

PEF3310

19/08/21

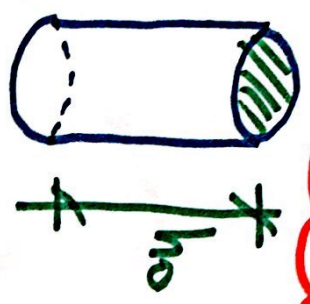
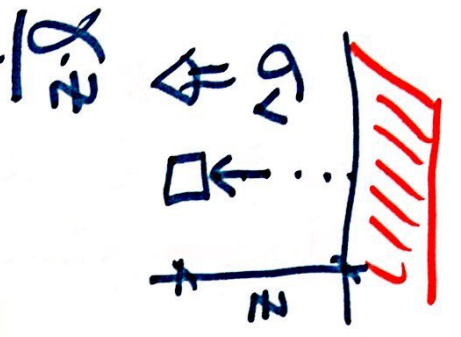
(1)

Resistência das Argilas

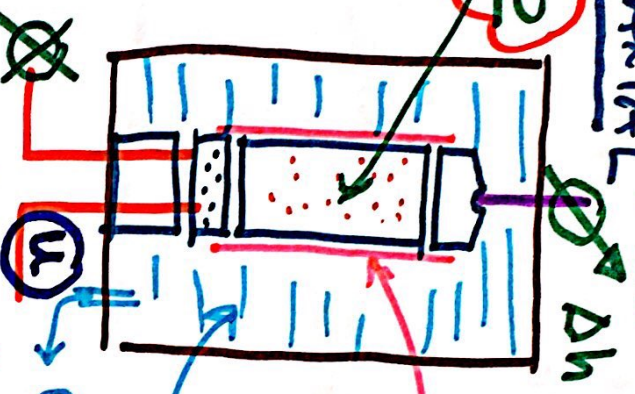
Propriedades de Engenharia

- RESISTÊNCIA - Triaxial / Cisalhamento Direto
- DEFORMABILIDADE - Triaxial / Compressão e dométrica
- PERMEABILIDADE - Permeômetro - carga constante
 - carga variável

ENSAIO TRIAXIAL \downarrow $(P + \Delta P) \rightarrow$ monitorada



SATURADO



membrana de borracha

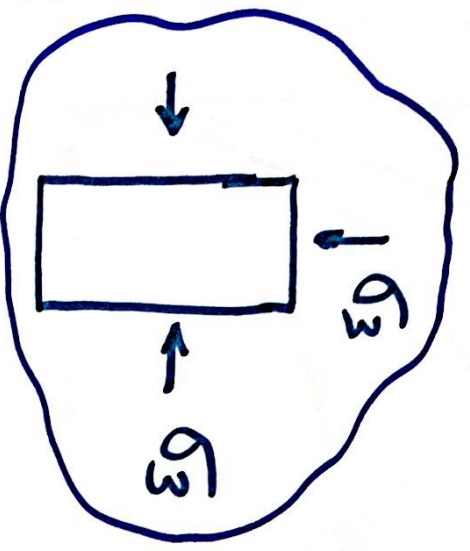
água

$$\epsilon = \frac{\Delta h}{h_0}$$

$$\sigma_3 + \Delta \sigma = \sigma_1$$

$$\bar{\sigma} = \sigma - u$$

$\downarrow \sigma_3 + \Delta \sigma = \sigma_1 \rightarrow$ tensão principal maior



