

## Chapter 9 Solutions

**9.1**  $\vec{E}_1 \cdot \vec{E}_2 = (1/2)(\vec{E}_1 e^{-i\omega t} + \vec{E}_1^* e^{i\omega t}) \cdot (1/2)(\vec{E}_2 e^{-i\omega t} + \vec{E}_2^* e^{i\omega t})$ , where

$$\text{Re}(z) = (1/2)(z + z^*).$$

$$\vec{E}_1 \cdot \vec{E}_2 = (1/4)[\vec{E}_1 \cdot \vec{E}_2 e^{-2i\omega t} + \vec{E}_1^* \cdot \vec{E}_2^* e^{2i\omega t} + \vec{E}_1 \cdot \vec{E}_2^* + \vec{E}_1^* \cdot \vec{E}_2].$$

The last two terms are time independent, while  $\langle \vec{E}_1 \cdot \vec{E}_2 e^{-2i\omega t} \rangle \rightarrow 0$  and  $\langle \vec{E}_1^* \cdot \vec{E}_2^* e^{2i\omega t} \rangle \rightarrow 0$  because of the  $1/T\omega$  coefficient. Thus

$$I_{12} = 2 \langle \vec{E}_1 \cdot \vec{E}_2 \rangle = (1/2)(\vec{E}_1 \cdot \vec{E}_2^* + \vec{E}_1^* \cdot \vec{E}_2).$$

**9.2** The largest value of  $r_1 - r_2$  is equal to  $a$ . Thus if  $\epsilon_1 = \epsilon_2$ ,  $\delta = k(r_1 - r_2)$  varies from 0 to  $ka$ . If  $a \gg \lambda$ ,  $\cos \delta$  and therefore  $I_{12}$  will have a great many maxima and minima and therefore average to zero over a large region of space. In contrast if  $a \ll \lambda$ ,  $\delta$  varies only slightly from 0 to  $ka \ll 2\pi$ . Hence  $I_{12}$  does not average to zero, and from Eq. (9.17),  $I$  deviates little from  $4I_0$ . The two sources effectively behave as a single source of double the original strength.

**9.3** Dropping the common time factor  $E_1 = E_0 \exp(2\pi iz/\lambda)$  and  $E_2 = E_0 \exp[(2\pi i/\lambda)(z \cos \theta + y \sin \theta)]$ , adding these at the  $z = 0$  plane yields  $E = E_0 \{1 + \exp[(2\pi i/\lambda)(y \sin \theta)]\}$ . The absolute square of this is the irradiance viz.

$$I(y) = 2E_0^2 \left[ 1 + \cos \left( \frac{2\pi}{\lambda} y \sin \theta \right) \right]$$

and the rest follows from the identity  $\cos 2\theta = 2 \cos^2 \theta - 1$ . The cosine squared has zeros at  $y = m\lambda/(2 \sin \theta)$  where  $m$  is an odd integer. The fringe separation is  $\lambda/\sin \theta$ . As  $\theta$  increases, the separation decreases.

**9.4** A bulb at  $S$  would produce fringes. We can imagine it as made up of a very large number of incoherent point sources. Each of these would generate an independent pattern, all of which would then overlap. Bulbs at  $S_1$  and  $S_2$  would be incoherent and could not generate detectable fringes.

**9.5**  $y_m = sm\lambda/a \approx 14.5 \times 10^{-2}$  m and  $\lambda = 0.0145$  m:  $\nu = v/\lambda = 23.7$  kHz.  
This is Young's Experiment with the sources out-of-phase.

**9.6** This is comparable to the "two-slit" configuration, (Figure 9.11), so we can use (9.29)  $a \sin \theta_m = m\lambda$  ( $\theta_m$  may not be "small"). Let  $m = 1$ ,  $\sin \theta = y/(s^2 + y^2)^{1/2}$ , so,

$$ay = \lambda(s^2 + y^2)^{1/2}; \quad (a^2 - \lambda^2)y^2 = \lambda^2 s^2;$$

$$y = \lambda s / (a^2 - \lambda^2)^{1/2}. \quad c = \nu \lambda,$$

so  $\lambda = c/\nu = (3 \times 10^8 \text{ m/s}) / (1.0 \times 10^6 \text{ Hz}) = 300$  m.

