C_{req} = F_R \left(\frac{L}{K_r . L_r}\right)^{0,3} \longrightarrow C_{req} = K_a . F_e \left(\frac{L}{K_r . L_r}\right)^{0,3}$$

Mancais de rolamento

Dimensionamento



Representative Bearing Design Lives

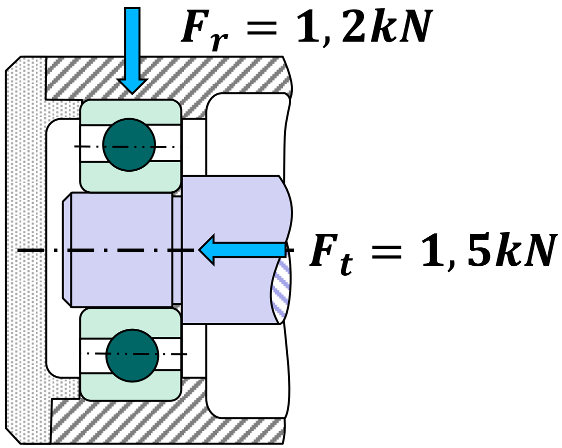
Type of Application	Design Life (thousands of hours)
Instruments and apparatus for infrequent use	0.1–0.5
Machines used intermittently, where service interruption is of minor importance	4–8
Machines intermittently used, where reliability is of great importance	8–14
Machines for 8-hour service, but not every day	14–20
Machines for 8-hour service, every working day	20–30
Machines for continuous 24-hour service	50–60
Machines for continuous 24-hour service where reliability is of extreme importance	100–200

Mancais de rolamento

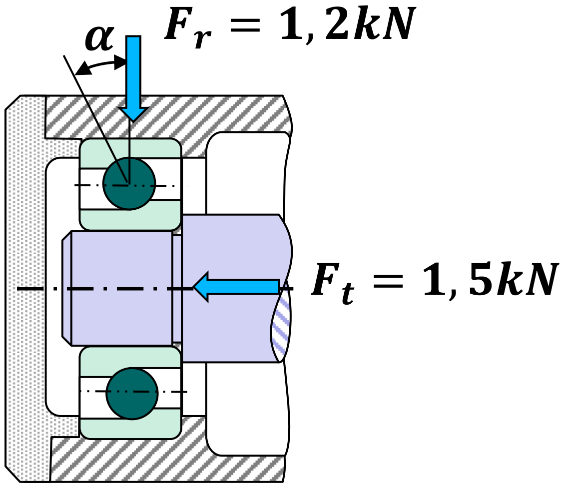
Exemplo

Selecione um rolamento de esferas para uso no eixo de um prensa industrial. A prensa operará de forma contínua em um turno de 8h/dia a 1800 rpm.

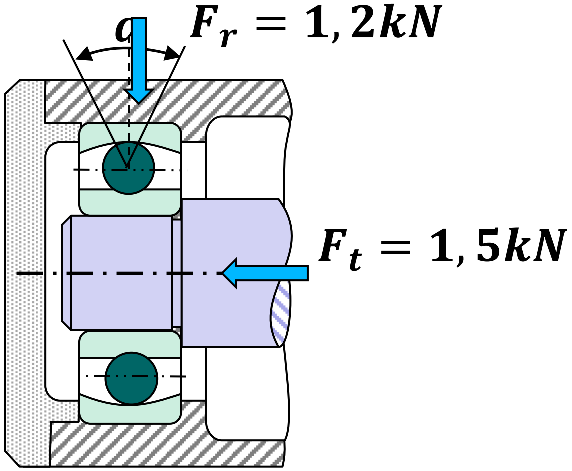
Cargas radiais e axiais são 1,2kN e 1,5kN, respectivamente, com impacto leve a moderado.



