



ESCOLA POLITÉCNICA DA UNIVERSIDADE DE SÃO PAULO

Elementos de Máquinas para Automação

PMR 3307 – A12

Mancais de elementos rolantes

2023.2



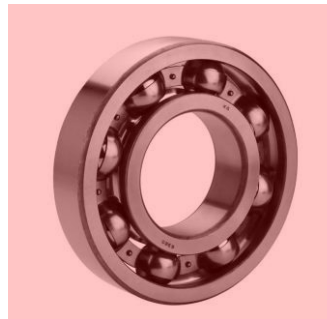
Mancais

classificação

Escorregamento



Rolamento



Fluídicos

Hidrodinâmicos



Hidrostáticos



Magnéticos





Mancais de rolamento

Exemplos





Introdução

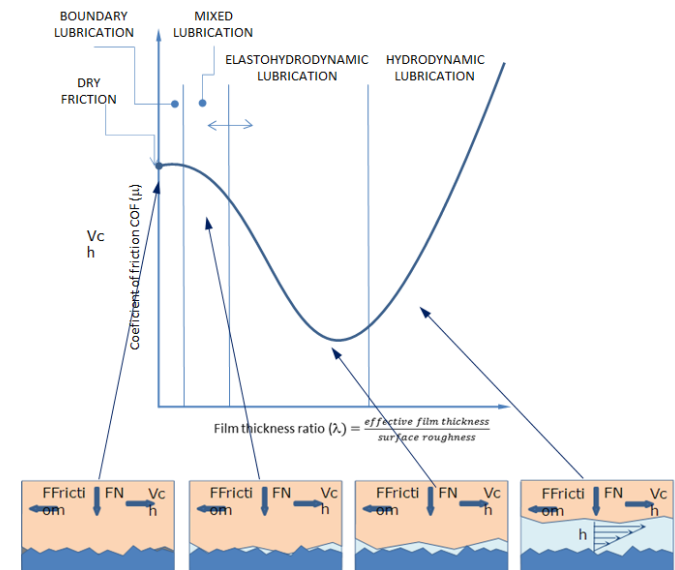
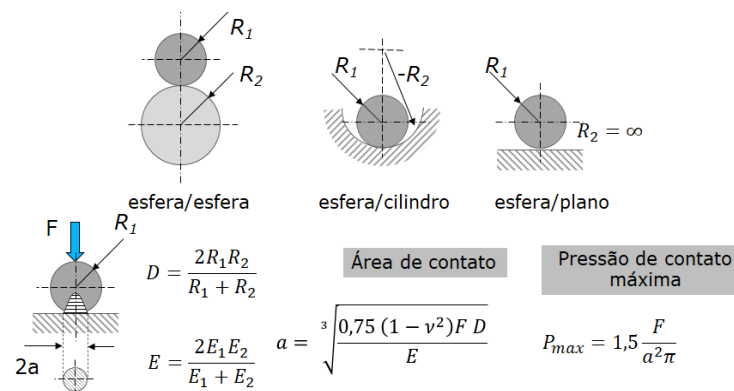
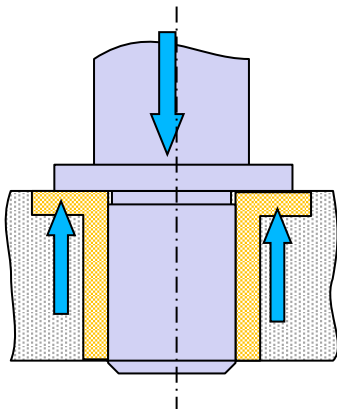
Mancais de escorregamento



Mecânica dos sólidos

Contatos de Hertz

Curva de Stribeck



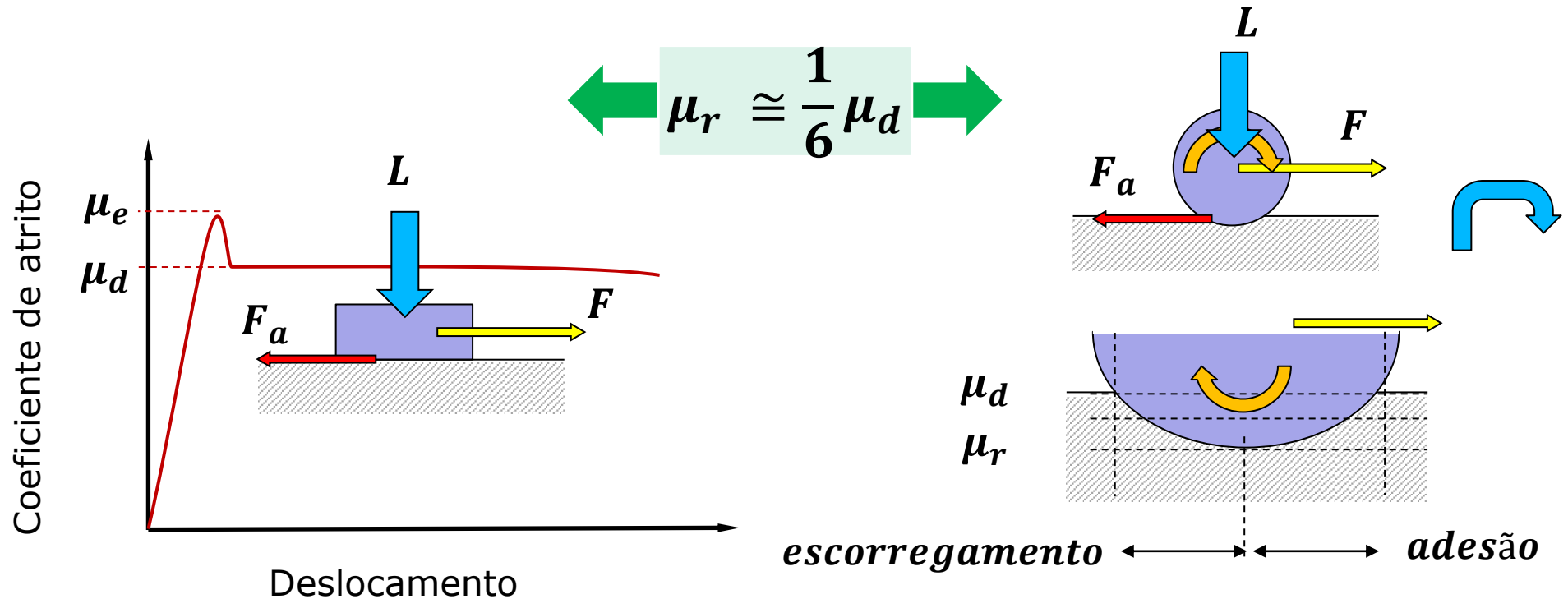


Introdução

Atrito

Atrito de escorregamento

Atrito de rolamento





Mancais de rolamento

Introdução

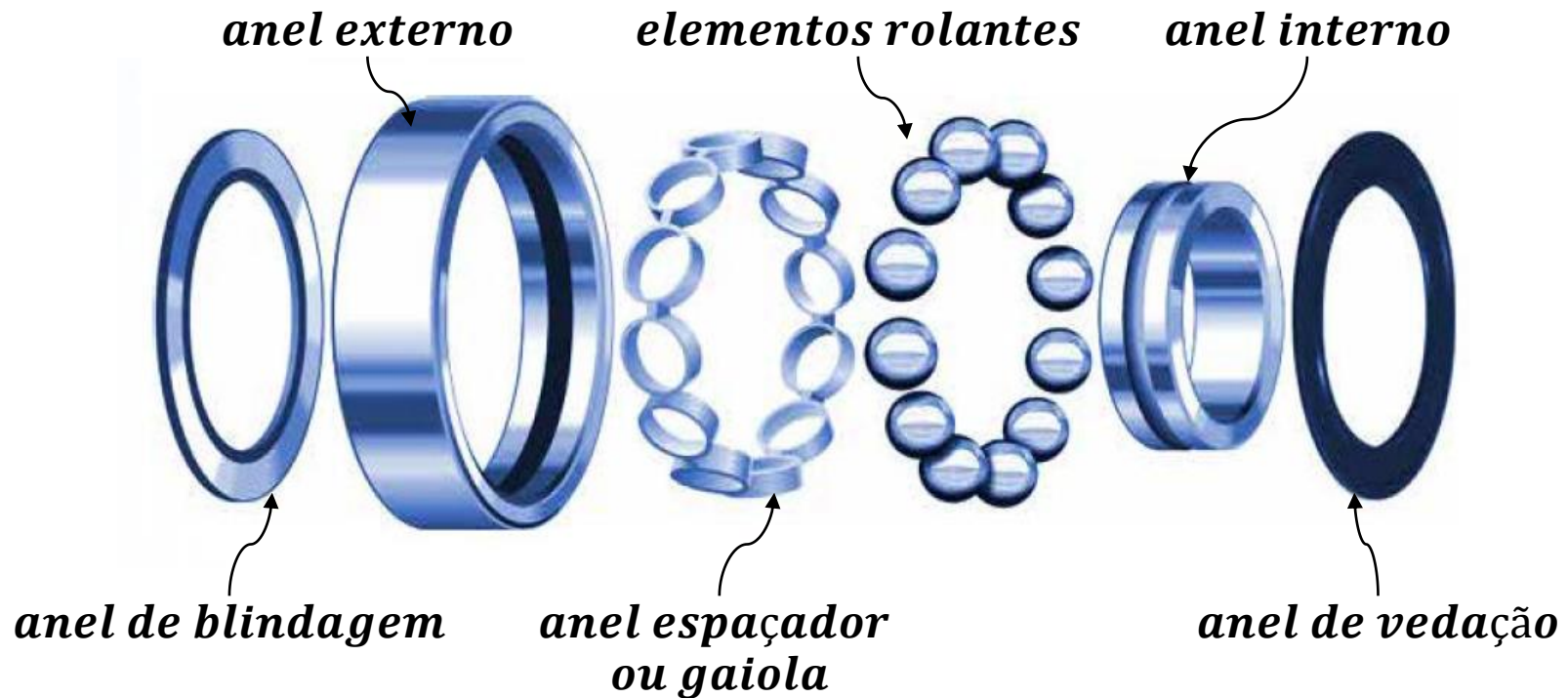
São os tipos de mancais mais utilizados, e são caracterizados por:

- Fácil movimentação
- Baixo atrito
- Elevado nível de padronização
- Baixo custo relativo



Mancais de rolamento

Constituintes



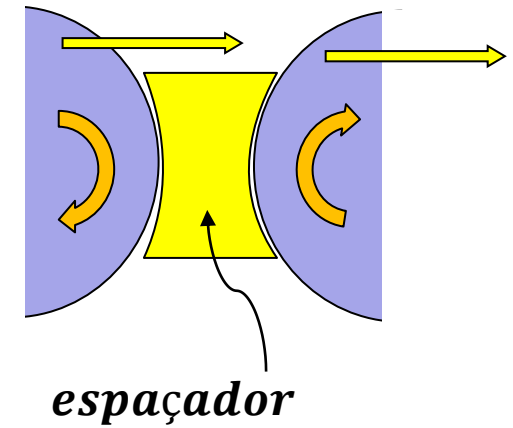
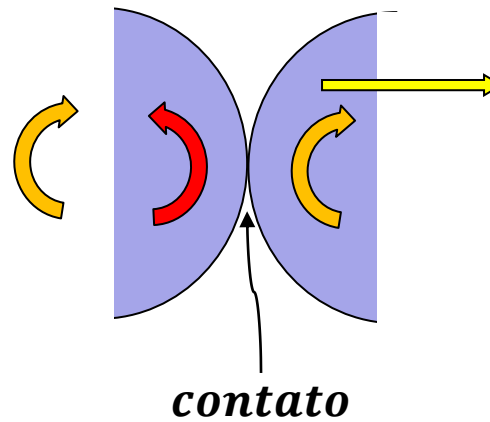
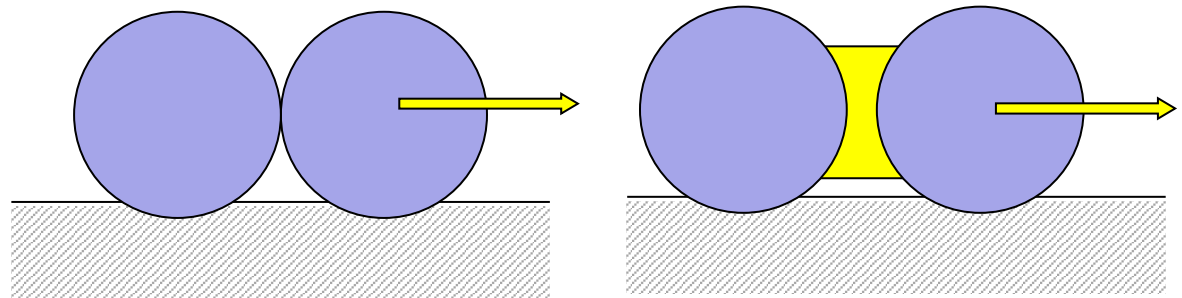