$\leftarrow \sigma_3 \rightarrow$ tensão principal menor

unconsolidated

undrained

consolidated

drained

2º CARREGAMENTO

1º CONFINAMENTO
SEM DRENAGEM - $\Delta V = 0$

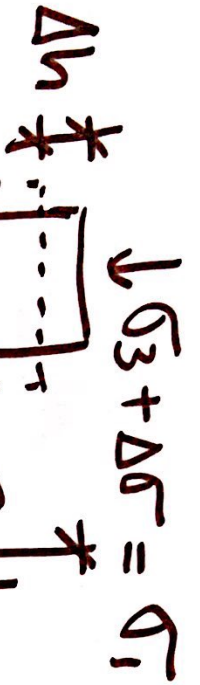
ADENSADO - $\Delta V \neq 0$

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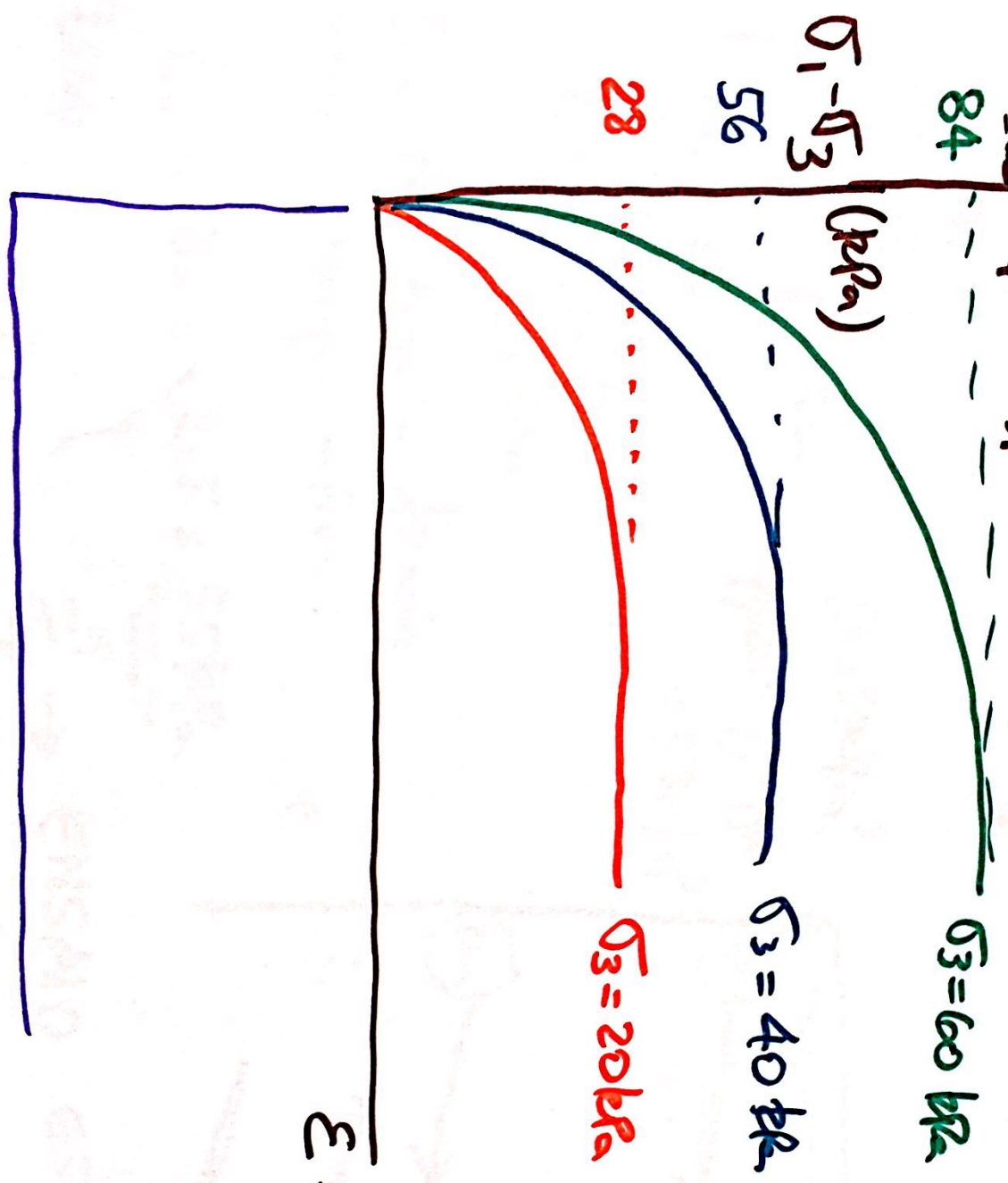
SEM DRENAGEM -