rolamento rígido de esferas



rolamento de contato angular



rolamento autocompensador

Mancais de rolamento

Exemplo

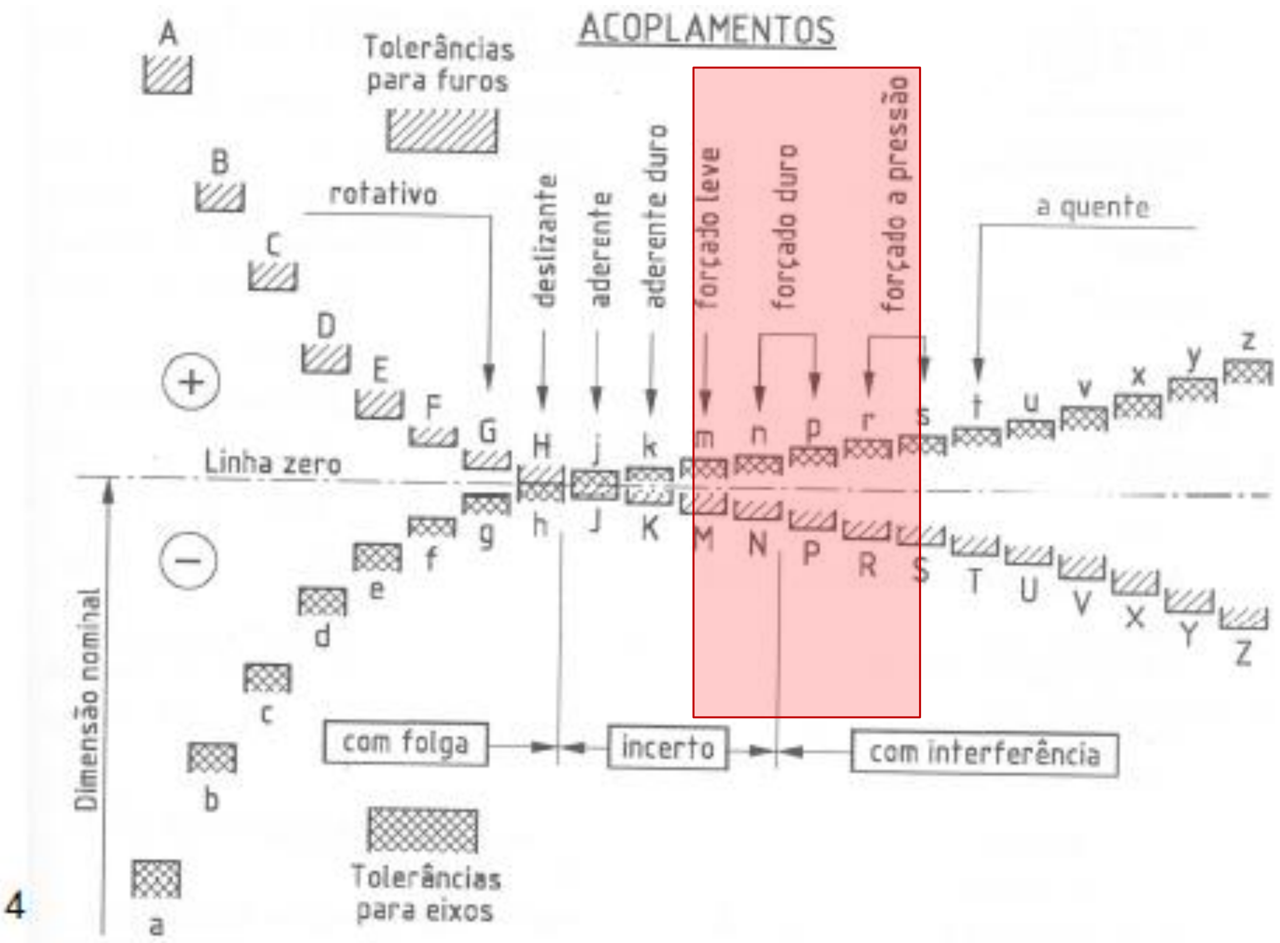


Figura 4

Campos de tolerância e ajustes mecânicos

Mancais de rolamento

Exemplo

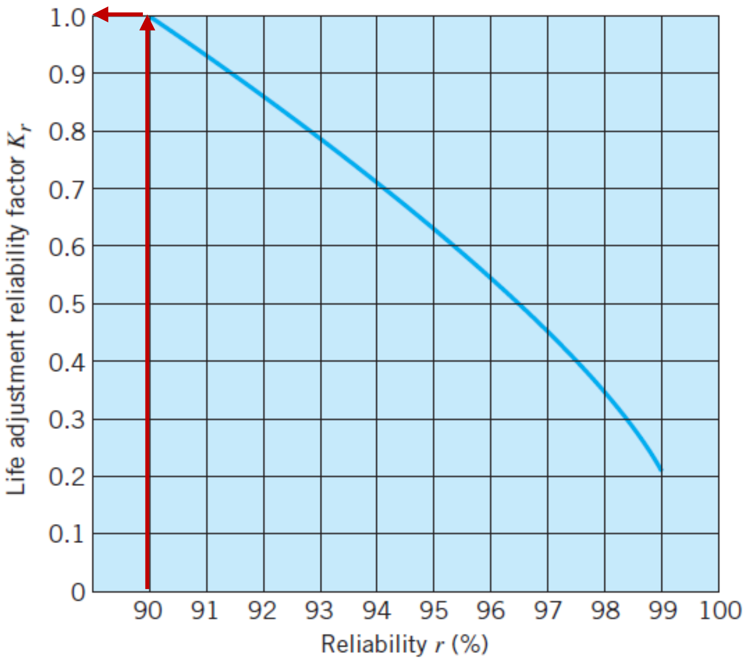
Premissas básicas:

- Projeto conservador para impacto leve a moderado.
- É necessária uma vida útil de projeto de 8 horas por dia de serviço contínuo.
- É necessária uma confiabilidade de 90%
- Tanto um rolamento de esferas radial quanto um angular podem ser selecionado. Um rolamento autocompensador vai depender da amplitude da flexão na ponta do eixo.
- A vida do rolamento de esferas varia inversamente com a potência da carga
- O ajuste prensado não afeta a vida útil do rolamento.

Mancais de rolamento

Exemplo

Fator de confiabilidade K_r



$$K_r = 1$$

Fator de impacto K_a

$$K_a = 1,5$$

Factors K_a

Type of Application	Ball Bearing	Roller Bearing
Uniform load, no impact	1.0	1.0
Gearing	1.0–1.3	1.0
Light impact	1.2–1.5	1.0–1.1
Moderate impact	1.5–2.0	1.1–1.5
Heavy impact	2.0–3.0	1.5–2.0

$$L_r = 30X10^3\ horas$$

Representative Bearing Design Lives

Type of Application	Design Life (thousands of hours)
Instruments and apparatus for infrequent use	0.1–0.5
Machines used intermittently, where service interruption is of minor importance	4–8
Machines intermittently used, where reliability is of great importance	8–14
Machines for 8-hour service, but not every day	14–20
Machines for 8-hour service, every working day	20–30
Machines for continuous 24-hour service	50–60
Machines for continuous 24-hour service where reliability is of extreme importance	100–200

