

Aula - Transições de fase (slide)

$$\frac{dm}{dt} = (a_c - a)m - bm^3$$

$$m \frac{dm}{dt} = (a_c - a)m^2 - bm^4$$

(1)

$$\frac{1}{2} \frac{dm^2}{dt} = (a_c - a)m^2 - bm^4$$

$$x = m^2$$

$$\left| \frac{dx}{dt} = 2 \underbrace{(a_c - a)}_{\alpha} x - \underbrace{2b}_{\beta} x^2 \right.$$

$$\frac{dx}{dx - \beta x^2} = 2 dt$$

$$\frac{dx}{x(\alpha - \beta x)} = 2 dt$$

$$\frac{1}{x(\alpha - \beta x)} = \frac{A}{x} + \frac{D}{\alpha - \beta x} \Leftrightarrow \frac{A(\alpha - \beta x) + Dx}{x(\alpha - \beta x)}$$

$$A\alpha = 1 \Rightarrow A = \frac{1}{\alpha}$$

$$-\beta A + D = 0$$
$$D = +\beta A = +\frac{\beta}{\alpha}$$

$$\frac{1}{x(\alpha - \beta x)} = \frac{1}{\alpha x} + \frac{\beta}{\alpha(\alpha - \beta x)} \quad (2)$$

$$\frac{dx}{x} + \frac{\beta dx}{\alpha - \beta x} = 2\alpha dt$$

$$\frac{dx}{x} + \frac{dx}{\frac{\alpha}{\beta} - x} = 2\alpha dt$$

$$\frac{dx}{x} - \frac{dx}{x - \frac{\alpha}{\beta}} = 2\alpha dt$$

$$\ln \frac{x(t)}{x_0} - \ln \frac{x(t) - \frac{\alpha}{\beta}}{x_0 - \frac{\alpha}{\beta}}$$

$$\ln \frac{x(t)}{x_0} \cdot \frac{x_0 - \alpha/\beta}{x - \alpha/\beta} = \ln \frac{1 - \alpha/\beta x_0}{1 - \alpha/\beta x(t)}$$

$$e^{2\alpha t} = \frac{1 - \frac{\alpha}{\beta x_0}}{1 - \frac{\alpha}{\beta x(t)}} \rightarrow A$$

$$1 - \frac{\alpha}{\beta x(t)} = A e^{-2\alpha t}$$

$$\frac{\alpha}{\beta x(t)} = 1 - A e^{-2\alpha t} \Rightarrow x(t) = \frac{\alpha}{\beta [1 - A e^{-2\alpha t}]}$$

$$m^2(t) = \frac{(a_c - a)}{b \left[1 - A e^{-2(a_c - a)t} \right]}$$

$$a_c < a \Rightarrow m^2(t) \longrightarrow 0 \text{ for } t \rightarrow \infty$$

$$a_c > a \Rightarrow m^2 \longrightarrow \frac{a_c - a}{b}$$

Conversely, the first-order phase transition can be studied through logistic equation

$$\frac{dm}{dt} = (a_b - a) - b m^3 + c m^5, \quad \left(\begin{array}{l} \text{for systems} \\ \text{with symmetry } \mathbb{Z}_2 \end{array} \right)$$

↑
control parameter

where $c > 0$ in order to ensure finite values of m .

Although the time behavior ^{of $m(t)$} toward the steady state is more complicated than the previous case, it is possible to establish some general portraits:

Steady state solutions

$m = 0$ and

$$(a_b - a) - b m^2 + c m^4 = 0, \quad \text{where}$$

$$m_*^2 = \frac{b \pm \sqrt{b^2 - 4(a_b - a)c}}{2c}$$

for $b^2 > 4(a_b - a)c \Rightarrow$ we have two solutions for m_*^2 .

At $a = a_b - \frac{b^2}{4c}$, the order parameter jumps from 0 to $\pm \frac{b}{2c}$.

Another way to see above features consists of evaluating the maximum of $a = a(m)$.