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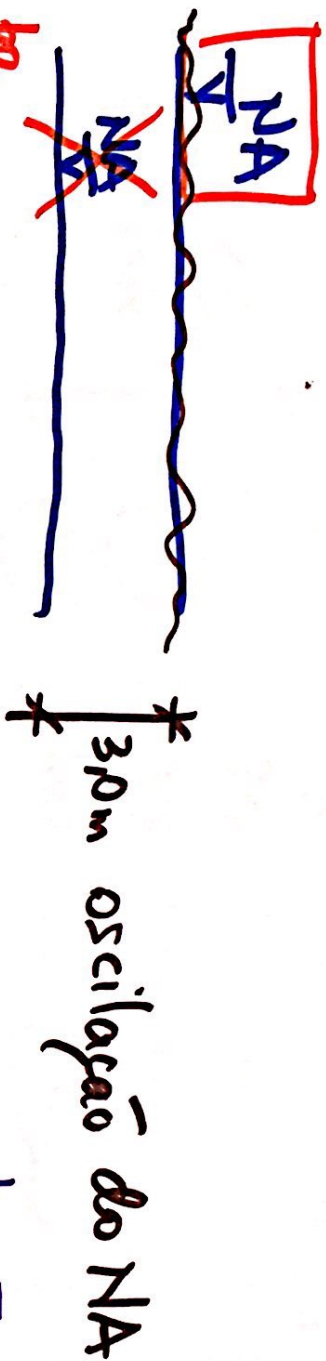
DRENADO -