Mancais de rolamento

Exemplo

Calculando o carregamento radial equivalente F_e

$$F_r = 1,2kN \qquad \frac{F_t}{F_r} = \frac{1,5}{1,2} = 1,25$$

$$F_t = 1,5kN$$

$$para\ mancais\ rígidos\ de\ esfera \Rightarrow\ \alpha = 0°$$

$$para:\quad 0 < F_t/F_r < 0.35, \quad F_e = F_r$$

$$para:\quad 0.35 < F_t/F_r < 10, \quad F_e = F_r\left[1 + 1.115\left(\frac{F_t}{F_r} - 0.35\right)\right]$$

$$para:\quad F_t/F_r > 10, \quad F_e = 1.176F_t$$

$$F_e = F_r\left[1 + 1,115\left(\frac{F_t}{F_r} - 0,35\right)\right]$$

$$F_{e_{esf}} = 2,4\ kN$$

$$para\ mancais\ de\ contato\ angular \Rightarrow\ \alpha = 25°$$

$$para:\quad 0 < F_t/F_r < 0.68, \quad F_e = F_r$$

$$para:\quad 0.68 < F_t/F_r < 10, \quad F_e = F_r\left[1 + 0.870\left(\frac{F_t}{F_r} - 0.68\right)\right]$$

$$para:\quad F_t/F_r > 10, \quad F_e = 0.911F_t$$

$$F_e = F_r\left[1 + 0,870\left(\frac{F_t}{F_r} - 0,68\right)\right]$$

$$F_{e_{cont}} = 1,8\ kN$$

Mancais de rolamento

Exemplo

$K_r = 1$

$K_a = 1,5$

$L_r = 30X10^3$

$$C_{req} = K_a . F_e \left(\frac{L}{K_r . L_r} \right)^{0,3}$$

$Vida\ L\ em\ [rpm] = n\ .\ L_r\ [mim]$

$L = 1800rpm\ .\ 30X10^3 h.\ 60min/h$

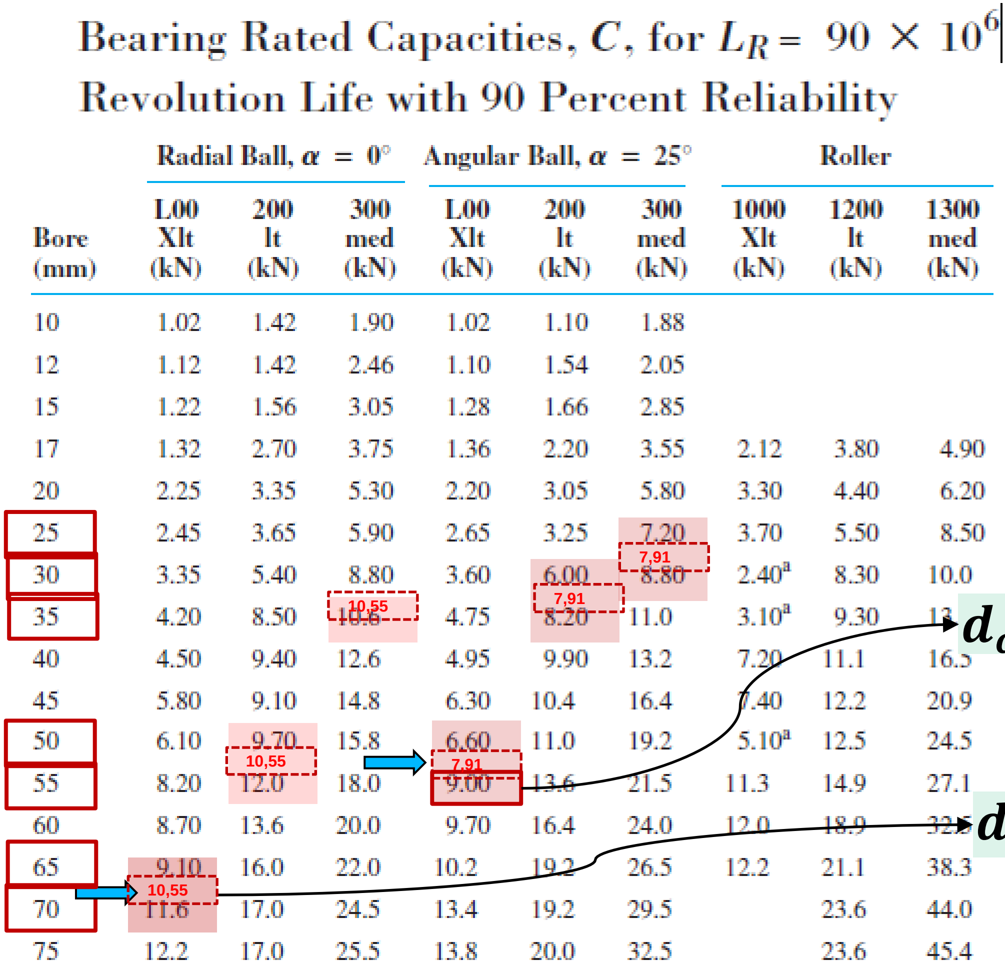
$L = 3240X10^6\ \text{revoluções}$

$F_{e_{esf}} = 2,4\ kN$ → $C_{req_{esf}} = 10,55kN$

$F_{e_{cont}} = 1,8\ kN$ → $C_{req_{cont}} = 7,91N$

Mancais de rolamento

Exemplo



Bearing Rated Capacities, C, for $L_R = 90 \times 10^6$ Revolution Life with 90 Percent Reliability