$$y = (300 \text{ m})(2000 \text{ m}) / ((600 \text{ m})^2 - (300 \text{ m})^2)^{1/2} = 1.15 \times 10^3 \text{ m}$$

$$9.7 \quad \Delta y = \frac{s}{a} \lambda$$

$$s = \frac{a \Delta y}{\lambda}$$

Using  $a = 1 \times 10^{-4}$  m,  $\lambda = 589$  nm,  $\Delta y = 3.00$  mm

$$s = \frac{(1 \times 10^{-4} \text{ m})(3 \times 10^{-3} \text{ m})}{5.89 \times 10^{-7} \text{ m}} = 0.509 \text{ m}$$

$$9.8 \quad \Delta y_{vac} = \frac{s}{a} \lambda_0$$

Using  $a = 1 \times 10^{-3}$  m,  $\lambda_0 = 589.3$  nm,  $s = 5.000$  m

$$\Delta y_{vac} = \frac{5.000 \text{ m}}{(1 \times 10^{-3} \text{ m})} (5.893 \times 10^{-7} \text{ m}) = 2.9465 \text{ mm}$$

$$n = \frac{c}{v} = \frac{v \lambda_0}{v \lambda} = \frac{\lambda_0}{\lambda}$$

$$\lambda = \frac{\lambda_0}{n}$$

$$\Delta y_{air} = \frac{s}{a} \lambda = \frac{s}{a} \frac{\lambda_0}{n}$$

$$\Delta y_{air} = \frac{5.000 \text{ m}}{(1 \times 10^{-3} \text{ m})} \frac{5.893 \times 10^{-7} \text{ m}}{1.00029} = 2.9456 \text{ mm}$$

Thus the pattern expands from 2.946 mm to 2.947 mm.

$$9.9 \quad (a) \quad r_1 - r_2 = \pm \lambda / 2, \text{ hence } a \sin \theta_1 = \pm \lambda / 2 \text{ and}$$

$$\theta_1 \approx \pm \lambda / 2a = \pm (1/2)(632.8 \times 10^{-9} \text{ m}) / (0.200 \times 10^{-3} \text{ m})$$

$$= \pm 1.58 \times 10^{-3} \text{ rad,}$$

or since

$$y_1 = s \theta_1 = (1.00 \text{ m})(\pm 1.58 \times 10^{-3} \text{ rad}) = \pm 1.58 \text{ mm.}$$

(b)  $y_5 = s 5 \lambda / a = (1.00 \text{ m}) 5 (632.8 \times 10^{-9}) / (0.200 \times 10^{-3} \text{ m}) = 1.582 \times 10^{-2} \text{ m}$ . (c) Since the fringes vary as cosine-squared and the answer to (a) is half a fringe width, the answer to (b) is 10 times larger.

$$9.10 \quad y_1 = \frac{s}{a} m \lambda = \frac{s}{a} m \frac{\lambda_0}{n}$$

Using  $a = 1 \times 10^{-3}$  m,  $\lambda_0 = 589.3$  nm,  $s = 3.000$  m,  $n = 1.33$

$$y_1 = \frac{3.000 \text{ m}}{(1 \times 10^{-3} \text{ m})} \frac{5.893 \times 10^{-7} \text{ m}}{1.33} = \pm 1.329 \text{ mm}$$

$$9.11 \quad \theta_m \text{ is "small," so we can use (9.28) } \theta_m = m \lambda / a, \theta_m \text{ is radian,}$$

$$a = m \lambda / \theta_m = [4(6.943 \times 10^{-7} \text{ m})] / [1^\circ (2\pi \text{ rad}/360^\circ)] = 1.59 \times 10^{-4} \text{ m.}$$

9.12  $\Delta y \approx (s/a)\lambda$ , so,

$$s = a\Delta y/\lambda = [(1.0 \times 10^{-4} \text{ m})(10 \times 10^{-3} \text{ m})]/(4.8799 \times 10^{-7} \text{ m}) = 2.05 \text{ m}.$$

9.13 (9.28)  $\theta_m = m\lambda/a$ . Want  $\theta_{1,\text{red}} = \theta_{2,\text{violet}}$ ;  $(1)\lambda_{\text{red}}/a = (2)\lambda_{\text{violet}}/a$ ;  $\lambda_{\text{violet}} = 390 \text{ nm}$ .