$\sigma_1 - \sigma_3 =$ acréscimo de tensão axial



$$\epsilon = \frac{\Delta h}{h_0}$$



$\bar{\sigma}_v = 25$ kPa
 $u = 50$
 $\sigma_v = 75$
 $\square 5m$

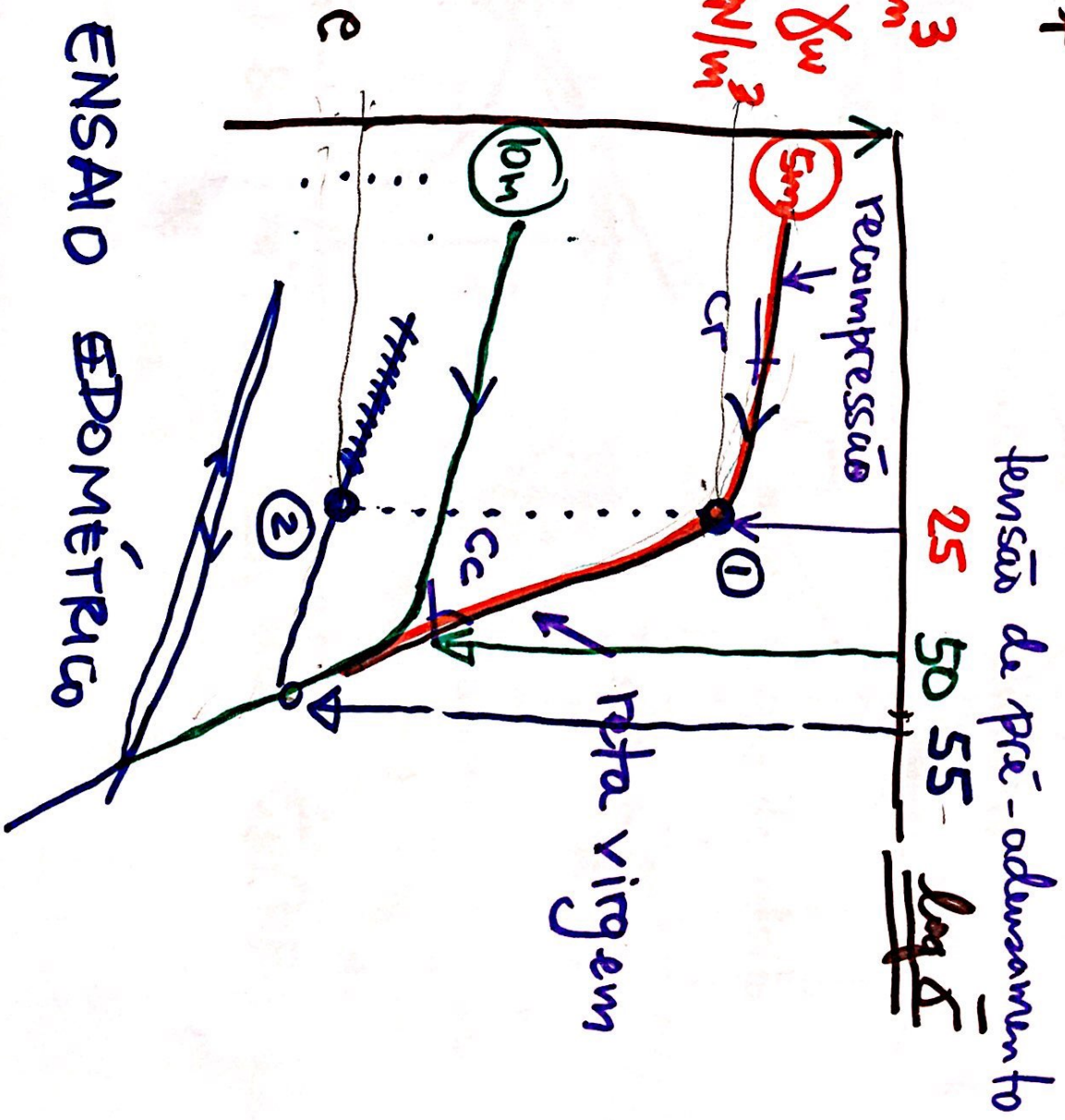
NORMALMENTE ADENSADA



Se o NA fixare fixado muito tempo - 3m:

$\bar{\sigma}_v = 3 \times 15 + 2 \times 5 = 55 \text{ kPa}$
 (5m)

$\gamma = 15 \text{ kN/m}^3$
 $\gamma_{sub} = \gamma - \gamma_w = 5 \text{ kN/m}^3$