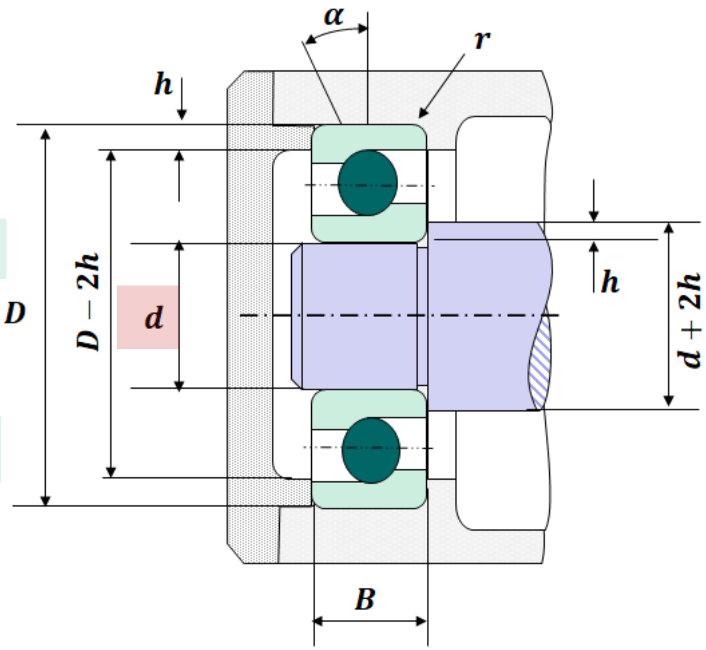
	Radial Ball, $\alpha = 0°$			Angular Ball, $\alpha = 25°$			Roller		
Bore (mm)	L00 Xlt (kN)	200 lt (kN)	300 med (kN)	L00 Xlt (kN)	200 lt (kN)	300 med (kN)	1000 Xlt (kN)	1200 lt (kN)	1300 med (kN)
10	1.02	1.42	1.90	1.02	1.10	1.88			
12	1.12	1.42	2.46	1.10	1.54	2.05			
15	1.22	1.56	3.05	1.28	1.66	2.85			
17	1.32	2.70	3.75	1.36	2.20	3.55	2.12	3.80	4.90
20	2.25	3.35	5.30	2.20	3.05	5.80	3.30	4.40	6.20
25	2.45	3.65	5.90	2.65	3.25	7.20	3.70	5.50	8.50
30	3.35	5.40	8.80	3.60	6.00	7,91 8.80	2.40[a]	8.30	10.0
35	4.20	8.50	10,55 10.6	4.75	7,91 8.20	11.0	3.10[a]	9.30	13
40	4.50	9.40	12.6	4.95	9.90	13.2	7.20	11.1	16.5
45	5.80	9.10	14.8	6.30	10.4	16.4	7.40	12.2	20.9
50	6.10	9.70	15.8	6.60	11.0	19.2	5.10[a]	12.5	24.5
55	8.20	10,55 12.0	18.0	7,91 9.00	13.6	21.5	11.3	14.9	27.1
60	8.70	13.6	20.0	9.70	16.4	24.0	12.0	18.9	32.5
65	9.10	16.0	22.0	10.2	19.2	26.5	12.2	21.1	38.3
70	10,55 11.6	17.0	24.5	13.4	19.2	29.5		23.6	44.0
75	12.2	17.0	25.5	13.8	20.0	32.5		23.6	45.4

