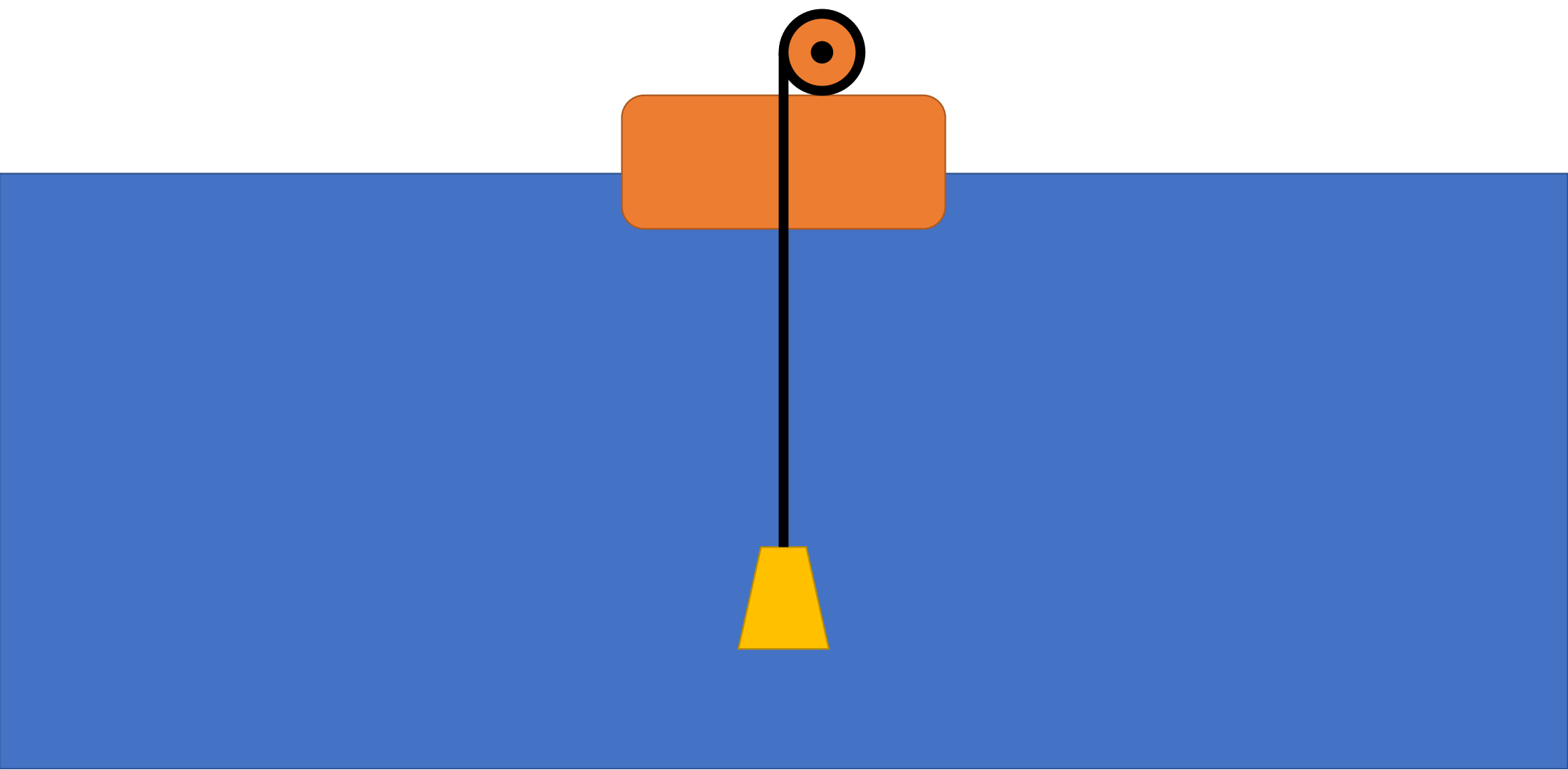


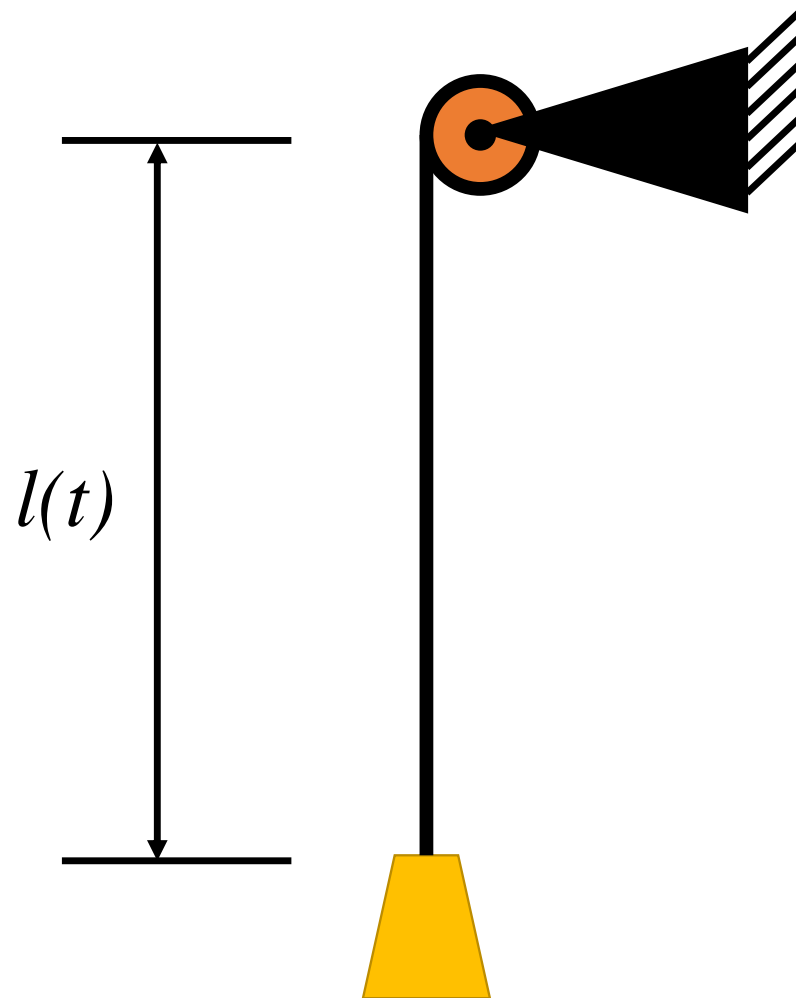
Dinâmica de Sistemas Navais e Oceânicos

PNV3314 Dinâmica de Sistemas

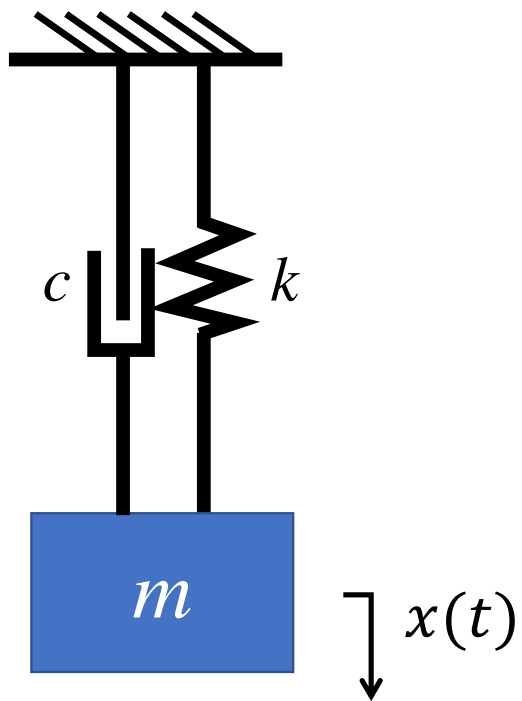
Aula 8

Simulação de sistema dinâmico