Mancais de rolamento

Espaçador



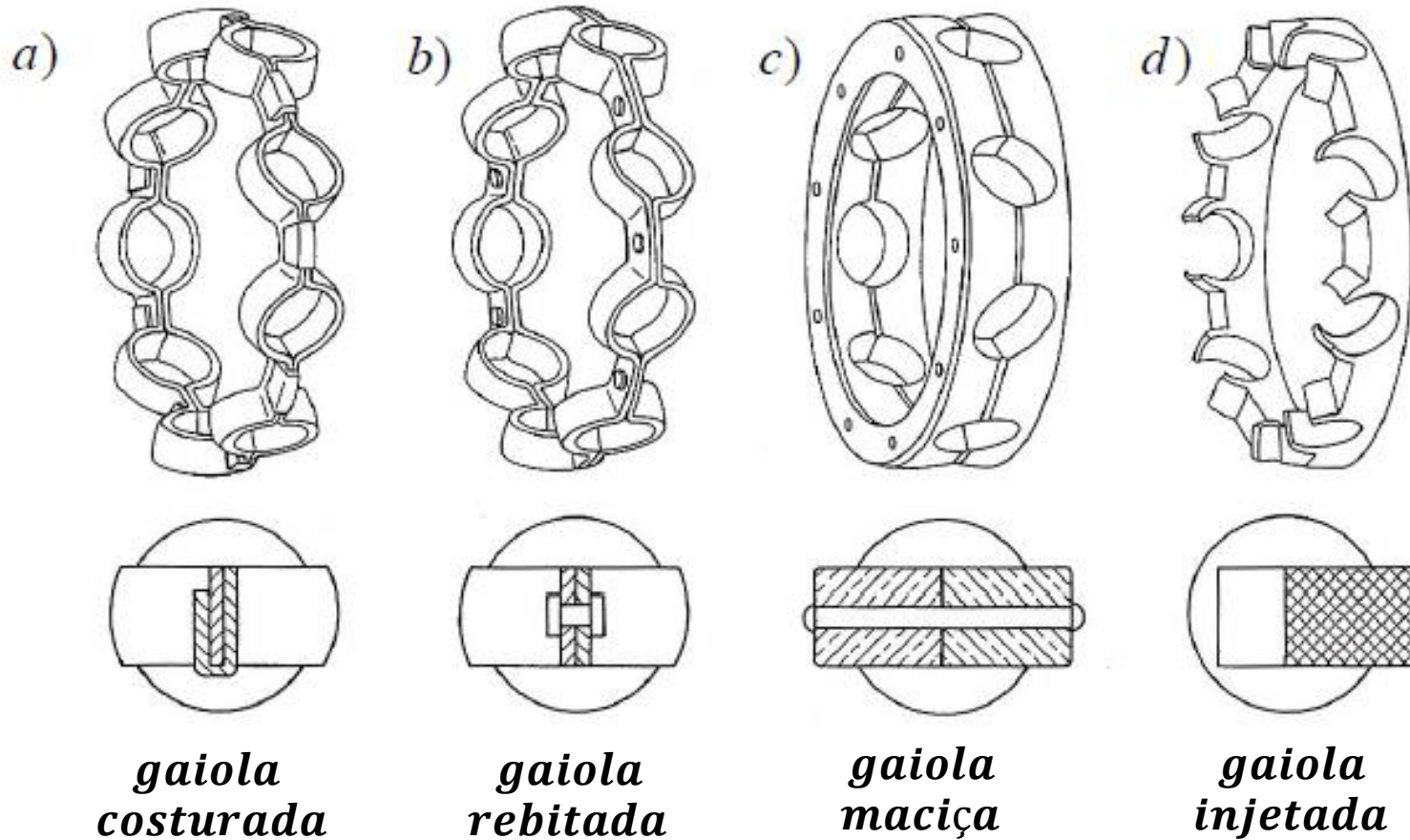
*anel espaçador
ou gaiola*





Mancais de rolamento

Espaçador

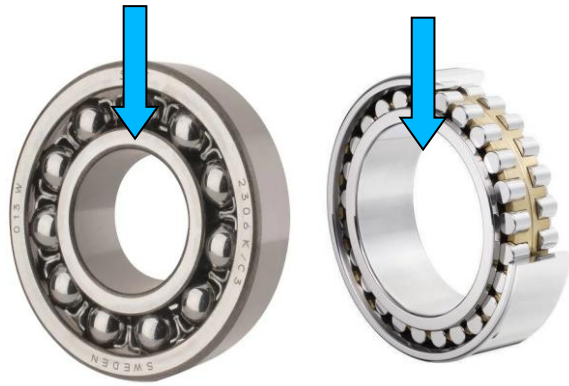




Mancais de rolamento

Carregamentos

Radiais



Axiais



Radiais/Axiais





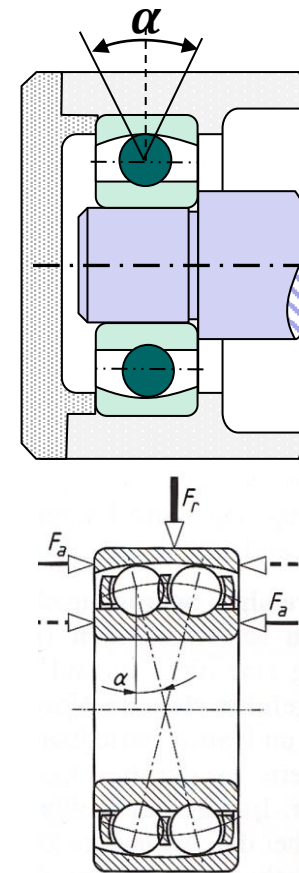
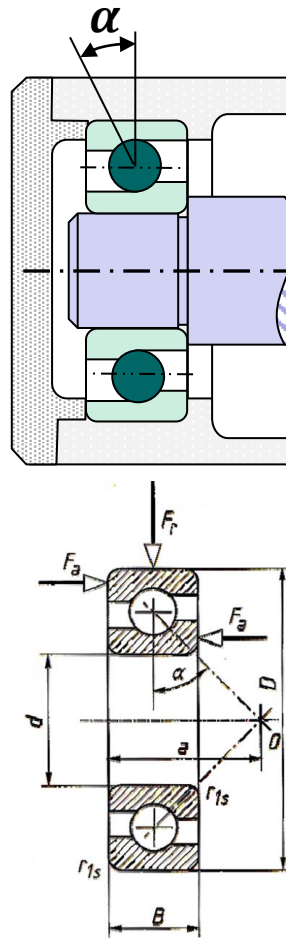
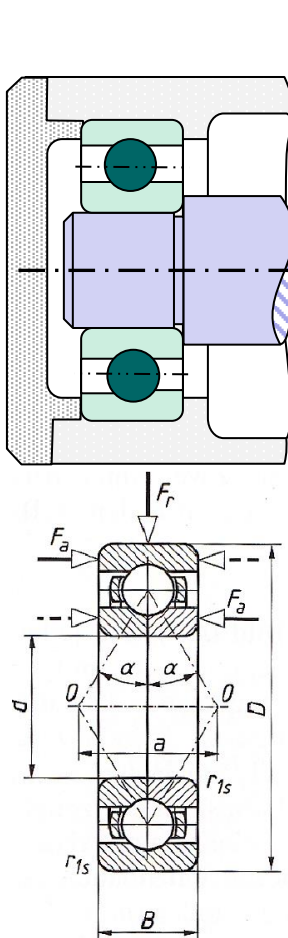
Mancais de rolamento

Radiais de esfera

rígidos

De contato angular

autocompensadores





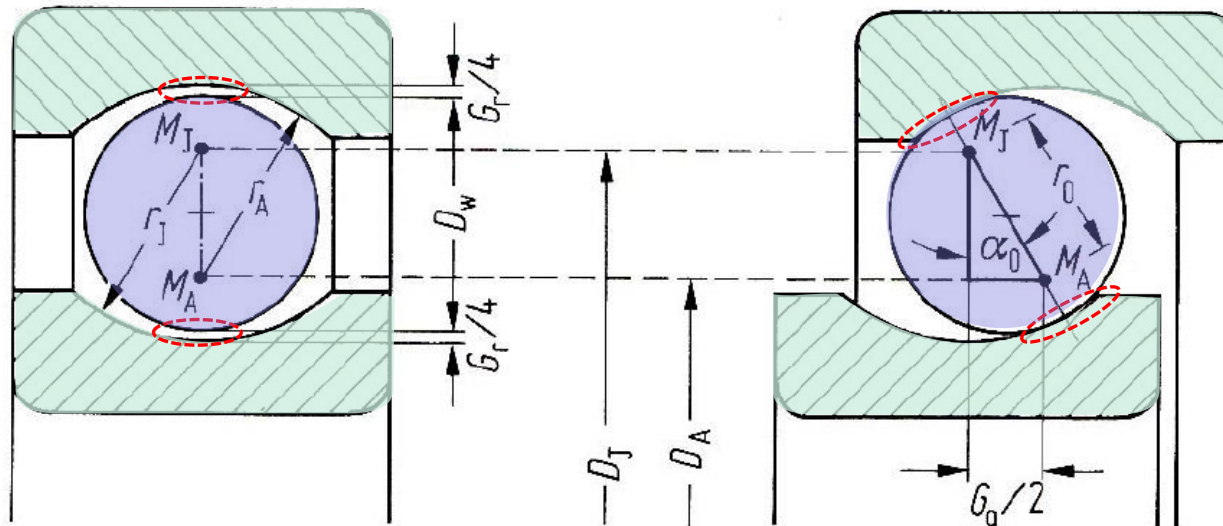
Mancais de rolamento

Radiais de esfera

rígidos



De contato angular

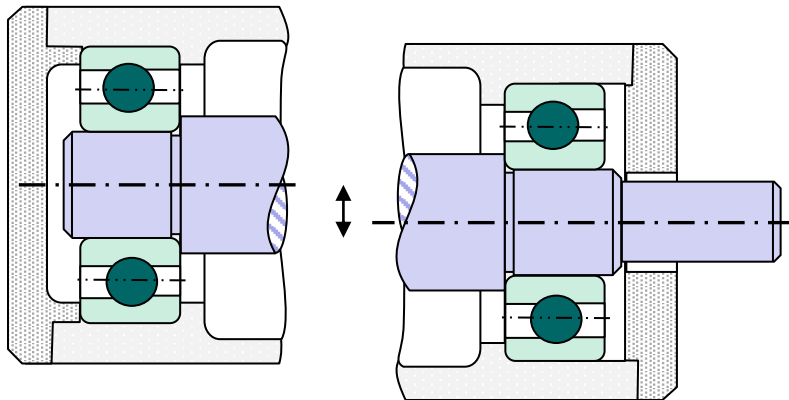




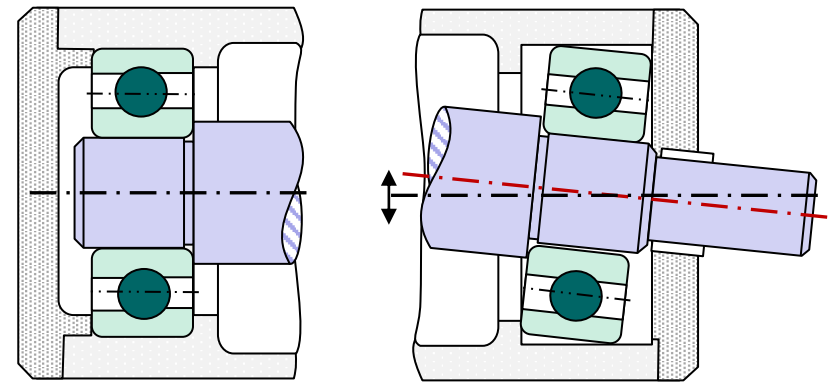
Mancais de rolamento

Quando usar mancais autocompensadores

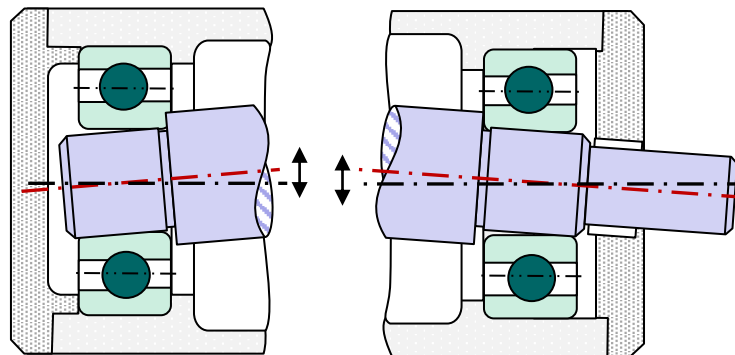
Desalinhamento



Montagem errada



Flexão dos eixos





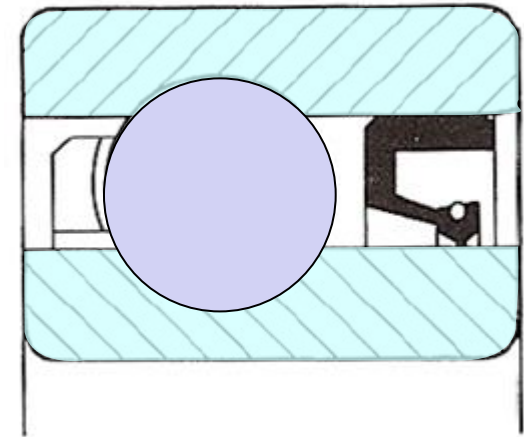
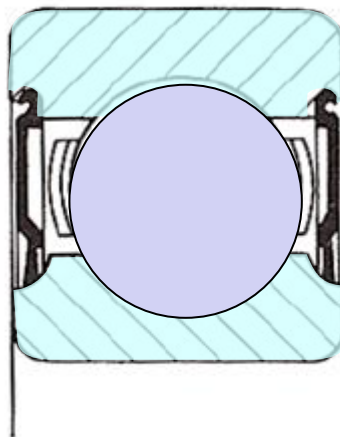
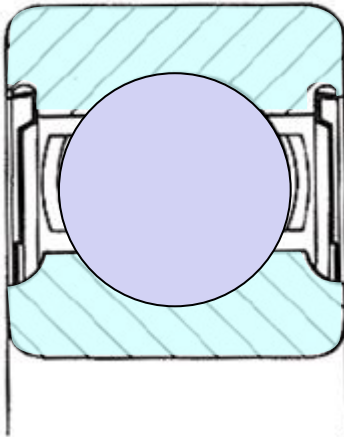
Mancais de rolamento