$$C_{req_{esf}} = 10,55kN$$

$$C_{req_{cont}} = 7,91N$$

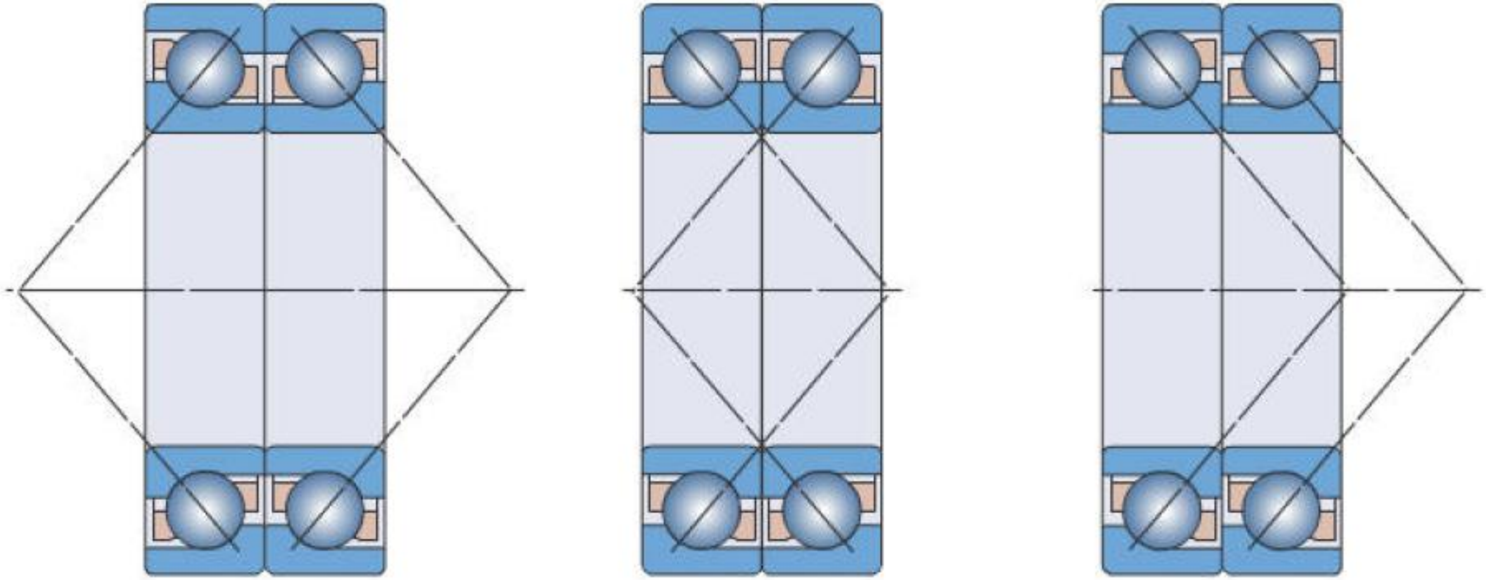
$$d_{cont} = 55mm$$

$$d_{esf} = 70mm$$



Mancais de rolamento

Considerações de montagem



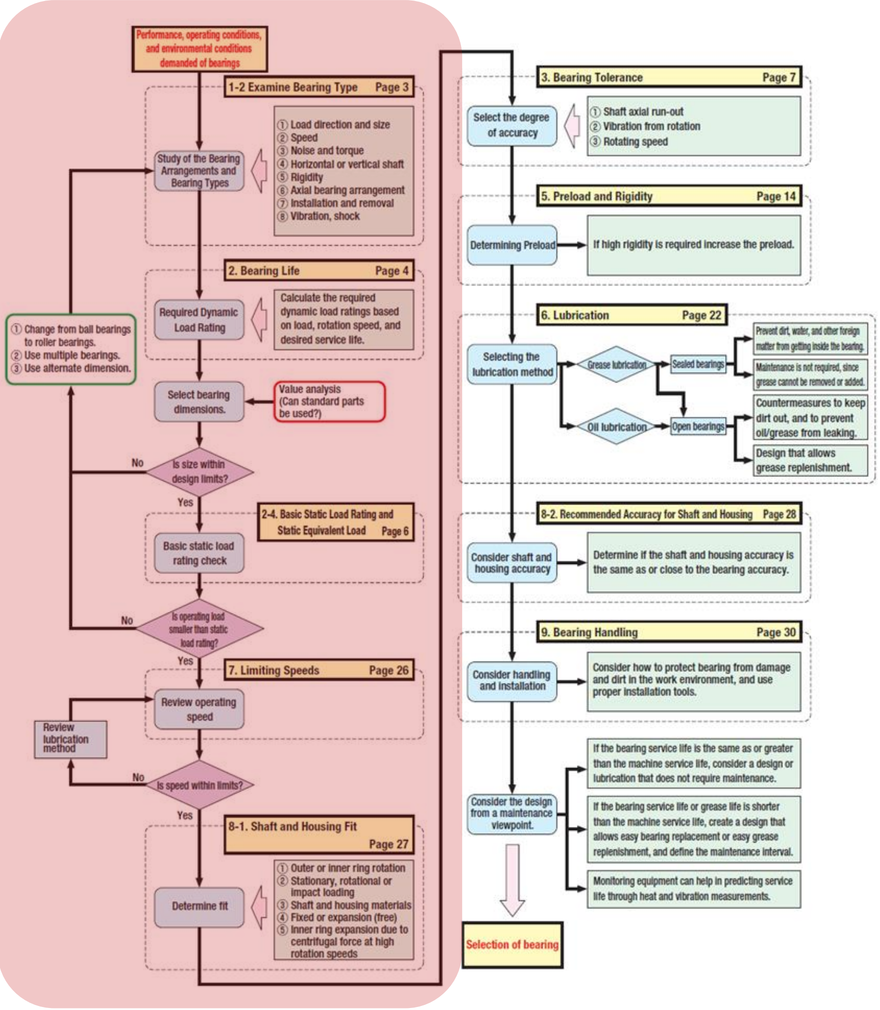
O-Anordnung

X-Anordnung

Tandem-Anordnung

Mancais de rolamento

Seleção


Performance, operating conditions, and environmental conditions demanded of bearings

1-2 Examine Bearing Type Page 3

Study of the Bearing Arrangements and Bearing Types

① Load direction and size
② Speed
③ Noise and torque
④ Horizontal or vertical shaft
⑤ Rigidity
⑥ Axial bearing arrangement
⑦ Installation and removal
⑧ Vibration, shock

2. Bearing Life Page 4

Required Dynamic Load Rating

Calculate the required dynamic load ratings based on load, rotation speed, and desired service life.

① Change from ball bearings to roller bearings.
② Use multiple bearings.
③ Use alternate dimension.

Select bearing dimensions.

Value analysis (Can standard parts be used?)

Is size within design limits? No / Yes

2-4. Basic Static Load Rating and Static Equivalent Load Page 6

Basic static load rating check

Is operating load smaller than static load rating? No / Yes

7. Limiting Speeds Page 26

Review operating speed

Review lubrication method

Is speed within limits? No / Yes

8-1. Shaft and Housing Fit Page 27

Determine fit

① Outer or inner ring rotation
② Stationary, rotational or impact loading
③ Shaft and housing materials
④ Fixed or expansion (free)
⑤ Inner ring expansion due to centrifugal force at high rotation speeds

3. Bearing Tolerance Page 7

Select the degree of accuracy

① Shaft axial run-out
② Vibration from rotation
③ Rotating speed

5. Preload and Rigidity Page 14

Determining Preload

If high rigidity is required increase the preload.

6. Lubrication Page 22

Selecting the lubrication method

Grease lubrication → Sealed bearings
- Prevent dirt, water, and other foreign matter from getting inside the bearing.
- Maintenance is not required, since grease cannot be removed or added.

Oil lubrication → Open bearings
- Countermeasures to keep dirt out, and to prevent oil/grease from leaking.
- Design that allows grease replenishment.

8-2. Recommended Accuracy for Shaft and Housing Page 28

Consider shaft and housing accuracy

Determine if the shaft and housing accuracy is the same as or close to the bearing accuracy.

9. Bearing Handling Page 30

Consider handling and installation

Consider how to protect bearing from damage and dirt in the work environment, and use proper installation tools.

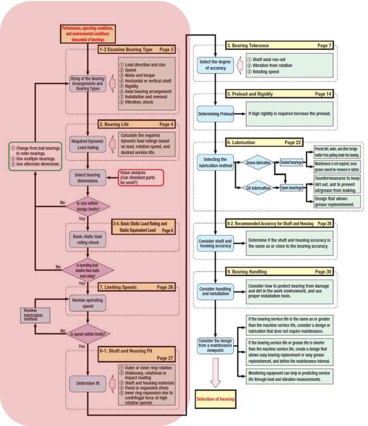
Consider the design from a maintenance viewpoint.
- If the bearing service life is the same as or greater than the machine service life, consider a design or lubrication that does not require maintenance.
- If the bearing service life or grease life is shorter than the machine service life, create a design that allows easy bearing replacement or easy grease replenishment, and define the maintenance interval.
- Monitoring equipment can help in predicting service life through heat and vibration measurements.