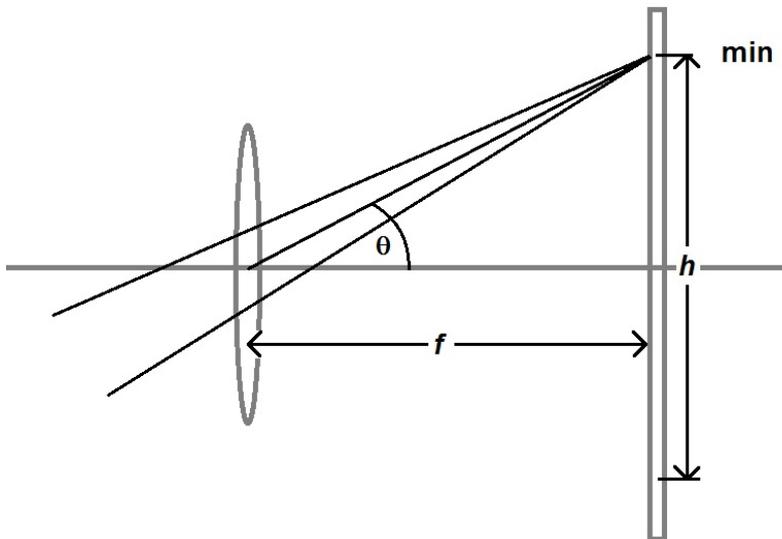
9.14  $y_1 = \frac{s}{a}m\lambda$

$$\theta_m \approx \frac{y_m}{s} = \frac{m\lambda}{a}$$

$$s = f$$

$$y_m = f\theta_m = \frac{mf\lambda}{a}$$

9.15



$$f\theta = \frac{h}{2}$$

$$r_1 - r_2 = \frac{\lambda}{2} = a\theta$$

$$\theta = \frac{\lambda}{2a}$$

$$\frac{h}{2} = f\theta = \frac{f\lambda}{2a}$$

$$h = \frac{f\lambda}{a}$$

9.16 Follow section (9.3.1), except that (9.26) becomes  $r_1 - r_2 = (2m' - 1)(\lambda/2)$  for destructive interference, where  $m' = \pm 1, \pm 2, \dots$ , so that  $(2m' - 1)$  is an odd integer. This leads to an expression equivalent to (9.28),  $\theta_{m'} = (2m - 1)\lambda/2a$ .

$$9.17 \quad y_m = \frac{s}{a} m \lambda$$

$$\lambda = y_m \frac{a}{ms}$$

Using  $a = 2.7 \times 10^{-3}$  m,  $s = 4.60$  m,  $m = 5$ :

$$\lambda = (5 \times 10^{-3} \text{ m}) \frac{2.7 \times 10^{-4} \text{ m}}{5(4.60 \text{ m})} = 587 \text{ nm}$$

9.18 Follow section (9.3.1), except that (9.26) becomes  $r_1 - r_2 + \Lambda = m\lambda$ , where  $\Lambda =$  Optical path differences in beam. Following  $r_1$ ,  $\Lambda = nd$  (for  $\theta_m$  “small”).

$$(r_1 - r_2) = m\lambda - \Lambda; \quad a\theta_m = m\lambda - nd; \quad \theta_m = (m\lambda - nd)/a.$$

9.19 As in section (9.3.1), we have constructive interference when  $OPD = m\lambda$ . There is an added OPD due to the angle,  $\theta$ , of the plane wave equal to  $a \sin \theta$ , so (9.26) becomes  $r_1 - r_2 + a \sin \theta = m\lambda$ .

(9.24)  $\theta_m \approx y/s$  and (9.25)  $r_1 - r_2 \approx ay/s$  are unchanged, for small  $\theta_m$  so

$$r_1 - r_2 = m\lambda - a \sin \theta = a(y/s) = a\theta_m; \quad \theta_m = (m\lambda/a) - \sin \theta.$$

$$9.20 \quad (9.27) \quad y_m = (s/a)m\lambda; \quad y_{1, \text{red}} = [(2.0 \text{ m})/(2.0 \times 10^{-4} \text{ m})](1)(4 \times 10^{-7} \text{ m}) \\ = 4.0 \times 10^{-3} \text{ m}.$$

$$y_{1, \text{violet}} = [(2.0 \text{ m})/(2.0 \times 10^{-4} \text{ m})](2)(6 \times 10^{-7} \text{ m}) = 12.0 \times 10^{-3} \text{ m}.$$

$$\text{Distance} = 8.0 \times 10^{-3} \text{ m}.$$

9.21  $r_2^2 = a^2 + r_1^2 - 2ar_1 \cos(90^\circ - \theta)$ . The contribution to  $\cos \delta/2$  from the third term in the Maclaurin expansion will be negligible if

$$(k/2)(a^2 \cos^2 \theta/2r_1) \ll \pi/2; \quad \text{therefore} \quad r_1 \ll a^2/\lambda.$$