1.1

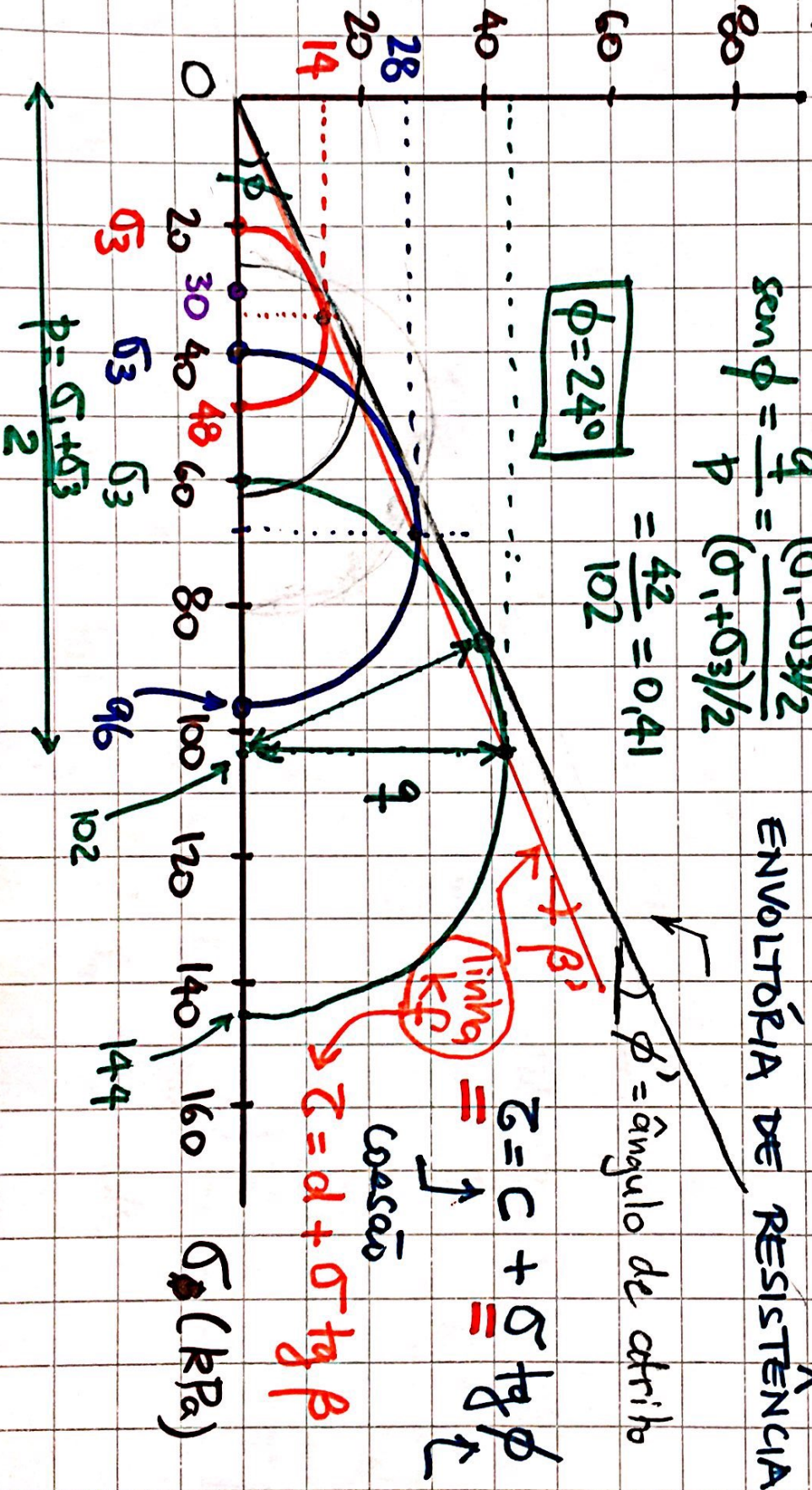
argila NA

Ensaio
 7
 8
 9

Ensaio	σ_3 (kPa)	$(\sigma_1 - \sigma_3)/2 = q$	$(\sigma_1 - \sigma_3)$	σ_1
7	20	14	28	48
8	40	28	56	96
9	60	42	84	144

5

τ (kPa)



$$\text{sen } \phi = \frac{q}{p} = \frac{(\sigma_1 - \sigma_3)/2}{(\sigma_1 + \sigma_3)/2} = \frac{42}{102} = 0,41$$

$$\phi = 24^\circ$$

ENVOLVÓRIA DE RESISTÊNCIA

ϕ' = ângulo de atrito

$$\tau = c + \sigma \text{ tg } \phi$$

coesão

$$\tau = d + \sigma \text{ tg } \beta$$

limite K_f

raio

diâmetro

$$p = \frac{\sigma_1 + \sigma_3}{2}$$

1.2: Para o ensaio CU, corpos de prova NA, Seta raios
 Vale também a proporcão validada

1.3: DRENADO SEM DRENAGEM
 Ensaio $\bar{\sigma}_3$ (kPa) $(\sigma_1 - \sigma_3)/2$ kPa