By inverting above relation we have

$$a = a_b + cy^2 - by \quad (y = m')$$

$$\left. \frac{\partial a}{\partial y} \right|_{a=a_f} = 0 \quad \Leftrightarrow \quad \begin{aligned} 2cy - b &= 0 \\ y^* &= \frac{b}{2c} \end{aligned}$$

$$\begin{aligned} a_f &= a_b + c \left(\frac{b}{2c} \right)^2 - b \left(\frac{b}{2c} \right) \\ &= a_b - \frac{b^2}{4c} \end{aligned}$$

For $a > a_f \Rightarrow m(t) \rightarrow 0$, irrespective of the initial condition

On the other hand, for $m(t) < 1$ the logistic equation becomes

$$\frac{dm}{dt} \approx (a_s - a)m \quad \text{and} \quad m(t) \sim e^{(a_s - a)t}$$

for $a_s - a < 0 \rightarrow m(t)$ vanishes for $t \rightarrow \infty$

$a_s - a > 0 \rightarrow m(t)$ increases for $t \rightarrow \infty$ and reach a finite value

Hence, there are three important regions:

$$a < a_b \rightarrow m(t) \rightarrow m_0(a)$$

$$\begin{aligned} a_b < a < a_f &\rightarrow m(t) \rightarrow m^*(f) \quad \text{if } m(t) > m^* \\ &\text{and } m(t) \rightarrow 0 \quad \text{if } m(t) < m^* \end{aligned}$$

(4)

This region corresponds to a bistable hysteretic branch and it is a hallmark of a discontinuous phase transition

for $a > a_f \rightarrow m(t) \rightarrow 0$ and

$$m(t) \sim e^{-(a_f - a)t} \quad \text{for } m(t) \ll 1$$

In order to describe/reproduce above features by means of microscopic systems/dynamics we resort to the master equation

$$\frac{d}{dt} P(\sigma, t) = \sum_{\sigma' \neq \sigma} \{ W(\sigma|\sigma') P(\sigma', t) - W(\sigma'|\sigma) P(\sigma, t) \}$$

Where $W(\sigma|\sigma') \rightarrow$ transition rate from $\sigma' \rightarrow \sigma$

$W(\sigma'|\sigma) \rightarrow$ transition rate from $\sigma \rightarrow \sigma'$,

and $\sigma = (\sigma_1, \sigma_2, \dots, \sigma_i, \dots, \sigma_N)$ denotes a microscopic configuration of a system with N sites. For systems with $\mathbb{Z}_2$ symmetry, one has 2^N microscopic configurations.

From now on, we shall consider/focus on our attention in system dynamics in

which the next configuration σ' differs from σ only for a spin of a given site. In other words

$$\sigma' \equiv (\sigma_1, \sigma_2, \dots, -\sigma_i, \dots, \sigma_N)$$

This simplifies things and we can rewrite the transition rate $w(\sigma/\sigma')$ and $w(\sigma'/\sigma)$ in the following way

$$w(\sigma'/\sigma) = \sum_{i=1}^N \delta(\sigma'_1, \sigma_1) \delta(\sigma'_2, \sigma_2) \dots \delta(\sigma'_i, -\sigma_i) \dots \delta(\sigma'_N, \sigma_N) w_i(\sigma)$$

where $\delta(\sigma'_i, \sigma_i)$ denotes the Kronecker delta and $w_i(\sigma)$ is the transition rate of the i -th spin change from σ_i to $-\sigma_i$. By inserting above

expression in the master equation the term $\sum_{\sigma' \neq \sigma} w(\sigma'/\sigma) P(\sigma, t) \rightarrow \sum_{i=1}^N w_i(\sigma) P_i(\sigma, t)$

Analogously

$$w(\sigma/\sigma') = \sum_{i=1}^N \delta(\sigma_1, \sigma'_1) \delta(\sigma_2, \sigma'_2) \dots \delta(\sigma_i, -\sigma'_i) \dots \delta(\sigma_N, \sigma'_N) w_i(\sigma')$$

and $\sum_{\sigma' \neq \sigma} w(\sigma/\sigma') P(\sigma', t) \rightarrow \sum_{i=1}^N w_i(\sigma') P(\sigma', t)$

where

$$\sigma' = (\sigma_1, \sigma_2, \dots, -\sigma_i, \dots, \sigma_N)$$

Hence

$$\frac{dP(\sigma)}{dt} = \sum_{i=1}^N \{ w_i(\sigma') P(\sigma', t) - w_i(\sigma) P(\sigma, t) \}$$