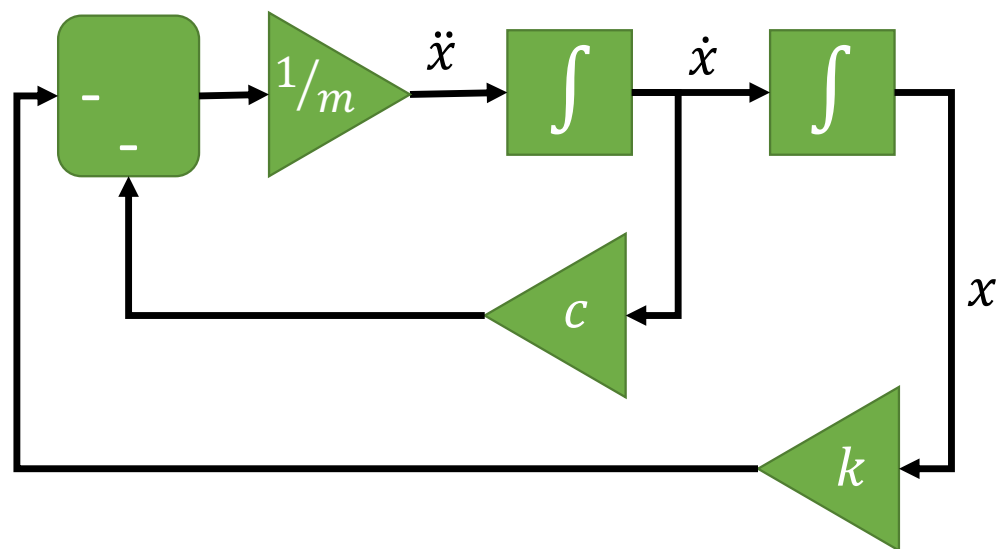


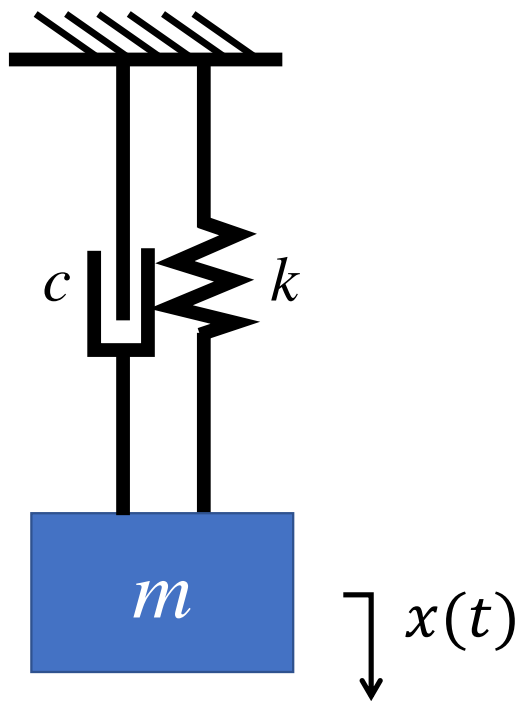
EM AR



$$m\ddot{x} + c\dot{x} + kx = 0$$

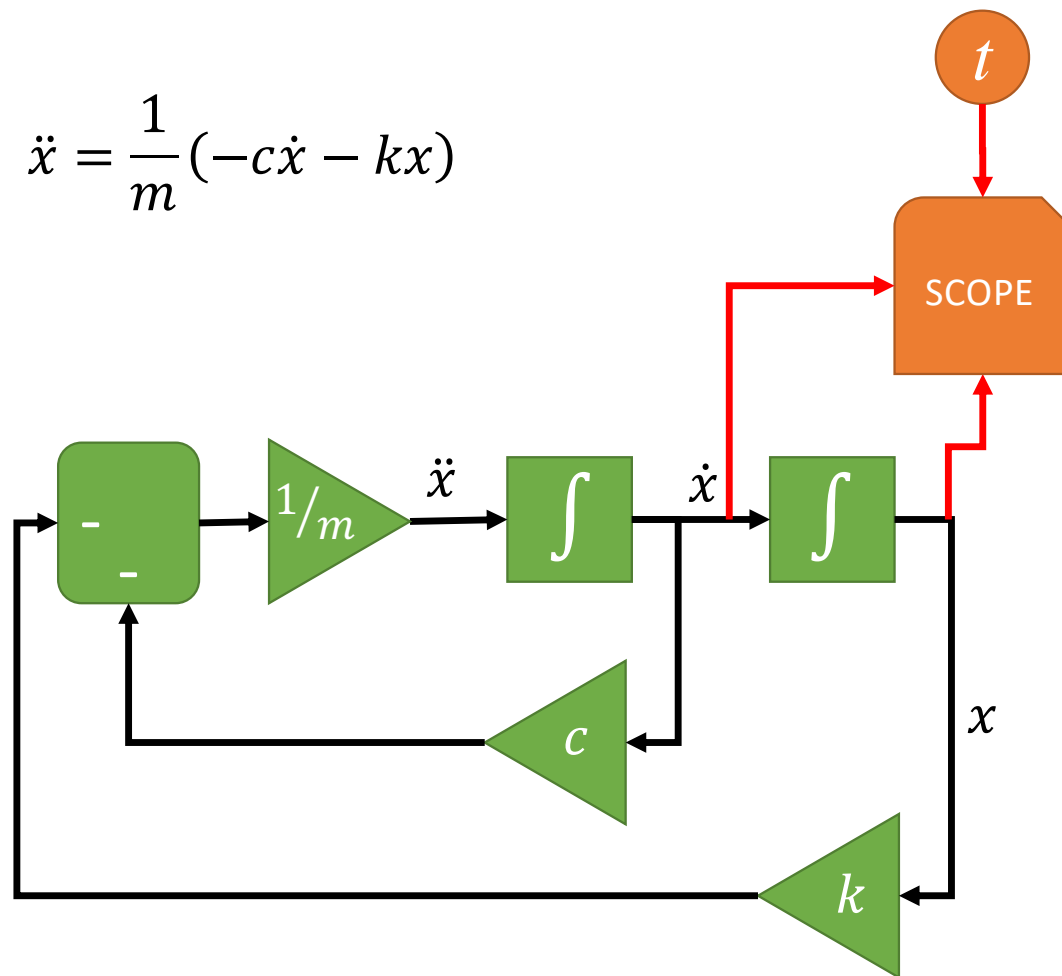
$$\ddot{x} = \frac{1}{m}(-c\dot{x} - kx)$$