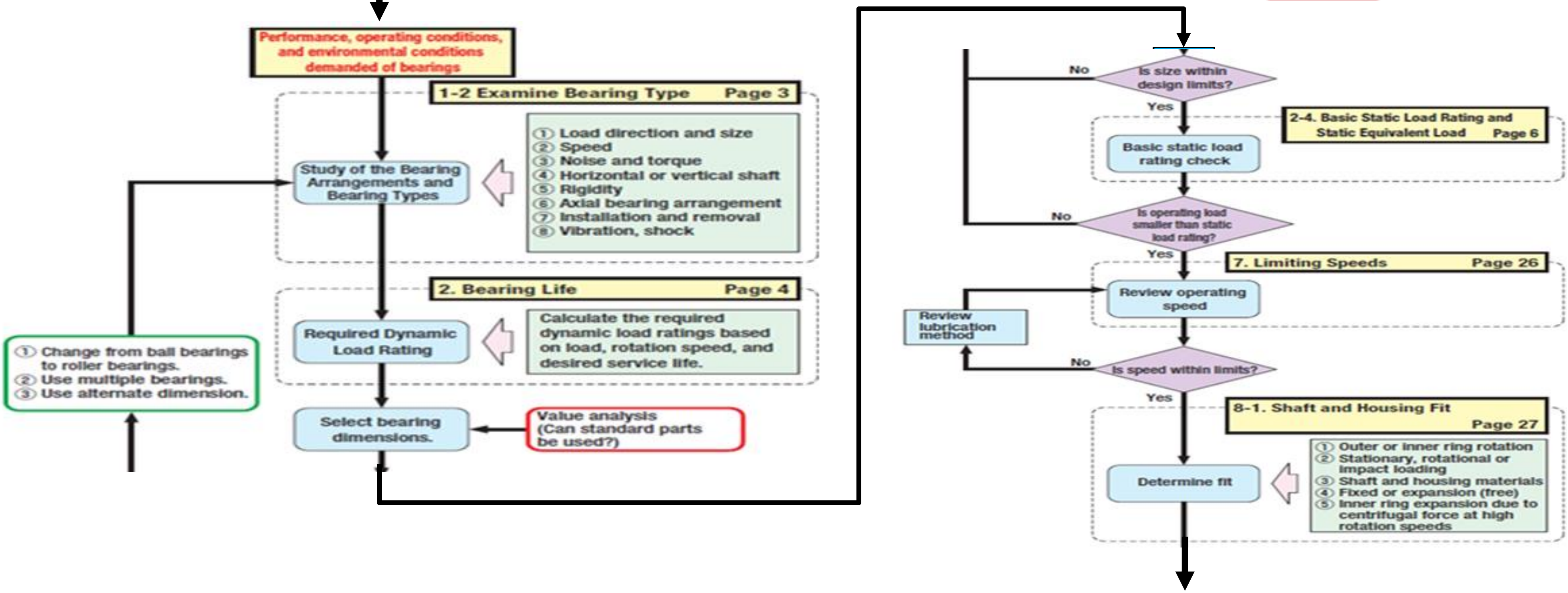
Selection of bearing

https://www.nachi-fujikoshi.co.jp/eng/web/pdf/B1031E-5.pdf

Mancais de rolamento

Seleção

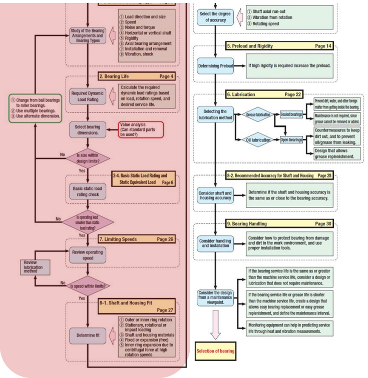


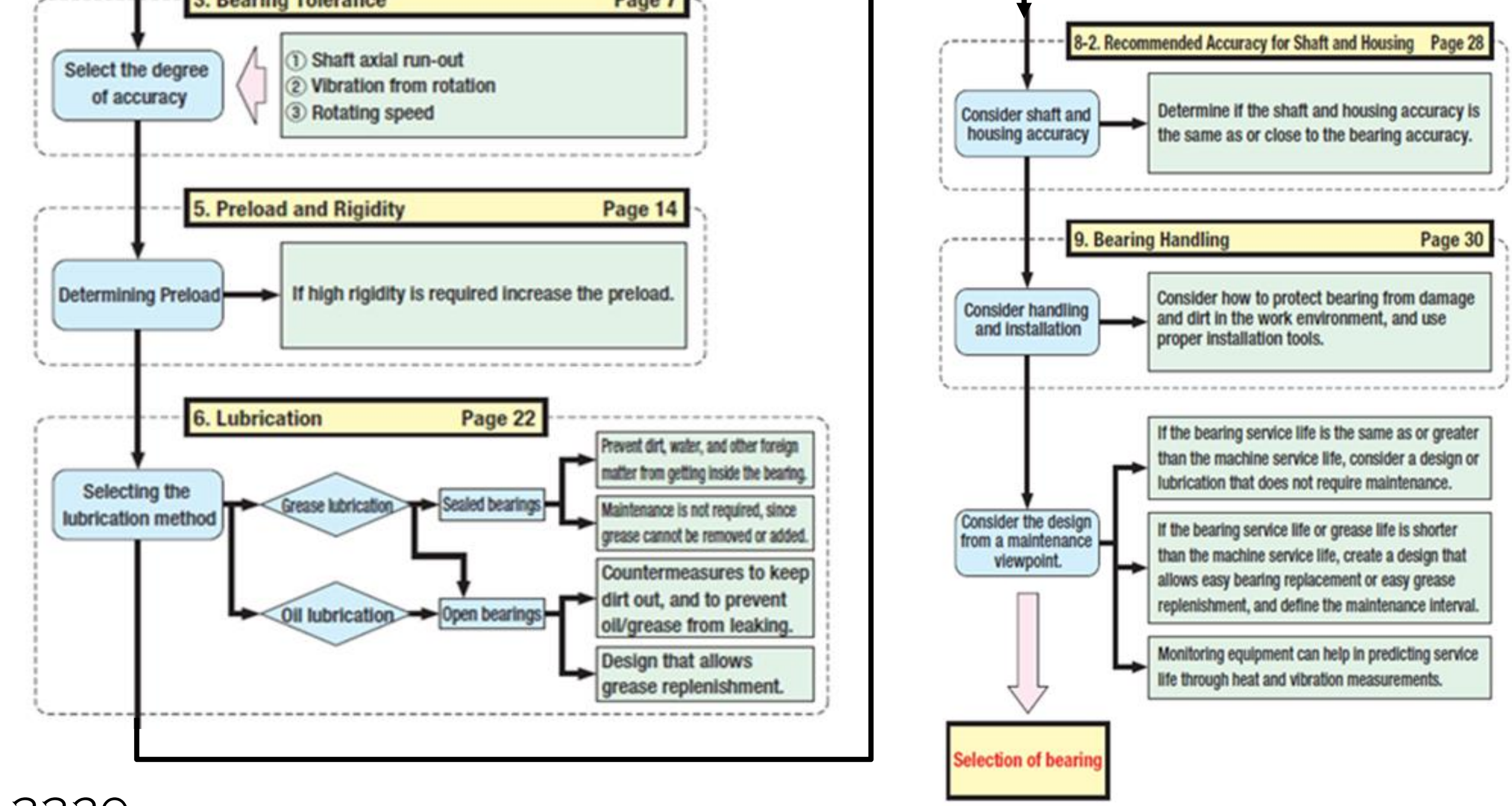


https://www.nachi-fujikoshi.co.jp/eng/web/pdf/B1031E-5.pdf

Mancais de rolamento

Seleção





3. Bearing Tolerance Page 7

Select the degree of accuracy

① Shaft axial run-out
② Vibration from rotation
③ Rotating speed

5. Preload and Rigidity Page 14

Determining Preload → If high rigidity is required increase the preload.

6. Lubrication Page 22

Selecting the lubrication method → Grease lubrication → Sealed bearings → Prevent dirt, water, and other foreign matter from getting inside the bearing. / Maintenance is not required, since grease cannot be removed or added.

Selecting the lubrication method → Oil lubrication → Open bearings → Countermeasures to keep dirt out, and to prevent oil/grease from leaking. / Design that allows grease replenishment.