proteção

vedados

blindados

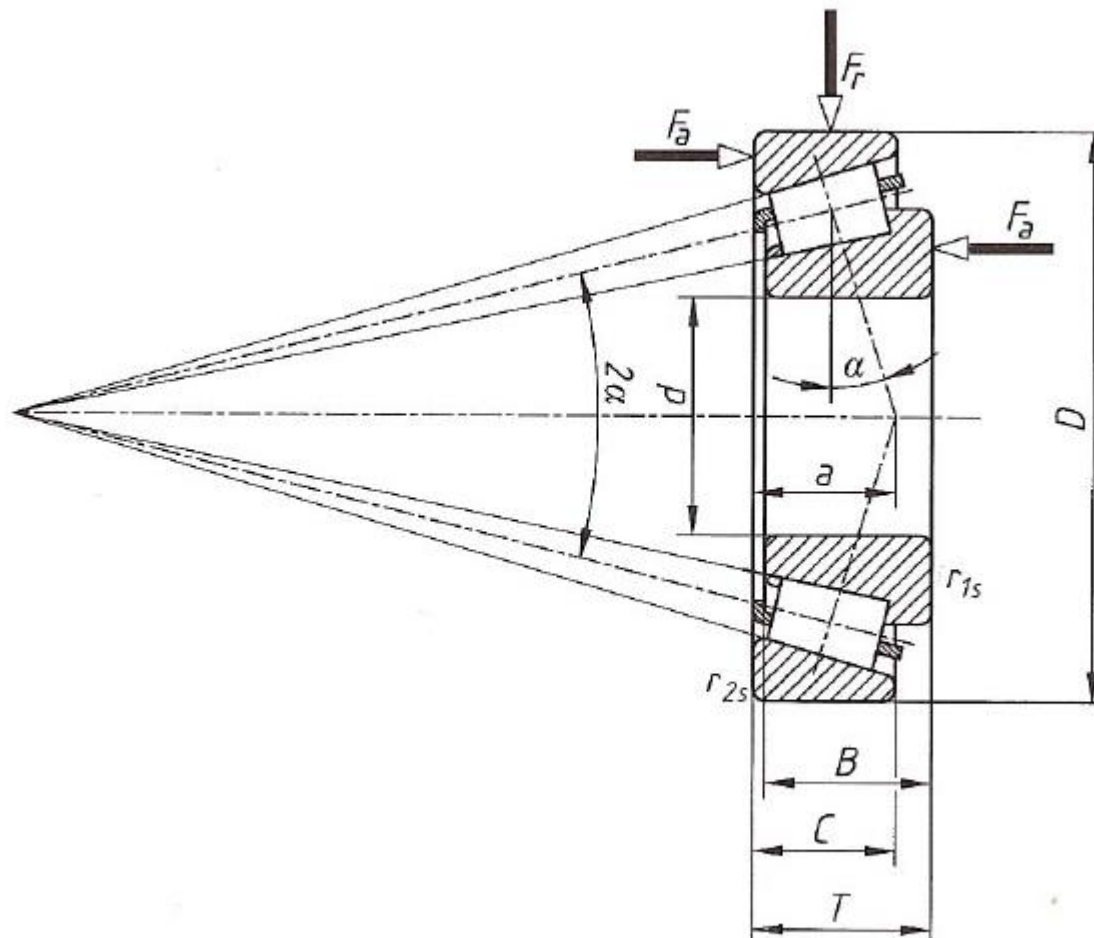
selados





Mancais de rolamento

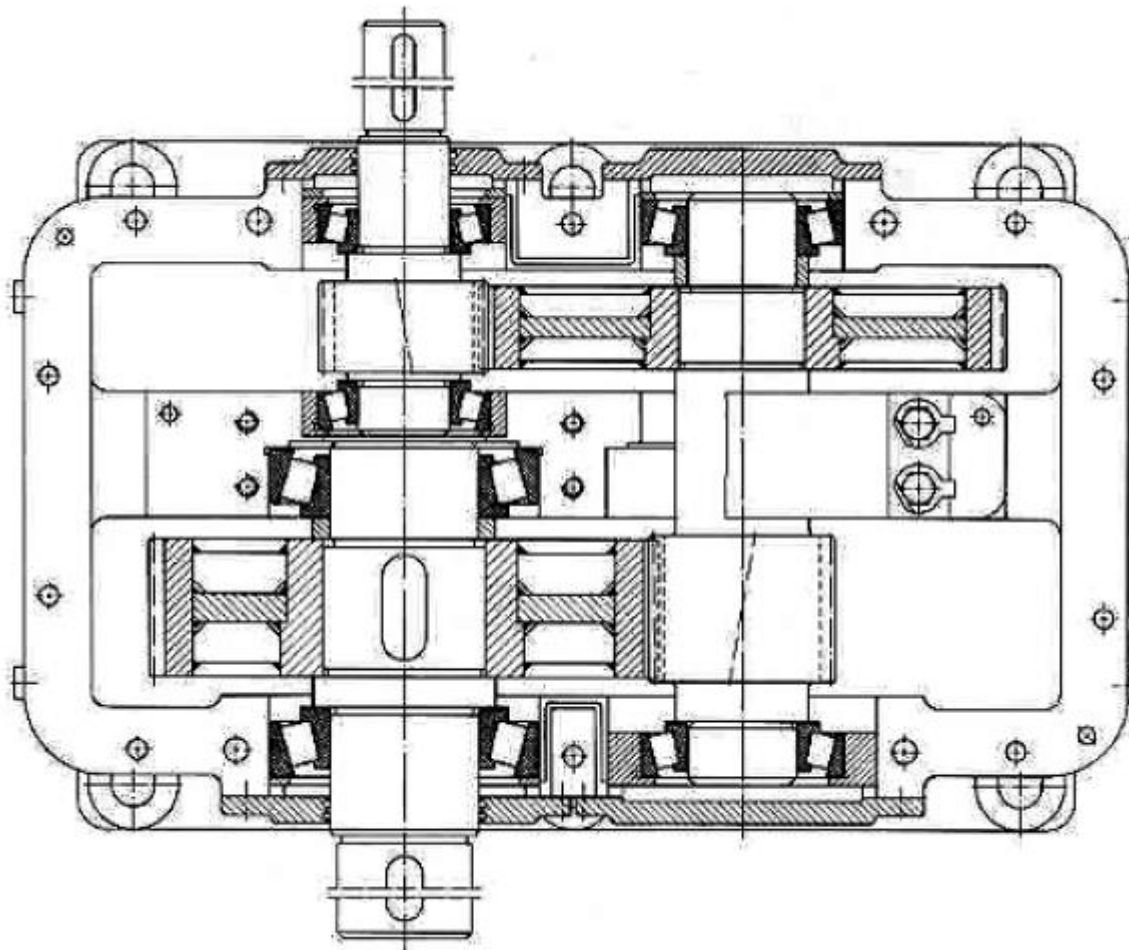
Rolos cônicos





Mancais de rolamento

Exemplo do uso de mancais de rolo cônicos



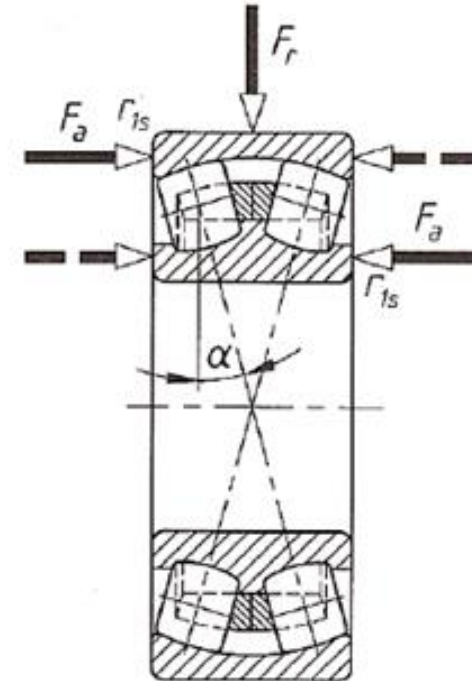
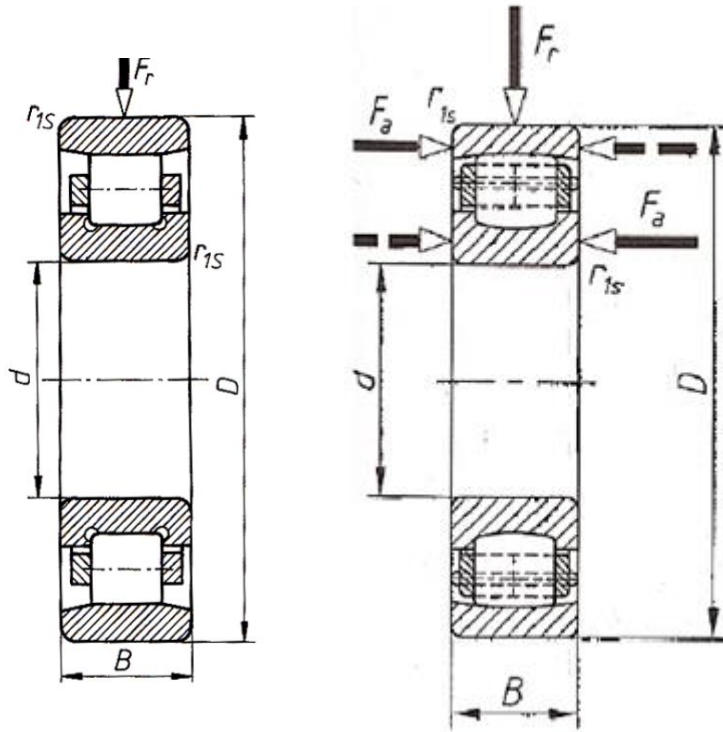


Mancais de rolamento

de rolo radiais

rígidos

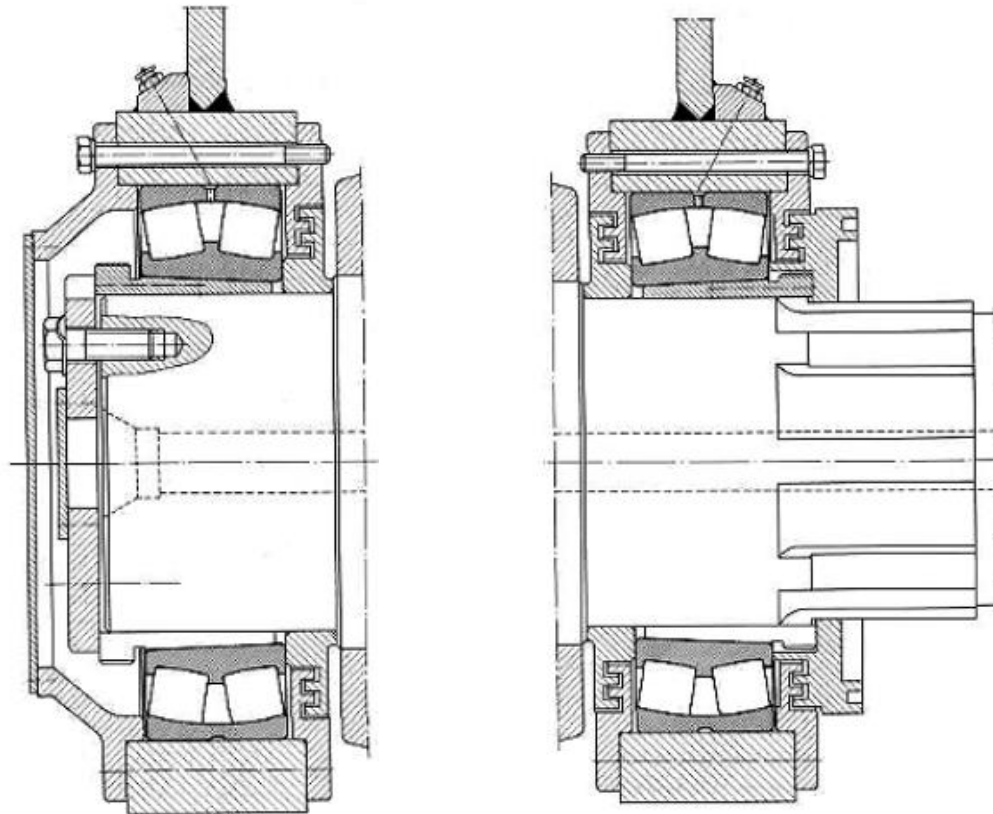
autocompensadores





Mancais de rolamento

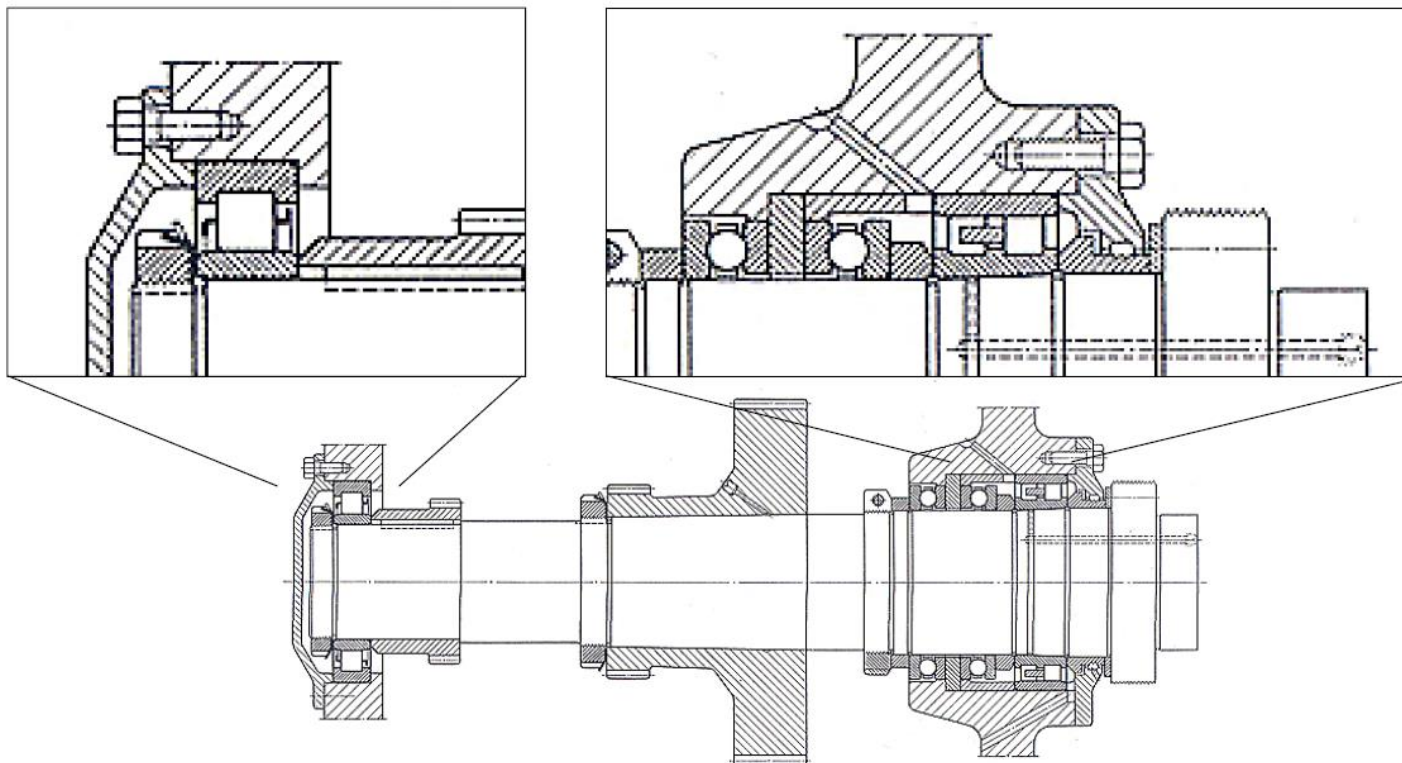
Exemplo do uso de mancais de rolo radiais autocompensadores





Mancais de rolamento

Exemplo do uso de mancais radiais de rolo e de esfera

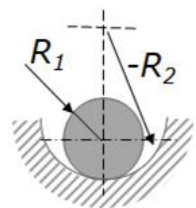
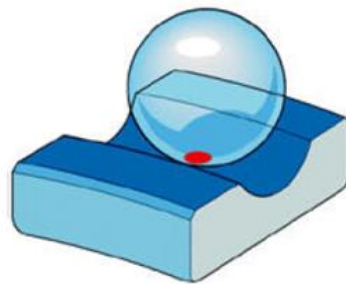