$$m\ddot{x} + c\dot{x} + kx = 0$$

$$\ddot{x} = \frac{1}{m}(-c\dot{x} - kx)$$

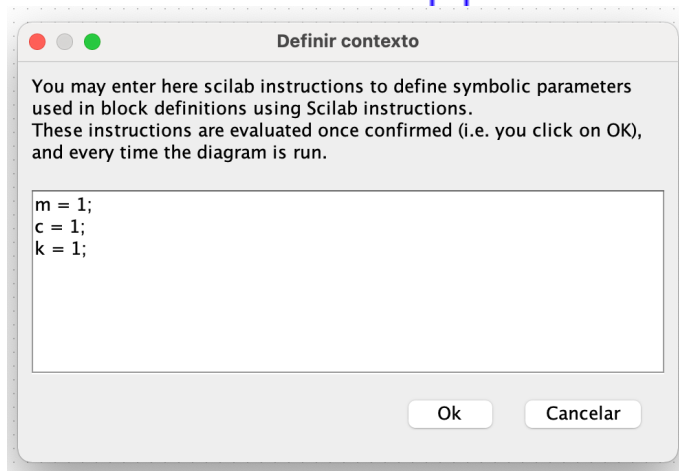
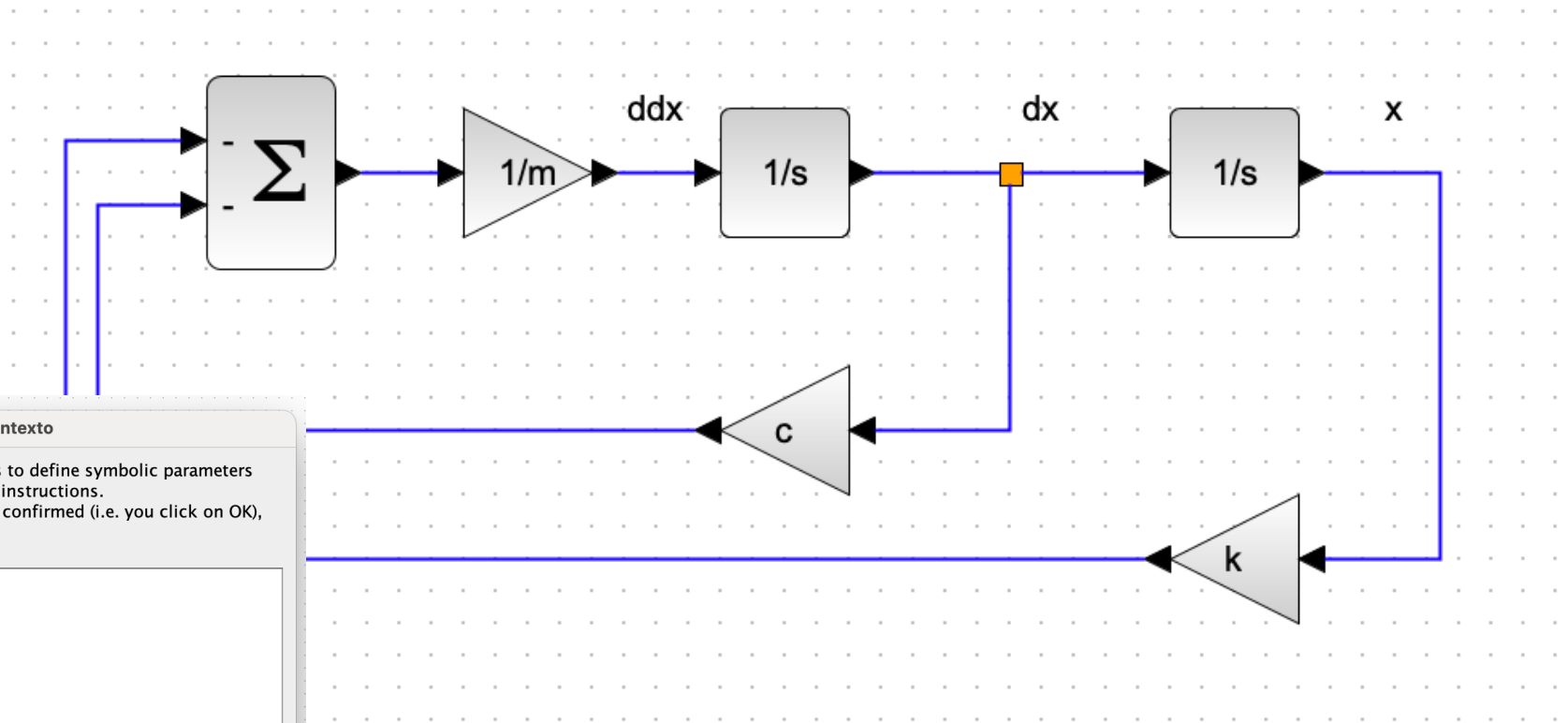


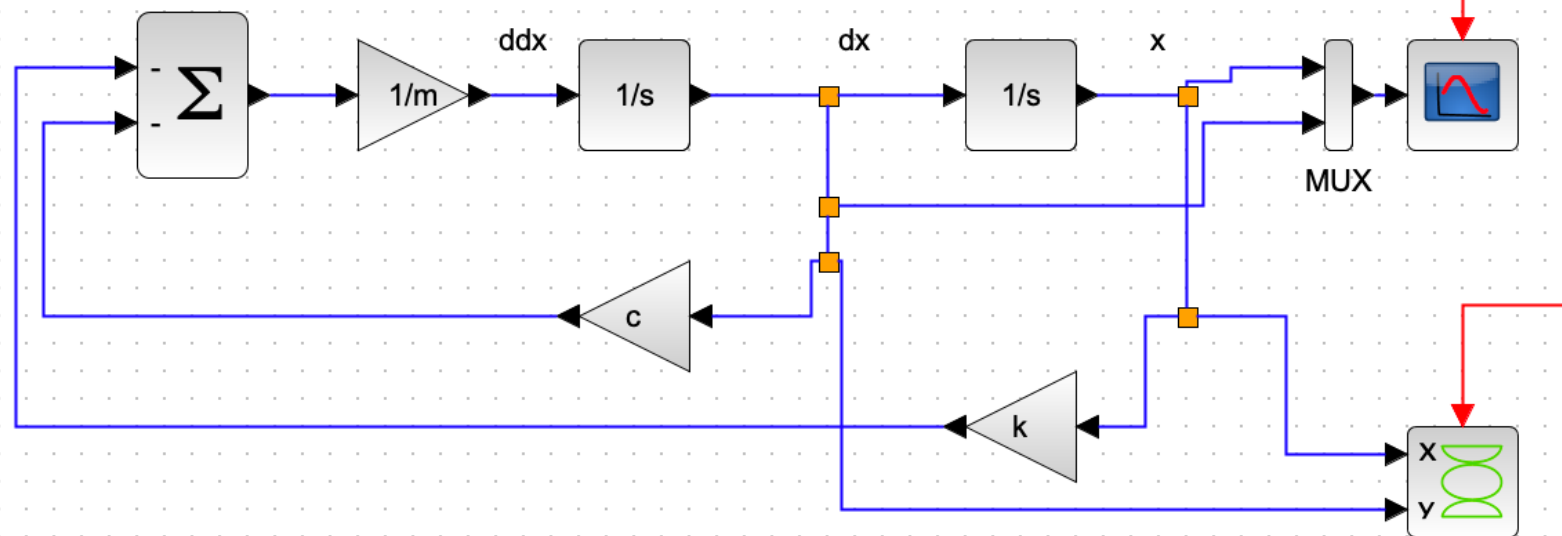
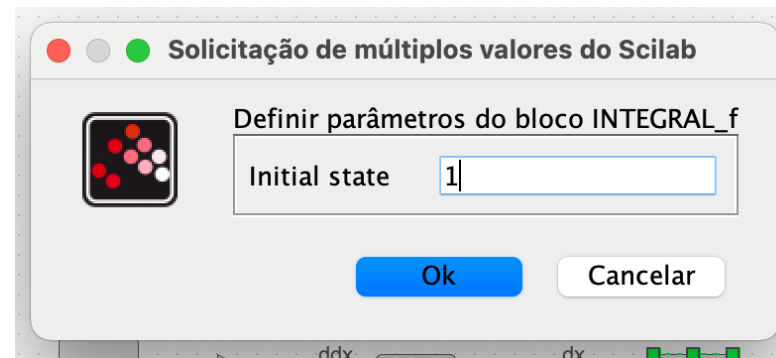
Simulação dinâmica no Scilab/XCOS

- Abrir Scilab.
- Na linha de comando, digitar XCOS. Abrirá ambiente de blocos.



Diagrama de bloques





Definir parâmetros

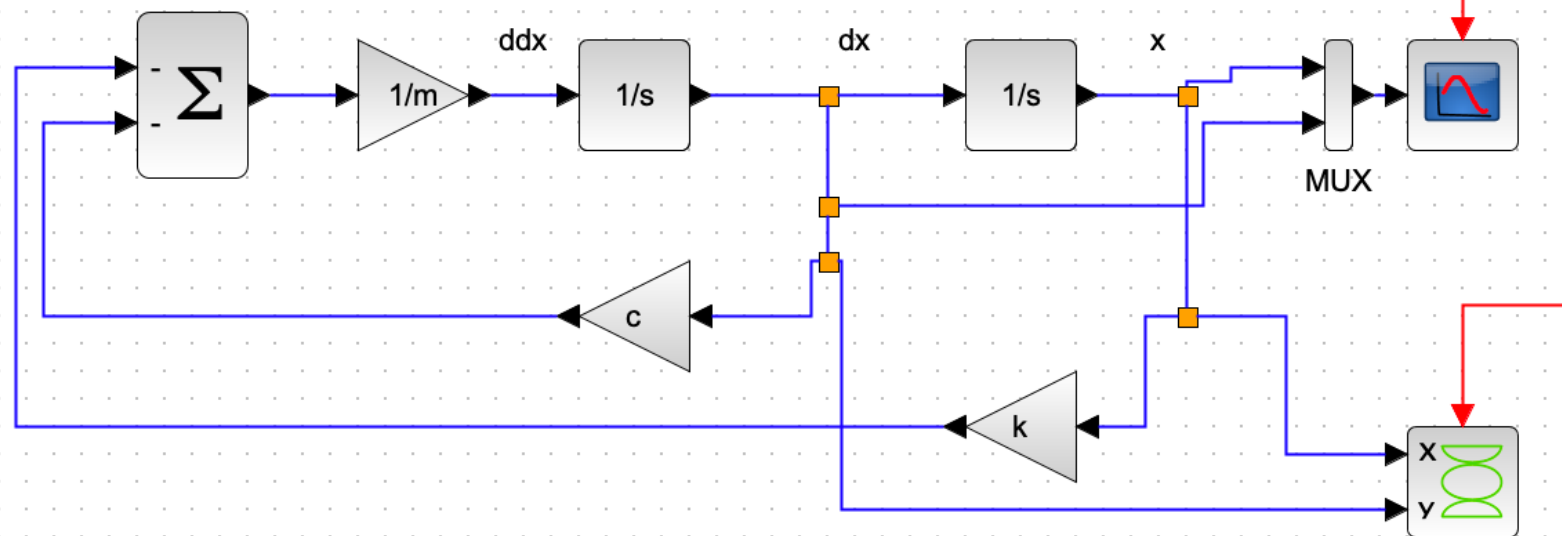
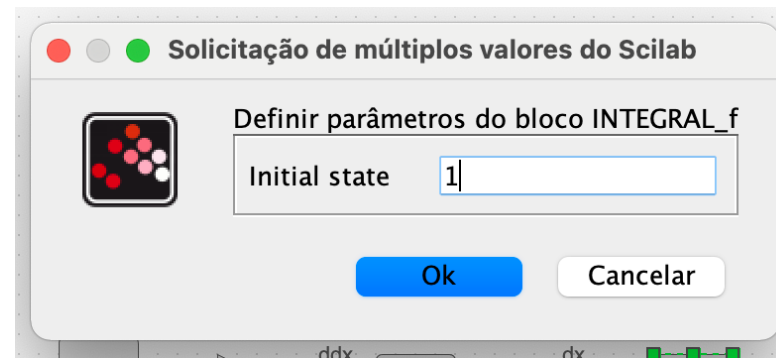
Tempo final de integração	3.0E01
Escala em tempo real	0.0E00
Tolerância absoluta do integrador	1.0E-06
Tolerância relativa do integrador	1.0E-06
Tolerância de tempo	1.0E-10
Intervalo máximo de tempo de integração	1.00001E05
Solver kind	Sundials/CVODE - BDF - NEWTON
Maximum step size (0 means no limit)	0.0E00