$$9.22 \quad E = mv^2/2; \quad v = 0.42 \times 10^6 \text{ m/s}; \quad \lambda = h/mv = 1.73 \times 10^{-9} \text{ m}; \quad \Delta y = s\lambda/a = 3.46 \text{ mm}.$$

$$9.23 \quad \Delta v/\Delta \lambda = v/\lambda; \quad \delta v = v\Delta \lambda/\lambda = 1/\Delta t_c;$$

$$c = v\lambda, \quad \text{so} \quad v = c/\lambda.$$

$$\delta v = (c/\lambda)\Delta \lambda/\lambda = c\Delta \lambda/\lambda^2;$$

$$\Delta t_c = \lambda^2/c\Delta \lambda; \quad \Delta t_c = c\Delta t_c = (\lambda^2/\Delta \lambda)$$

$$= (500 \text{ nm})^2/(2.5 \times 10^{-3} \text{ nm})$$

$$= 1 \times 10^8 \text{ nm} = 0.1 \text{ m} \approx \Lambda.$$

$$9.24 \quad \bar{E} = E_o e^{i\omega t} + E_o e^{i\omega t + \delta} + E_o e^{i(\omega t + 5\delta/2)}. \quad I = \langle \bar{E}^2 \rangle_T = \langle \bar{E} \cdot \bar{E} \rangle_T, \quad \text{so, as in section 9.1,}$$

$I = (3/2)E_o^2 + 2E_o^2 \{ \frac{1}{2}(\cos \delta + \cos(3\delta/2) + \cos(5\delta/2)) \}$  (three terms of  $\bar{E}_i \cdot \bar{E}_i$ , 3 cross terms of  $\bar{E}_i \cdot \bar{E}_j$ ). For each beam,

$$I_i = \langle \bar{E}_i^2 \rangle_T = \frac{1}{2} E_o^2,$$

at  $\theta = 0$ , so that for all three together  $I(\theta = 0) = \frac{3}{2} E_o^2$ . Note that  $(r_2 - r_1) = a \sin \theta$  so that

$$\delta_2 = k(r_2 - r_1) = k(a \sin \theta); \quad (r_3 - r_1) = (5a/2) \sin \theta$$

so that  $\delta_3 = k(r_3 - r_1) = k(\frac{5}{2}a \sin \theta)$  where  $\delta = ka \sin \theta$ . So,

$$I(\theta) = I(0)/3 + (2I(0)/9)(\cos \delta + \cos(3\delta/2) + \cos(5\delta/2))$$

When  $\theta = 0$ , the second term is zero.

$$\begin{aligned} 9.25 \quad \Delta y &= \frac{(R+d)\lambda}{2R\theta} \\ \theta &= \frac{(R+d)\lambda}{2R\Delta y} \end{aligned}$$

Using  $\lambda = 6.000 \times 10^{-7}$  m,  $R = 1.000$  m,  $d = 3.900$  m,  $\Delta y = 2 \times 10^{-3}$  m:

$$\theta = \frac{(1.000 \text{ m} + 3.900 \text{ m})(6.000 \times 10^{-7} \text{ m})}{2(1.000 \text{ m})(2 \times 10^{-3} \text{ m})} = 0.000735 \text{ rad} = 0.0421^\circ$$

$$\begin{aligned} 9.26 \quad S &= Z = R + d = 1 + d \\ d &= 1 \end{aligned}$$

$$\begin{aligned} \Delta y &= \frac{(R+d)\lambda}{2R\theta} \\ \theta &= \frac{\lambda}{\Delta y} = \frac{5.89 \times 10^{-7} \text{ m}}{5 \times 10^{-4} \text{ m}} = 0.00118 \text{ rad} \end{aligned}$$

9.27 A ray from  $S$  hits the biprism at an angle  $\theta_i$  (w.r.t normal), is refracted at angle  $\theta_r$ , and hits the second face at angle  $(\theta_r + \alpha)$ .

(4.4) (1)  $\sin \theta_i = (n) \sin \theta_r$ .  $(n) \sin(\theta_r + \alpha) = (1) \sin(\theta/2 + \alpha)$ , where angle  $\theta$  is defined in Figure 9.24.

As  $\theta_i \rightarrow 0$ ,  $\theta_r \rightarrow 0$ ;  $\alpha, \theta$  are both "small."