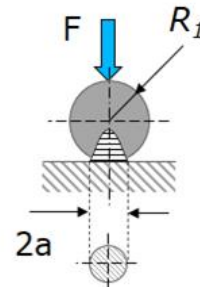
Mancais de rolamento

Classificação quanto a forma do elemento rolante

esféricos



esfera/cilindro



$$D = \frac{2R_1R_2}{R_1 + R_2}$$

Área de contato

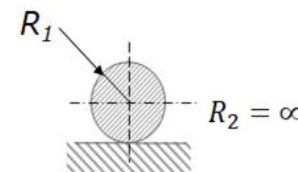
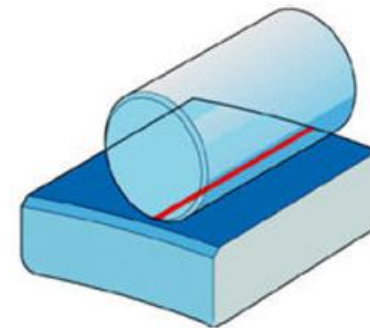
Pressão de contato máxima

$$E = \frac{2E_1E_2}{E_1 + E_2}$$

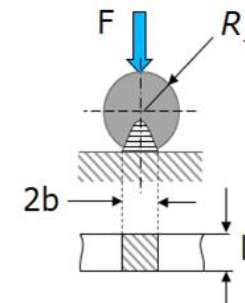
$$a = \sqrt[3]{\frac{0,75 (1 - \nu^2) F D}{E}}$$

$$P_{max} = 1,5 \frac{F}{a^2 \pi}$$

Cilíndricos/cônicos



cilindro/plano



$$E = \frac{2E_1E_2}{E_1 + E_2}$$

Área de contato

Pressão de contato máxima

$$D = \frac{2R_1R_2}{R_1 + R_2}$$

$$b = \sqrt{\frac{4 F D (1 - \nu^2)}{\pi E l}}$$

$$P_{max} = \frac{2F}{\pi b l}$$

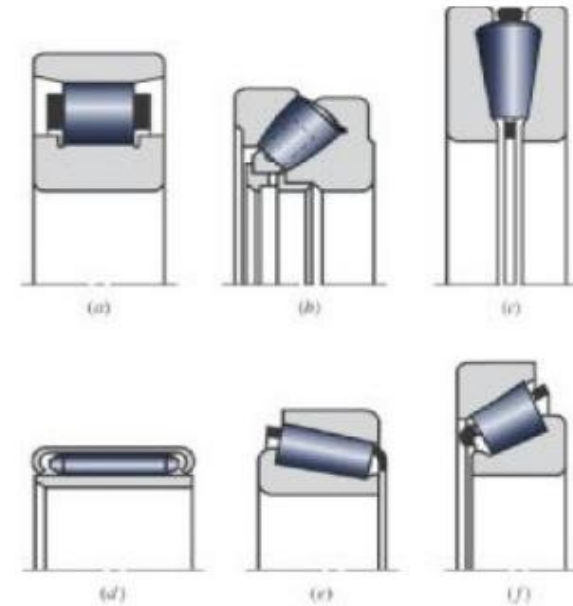
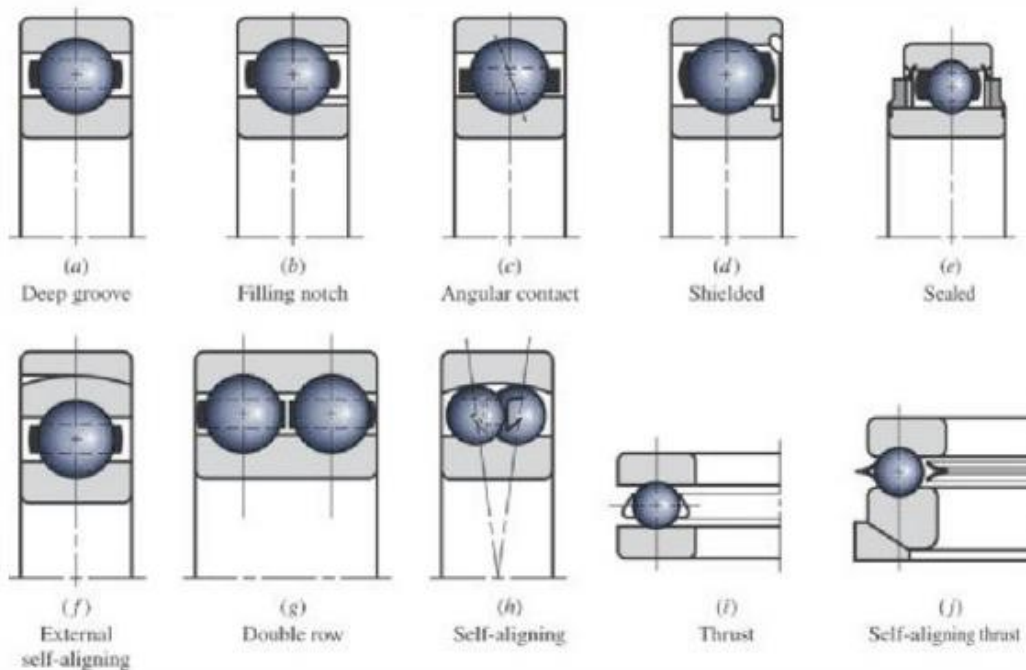


Mancais de rolamento

Tipos de elementos rolante

esféricos

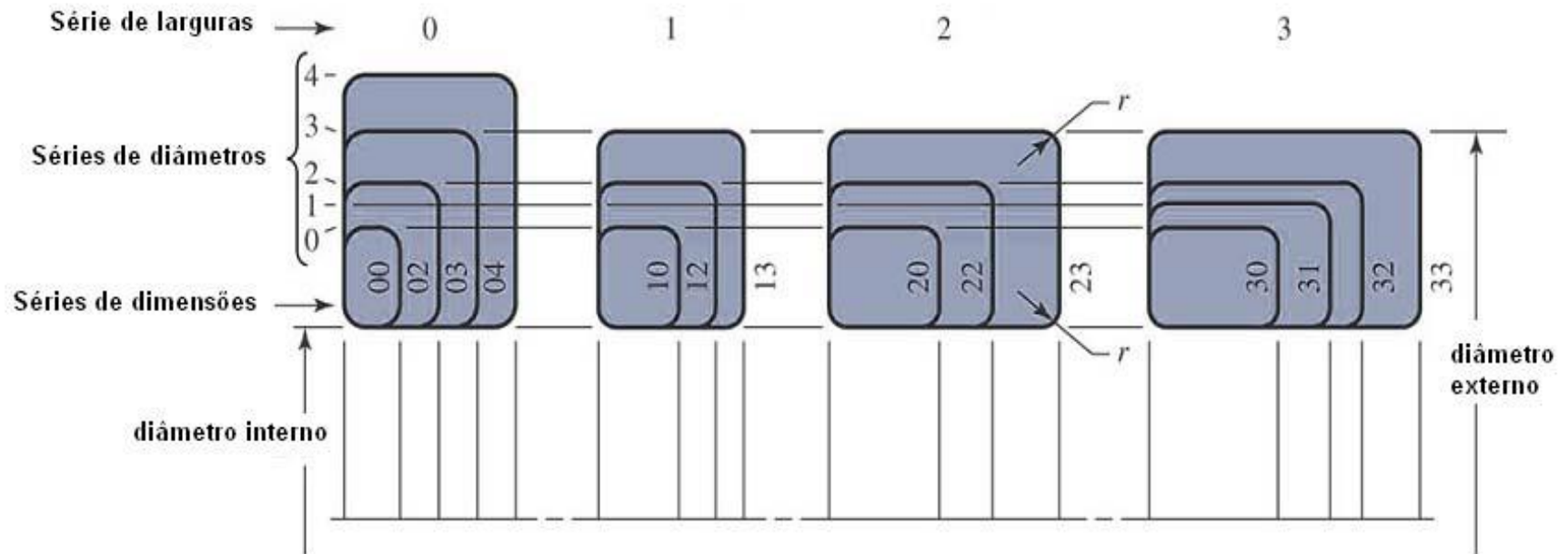
Cilíndricos/cônicos





Mancais de rolamento

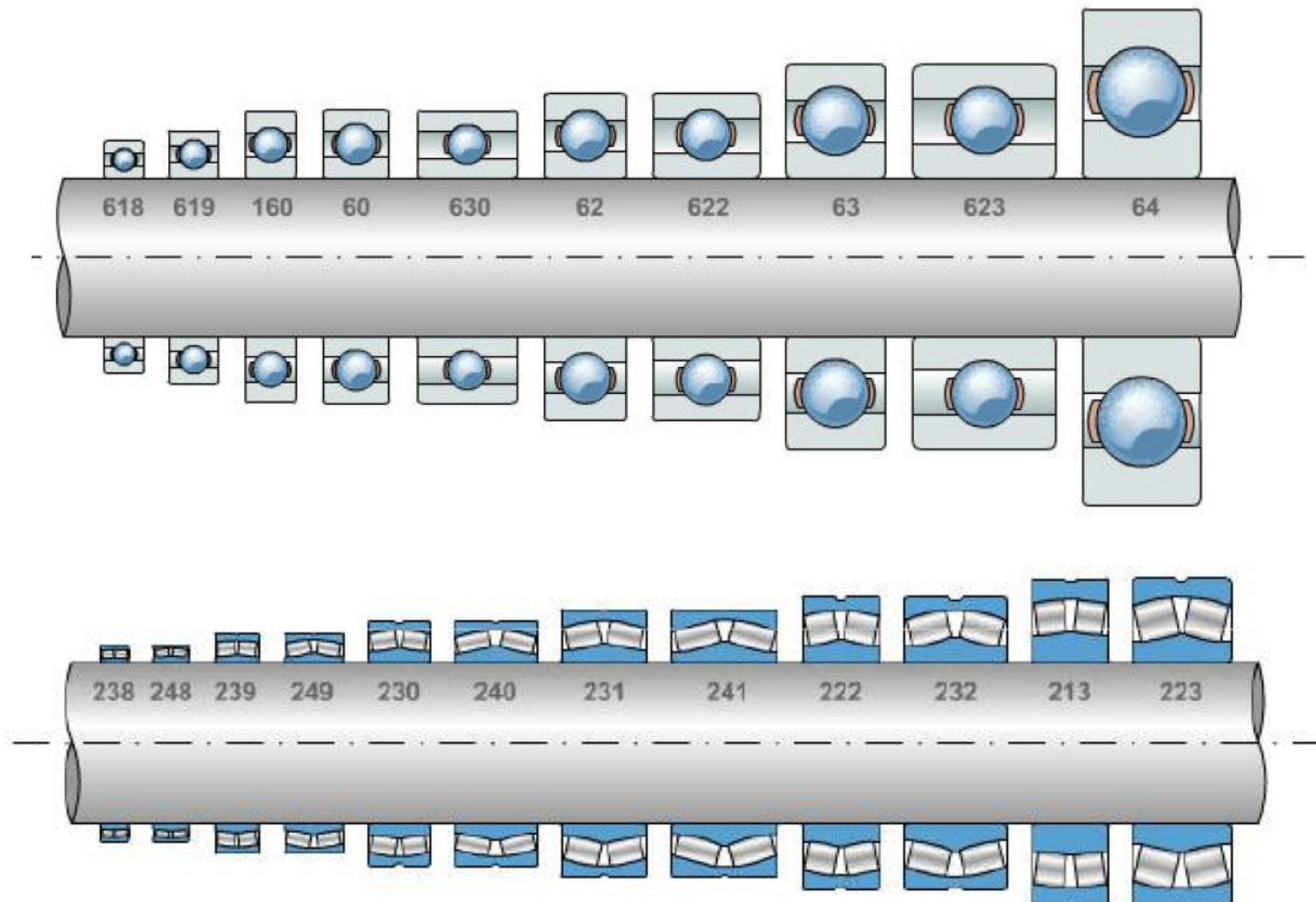
Classes de dimensões





Mancais de rolamento

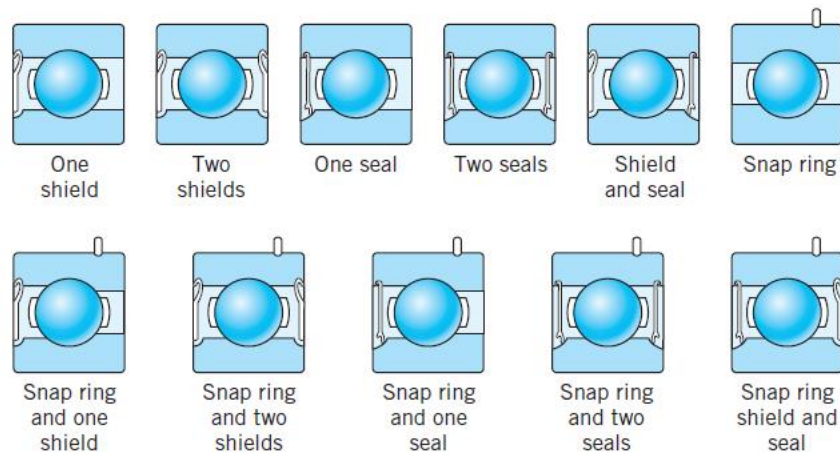
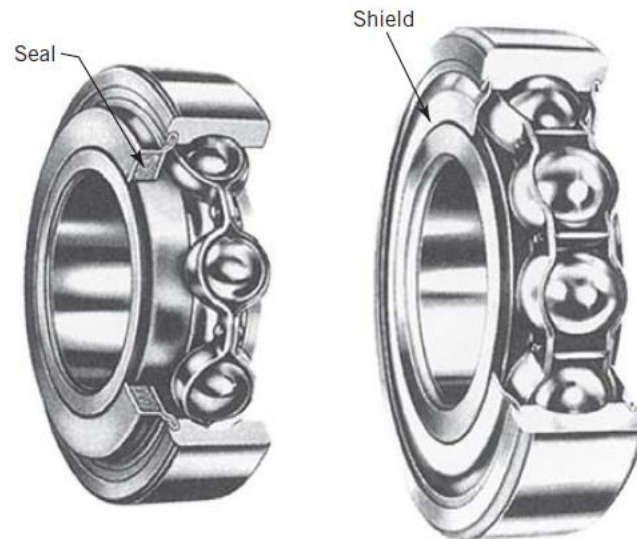
Classes de dimensões





Mancais de rolamento

Classes de dimensões





Mancais de rolamento

Precisão

Tolerâncias geométricas e dimensionais

- › Tolerances for bore and outside diameters, ring and bearing width
- › Tolerances for inscribed and circumscribed circle diameters of rollers
- › Tolerances for chamfer dimensions
- › Tolerances for width variation
- › Tolerances for tapered bore diameters

Precisão de giro (radial e axial)

- › Permissible radial run-out of inner and outer rings
- › Permissible face run-out with raceway inner and outer rings
- › Permissible inner ring face run-out with bore
- › Permissible outer ring variation of outside surface generatrix inclination with face
- › Permissible raceway-to-back-face thickness variation of thrust bearings



Mancais de rolamento

Classes de tolerâncias

ABEC SYSTEM	ISO SYSTEM	DIN SYSTEM
ABEC 1	Normal	P0
ABEC 3	Class 6	P6
ABEC 5	Class 5	P5
ABEC 7	Class 4	P4
ABEC 9	Class 2	P2

System bearing type			Precision bearing class			
Metric	Timken	Tapered roller bearings	C	B	A	AA
		Crossed roller bearings	S	P	–	–
	ISO/DIN	All bearing types	P5	P4	P2	–
	ABMA	Non-tapered roller bearings	RBEC 5	RBEC 7	RBEC 9	–
		Ball bearings	ABEC 5	ABEC 7	ABEC 9	–
		Tapered roller bearings	C	B	A	–



Mancais de rolamento

Classes de tolerâncias

Referenced from ANSI/ABMA Std. 20

Inner Ring: $0.6\text{mm} < d \leq 2.5\text{mm}$

Unit: μm

Grade	Dimensional Difference					Radial Runout	Perpendicularity	Axial Runout	Dimensional Difference of Width		Variation of Width
	Δd_{ep}		Δd_s			K_a	S_a	S_v	ΔB_s		V_{B_s}
	ABEC	High	Low	High	Low	MAX	MAX	MAX	High	Low	MAX
1	0	-8	-	-	-	10	-	15	0	-40	12
3	0	-7	-	-	-	5	-	10	0	-40	12
5	0	-5	-	-	-	4	7	7	0	-40	5
7	0	-4	0	-4	2.5	3	3	3	0	-40	2.5
9	0	-2.5	0	-2.5	1.5	1.5	1.5	1.5	0	-40	1.5