8-2. Recommended Accuracy for Shaft and Housing Page 28

Consider shaft and housing accuracy → Determine if the shaft and housing accuracy is the same as or close to the bearing accuracy.

9. Bearing Handling Page 30

Consider handling and installation → Consider how to protect bearing from damage and dirt in the work environment, and use proper installation tools.

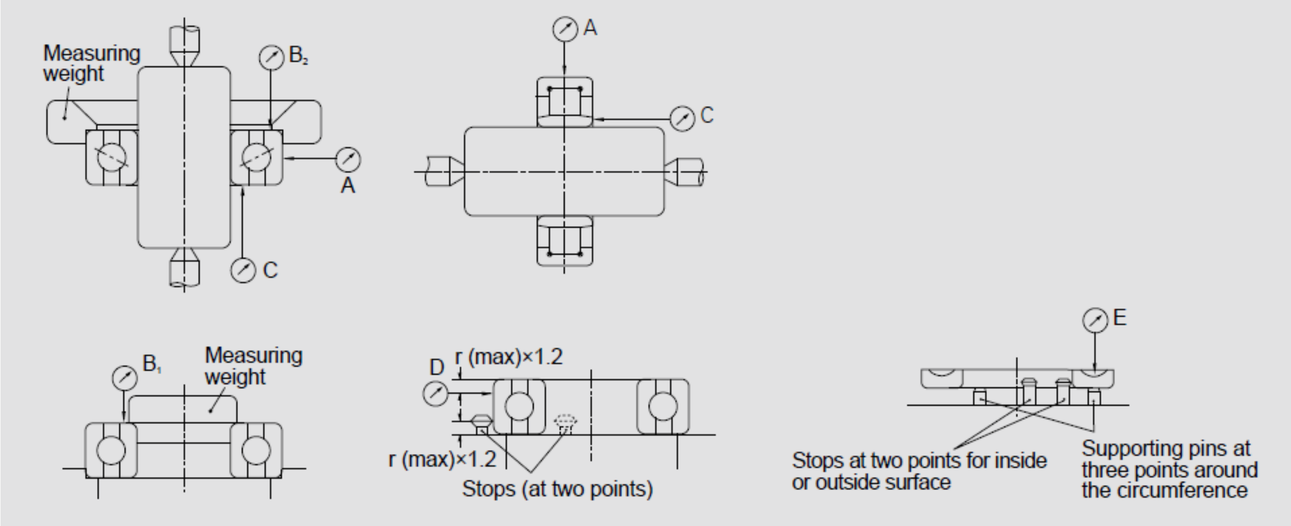
Consider the design from a maintenance viewpoint.

- If the bearing service life is the same as or greater than the machine service life, consider a design or lubrication that does not require maintenance.
- If the bearing service life or grease life is shorter than the machine service life, create a design that allows easy bearing replacement or easy grease replenishment, and define the maintenance interval.
- Monitoring equipment can help in predicting service life through heat and vibration measurements.

