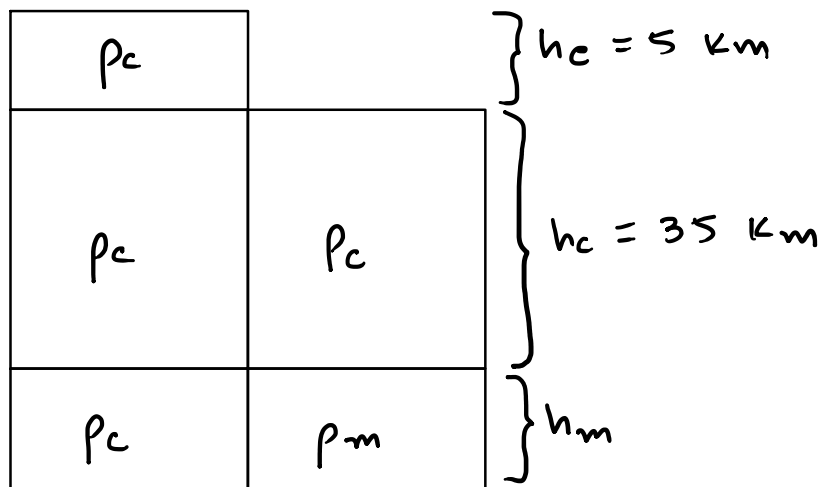


Gabarito Lista 1

①



$$\rho_c h_c + \rho_c h_c + \rho_c h_m = \rho_c h_c + \rho_m h_m$$

$$\rho_c h_c = (\rho_m - \rho_c) h_m$$

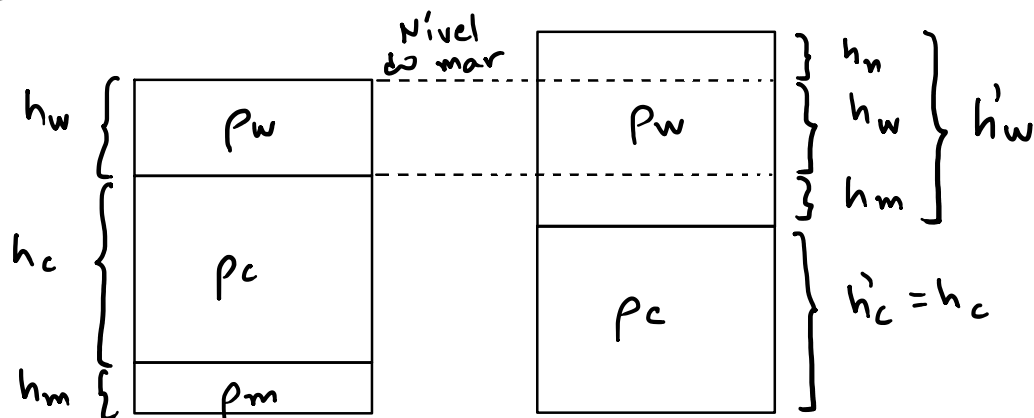
$$\frac{\rho_c h_c}{\rho_m - \rho_c} = h_m = \frac{2800 \cdot 5}{3300 - 2800} = 28 \text{ km}$$

$\therefore$ A espessura da crosta na região da cordilheira é $L = h_c + h_c + h_m = 68 \text{ km}$.

②

Atual

Cretáceo



Onde $h_m = 200 \text{ m}$

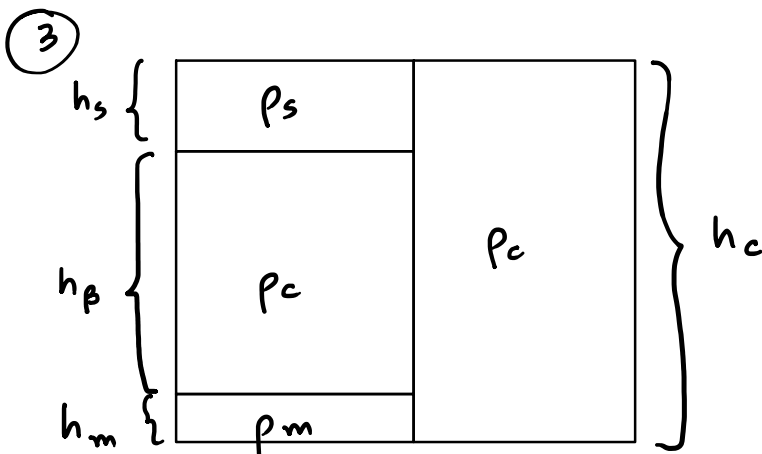
$$\rho_w h_w + \rho_c h_c + \rho_m h_m = \rho_w h'_w + \rho_w h_m + \rho_w h_n + \rho_c h_c$$

$$p_m h_m = p_w h_m + p_w h_n$$

$$(p_m - p_w) h_m = p_w h_n$$

$$h_m = \frac{p_w h_n}{p_m - p_w} = \frac{1000 \cdot 200}{3300 - 1000} \approx 87 \text{ m}$$

$\therefore$ O aumento real da profundidade da lâmina d'água foi de $H = h_n + h_m = 287 \text{ m}$.