Inner Ring: $2.5\text{mm} < d \leq 10\text{mm}$

Unit: μm

Grade	Dimensional Difference				Radial Runout	Perpendicularity	Axial Runout	Dimensional Difference of Width		Variation of Width	
	Δd_{ep}		Δd_s		K_a	S_a	S_a	ΔB_s		V_{B_s}	
	ABEC	High	Low	High	Low	MAX	MAX	MAX	High	Low	MAX
1	0	-8	-	-	-	10	-	20	0	-120	15
3	0	-7	-	-	-	6	-	15	0	-120	15
5	0	-5	-	-	-	4	7	7	0	-40	5
7	0	-4	0	-4	2.5	3	3	3	0	-40	2.5
9	0	-2.5	0	-2.5	1.5	1.5	1.5	0	-40	1.5	

Inner Ring: $10\text{mm} < d \leq 18\text{mm}$

Unit: μm

Grade	Dimensional Difference					Radial Runout	Perpendicularity	Axial Runout	Dimensional Difference of Width		Variation of Width
	Δd_{ep}		Δd_s			K_a	S_a	S_a	ΔB_s		V_{B_s}
	ABEC	High	Low	High	Low	MAX	MAX	MAX	High	Low	MAX
1	0	-8	-	-	-	10	-	20	0	-120	20
3	0	-7	-	-	-	7	-	20	0	-120	20
5	0	-5	-	-	-	4	7	7	0	-80	5
7	0	-4	0	-4	2.5	3	3	3	0	-80	2.5
9	0	-2.5	0	-2.5	1.5	1.5	1.5	1.5	0	-80	1.5

Referenced from ANSI/ABMA Std. 20.0

Outer Ring: $2.5\text{mm} < D \leq 6\text{mm}$

Unit: μm

Grade	Dimensional Difference					Radial Runout	Perpendicularity	Axial Runout	Dimensional Difference of Width		Variation of Width
	ΔD_{ep}		ΔD_s			$K_{..}$	S_o	$S_{..}$	ΔC_s		V_{cs}
	ABEC	High	Low	High	Low	MAX	MAX	MAX	High	Low	MAX
1	0	-8	-	-	15	-	15	0	-40	12	
3	0	-7	-	-	8	-	10	0	-40	12	
5	0	-5	-	-	5	8	8	0	-40	5	
7	0	-4	0	-4	3	4	5	0	-40	2.5	
9	0	-2.5	0	-2.5	1.5	1.5	1.5	0	-40	1.5	

Outer Ring: $6\text{mm} < D \leq 18\text{mm}$

Unit: μm

Grade	Dimensional Difference					Radial Runout	Perpendicularity	Axial Runout	Dimensional Difference of Width		Variation of Width
	ΔD_{ep}		ΔD_s			K_a	S_a	S_{as}	ΔC_s		V_{cs}
	ABEC	High	Low	High	Low	MAX	MAX	MAX	High	Low	MAX
1	0	-8	-	-	15	-	20	0	-120	15	
3	0	-7	-	-	8	-	15	0	-120	15	
5	0	-5	-	-	5	8	8	0	-40	5	
7	0	-4	0	-4	3	4	5	0	-40	2.5	
9	0	-2.5	0	-2.5	1.5	1.5	1.5	0	-40	1.5	

Outer Ring: $18\text{mm} < D \leq 30\text{mm}$

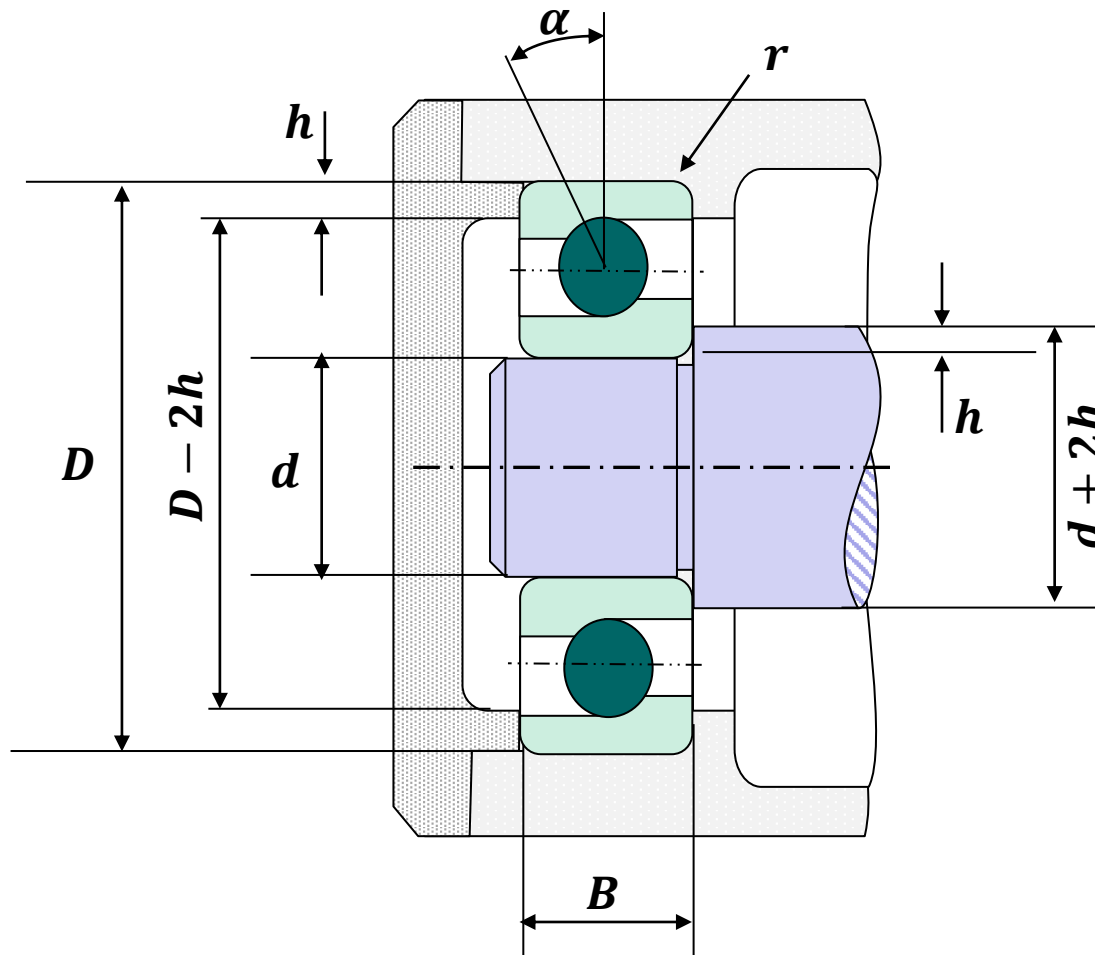
Unit: μm

Grade	Dimensional Difference				Radial Runout	Perpendicularity	Axial Runout	Dimensional Difference of Width		Variation of Width	
	ΔD_{av}		ΔD_s		K_{ss}	S_0	S_{ss}	ΔC_s		V_{ss}	
	ABEC	High	Low	High	Low	MAX	MAX	MAX	High	Low	MAX
1	0	-9	-	-	-	15	-	25	0	-120	20
3	0	-8	-	-	-	9	-	15	0	-120	20
5	0	-6	-	-	-	6	8	8	0	-80	5
7	0	-5	0	-5	4	4	5	5	0	-80	2.5
9	0	-4	0	-4	2.5	1.5	2.5	0	-80	1.5	



Mancais de rolamento

Dimensionamento





Mancais de rolamento

Dimensionamento

$$L = L_R \left(\frac{C}{F_r} \right)^{3,33}$$

capacidade nominal

Vida correspondente a 9×10^6 rotações

Vida correspondente ao carregamento radial F_r

$$C_{req} = F_R \left(\frac{L}{L_r} \right)^{0,3}$$

Capacidade nominal corrigida em função da aplicação



Mancais de rolamento

Dimensionamento

Bearing Rated Capacities, C , for $L_R = 90 \times 10^6$
 Revolution Life with 90 Percent Reliability

Bore (mm)	Radial Ball, $\alpha = 0^\circ$			Angular Ball, $\alpha = 25^\circ$			Roller			Bore (mm)	Radial Ball, $\alpha = 0^\circ$			Angular Ball, $\alpha = 25^\circ$			Roller		
	L00 Xlt (kN)	200 lt (kN)	300 med (kN)	L00 Xlt (kN)	200 lt (kN)	300 med (kN)	1000 Xlt (kN)	1200 lt (kN)	1300 med (kN)		L00 Xlt (kN)	200 lt (kN)	300 med (kN)	L00 Xlt (kN)	200 lt (kN)	300 med (kN)	1000 Xlt (kN)	1200 lt (kN)	1300 med (kN)
10	1.02	1.42	1.90	1.02	1.10	1.88				80	14.2	18.4	28.0	16.6	22.5	35.5	17.3	26.2	51.6
12	1.12	1.42	2.46	1.10	1.54	2.05				85	15.0	22.5	30.0	17.2	26.5	38.5	18.0	30.7	55.2
15	1.22	1.56	3.05	1.28	1.66	2.85				90	17.2	25.0	32.5	20.0	28.0	41.5		37.4	65.8
17	1.32	2.70	3.75	1.36	2.20	3.55	2.12	3.80	4.90	95	18.0	27.5	38.0	21.0	31.0	45.5		44.0	65.8
20	2.25	3.35	5.30	2.20	3.05	5.80	3.30	4.40	6.20	100	18.0	30.5	40.5	21.5	34.5		20.9	48.0	72.9
25	2.45	3.65	5.90	2.65	3.25	7.20	3.70	5.50	8.50	105	21.0	32.0	43.5	24.5	37.5			49.8	84.5
30	3.35	5.40	8.80	3.60	6.00	8.80	2.40 ^a	8.30	10.0	110	23.5	35.0	46.0	27.5	41.0	55.0	29.4	54.3	85.4
35	4.20	8.50	10.6	4.75	8.20	11.0	3.10 ^a	9.30	13.1	120	24.5	37.5		28.5	44.5			61.4	100.1
40	4.50	9.40	12.6	4.95	9.90	13.2	7.20	11.1	16.5	130	29.5	41.0		33.5	48.0	71.0	48.9	69.4	120.1
45	5.80	9.10	14.8	6.30	10.4	16.4	7.40	12.2	20.9	140	30.5	47.5		35.0	56.0			77.4	131.2
50	6.10	9.70	15.8	6.60	11.0	19.2	5.10 ^a	12.5	24.5	150	34.5			39.0	62.0		58.7	83.6	
55	8.20	12.0	18.0	9.00	13.6	21.5	11.3	14.9	27.1	160								113.4	
60	8.70	13.6	20.0	9.70	16.4	24.0	12.0	18.9	32.5	180	47.0			54.0			97.9	140.1	
65	9.10	16.0	22.0	10.2	19.2	26.5	12.2	21.1	38.3	200								162.4	
70	11.6	17.0	24.5	13.4	19.2	29.5		23.6	44.0	220								211.3	
75	12.2	17.0	25.5	13.8	20.0	32.5		23.6	45.4	240								258.0	



Mancais de rolamento

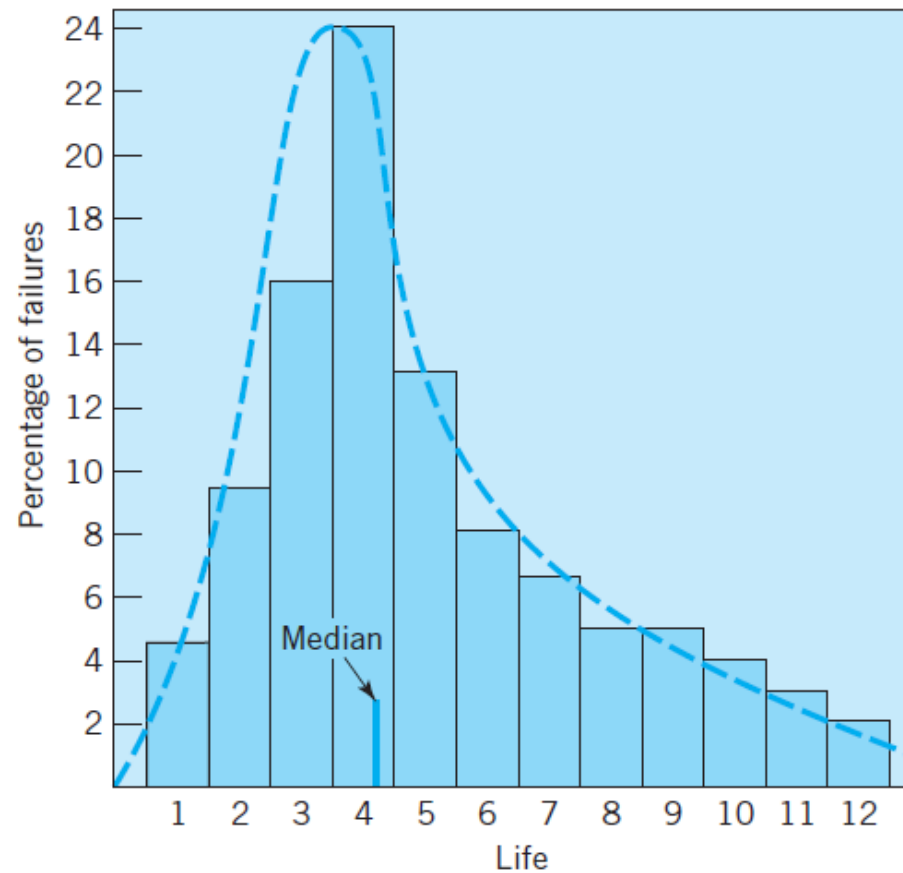
Dimensionamento

- A vida padrão é comumente designada como a vida L_{10} .
- A vida L_{10} corresponde a uma probabilidade de falha de 10%, isso representa que 90% dos rolamentos não falharam quando essa vida é atingida, correspondendo a 90% de confiabilidade
- Os testes mostram que a vida média de rolamentos (rolamentos de esferas em particular) é cerca de cinco vezes a vida de fadiga padrão para L_{10}
- Muitos projetos exigem mais de 90% de confiabilidade
- A probabilidade de falha de mancais de elementos rolantes não segue uma distribuição gaussiana, mas sim uma distribuição de Weibull
- Isso leva a necessidade do ajuste da curva de vida por meio do fator de confiabilidade K_r