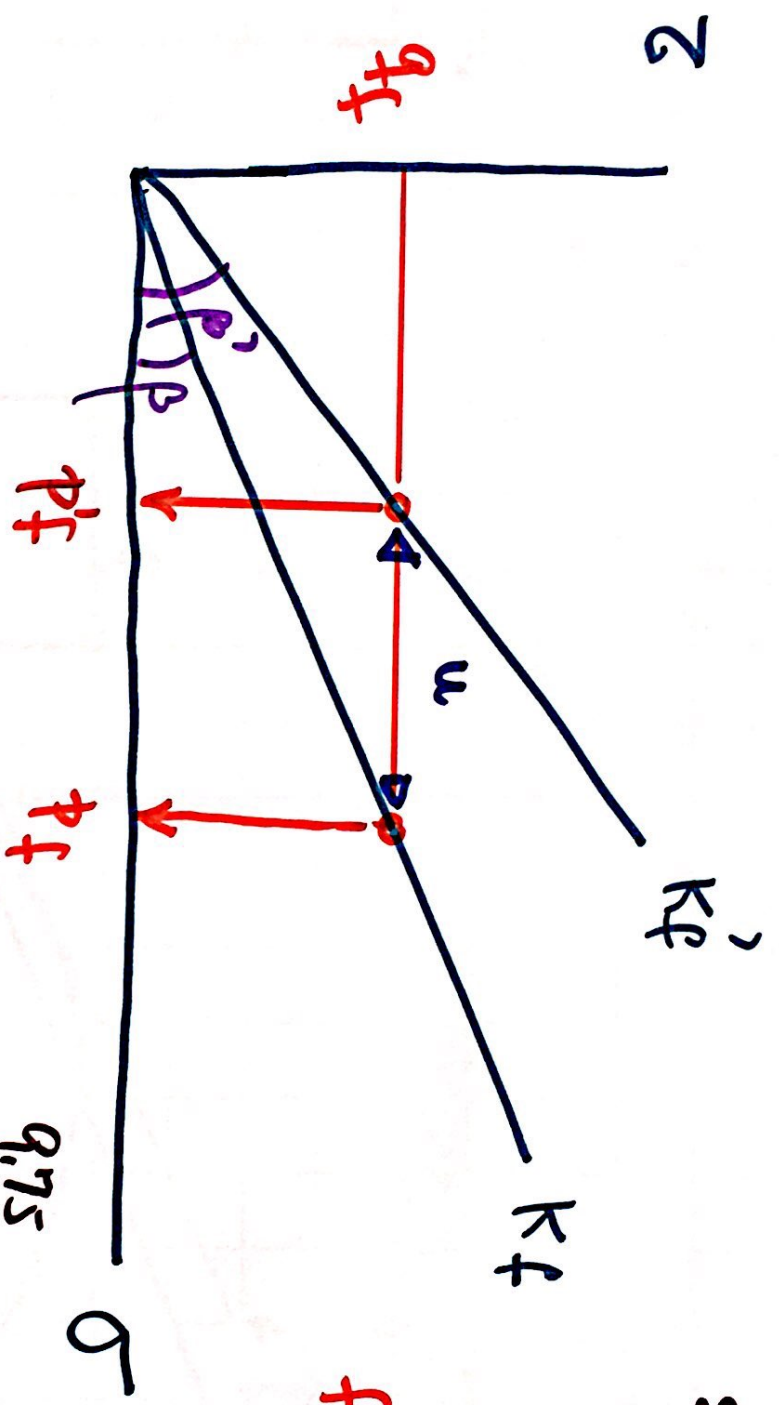
	$\frac{\sigma_1 + \sigma_3}{2} = P$	σ_1	$q = \frac{\sigma_1 - \sigma_3}{2}$	σ_3	RR = Razão de Resistência
NA 4	26,5	33	6,5	16,5	$RR = \frac{6,5}{20} = \frac{13}{40} \dots$
NA 5	30	49,5	9,75	13,0	
NA 6	60	19,5			

$RR = 0,325$

1.4: $\bar{\sigma}_3 = 30$ kPa drenado
 $\Delta \sigma_3 = 30$ kPa $\rightarrow \sigma_3 = 60$ kPa \downarrow sem drenagem
 $\Delta V = 0$ e = cte

$\text{Slope} = \tan \beta$

f: failure (rupture)