$n \sin \alpha = \sin(\theta/2 + \alpha)$ , so  $n\alpha = (\theta/2) + \alpha$ ,  $\theta = 2(n-1)\alpha$ . From the figure  $\tan(\theta/2) = (a/2)/d$ , so

$$\theta/2 \approx (a/2)/d, \quad \theta = a/d. \quad a/d = 2(n-1)\alpha, \quad a = 2d(n-1)\alpha.$$

9.28 From Problem 9.19,  $a = 2d(n-1)\alpha$ ;  $s = 2d$ , so  $d = 1m$ .

$$\begin{aligned} \Delta y &= (s/a)\lambda = s\lambda/2d(n-1)\alpha; \quad \alpha = s\lambda/2d(n-1)\Delta y \\ &= [(2m)(5.00 \times 10^{-7} \text{ m})]/[2(1 \text{ m})(1.5-1)(5 \times 10^{-4} \text{ m})] = 0.002 \text{ rad}. \end{aligned}$$

$$9.29 \quad \Delta y = s\lambda_0/2d\alpha(n-n').$$

9.30 Using  $\lambda = 5.893 \times 10^{-7}$  m,  $s = 5.00$  m,  $a = 1 \times 10^{-2}$  m:

$$2\Delta y = 2 \frac{s}{a} \lambda = 2 \frac{(5.00 \text{ m})(5.893 \times 10^{-7} \text{ m})}{2(1 \times 10^{-2} \text{ m})} = 0.295 \text{ mm}$$

$$9.31 \quad \Delta y = (s/a)\lambda, \quad a = 10^{-2} \text{ cm}, \quad a/2 = 5 \times 10^{-3} \text{ cm}.$$

9.32  $\delta = k(r_1 - r_2) + \pi$  Lloyd's mirror,

$$\begin{aligned} \delta &= k((a/2) \sin \alpha - [\sin(90^\circ - 2\alpha)] (a/2) \sin \alpha) + \pi, \\ \delta &= ka(1 - \cos 2\alpha)/2 \sin \alpha + \pi, \end{aligned}$$

maximum occurs for  $\delta = 2\pi$  when  $\sin \alpha(\lambda/a) = (1 - \cos 2\alpha) = 2 \sin^2 \alpha$ .

First maximum  $\alpha = \sin^{-1}(\lambda/2a)$ .

- 9.33**  $E_{1r}$  is reflected once.  $E_{1r} = E_{oi} r_{\theta=0}$  (see 4.47)  
 $= E_{oi} (n-1)/(n+1) = E_{oi} (1.52-1)/(1.52+1) = 0.206E_{oi}$ .  
 $E_{2r}$  is transmitted once, reflected once, then transmitted.  
 $E_{2r} = E_{oi} (t_{\theta=0})(r'_{\text{glass-air}})(t'_{\text{glass-air}}) = E_{oi} [2/(1+n)][(1-n)/(1+n)][2n/(n+1)]$   
 $= 4n(1-n)/(n+1)^3 = E_{oi} [4(1.52)(1-1.52)]/(1+1.52)^3 = -0.198E_{oi}$ ,  
 (see 4.48) (- indicates  $\pi$  phase changed).

$E_{3r}$  is transmitted, reflected 3 times (internally), and then transmitted.

$$\begin{aligned} E_{3r} &= E_{oi} t(r')^3 t' = E_{oi} [2/(1+n)][(1-n)/(1+n)]^3 [(2n)/(n+1)] \\ &= [4n(1-n)^3]/(n+1)^5 = E_{oi} [4(1.52)(1-1.52)^3]/(1.52+1)^5 \\ &= -0.008E_{oi} \end{aligned}$$

for water in air.

$$\begin{aligned} E_{1r} &= E_{oi} (1.333-1)/(1.333+1) = 0.143E_{oi}. \\ E_{2r} &= E_{oi} [4(1.333)(1-1.333)]/(1+1.333)^3 = -0.140E_{oi}. \\ E_{3r} &= E_{oi} [4(1.333)(1-1.333)^3]/(1.333+1)^5 = -0.003E_{oi}. \end{aligned}$$

- 9.34** Here  $1.00 < 1.34 < 2.00$ , hence from Eq. (9.36) with  $m = 0$ ,  
 $d = (0 + 1/2)(633 \text{ nm})/2(1.34) = 118 \text{ nm}$ .
- 9.35** (9.36)  $d \cos \theta_i = (2m+1)(\lambda_f)/4$  for a maximum at (near) normal incidence, and taking  $m = D$  (lowest value)

$$d = \lambda_f/4 = \lambda_o/4n = (5.00 \times 10^{-7} \text{ m})/4(1.36) = 9.2 \times 10^{-6} \text{ m}.$$