(1)
The time evolution of a given average
of a state function, $\langle f(\sigma) \rangle = \sum_{\sigma} f(\sigma) P(\sigma, t)$
is given by

$$\frac{d}{dt} \langle f(\sigma) \rangle = \sum_{\sigma} f(\sigma) \frac{dP(\sigma, t)}{dt} \quad \text{or}$$

$$\frac{d}{dt} \langle f(\sigma) \rangle = \sum_{\sigma} f(\sigma) \sum_{\sigma'} \left\{ \underbrace{w_1(\sigma')}_{1} P(\sigma', t) - \underbrace{w_2(\sigma)}_{2} P(\sigma, t) \right\}$$

The term 2 is just

$$\sum_{\sigma'} \sum_{\sigma} f(\sigma) w_2(\sigma) P(\sigma, t) \rightarrow \sum_{\sigma'} \langle f(\sigma) w_2(\sigma) \rangle.$$

For the term (1) we can perform the
transformation $\sigma' \rightarrow \sigma$ and

$$f(\sigma) \rightarrow f(\sigma')$$

$$w_1(\sigma') \rightarrow w_1(\sigma)$$

$$P(\sigma', t) \rightarrow P(\sigma, t).$$

We note that $\sum_{\sigma} = \sum_{\sigma'} \quad (\text{summation of all configurations})$

(and hence)

$$\sum_{\sigma'} \sum_{\sigma} f(\sigma) w_1(\sigma') P(\sigma', t) = \sum_{\sigma'} \langle f(\sigma') w_1(\sigma) \rangle.$$

Therefore

$$\frac{d}{dt} \langle f(\sigma) \rangle = \sum_{i=1}^N \langle \{ f(\sigma^i) - f(\sigma) \} w_i(\sigma) \rangle.$$

In particular the average $m = \langle \sigma_j \rangle$

has the following time evolution

$$\frac{d}{dt} \langle \sigma_j \rangle = \sum_{i=1}^N \langle \{ (\sigma_j)^i - \sigma_j \} w_i(\sigma) \rangle.$$

$$(\sigma_j)^i = -\sigma_j \text{ if } i = j$$

$$\text{and } (\sigma_j)^i = \sigma_j \text{ if } i \neq j.$$

Hence

$$\frac{d}{dt} \langle \sigma_j \rangle = -2 \langle \sigma_j w_j(\sigma) \rangle.$$

In the case of majority vote model

$$w_j(\sigma) = \frac{1}{2} \left\{ 1 - (1-2\sigma_j) S\left(\sum_{\delta} \sigma_{j+\delta}\right) \right\} \text{ one}$$

has the following logistic equation

$$\frac{d}{dt} \langle \sigma_j \rangle = - \left\langle \sigma_j \left(1 - (1-2\sigma_j) S\left(\sum_{\delta} \sigma_{j+\delta}\right) \right) \right\rangle$$

$$= - \langle \sigma_j \rangle + (1-2\sigma_j) \langle \sigma_j^2 S\left(\sum_{\delta} \sigma_{j+\delta}\right) \rangle$$

$$\text{since } \sigma_j^2 = 1, \text{ one has } \frac{d}{dt} m = -m + (1-2\sigma_j) \langle S\left(\sum_{\delta} \sigma_{j+\delta}\right) \rangle.$$

We need to evaluate $\langle S(\sum_{\delta} \sigma_{i+\delta}) \rangle$

(6)

I will evaluate for $k=4$ and $k \gg 1$, illustrating the regime of low and large connectivities.