$u = p_f - p'_f$

$\tan \beta = \frac{q_f}{p_f}$

$\tan \beta' = \frac{q_f}{p'_f}$

$u = \frac{q_f}{\tan \beta} - \frac{q_f}{\tan \beta'} = q$

$\frac{1}{\tan \beta} - \frac{1}{\tan \beta'}$

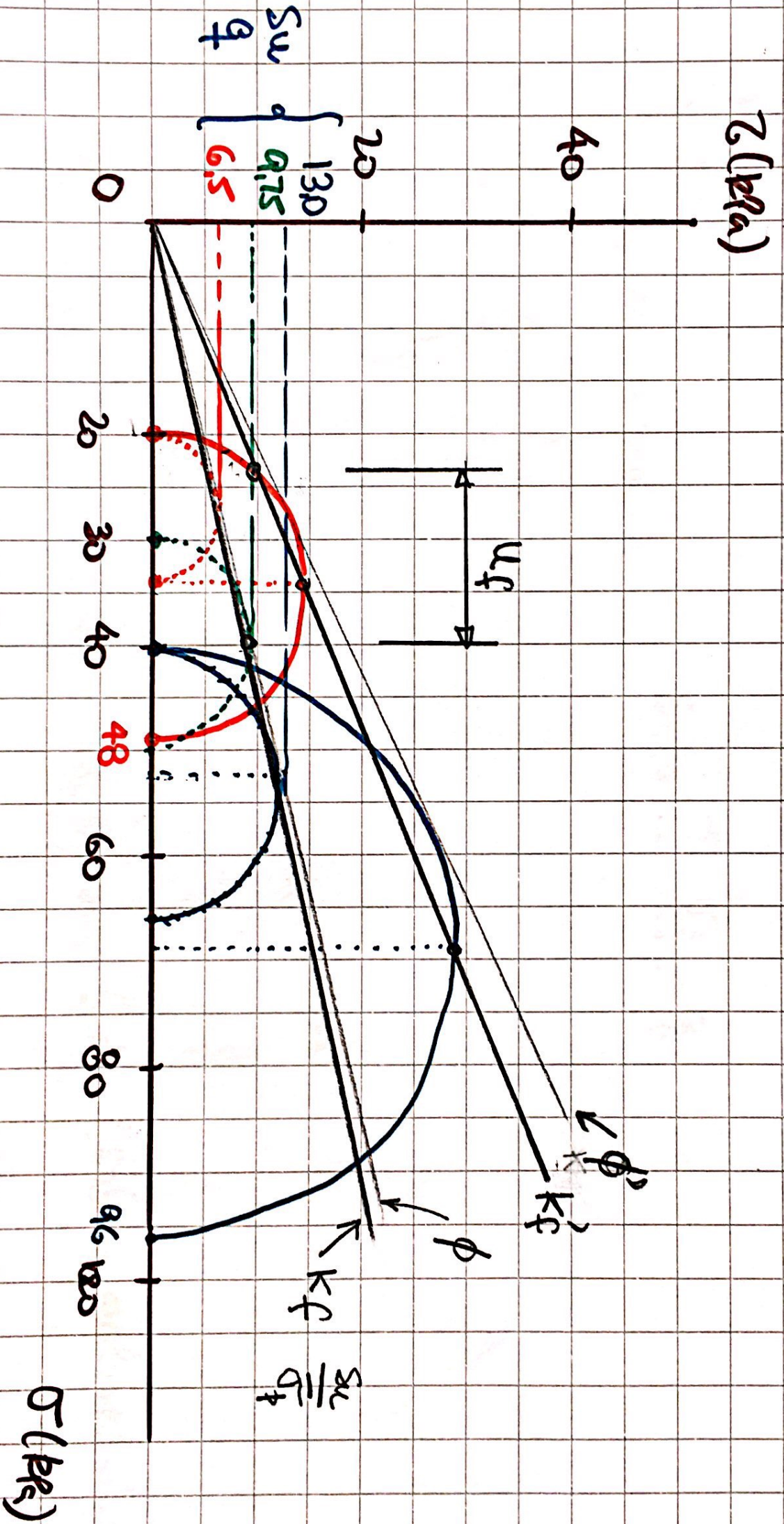
$q \left(\frac{1}{\tan \beta} - \frac{1}{\tan \beta'} \right)$