Mancais de rolamento

Dimensionamento

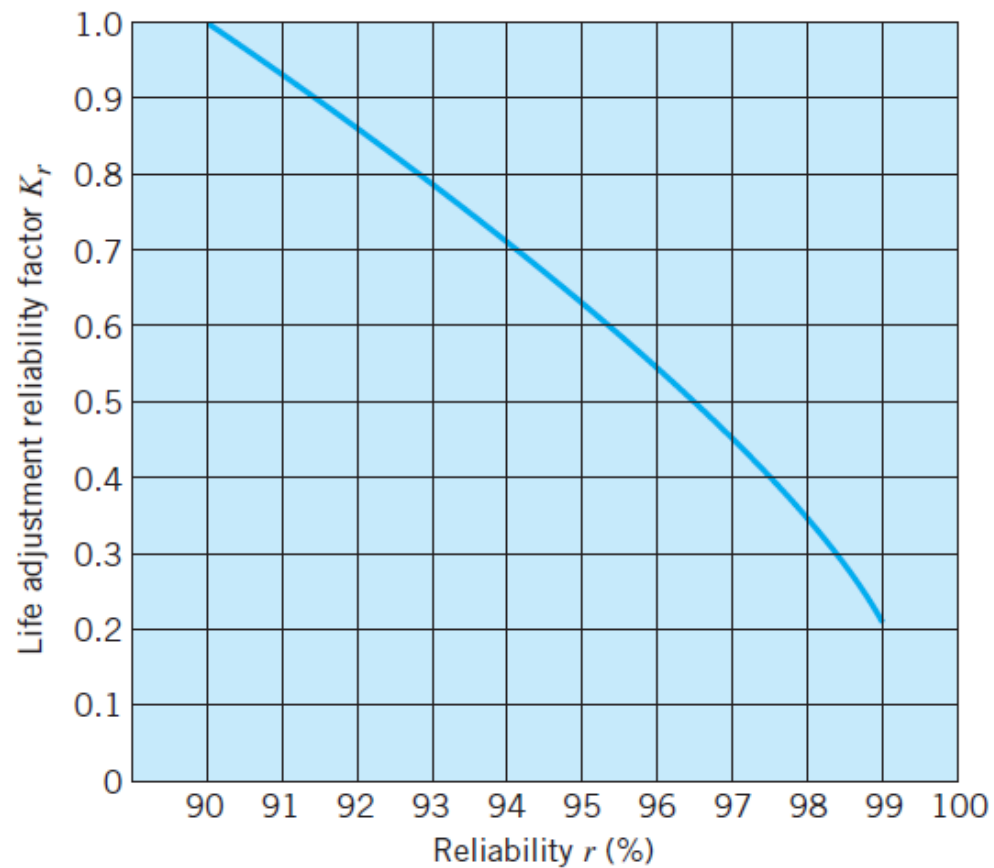


Distribuição de Weibull para vida em fadiga de mancais de elementos rolantes



Mancais de rolamento

Dimensionamento



Fator de confiabilidade K_r



Mancais de rolamento

Dimensionamento

corrigindo L_r e C_{req} em termos de K_r , temos $\Rightarrow$

$$L = L_R \left(\frac{C}{F_r} \right)^{3,33}$$



$$L = K_r L_R \left(\frac{C}{F_r} \right)^{3,33}$$

$$C_{req} = F_R \left(\frac{L}{L_r} \right)^{0,3}$$



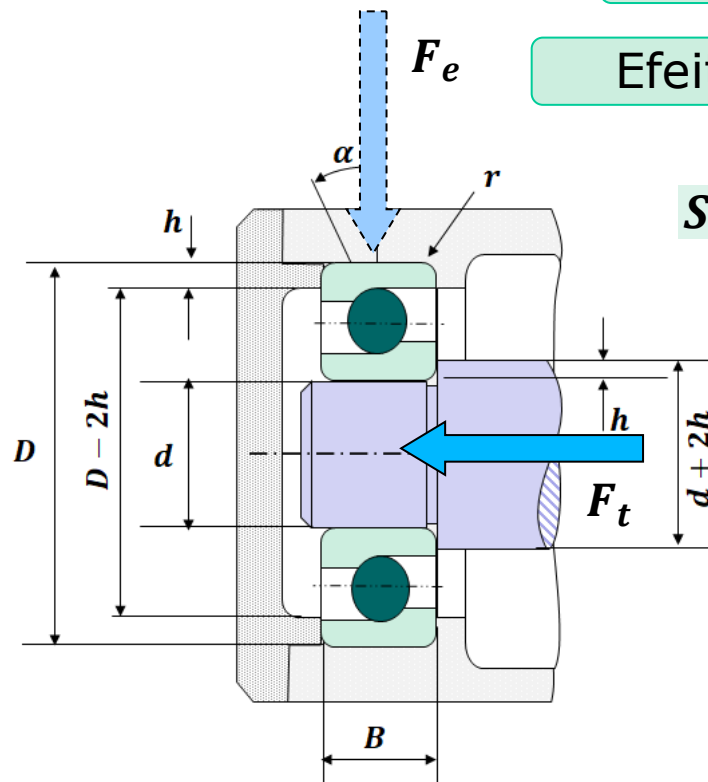
$$C_{req} = F_R \left(\frac{L}{K_r \cdot L_r} \right)^{0,3}$$



Mancais de rolamento

Dimensionamento

Efeito do carregamento axial



Sendo F_e o carregamento radial equivalente

para mancais rígidos de esfera $\Rightarrow \alpha = 0^\circ$

para: $0 < F_t/F_r < 0.35$, $F_e = F_r$

para: $0.35 < F_t/F_r < 10$, $F_e = F_r \left[1 + 1.115 \left(\frac{F_t}{F_r} - 0.35 \right) \right]$

para: $F_t/F_r > 10$, $F_e = 1.176 F_t$

para mancais de contato angular $\Rightarrow \alpha = 25^\circ$

para: $0 < F_t/F_r < 0.68$, $F_e = F_r$

para: $0.68 < F_t/F_r < 10$, $F_e = F_r \left[1 + 0.870 \left(\frac{F_t}{F_r} - 0.68 \right) \right]$

para: $F_t/F_r > 10$, $F_e = 0.911 F_t$



Mancais de rolamento

Dimensionamento

Efeito de choques e impactos

- O dimensionamento de mancais de elementos rolantes em geral é feito para condições de carregamento uniforme.
- Na presença de choques ou impactos, o fator K_a deve ser aplicado para corrigir a vida

Factors K_a

Type of Application	Ball Bearing	Roller Bearing
Uniform load, no impact	1.0	1.0
Gearing	1.0–1.3	1.0
Light impact	1.2–1.5	1.0–1.1
Moderate impact	1.5–2.0	1.1–1.5
Heavy impact	2.0–3.0	1.5–2.0



Mancais de rolamento

Dimensionamento

corrigindo L_r em termos de K_a ,

e expressando o carregamento em termos de F_e temos $\Rightarrow$

$$L = K_r L_R \left(\frac{C}{F_r} \right)^{3,33}$$



$$L = K_r L_R \left(\frac{C}{K_a \cdot F_e} \right)^{3,33}$$

$$C_{req} = F_R \left(\frac{L}{K_r \cdot L_r} \right)^{0,3}$$



$$C_{req} = K_a \cdot F_e \left(\frac{L}{K_r \cdot L_r} \right)^{0,3}$$



Mancais de rolamento

Dimensionamento

Representative Bearing Design Lives

Type of Application	Design Life (thousands of hours)
Instruments and apparatus for infrequent use	0.1–0.5
Machines used intermittently, where service interruption is of minor importance	4–8
Machines intermittently used, where reliability is of great importance	8–14
Machines for 8-hour service, but not every day	14–20
Machines for 8-hour service, every working day	20–30
Machines for continuous 24-hour service	50–60
Machines for continuous 24-hour service where reliability is of extreme importance	100–200

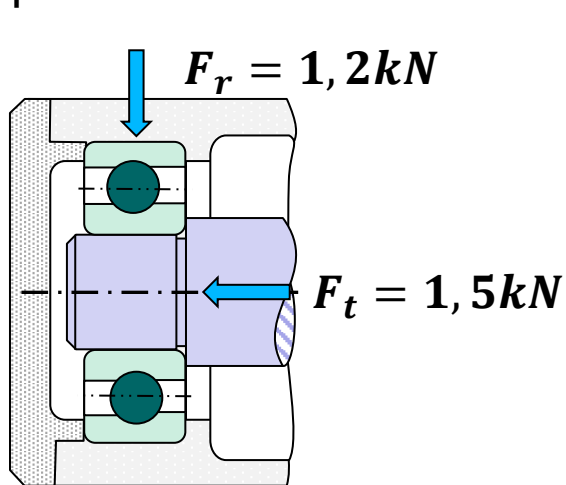


Mancais de rolamento

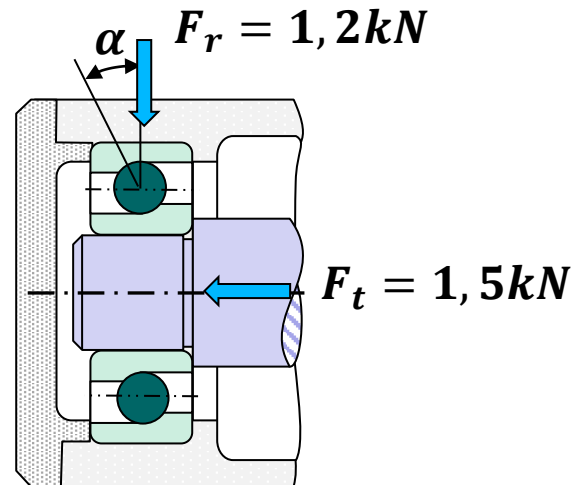
Exemplo

Selecione um rolamento de esferas para uso no eixo de um prensa industrial. A prensa operará de forma contínua em um turno de 8h/dia a 1800 rpm.

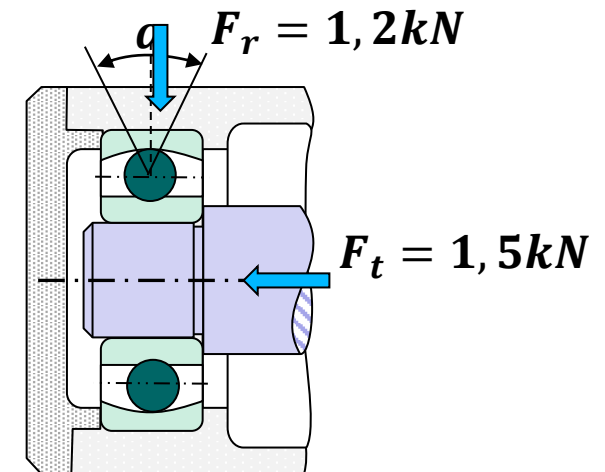
Cargas radiais e axiais são 1,2kN e 1,5kN, respectivamente, com impacto leve a moderado.



rolamento rígido
de esferas



rolamento de
contato angular

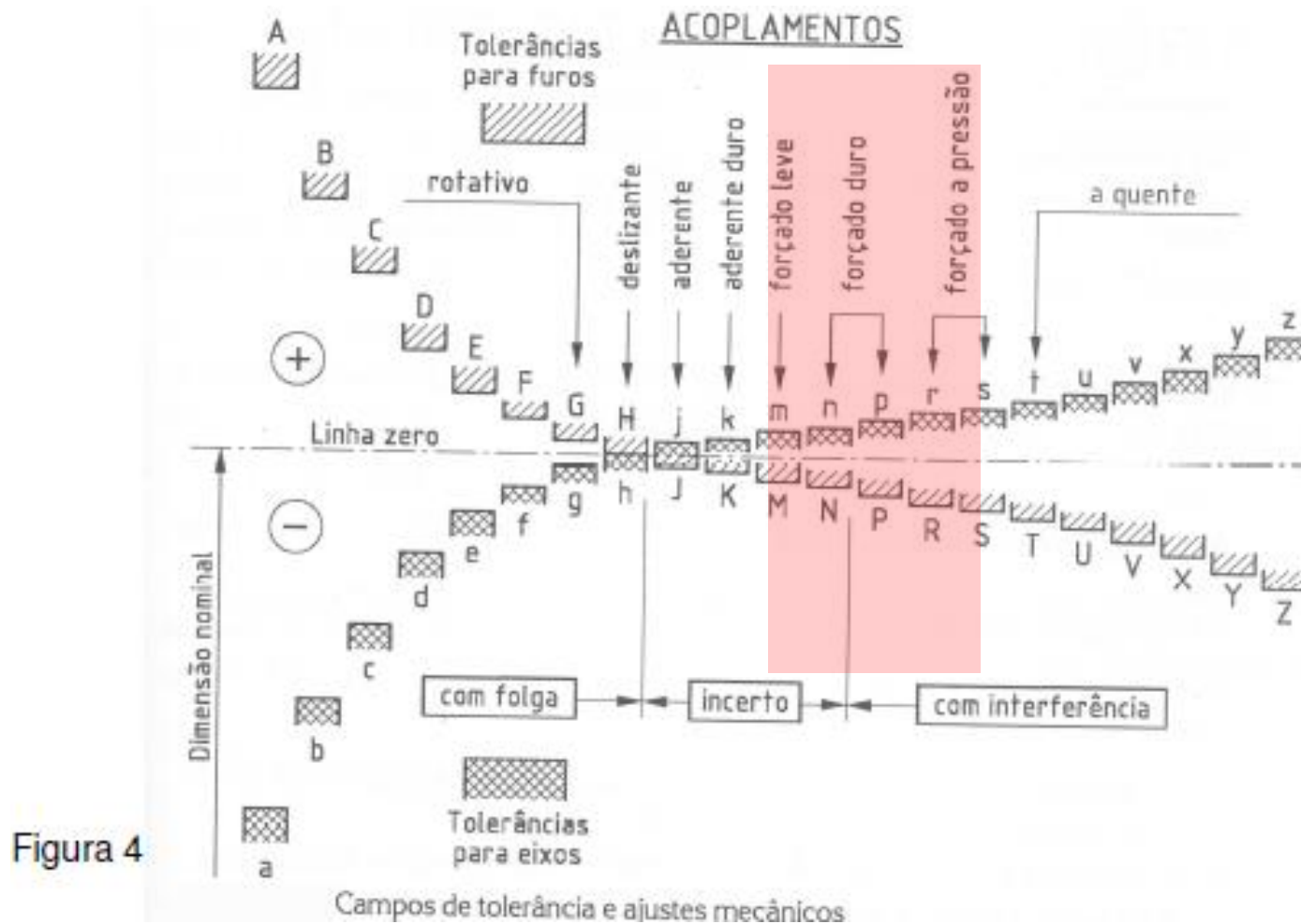


rolamento
autocompensador



Mancais de rolamento

Exemplo





Mancais de rolamento

Exemplo

Premissas básicas:

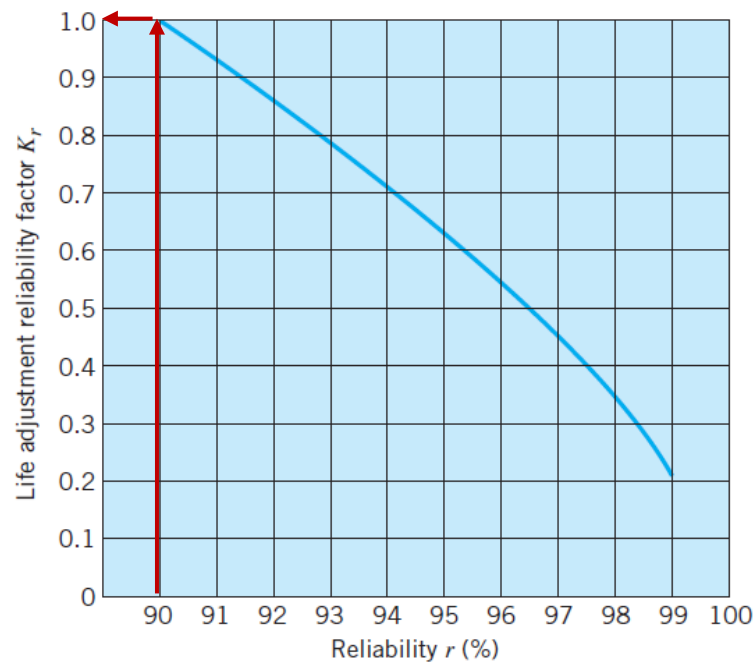
- Projeto conservador para impacto leve a moderado.
- É necessária uma vida útil de projeto de 8 horas por dia de serviço contínuo.
- É necessária uma confiabilidade de 90%
- Tanto um rolamento de esferas radial quanto um angular podem ser selecionado. Um rolamento autocompensador vai depender da amplitude da flexão na ponta do eixo.
- A vida do rolamento de esferas varia inversamente com a potência da carga
- O ajuste prensado não afeta a vida útil do rolamento.