Starting with $k=4$, $\langle S(\sum_{\delta} \sigma_{i+\delta}) \rangle$ can be splitted in two parts:

$$\langle S(\sum_{\delta} \sigma_{i+\delta}) \rangle = \underbrace{S_+(\sum_{\delta} \sigma_{i+\delta})}_{\text{signal function}} - \underbrace{S_-(\sum_{\delta} \sigma_{i+\delta})}_{\text{is positive and}} \quad \text{majority of neighboring spins are positive}$$

majority of neighboring spins are positive

majority of (neighbouring) spins are negative

In the case of one-site MFT, we neglect all correlations between nearest neighbor spins and a given joint probability

$$P(\sigma_1, \sigma_2, \dots, \sigma_N) \approx P(\sigma_1) P(\sigma_2) \dots P(\sigma_N).$$

Hence

$$S_+(\sum_{\delta} \sigma_{i+\delta}) \approx \sum_{n=\lfloor \frac{k}{2} \rfloor}^k C_n^k P_+^n P_-^{k-n}$$

$$S_-(\sum_{\delta} \sigma_{i+\delta}) \approx \sum_{n=\lfloor \frac{k}{2} \rfloor}^k C_n^k P_-^n P_+^{k-n}$$

Since $P_+ + P_- = 1$ and $m = P_+ - P_-$

$$P_+ = \frac{1+m}{2}$$

$$P_- = \frac{1-m}{2}$$

$k=4$ (rede quadrada)

(7)

$$\sum_{n=3}^4 C_n^k P_+^n P_-^{k-n} - \sum_{n=3}^4 C_n^k P_-^n P_+^{k-n}$$

$$= 4 \left(\frac{1+m}{2} \right)^3 \left(\frac{1-m}{2} \right) + \left(\frac{1+m}{2} \right)^4 - 4 \left(\frac{1-m}{2} \right)^3 \left(\frac{1+m}{2} \right)$$

$$+ (1-m)^4 - \left(\frac{1-m}{2} \right)^4$$

$$= \frac{1}{16} \left[4(1+m)^2 (1-m^2) + (1+m)^4 - (1-m)^4 - 4(1-m)^2 (1+m^2) \right]$$

$$= \frac{1}{16} \left[4(1-m^2) \left[\underbrace{(1+m)^2 - (1-m)^2}_{4m} \right] + \underbrace{(1+m)^4 - (1-m)^4}_{8(m+m^3)} \right]$$

$$= \frac{1}{16} \left[16m(1+m^2) + 8(m+m^3) \right]$$

$$= \frac{1}{16} \left[24m - 8m^3 \right] = \frac{3m}{2} - \frac{m^3}{2} = \frac{(3m-m^3)}{2}$$

$$\frac{d}{dt} m = -m + \frac{(1-2\beta)}{2} (3m-m^3)$$

$$\frac{dm}{dt} = \left[-2 + \frac{3(1-2\beta)}{2} \right] m - \frac{1}{2} (1-2\beta) m^3$$

$$\boxed{\frac{dm}{dt} = (1-6\beta)m - (1-2\beta)m^3} \quad (4)$$

above procedure is analogous to that used by rewriting the signal function in terms of products of σ 's.

For $k=4$ $S(\sum_{j=1}^4 \sigma_j)$ can be rewritten as

$$S\left(\sum_{j=1}^4 \sigma_j\right) = \frac{3}{8} (\sigma_1 + \sigma_2 + \sigma_3 + \sigma_4) + \frac{1}{8} (\sigma_1 \sigma_2 \sigma_3 + \sigma_1 \sigma_2 \sigma_4 + \sigma_1 \sigma_3 \sigma_4 + \sigma_2 \sigma_3 \sigma_4).$$

and one obtains the same equation to (*) in the previous page.

For $k=6, 8, \dots$ and so on $S(\sigma)$ has to consider terms of like $\sigma_1 \sigma_3 \sigma_4 \sigma_5$, $\sigma_1 \sigma_3 \sigma_4 \sigma_5 \sigma_6$, ... and so on.

Entropy production

Since the above mean-field description hides the irreversible character which we are interested, we shall derive a phenomenological general expression for the entropy production taking into account