Definir contexto

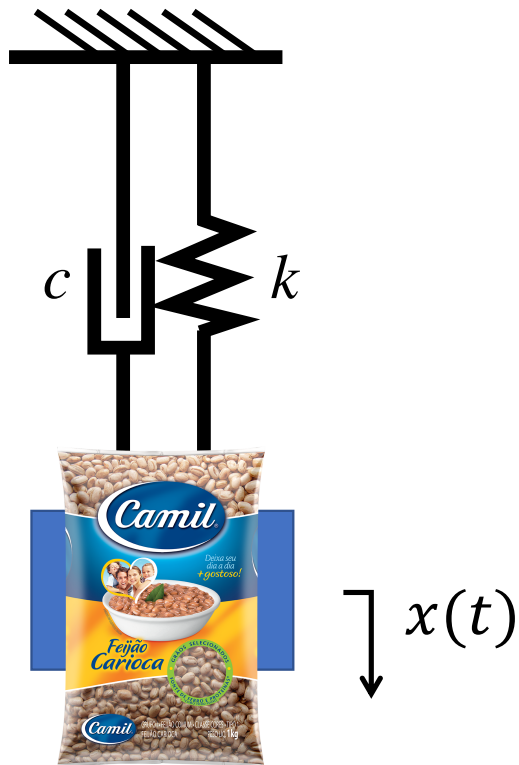
Ok

Cancelar

Padrão



Pense num sistema real... não amortecido



$$m = 1\text{kg}$$

$$c = 0$$

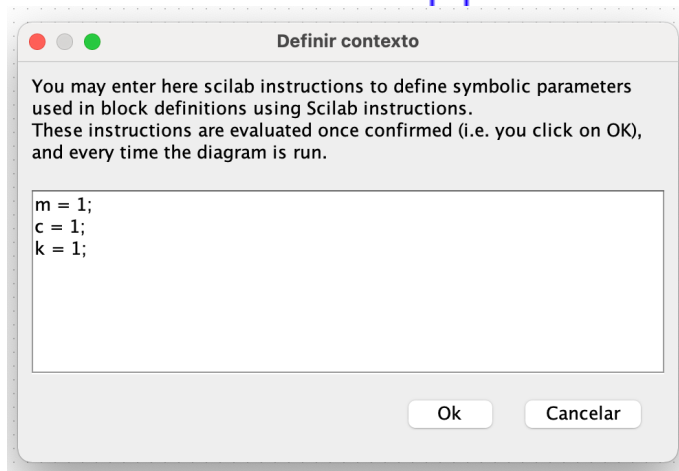
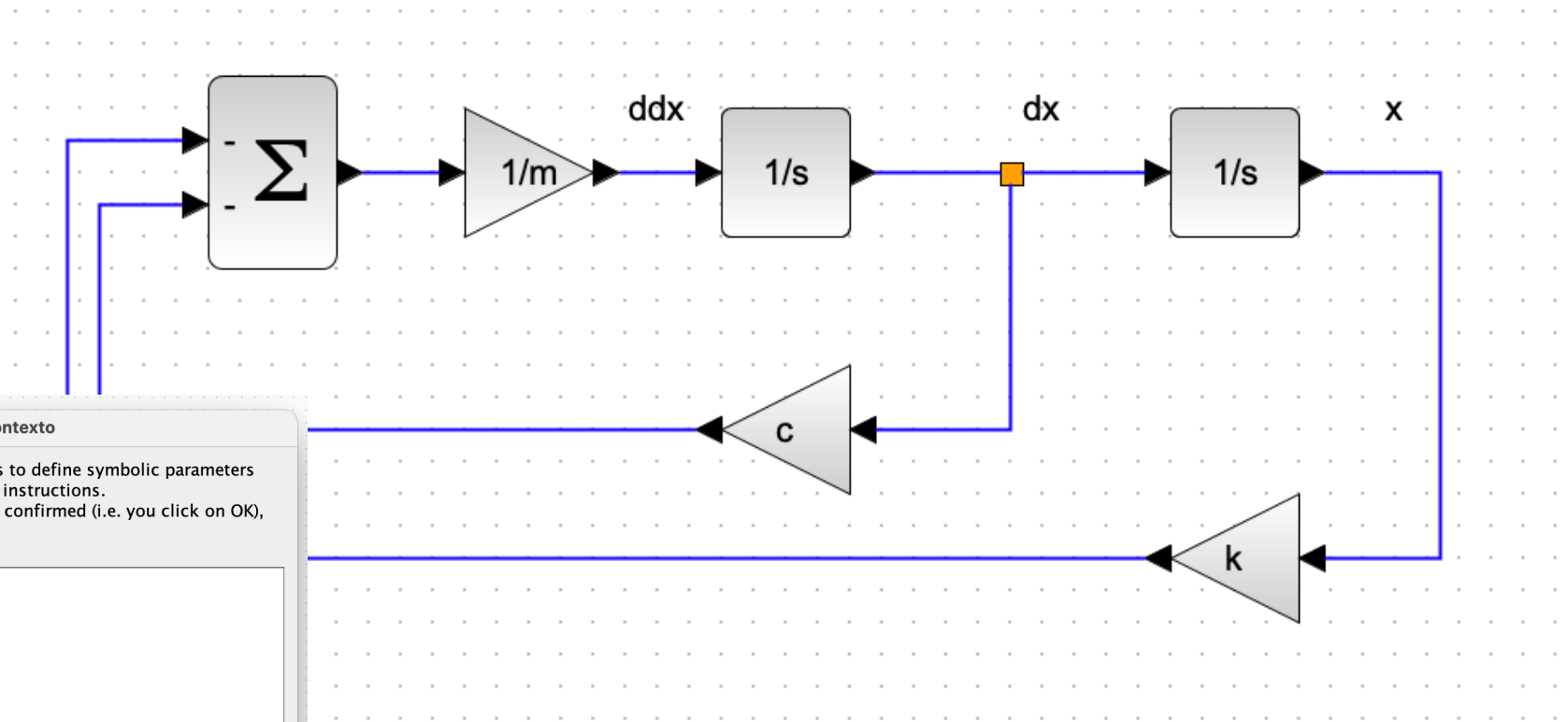
$$k = ?$$