- 9.36**  $d \cos \theta_i = 2m \left( \frac{\lambda_m}{4} \right)$  for minimum reflection  $= 2m(\lambda_o/4n)$   
 at  $\theta \approx 0, \lambda_o = \frac{2nd}{m} = \frac{[2(1.34)(550.0 \text{ nm})]}{m} = \frac{(1474 \text{ nm})}{m}$   
 for  $m = 1, 2, 3, \dots$ ;  $\lambda_o = 1474 \text{ nm}, 737 \text{ nm}, 368.5 \text{ nm}, \dots$

- 9.37** In this case, one drops the relative phase shift of  $\pi$  from (9.34):

$$\begin{aligned} \delta &= \frac{4\pi n_f}{\lambda_o} d \cos \theta_i \\ 2\pi &= \frac{4\pi n_f}{\lambda_o} d \cos \theta_i \\ \cos \theta_i &= \frac{\lambda_o}{2n_f d} = \frac{(4.60 \times 10^{-7} \text{ m}) 25 \text{ nm}}{2(1.333)(2.50 \times 10^{-8} \text{ m})} = 2.5 \times 10^{-8} \text{ m} \\ \theta_i &= 46.356^\circ \\ \sin \theta_i &= (1.333) \sin(46.356^\circ) = 0.9646 \\ \theta_i &= 74.7^\circ \end{aligned}$$

- 9.38** Eq. (9.37)  $m = 2n_f d/\lambda_o = 10,000$ . A minimum, therefore central dark region.
- 9.39** The fringes are generally a series of fine jagged bands, which are fixed with respect to the glass.
- 9.40**  $\Delta x = \lambda_f/2\alpha$ ,  $\alpha = \lambda_o/2n_f \Delta x$ ,  $\alpha = 5 \times 10^{-5} \text{ rad} = 10.2 \text{ seconds}$ .

9.41 (9.40)  $\Delta x = \lambda_f/2\alpha$  for fringe separation where  $\alpha = d/x$ .

$\Delta x = \lambda_f/2(d/x) = x\lambda_f/2d$ . Number of fringes = (length)/(separation) =  $x/\Delta x$  so,

$$x/\Delta x = 2d/\lambda_f = [2(7.618 \times 10^{-5} \text{ m})]/(5.00 \times 10^{-7} \text{ m}) = 304.72 = 304 \text{ fringes.}$$

9.42 
$$d_m = \left(m + \frac{1}{2}\right) \frac{\lambda_f}{2}$$

$$d_{172} = \left(172 + \frac{1}{2}\right) \frac{(5.893 \times 10^{-7} \text{ m})}{2} = 50.8 \mu\text{m}$$

9.43  $x^2 = d_1[(R_1 - d_1) + R_1] = 2R_1d_1 - d_1^2$ . Similarly  $x^2 = 2R_2d_2 - d_2^2$ .

$d = d_1 - d_2 = (x^2/2)(1/R_1 - 1/R_2)$ ,  $d = m\lambda_f/2$ . As  $R_2 \rightarrow \infty$ ,  $x_m$  approaches Eq. (9.43).

9.44 (9.42)  $x_m = [(m + 1/2)\lambda_f R]^{1/2}$ , air film,  $n_f = 1$ , so  $\lambda_f = \lambda_o$ .

$$R = x_m^2 / (m + 1/2)\lambda_o = (0.01 \text{ m})^2 / (20.5)(5 \times 10^{-7} \text{ m}) = 9.76 \text{ m.}$$

9.45 
$$x_m^2 - x_{m-1}^2 = \lambda_f R(m_m - m_{m-1})$$

$$R = \frac{x_m^2 - x_{m-1}^2}{\lambda_f R(m_m - m_{m-1})}$$

Use

$$2d_m = \left(m + \frac{1}{2}\right) \lambda_0$$

$$m = \frac{2d_m - \frac{1}{2}\lambda_0}{\lambda_0}$$

Since the offset is a constant  $\Delta d$ :

$$R = \frac{x_m^2 - x_{m-1}^2}{\frac{\lambda_f}{\lambda_0} R \left( 2d_m + \Delta d - \frac{1}{2} - \left( 2d_{m-1} + \Delta d - \frac{1}{2} \right) \right)}$$

$$R = \frac{n_f (x_m^2 - x_{m-1}^2)}{2R(d_m - d_{m-1})}$$

Thus the radius of curvature can be measured independent of  $\Delta d$ .