Mancais de rolamento

Exemplo

Fator de confiabilidade K_r



$$K_r = 1$$

Fator de impacto K_a $K_a = 1,5$

Factors K_a

Type of Application	Ball Bearing	Roller Bearing
Uniform load, no impact	1.0	1.0
Gearing	1.0–1.3	1.0
Light impact	1.2–1.5	1.0–1.1
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Representative Bearing Design Lives

Type of Application	Design Life (thousands of hours)
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Machines for 8-hour service, every working day	20–30
Machines for continuous 24-hour service	50–60
Machines for continuous 24-hour service where reliability is of extreme importance	100–200

$$L_r = 30 \times 10^3 \text{ horas}$$



Mancais de rolamento

Exemplo

Calculando o carregamento radial equivalente F_e

$$\begin{aligned} F_r &= 1,2 \text{ kN} & \frac{F_t}{F_r} &= \frac{1,5}{1,2} = 1,25 \\ F_t &= 1,5 \text{ kN} \end{aligned}$$

para mancais rígidos de esfera $\Rightarrow \alpha = 0^\circ$

para: $0 < F_t/F_r < 0,35$, $F_e = F_r$

para: $0,35 < F_t/F_r < 10$, $F_e = F_r \left[1 + 1,115 \left(\frac{F_t}{F_r} - 0,35 \right) \right]$

para: $F_t/F_r > 10$, $F_e = 1,176 F_t$

$$F_e = F_r \left[1 + 1,115 \left(\frac{F_t}{F_r} - 0,35 \right) \right]$$

$$F_{e_{esf}} = 2,4 \text{ kN}$$

para mancais de contato angular $\Rightarrow \alpha = 25^\circ$

para: $0 < F_t/F_r < 0,68$, $F_e = F_r$

para: $0,68 < F_t/F_r < 10$, $F_e = F_r \left[1 + 0,870 \left(\frac{F_t}{F_r} - 0,68 \right) \right]$

para: $F_t/F_r > 10$, $F_e = 0,911 F_t$

$$F_e = F_r \left[1 + 0,870 \left(\frac{F_t}{F_r} - 0,68 \right) \right]$$

$$F_{e_{cont}} = 1,8 \text{ kN}$$



Mancais de rolamento

Exemplo

$$K_r = 1$$

$$K_a = 1,5$$

$$L_r = 30 \times 10^3$$

$$C_{req} = K_a \cdot F_e \left(\frac{L}{K_r \cdot L_r} \right)^{0,3}$$

$$Vida L em [rpm] = n \cdot L_r [min]$$

$$L = 1800 rpm \cdot 30 \times 10^3 h \cdot 60 min/h$$

$$L = 3240 \times 10^6 \text{ revoluções}$$

$$F_{esf} = 2,4 \text{ kN}$$

$$F_{cont} = 1,8 \text{ kN}$$

$$C_{req_{esf}} = 10,55 \text{ kN}$$

$$C_{req_{cont}} = 7,91 \text{ N}$$



Mancais de rolamento

Exemplo

Bearing Rated Capacities, C , for $L_R = 90 \times 10^6$

Revolution Life with 90 Percent Reliability

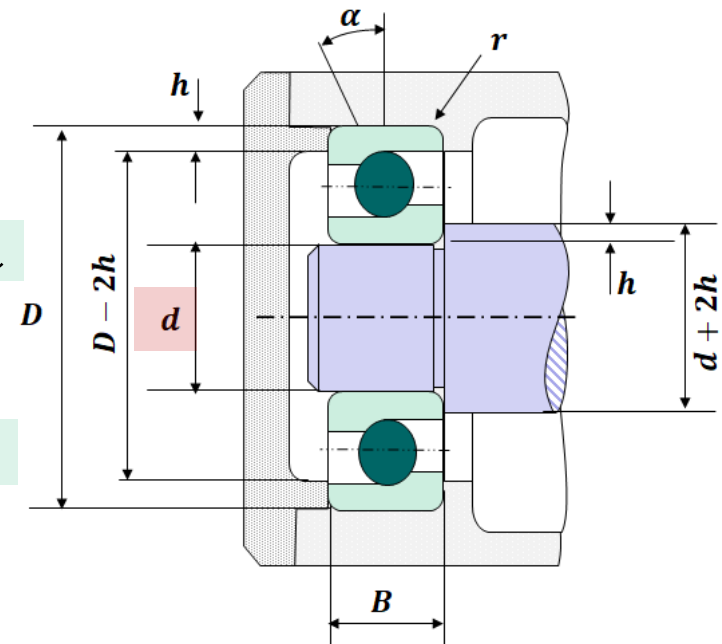
Bore (mm)	Radial Ball, $\alpha = 0^\circ$			Angular Ball, $\alpha = 25^\circ$			Roller		
	L00 Xlt (kN)	200 lt (kN)	300 med (kN)	L00 Xlt (kN)	200 lt (kN)	300 med (kN)	1000 Xlt (kN)	1200 lt (kN)	1300 med (kN)
10	1.02	1.42	1.90	1.02	1.10	1.88			
12	1.12	1.42	2.46	1.10	1.54	2.05			
15	1.22	1.56	3.05	1.28	1.66	2.85			
17	1.32	2.70	3.75	1.36	2.20	3.55	2.12	3.80	4.90
20	2.25	3.35	5.30	2.20	3.05	5.80	3.30	4.40	6.20
25	2.45	3.65	5.90	2.65	3.25	7.20	3.70	5.50	8.50
30	3.35	5.40	8.80	3.60	6.00	8.80	2.40 ^a	8.30	10.0
35	4.20	8.50	10.55	4.75	7.91	11.0	3.10 ^a	9.30	13.0
40	4.50	9.40	12.6	4.95	9.90	13.2	7.20	11.1	16.5
45	5.80	9.10	14.8	6.30	10.4	16.4	7.40	12.2	20.9
50	6.10	9.70	15.8	6.60	11.0	19.2	5.10 ^a	12.5	24.5
55	8.20	10.55	18.0	7.91	13.6	21.5	11.3	14.9	27.1
60	8.70	13.6	20.0	9.70	16.4	24.0	12.0	18.9	32.5
65	9.10	16.0	22.0	10.2	19.2	26.5	12.2	21.1	38.3
70	10.55	17.0	24.5	13.4	19.2	29.5		23.6	44.0
75	12.2	17.0	25.5	13.8	20.0	32.5		23.6	45.4

$$C_{req_{esf}} = 10,55kN$$

$$C_{req_{cont}} = 7,91N$$

$$d_{cont} = 55mm$$

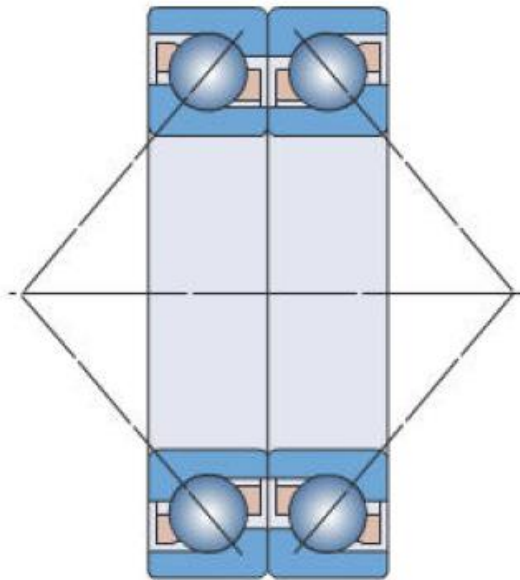
$$d_{esf} = 70mm$$



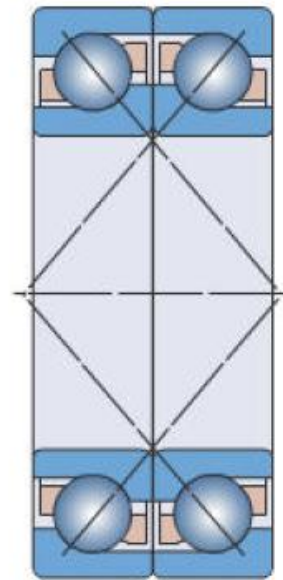


Mancais de rolamento

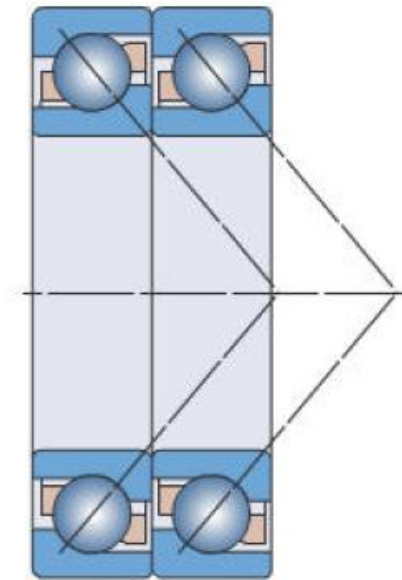
Considerações de montagem



O-Anordnung



X-Anordnung

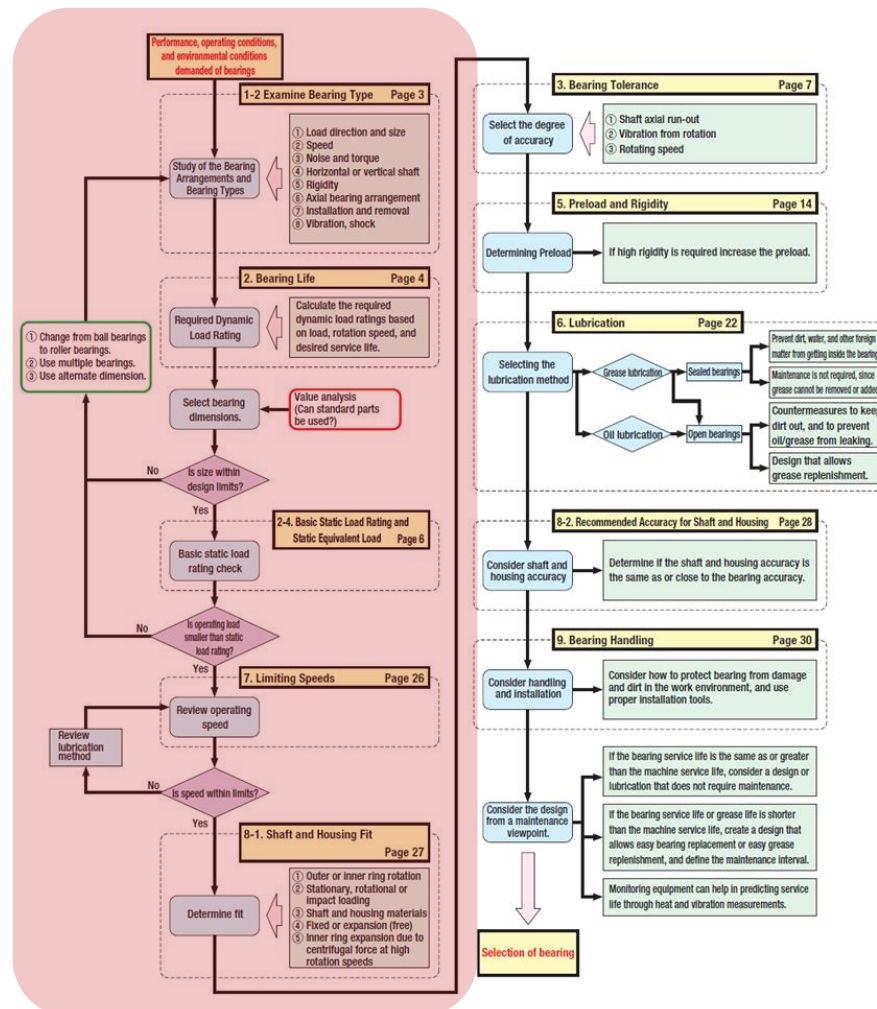


Tandem-Anordnung



Mancais de rolamento

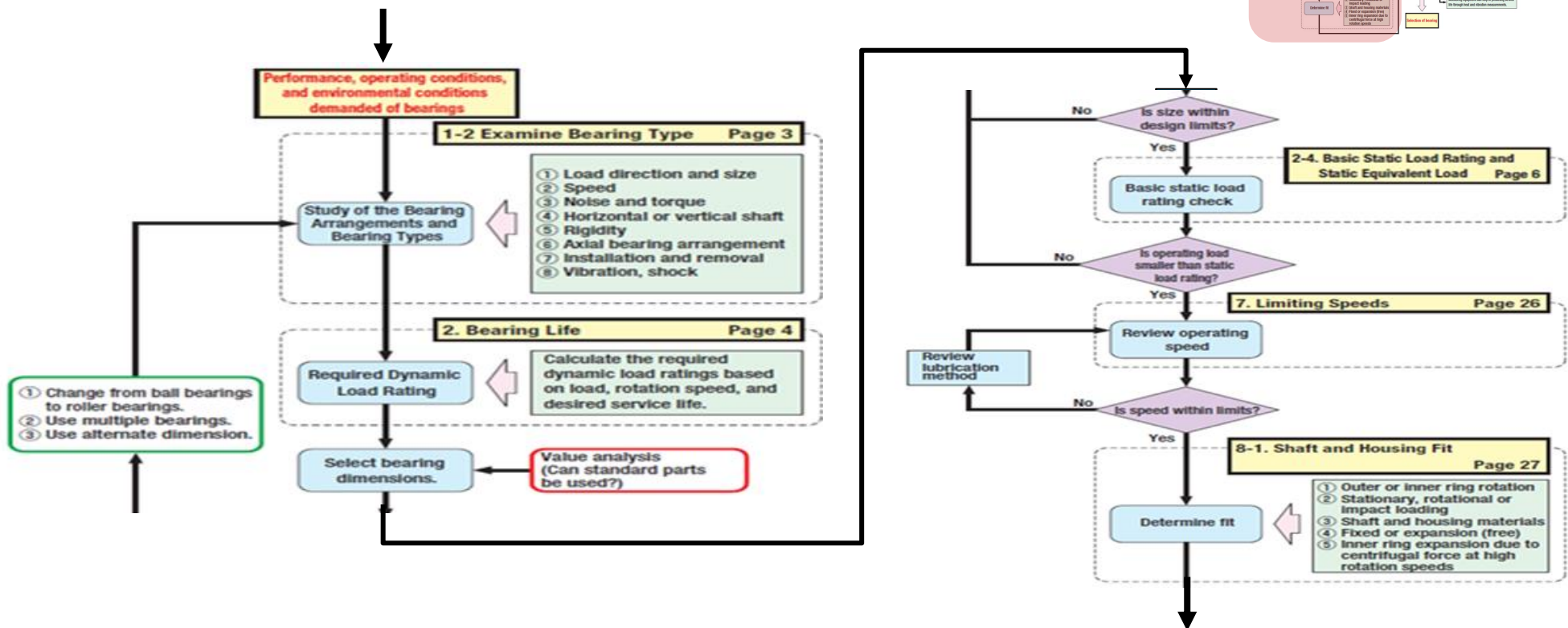
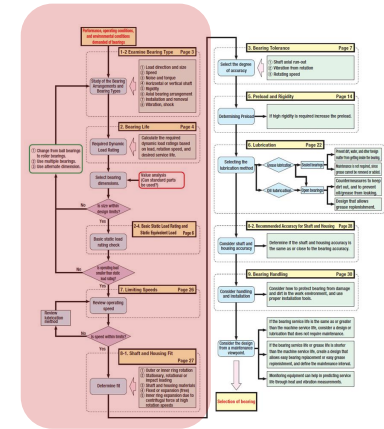
Seleção