$$f_n = \frac{1}{2\pi} \sqrt{\frac{k}{m}} = 1\text{Hz}$$

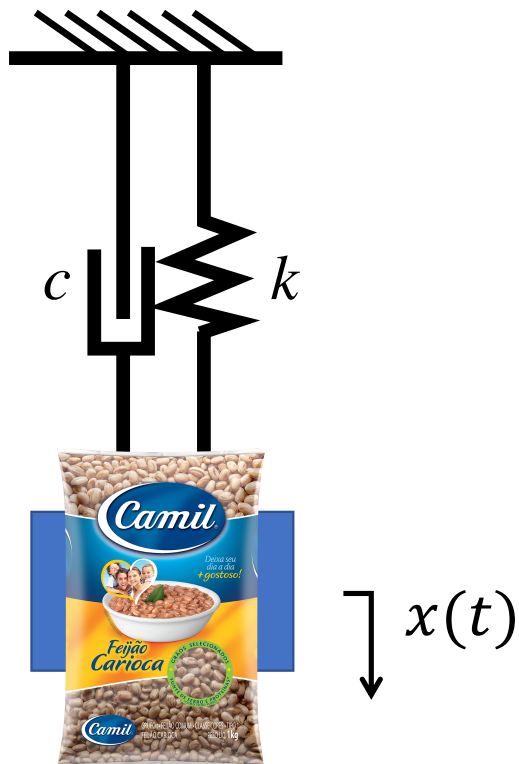
$$k = 4\pi^2 m f_n^2 = 39,47\text{N/m}$$

$$1\text{kgf} = kx_0 = 0,25\text{m}$$

Diagrama de bloques



Agora amortecido...



$$m = 1\text{kg}$$

$$k = 4\pi^2 m f_n^2 = 39,47\text{N/m}$$

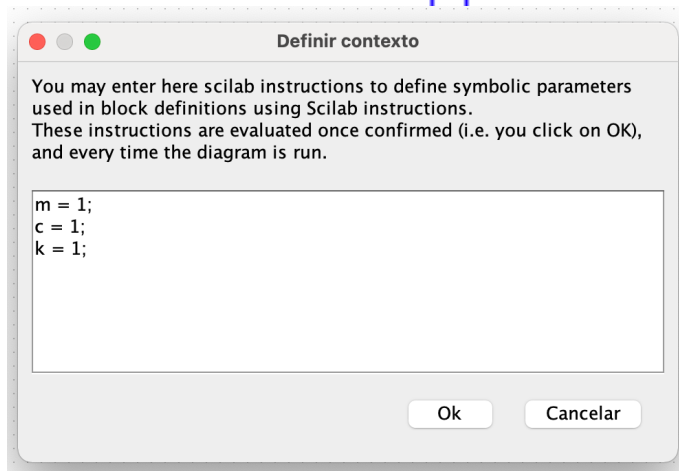
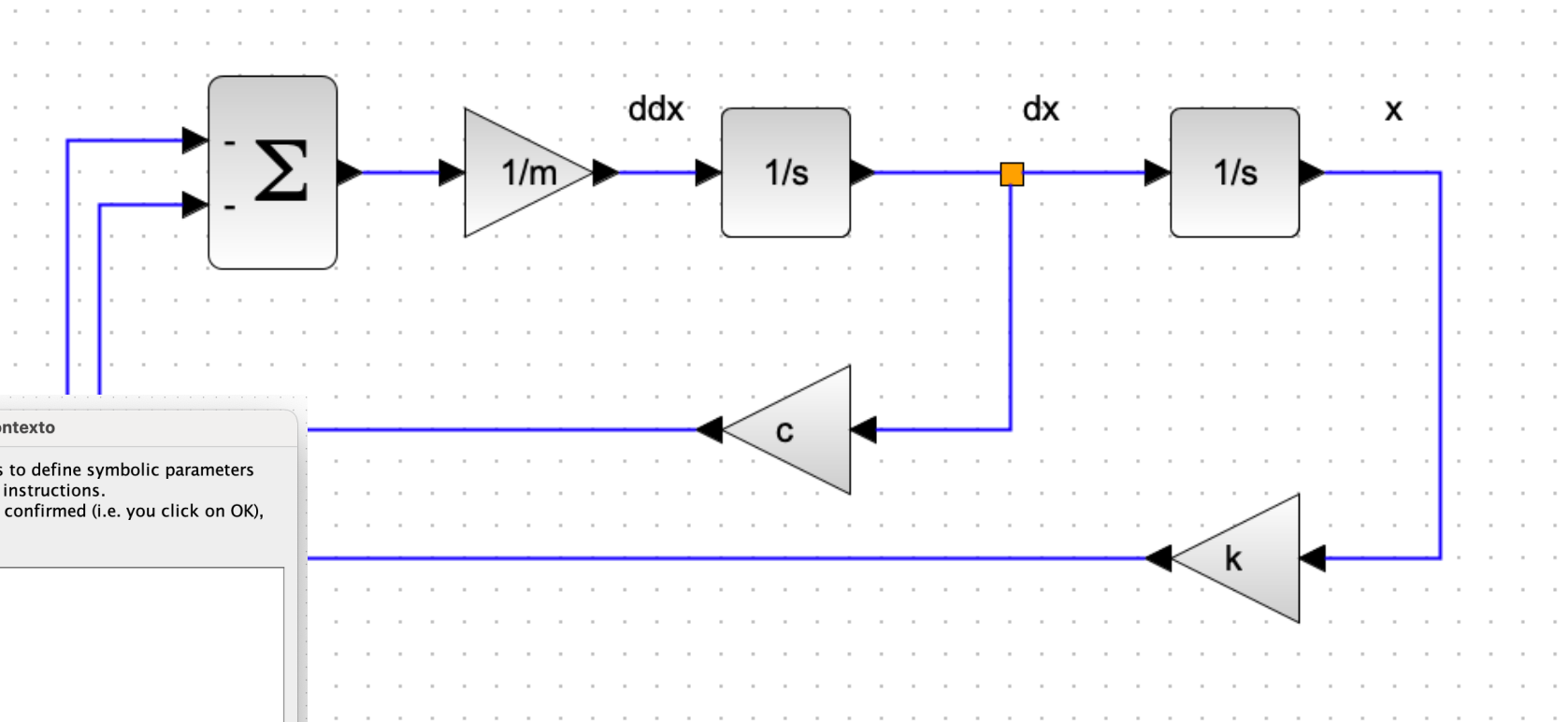
$$\zeta = ?$$