Selection of bearing

Mancais de rolamento

Erros de movimento



Running accuracy	Inner ring	Outer ring	Measuring point
K_{ia}	rotating	stationary	A
K_{ea}	stationary	rotating	A
S_{ia}	rotating	stationary	B_1
S_{ea}	stationary	rotating	B_2
S_d	rotating	stationary	C
S_D	–	rotating	D
S_i , S_e	Only the shaft or housing or central washer is to be rotated		E

https://www.nskeurope.com/downloads/literature_bearing/EN-TI-0112-FINAL.pdf

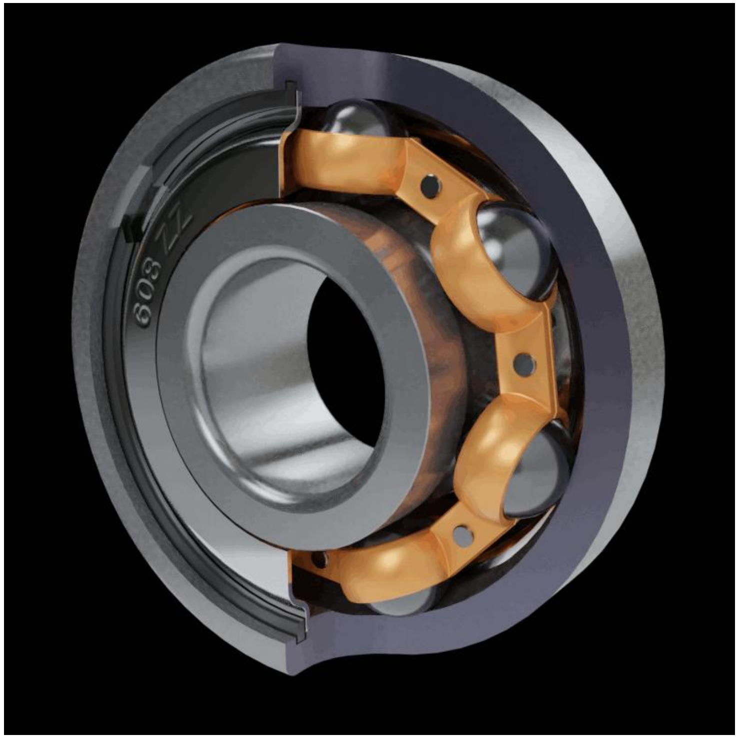
Mancais de rolamento

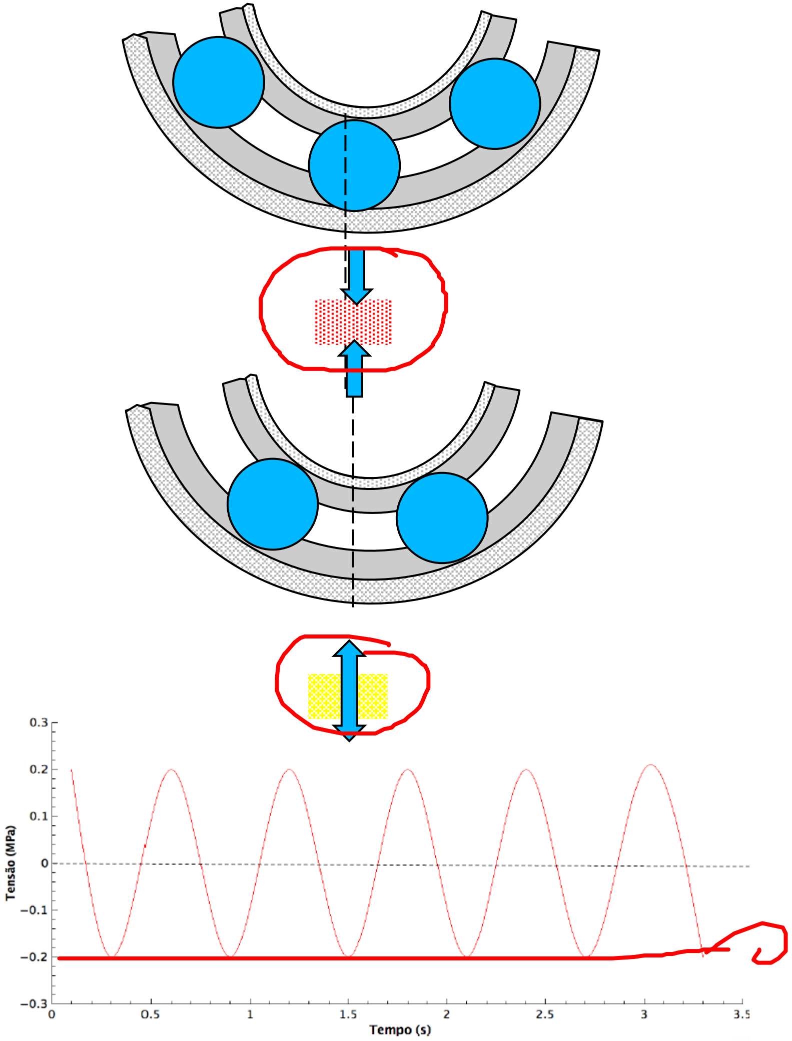
Falhas em mancais de rolamento

- Desalinhamento
- Flexão dos eixos
- Montagem errada
- Ciclo de carregamento
- Velocidade de operação
- Choques
- Sobrecargas
- Tipo de mancal
- Contaminação na interface
- Acabamento superficial
- Condições de lubrificação
- Tipo de lubrificante
- Material do mancal
- Tipo de elemento
- Seleção errada

Mancais de rolamento

Falhas em mancais de rolamento





Mancais de rolamento

Falhas em mancais de rolamento

FIM DA AULA