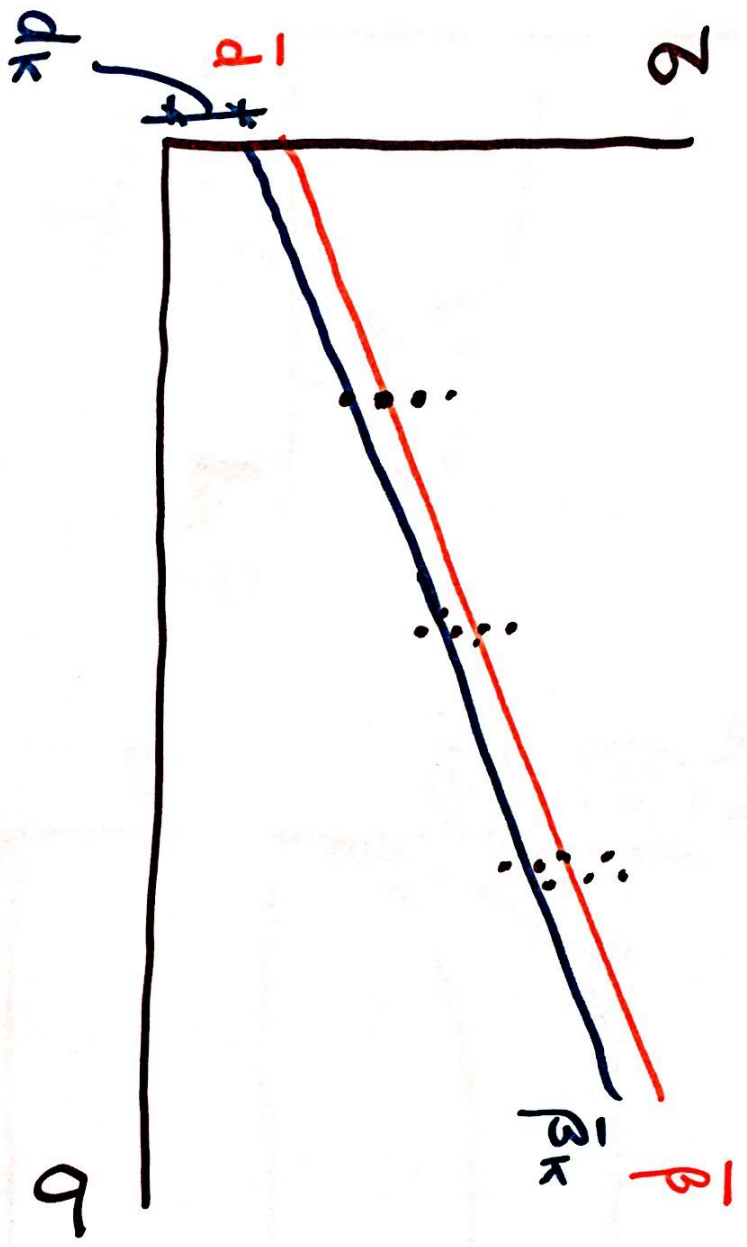
13.8°

22°

$\beta = 13.8^\circ$
 $\beta' = 22^\circ$

$u = 45.15 \text{ kPa}$





$$\text{Sen } \phi = \frac{d}{\beta}$$
$$c = \frac{d}{\text{cos } \phi}$$

NBR 11682
Estabilidade de
Encostas

$S_u = S \Rightarrow$ Strength } Resistência Não Drenada
 $u \Rightarrow$ undrained

CV τ undrained $S_u = \frac{\sigma_1 - \sigma_3}{2} = q$

$R_R = \frac{\sigma_1}{\sigma_p}$

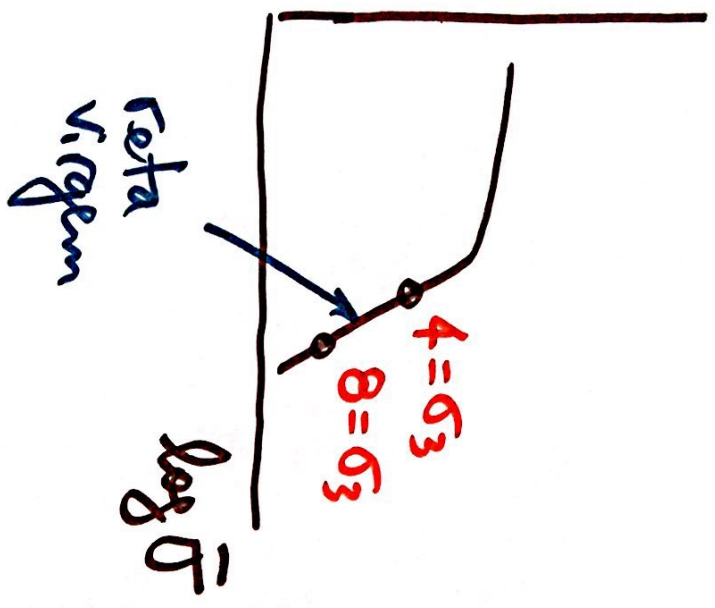
$\bar{\sigma}_3 > \bar{\sigma}_p$ \Rightarrow corpo de prova N.A.

in situ

$\bar{\sigma}_3 < \bar{\sigma}_p$ \Rightarrow corpo de prova S.A. (caso adensado)

in situ

e



cedușă
valutăria =
confracă