$$c_c = 2\sqrt{km} = 2m\omega_n = 12,56$$

$$c = \zeta c_c = \zeta 2\sqrt{km} = 12,56 \zeta$$

$$f_n = \frac{1}{2\pi} \sqrt{\frac{k}{m}} = 1\text{Hz}$$

Diagrama de bloques





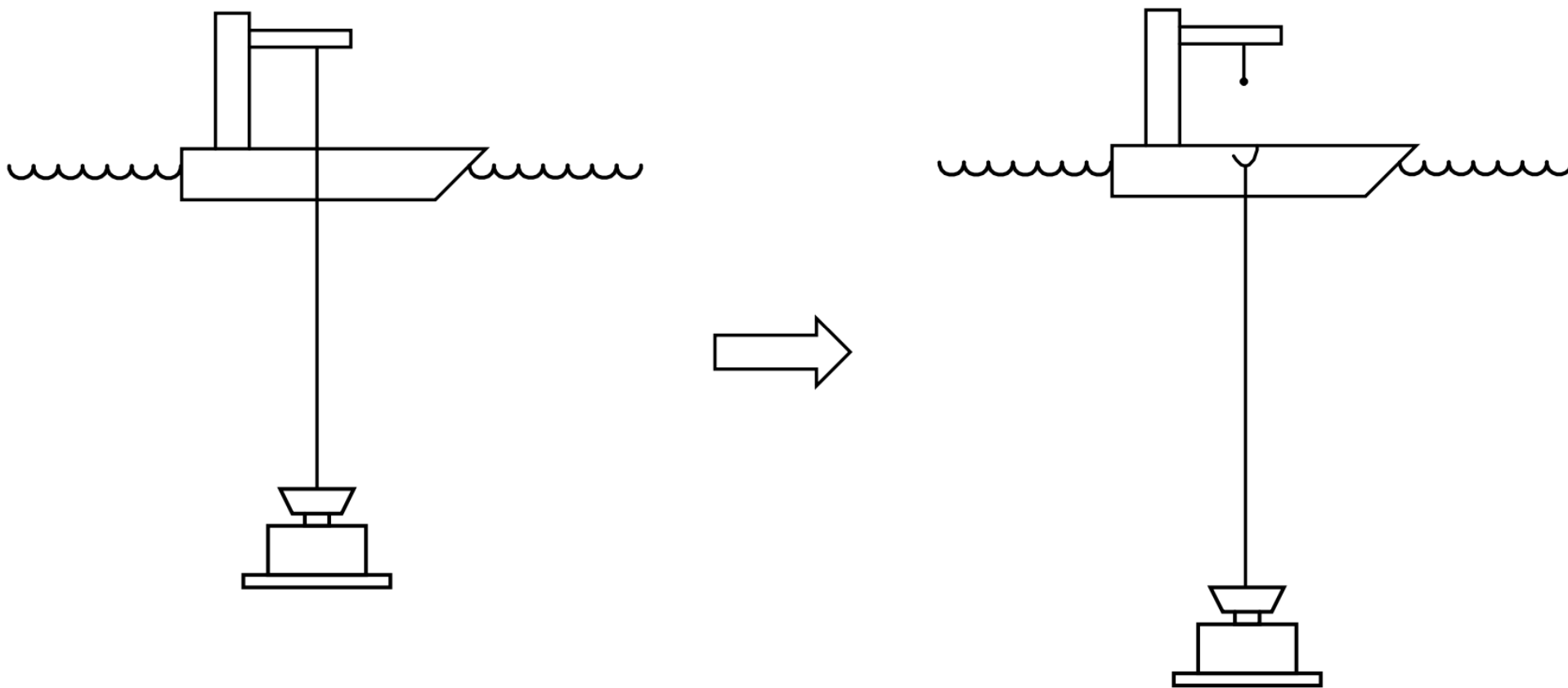
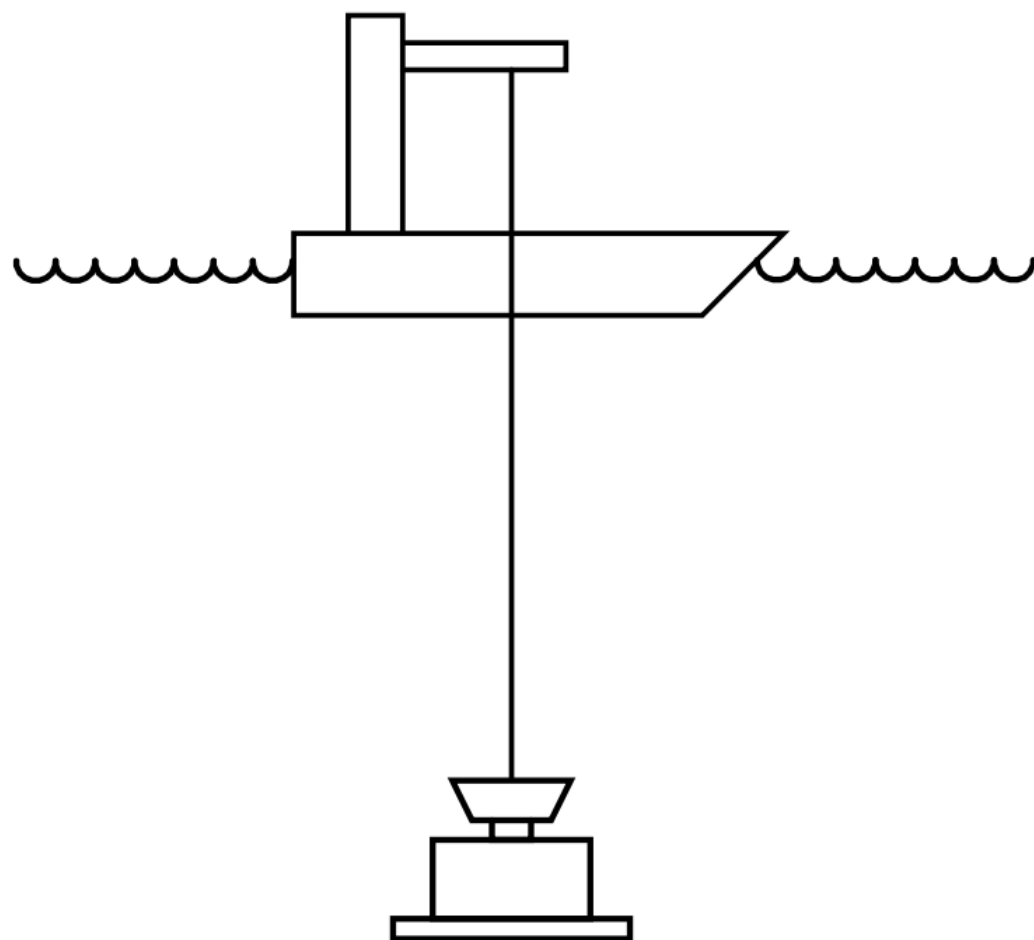
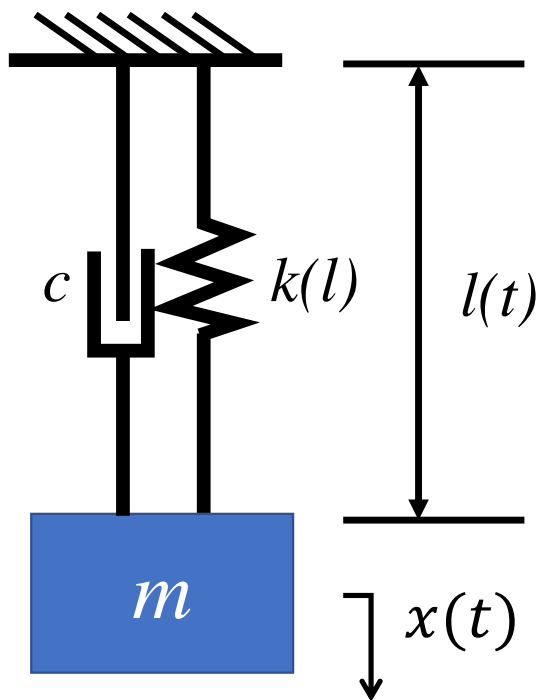


Figura 1.5: Instalação de equipamento submarino por múltiplas lingas.



Modelagem do manifold “em ar”



$$m = 100.000 \text{ kg}$$

$$D = 0,04\text{m}$$

$$L = 3.000 \text{ m}$$

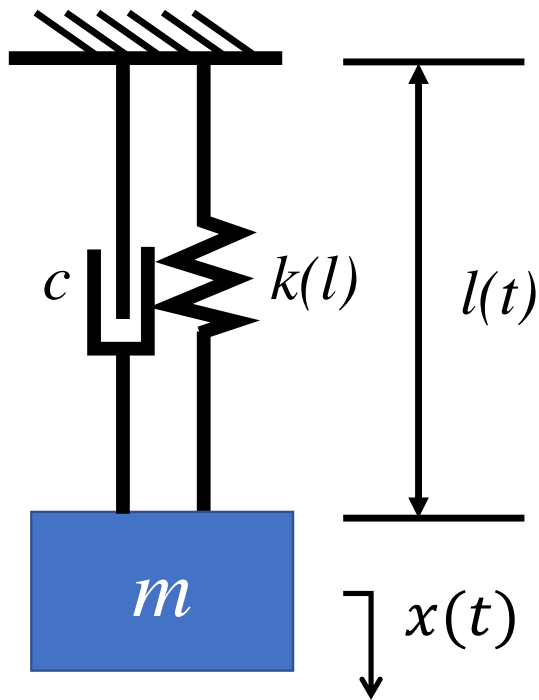
$$k(l) = \frac{AE}{l}$$

$$A = \frac{\pi D^2}{4}$$

Considerando apenas a massa no equipamento

$$f_n = \frac{1}{2\pi} \sqrt{\frac{AE}{lm}}$$

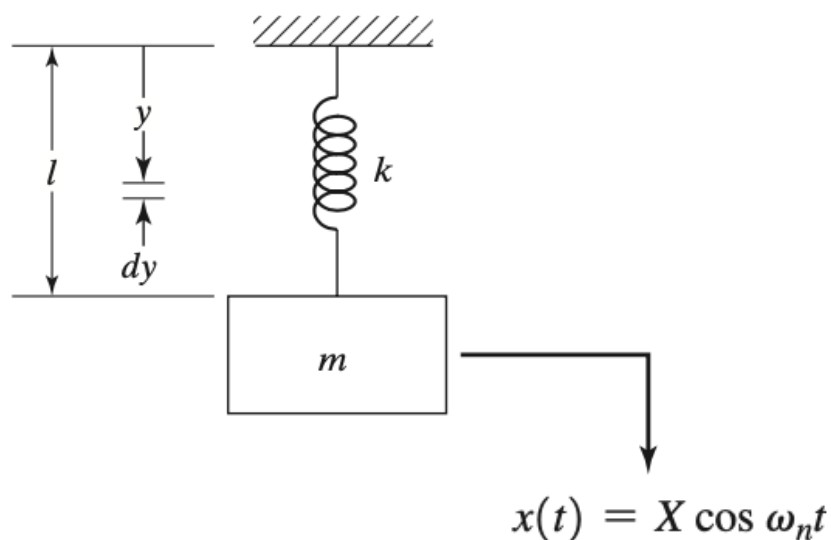
Modelagem do manifold “em ar”