$$p_s h_s + p_c h_\beta + p_m h_m = p_c h_c$$

Como $h_m = h_c - h_\beta - h_s$

$$p_s h_s + p_c h_\beta + p_m h_c - p_m h_\beta - p_m h_s = p_c h_c$$

$$(p_c - p_m) h_\beta = p_c h_c - p_s h_s - p_m h_c + p_m h_s$$

$$h_\beta = \frac{p_c h_c - p_s h_s + p_m (h_s - h_c)}{p_c - p_m} =$$

$$= \frac{2750 \cdot 35 - 2450 \cdot 4 + 3300 (4 - 35)}{2750 - 3300} =$$

$$\approx 28,82 \text{ km}$$

Como $\beta = \frac{h_c}{h_\beta} \Rightarrow \beta = \frac{35}{28,82} \approx 1,21$

④ Dada a pressão P_1 na base da coluna não estirada:

$$P_1 = p_c \left(1 - \alpha \frac{T_1 T_c}{2a} \right) g T_c + p_L \left(1 - \alpha T_1 \left(\frac{T_c - a}{2} \right) \right) g (a + T_c)$$

e a pressão P_2 na base da coluna estirada e com subsidência inicial S

$$P_2 = p_c \left(1 - \alpha \frac{T_1 T_c}{2a} \right) g \frac{T_c}{\beta} + p_L \left(1 - \alpha T_1 \left(\frac{T_c - a}{2} \right) \right) g \left(\frac{a + T_c}{\beta} \right) + S p_w g + p_L (1 - \alpha T_1) g \left(a - S - \frac{a}{\beta} \right)$$

Iguando $P_1 = P_2$, temos:

$$p_c \left(1 - \alpha \frac{T_1 T_c}{2a} \right) g T_c + p_L \left(1 - \alpha \frac{T_1 (T_c - a)}{2a} \right) g (a + T_c) =$$

$$p_c \left(1 - \alpha \frac{T_1 T_c}{2a} \right) g \frac{T_c}{\beta} + p_L \left(1 - \alpha \frac{T_1 (T_c - a)}{2a} \right) g \left(\frac{a + T_c}{\beta} \right) +$$

$$p_w S g + p_L (1 - \alpha T_1) g \left(a - S - \frac{a}{\beta} \right)$$

O termo $\left(1 - \alpha \frac{T_1 (T_c - a)}{2a} \right)$ pode ser reescrito como

$$\left(1 - \alpha \frac{T_1 (T_c - a)}{2a} \right) = \left(1 - \alpha \frac{T_1 T_c}{2a} \right) - \frac{\alpha T_1}{2} = \psi - \frac{\alpha T_1}{2}$$

$$\therefore p_c \psi g T_c + p_L \left(\psi - \frac{\alpha T_1}{2} \right) g (a - T_c) = p_c \psi g \frac{T_c}{\beta} +$$

$$p_L \left(\psi - \frac{\alpha T_1}{2} \right) g \left(\frac{a - T_c}{\beta} \right) - S \left(p_L (1 - \alpha T_1) g - p_w g \right)$$

$$+ p_L (1 - \alpha T_1) g \left(1 - \frac{1}{\beta} \right) a \quad (I)$$

Dividindo a expressão (I) por g

$$p_c \psi T_c + p_L \left(\psi - \frac{\alpha T_1}{2} \right) (a - T_c) = p_c \psi \frac{T_c}{\beta} + p_L \left(\psi - \frac{\alpha T_1}{2} \right) \frac{(a - T_c)}{\beta} \\ - S (p_L (1 - \alpha T_1) - p_w) \\ + p_L (1 - \alpha T_1) \left(1 - \frac{1}{\beta} \right) a$$

$$\therefore S (p_L (1 - \alpha T_1) - p_w) = \left(1 - \frac{1}{\beta} \right) \left(-p_c \psi T_c - p_L \left(\psi - \frac{\alpha T_1}{2} \right) (a - T_c) \right. \\ \left. + p_L (1 - \alpha T_1) a \right) \\ = \left(1 - \frac{1}{\beta} \right) \left(-p_c \psi T_c - p_L \psi a + p_L \psi T_c \right. \\ \left. + p_L \frac{\alpha T_1}{2} a - p_L \frac{\alpha T_1}{2} T_c + p_L (1 - \alpha T_1) a \right) \\ = \left(1 - \frac{1}{\beta} \right) \left((p_L - p_c) \psi T_c - p_L \psi a + p_L \frac{\alpha T_1}{2} a \right. \\ \left. - p_L \frac{\alpha T_1}{2} T_c + p_L a - p_L \alpha T_1 a \right) \\ = \left(1 - \frac{1}{\beta} \right) \left((p_L - p_c) \psi T_c - \frac{p_L \alpha T_1}{2} a \right)$$

Substituindo ψ e isolando S

$$S = \frac{(p_L - p_c) \left(1 - \frac{\alpha T_1 T_c}{2a} \right) T_c - \frac{p_L \alpha T_1}{2} a}{p_L (1 - \alpha T_1) - p_w} \left(1 - \frac{1}{\beta} \right)$$