9.46  $x_m = (m\lambda_f R)^{1/2}$

$$x_{m+1} - x_m = (\lambda_f R)^{1/2} (\sqrt{m+1} - \sqrt{m})$$

$$x_{m+2} - x_{m+1} = (\lambda_f R)^{1/2} (\sqrt{m+2} - \sqrt{m+1})$$

$$\frac{x_{m+1} - x_m}{x_{m+2} - x_{m+1}} = \frac{(\lambda_f R)^{1/2} (\sqrt{m+1} - \sqrt{m})}{(\lambda_f R)^{1/2} (\sqrt{m+2} - \sqrt{m+1})} = \frac{\sqrt{m+1} - \sqrt{m}}{\sqrt{m+2} - \sqrt{m+1}}$$

Expand the square roots for large  $m$  (keeping only the first few terms):

$$\begin{aligned}\sqrt{m} &= m^{1/2} \\ \sqrt{m+1} &= m^{1/2} + \frac{1}{2}m^{-1/2} - \frac{1}{8}m^{-3/2} \\ \sqrt{m+2} &= m^{1/2} + m^{-1/2} - \frac{1}{2}m^{-3/2} \\ \frac{x_{m+1} - x_m}{x_{m+2} - x_{m+1}} &= \frac{m^{1/2} + \frac{1}{2}m^{-1/2} - \frac{1}{8}m^{-3/2} - m^{1/2}}{m^{1/2} + m^{-1/2} - \frac{1}{2}m^{-3/2} - m^{1/2} - \frac{1}{2}m^{-1/2} + \frac{1}{8}m^{-3/2}} \\ &= \frac{\frac{1}{2}m^{-1/2} - \frac{1}{8}m^{-3/2}}{\frac{1}{2}m^{-1/2} - \frac{3}{8}m^{-3/2}} = \frac{m^{-1/2} - \frac{1}{4}m^{-3/2}}{m^{-1/2} - \frac{3}{4}m^{-3/2}} = \frac{1 - \frac{1}{4}m^{-1}}{1 - \frac{3}{4}m^{-1}} = \frac{4m-1}{4m-3} \approx 1 + \frac{1}{2m}\end{aligned}$$

For  $m = 50$

$$\begin{aligned}\frac{\sqrt{50+1} - \sqrt{50}}{\sqrt{50+2} - \sqrt{50+1}} &= 1.0099 \\ 1 + \frac{1}{2(50)} &= 1.01\end{aligned}$$

**9.47** A motion of  $\lambda/2$  causes a single fringe pair to shift past, hence  $92(\lambda/2) = 2.53 \times 10^{-5} \text{ m}$  and  $\lambda = 550 \text{ nm}$ .

**9.48**  $\Delta d = N(\lambda_0/2) = (1000)(5.00 \times 10^{-7} \text{ m})/2 = 2.50 \times 10^{-4} \text{ m}$ .

**9.49**  $\Delta d = N \frac{\lambda_0}{2}$

$$N = \frac{2\Delta d}{\lambda_0} = \frac{2(1 \times 10^{-4} \text{ m})}{5 \times 10^{-7} \text{ m}} = 400$$

**9.50**  $\Lambda = \Delta d = N(\lambda_0/2)$ ;  $\Lambda = (n_{\text{air}}x - n_{\text{vacuum}}x)$ ;

$$N = 2\Lambda/\lambda_0 = [2(1.00029 - 1.00000)(0.10 \text{ m})]/(6.00 \times 10^{-7} \text{ m}) = 97.$$

**9.51** Differentiating  $v = \frac{\lambda}{c}$ :

$$\Delta\lambda_0 = \frac{c}{v^2} \Delta v = \frac{\lambda_0^2}{c} \Delta v$$

$$\Delta v = \frac{1}{\Delta t}$$

$$\Delta l_c = c\Delta t$$

$$\Delta\lambda_0 = \frac{\lambda_0^2}{c} \frac{1}{\Delta t} = \frac{\lambda_0^2}{\Delta l_c}$$

$$2D = \Delta l_c$$

$$\Delta\lambda_0 = \frac{\lambda_0^2}{2D}$$

$$D = \frac{\lambda_0^2}{2\Delta\lambda_0} = \frac{(6.43847 \times 10^{-7} \text{ m})^2}{2(0.0013 \text{ nm})} = 0.1594 \text{ m}$$

**9.52** Fringe pattern comes from the interference of two beams, one that passes through the lower medium ( $n_1$ ), and is reflected off its mirror, one that passes through the top medium ( $n_2$ ) and is reflected off its mirror. The two beams reflect off the front surface of the other medium.