Mas o cabo de aço também contribui com sua massa.

$$m_c(l) = \rho_c A l$$

Contribuição da massa da mola



$$dT_s = \frac{1}{2} \left(\frac{m_s}{l} dy \right) \left(\frac{y\dot{x}}{l} \right)^2$$

$$T = T_m + T_s$$

$$= \frac{1}{2} m \dot{x}^2 + \int_{y=0}^l \frac{1}{2} \left(\frac{m_s}{l} dy \right) \left(\frac{y^2 \dot{x}^2}{l^2} \right)$$

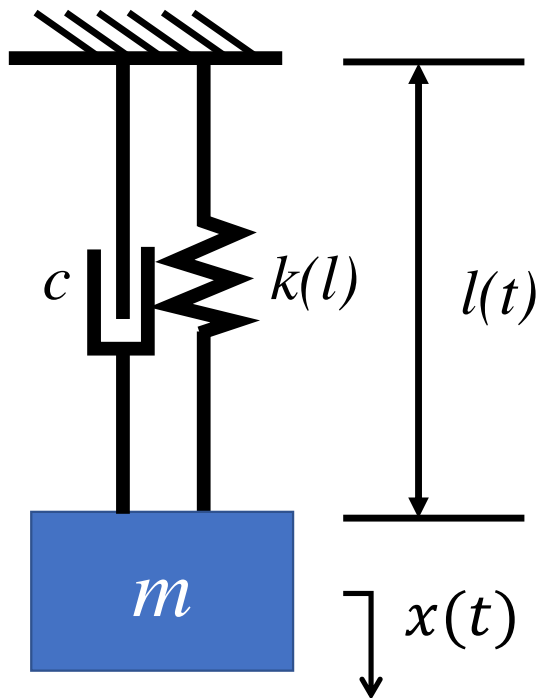
$$= \frac{1}{2} m \dot{x}^2 + \frac{1}{2} \frac{m_s}{3} \dot{x}^2$$

$$T_{\max} = \frac{1}{2} \left(m + \frac{m_s}{3} \right) X^2 \omega_n^2$$

$$U_{\max} = \frac{1}{2} k X^2$$

$$\omega_n = \left(\frac{k}{m + \frac{m_s}{3}} \right)^{1/2}$$

Modelagem do manifold “em ar”



Mas o cabo de aço também contribui com sua massa.

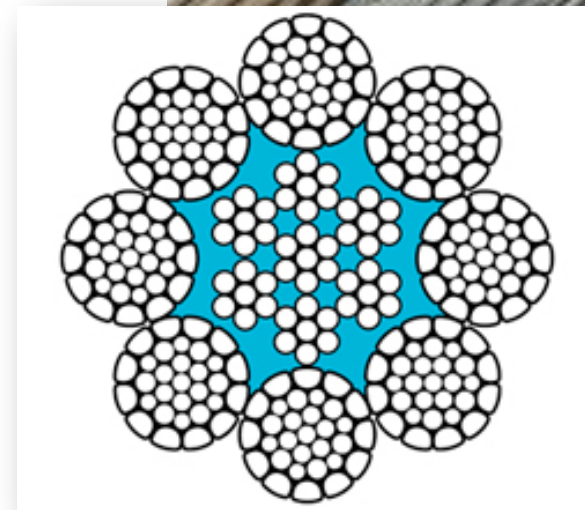
$$m_c(l) = \rho_c A l$$

A frequência natural considerando a massa do equipamento e a massa do cabo...

$$f_n = \frac{1}{2\pi} \sqrt{\frac{AE}{l \left(m + \frac{\rho_c A l}{3} \right)}}$$

Cabo de aço

- Redução do módulo de elasticidade em relação a uma peça sólida.