Mancais de rolamento

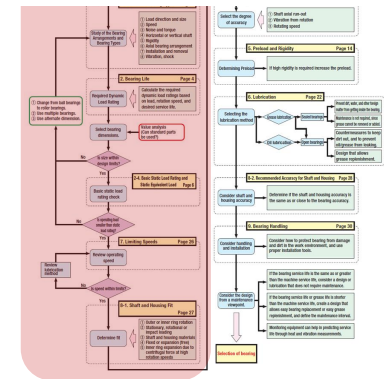
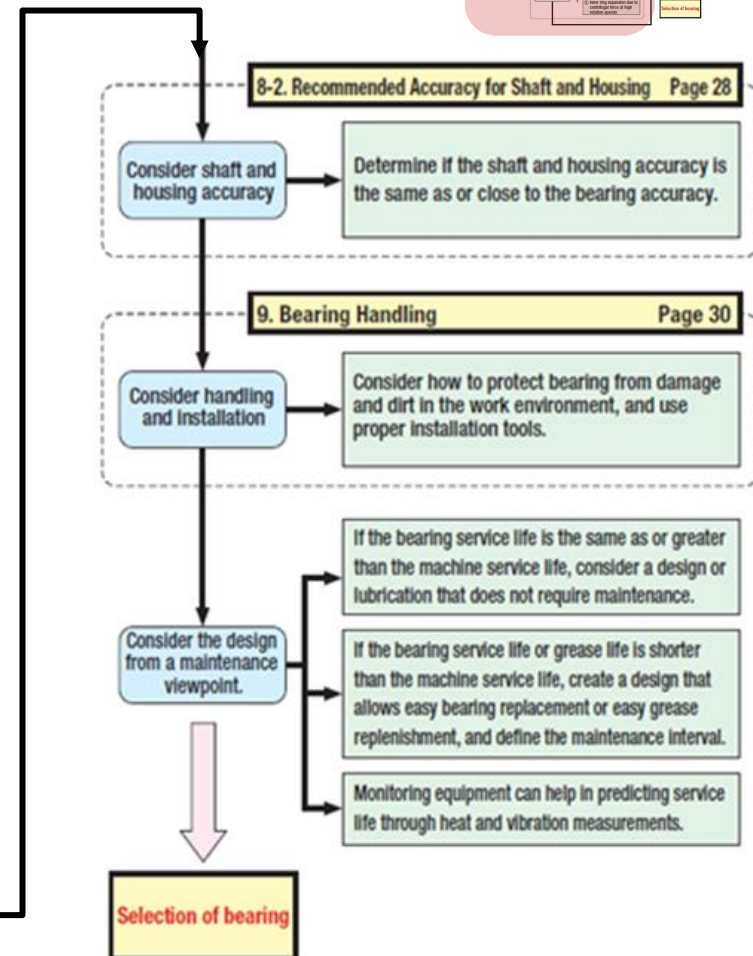
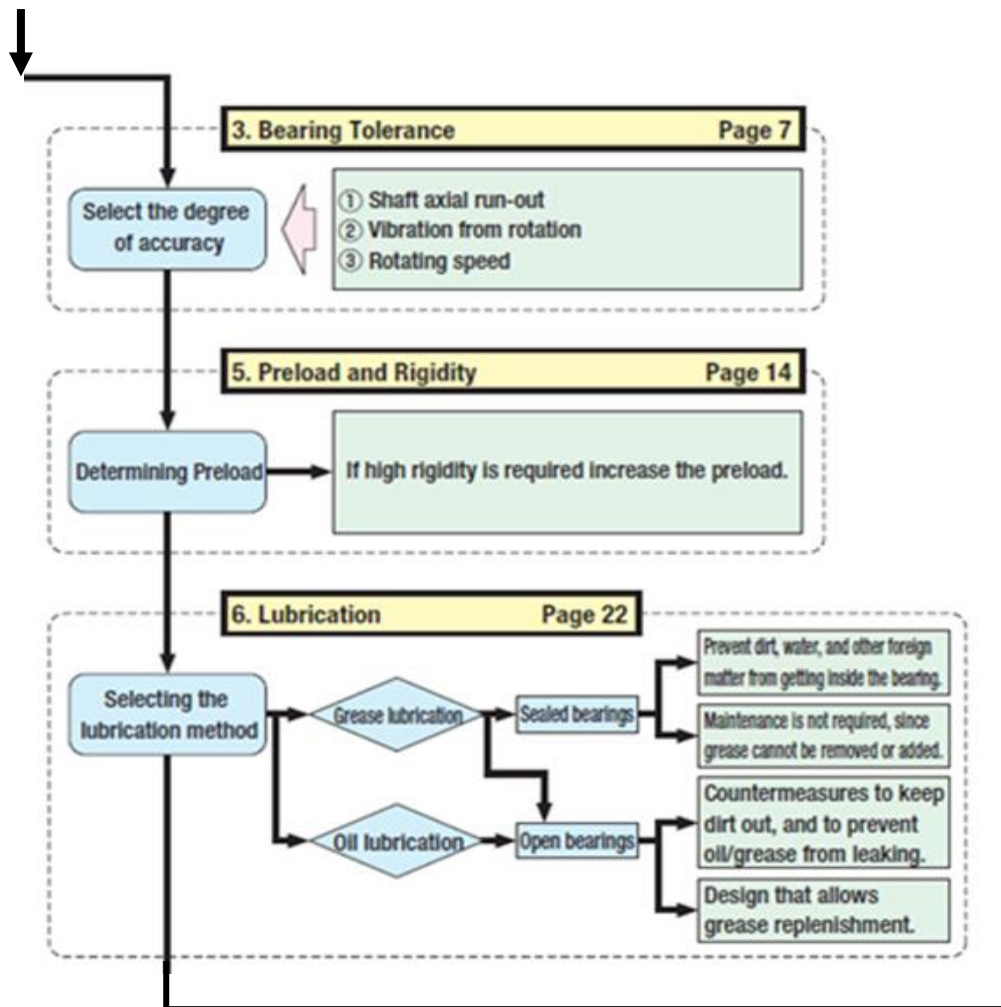
Seleção





Mancais de rolamento

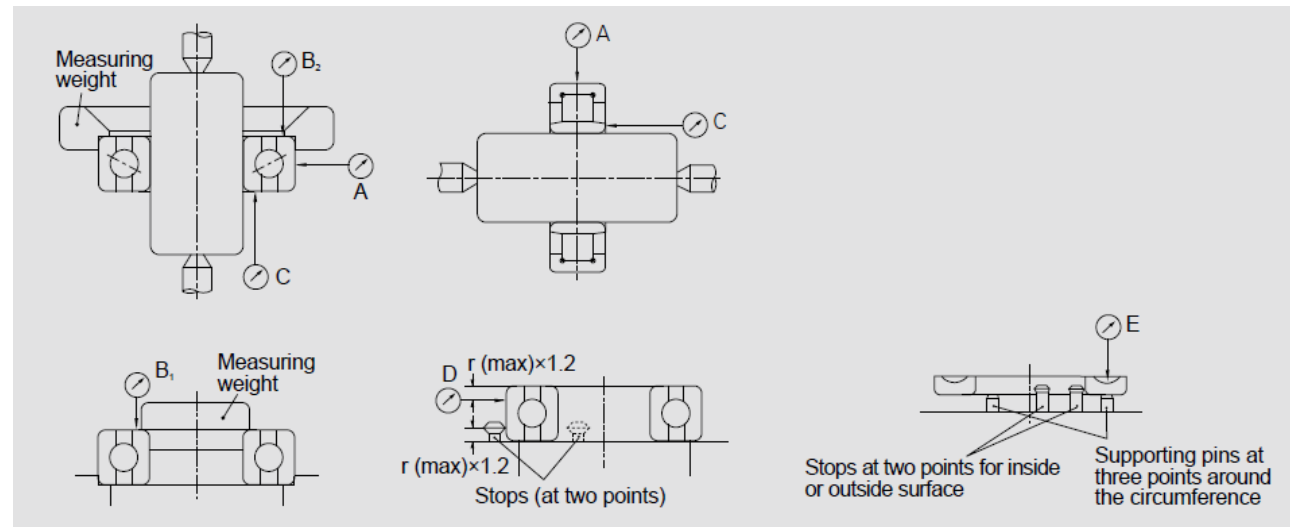
Seleção





Mancais de rolamento

Erros de movimento



Running accuracy	Inner ring	Outer ring	Measuring point
K_{ia}	rotating	stationary	A
K_{ea}	stationary	rotating	A
S_{ia}	rotating	stationary	B ₁
S_{ea}	stationary	rotating	B ₂
S_d	rotating	stationary	C
S_D	—	rotating	D
S_i, S_e	Only the shaft or housing or central washer is to be rotated		E



Mancais de rolamento

Falhas em mancais de rolamento

Desalinhamento

Flexão dos eixos

Contaminação na interface

Montagem errada

Acabamento superficial

Ciclo de carregamento

Condições de lubrificação

Velocidade de operação

Tipo de lubrificante

Choques

Material do mancal

Sobrecargas

Tipo de elemento

Tipo de mancal

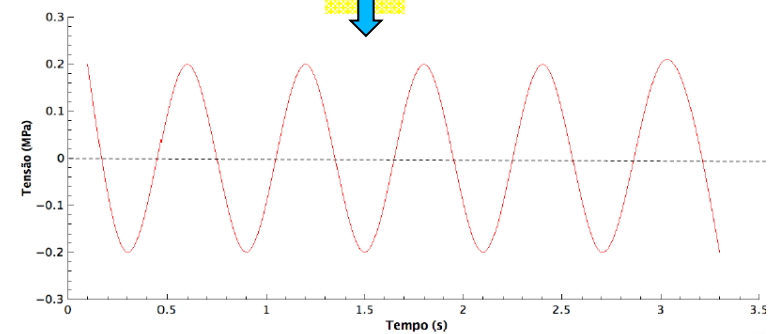
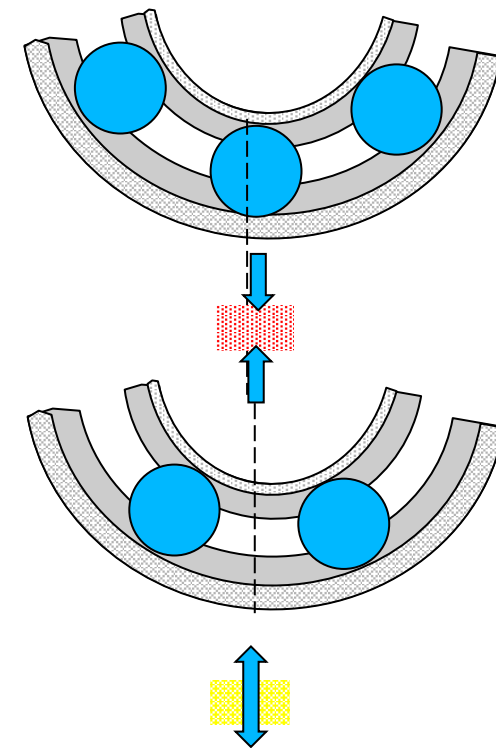
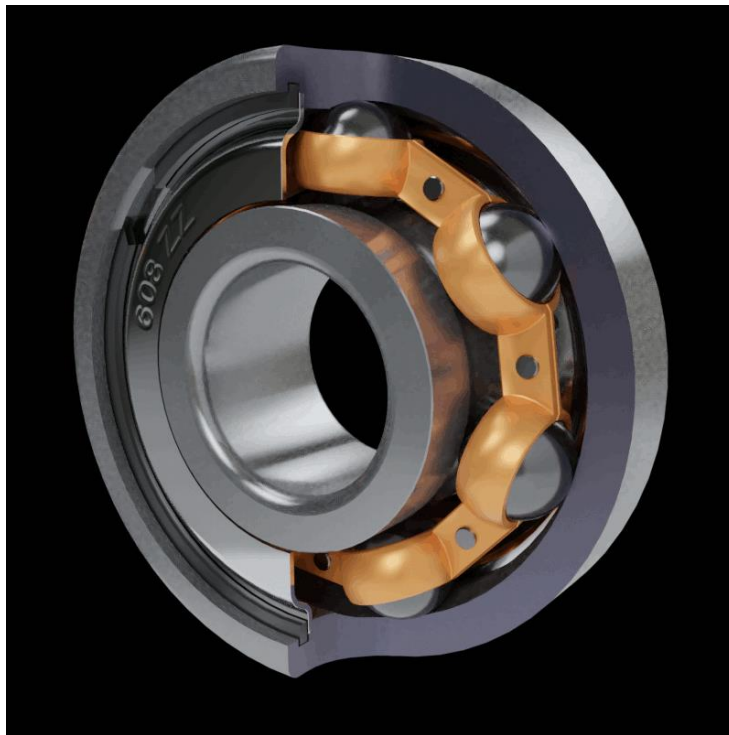
Seleção errada





Mancais de rolamento

Falhas em mancais de rolamento





Mancais de rolamento

Falhas em mancais de rolamento





FIM DA AULA