It might be used to compare  $n_1$  and  $n_2$  (especially if one changes, such as due to pressure or temperature), or compare the flatness of one surface, to a known optically flat surface.

$$\mathbf{9.53} \quad E_t^2 = E_i E_i^* = E_0^2 (tt')^2 / (1 - r^2 e^{-i\delta})(1 - r^2 e^{i\delta}),$$

$$I_t = I_i (tt')^2 / (1 - r^2 e^{-i\delta} - r^2 e^{i\delta} + r^4).$$

$$\mathbf{9.54} \quad (\text{a}) \quad R = 0.8944, \text{ therefore } F = 4R/(1 - R)^2 = 321.$$

$$(\text{b}) \quad \gamma = 4 \sin^{-1} \left( \frac{1}{\sqrt{F}} \right) = 0.223. \quad (\text{c}) \quad F = 2\pi/0.223. \quad (\text{d}) \quad C = 1 + F.$$

$$\mathbf{9.55} \quad \frac{2}{[1 + F(\Delta\delta/4)^2]} = 0.81[1 + 1/(1 + F(\Delta\delta/2)^2)],$$

$$F^2(\Delta\delta)^4 - 15.5F(\Delta\delta)^2 - 30 = 0.$$

$$\mathbf{9.56} \quad I = I_{\max} \cos^2 \delta/2, \quad I = I_{\max}/2 \text{ when } \delta = \pi/2, \text{ therefore } \gamma = \pi. \text{ Separation between maxima is } 2\pi. \quad F = 2\pi/\gamma = 2.$$

**9.57** (4.47)  $r_{\theta_i=0} = (n_t - n_i)/(n_t + n_i)$ . Bare substrate:  $r = (n_s - 1)/(n_s + 1)$ . Substrate with film:  $r' = t_{o-f} r_{f-s} t_{f-o}$ . (4.48)  $t_{\theta_i=0} = 2n_i/(n_i + n_t)$ , so,  $r' = [2/(1 + n_f)][(n_s - n_f)/(n_s + n_f)][2n_f/(n_f + 1)]$ , where  $n_f = n$ . Note that for  $n_s > n_f > 1$ , both  $r$  and  $r'$  are positive. But, with thickness  $\lambda_f/4$ , a  $\pi$  phase shift occurs due to the OPD in the  $r'$  beam, so  $r_{\text{net}} = r - r'$ .

Thus, the  $r'$  beam (partially) cancels the  $r$  beam.

**9.58** At near normal incidence ( $\theta_i \approx 0$ ) the relative phase shift between an internally and externally reflected beam is  $\pi$  rad. That means a total relative phase difference of  $(2\pi/\lambda_f)[2(\lambda_f/4)] + \pi$  or  $2\pi$ . The waves are in phase and interfere constructively.

$$\mathbf{9.59} \quad n_0 = 1, \quad n_s = n_g, \quad n_1 = \sqrt{n_g}.$$

$$\sqrt{1.54} = 1.24, \quad d = \lambda_f/4 = \lambda_0/4n_1 = 540/4(1.24) \text{ nm} = 167 \text{ nm}.$$

No relative phase shift between two waves.

**9.60** The refracted wave will traverse the film twice, and there will be no relative phase shift on reflection. Hence  $d = \lambda_0/4n_f = (550 \text{ nm})/4(1.38) = 99.6 \text{ nm}$ .

$$\mathbf{9.61} \quad d \cos \theta_i = (2m + 1) \left( \frac{\lambda_m}{4} \right). \text{ Let } \theta_i = 0, \quad m = 0, \text{ (minimum thickness).}$$

$$d = \frac{\lambda_0}{4n_f} = \frac{5.00 \times 10^{-7} \text{ m}}{4(1.30)} = 96 \text{ nm}$$

**9.62** Note that in the triangle including  $\theta$  and  $r_1$ , the length of the side from  $P_1$  to a plane, parallel to the surface, and containing point  $z(x)$  is  $r_1 \cos \theta$ . So, from zero elevation,

$$h = r_1 \cos \theta + z(x) \text{ or } z(x) = h - r_1 \cos \theta.$$

(9.108) can be demonstrated on the triangle ( $a, r_1, r_2$ ), where  $a$  is the length of the boom:

$$r_2^2 = r_1^2 + a^2 - 2r_1 a \cos(\alpha + 90^\circ - \theta) = \sin(\gamma) = -\cos(90^\circ + \gamma)$$

$$\text{and } \delta = k(r_2 - r_1) = (2\pi/\lambda)(r_2 - r_1).$$