Módulo de elasticidade do cabo

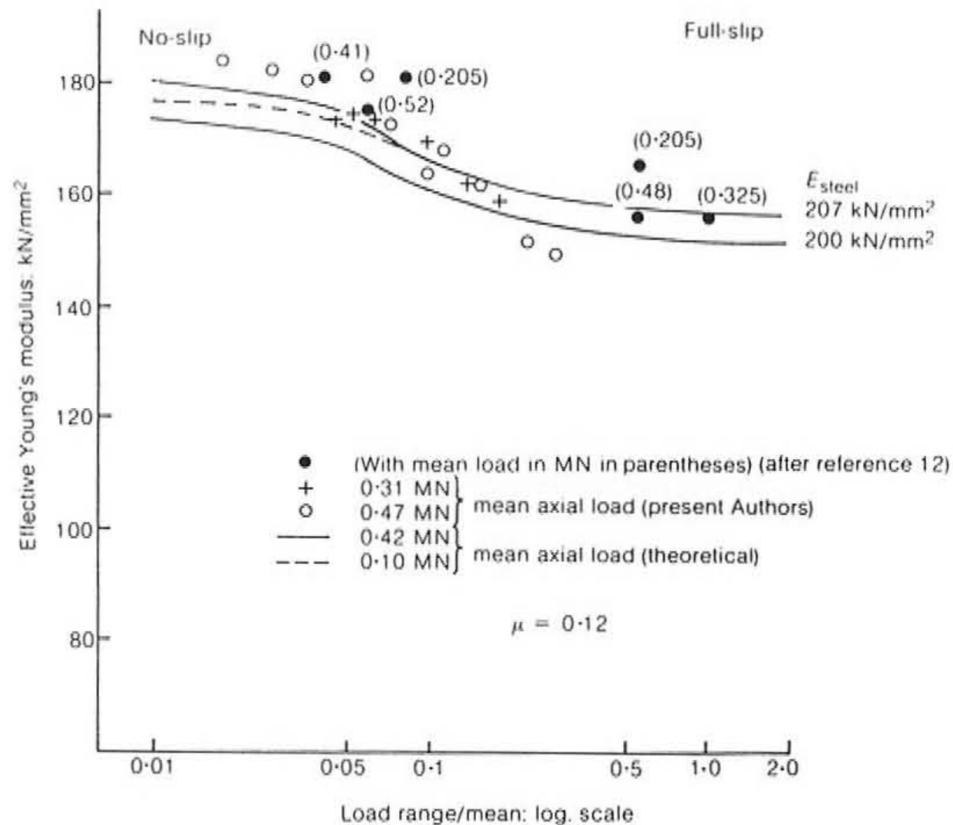


Fig. 3. Axial stiffness results for 39 mm OD strand

$$E_{\text{aço}} = 200 \text{ GPa}$$

$$E_{\text{cabo}} = 160 \text{ GPa}$$

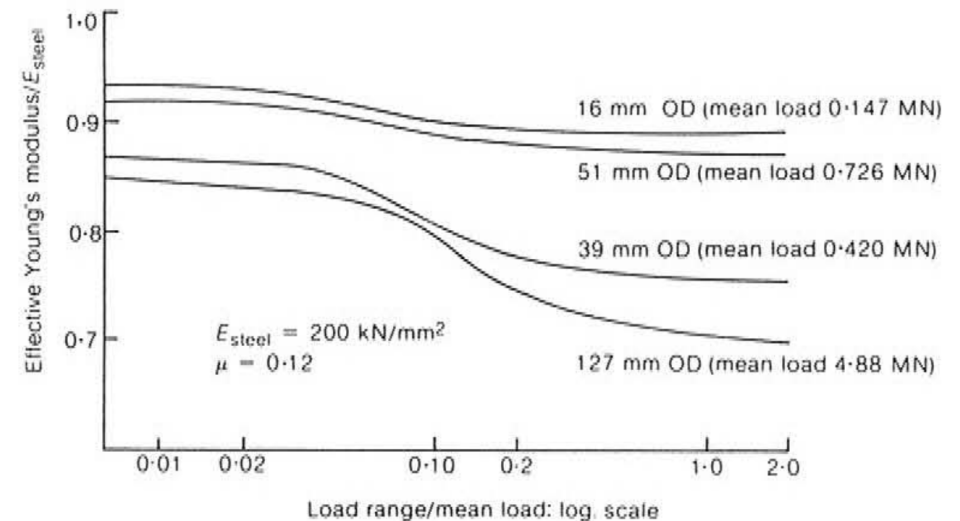
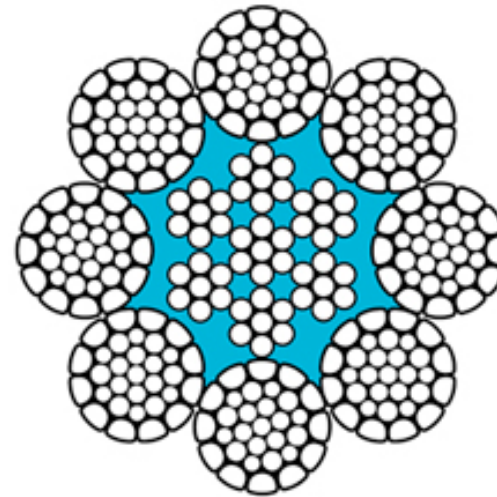


Fig. 4. Axial stiffness results for various cable constructions

Cabo de aço

- Amortecimento histerético: dissipação por atrito nos elementos dentro do cabo
 - Entre fios (domina para grandes cargas)
 - Dentro dos fios sólidos (domina para pequenas cargas)
- Combinação de amortecimento viscoso e de Coulomb (seco)



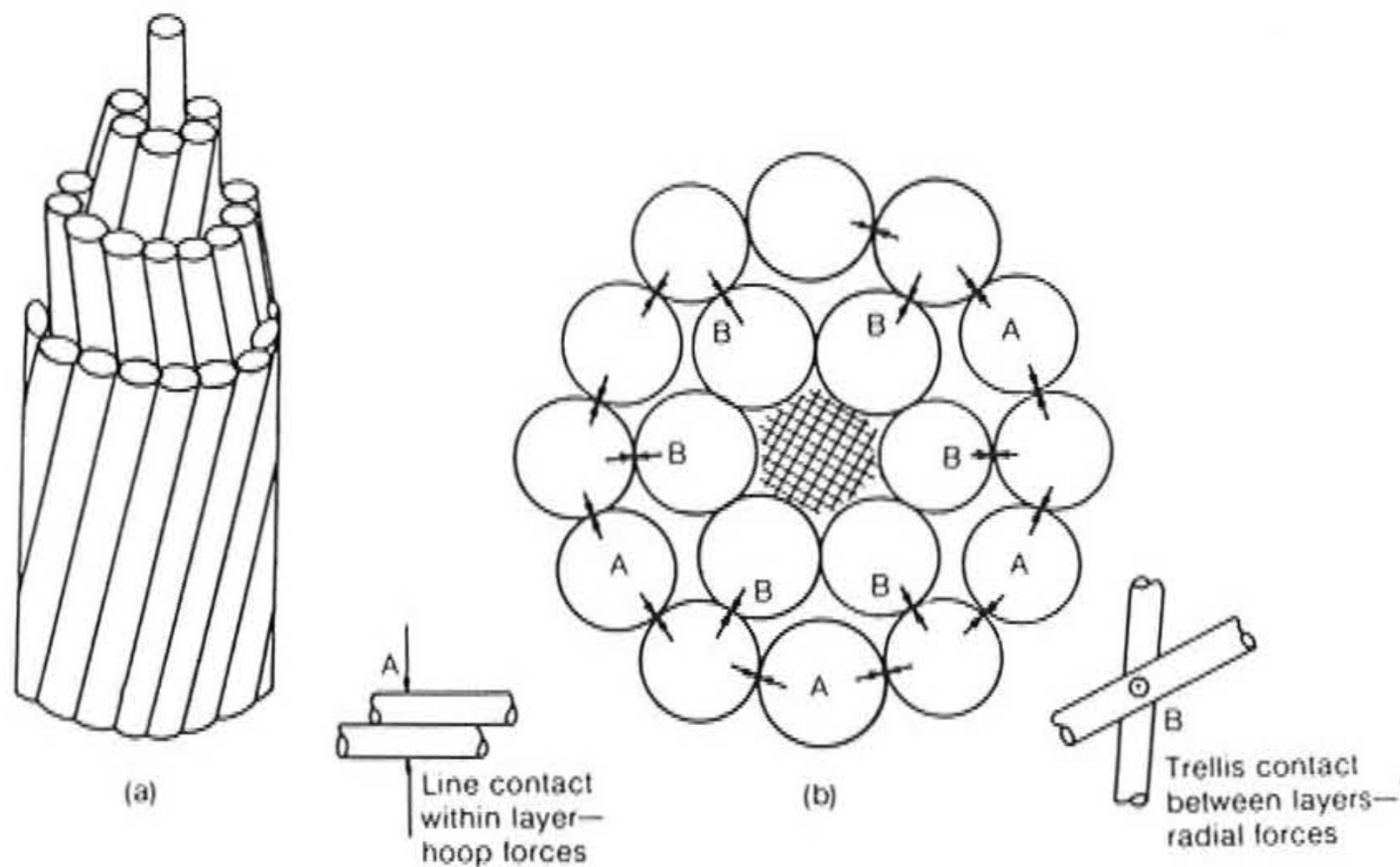
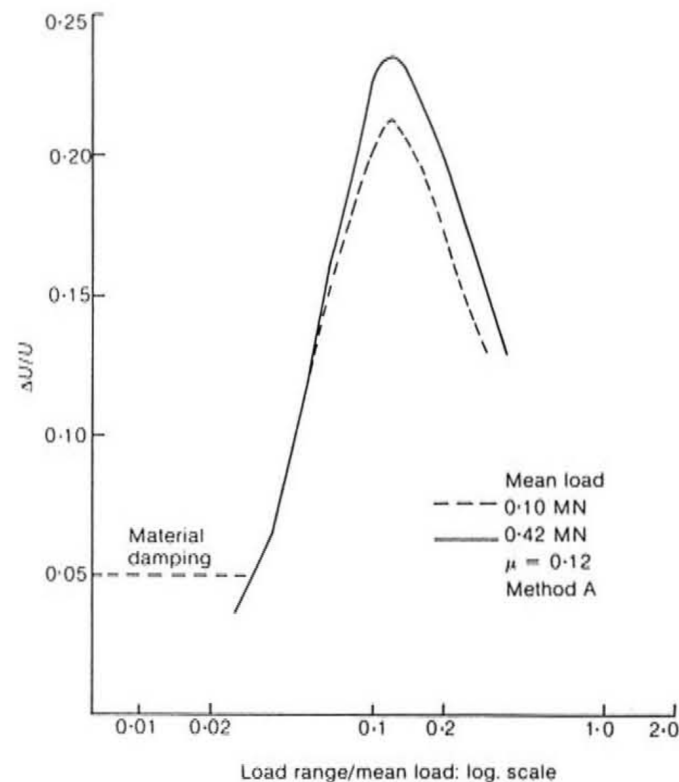


Fig. 1. Interwire contact forces in a multi-layered strand

Amortecimento histerético do cabo



$$U_{max} = \frac{1}{2} k X^2$$

$$\Delta U = \pi \omega c X^2 = \pi h X^2$$

$$h = \frac{\Delta U}{U} \frac{k}{2\pi}$$

$$c = \frac{\Delta U}{U} \frac{k}{4\pi^2 f}$$

Constante de amortecimento histerético

$$c = \frac{h}{\omega}$$

Amortecimento é inversamente proporcional à frequência

Fig. 8. Axial energy dissipation in the 39 mm OD strand—effect of mean axial load

Trabalho de Dinâmica – Parte 1

Considerando a manobra de lançamento vertical de um manifold submarino, apresente:

- Um gráfico da frequência natural do sistema não amortecido em ar em função do comprimento do cabo.
 - Considere a massa do manifold, a massa do cabo e a rigidez do cabo.
- Um gráfico da tensão no topo do cabo em função do comprimento do cabo.

$$m = 100.000 \text{ kg}$$

$$D = 0,04\text{m}$$

$$L = 3.000 \text{ m}$$

$$E_{cabo} = 160\text{GPa}$$