



Escola Politécnica da
Universidade de São Paulo



Equação do Biocalor

Problemas

Problema #10.13



Studies have concluded that the plates on the back of the dinosaur Stegosaurus served a thermoregulatory function as heat dissipating fins*. There are indications that the network of channels within the plates may be blood vessels. Model the plate as a rectangular fin of width W , length L and thickness t . Use the Pennes model to formulate the heat equation for this blood perfused plate. The plate exchanges heat with the ambient air by convection. The heat transfer coefficient is h and the ambient temperature is T . Assume that blood reaches each part of the plate at temperature T_{a0} and that it equilibrates at the local temperature T . Assume further that (1) blood perfusion is uniform, (2) negligible metabolic heat production, (3) negligible temperature variation along plate thickness t (fin approximation is valid, $Bi \ll 1$), (4) steady state and (5) constant properties. Show that the heat equation for this model is given by

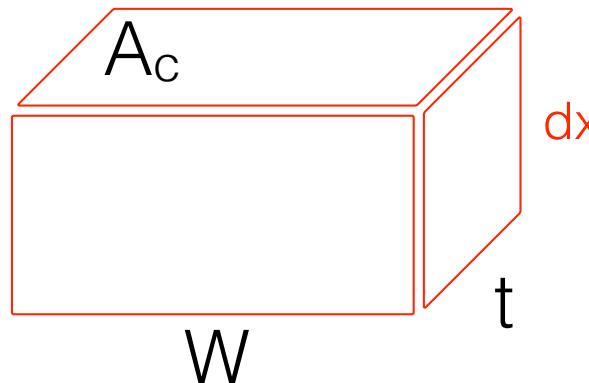
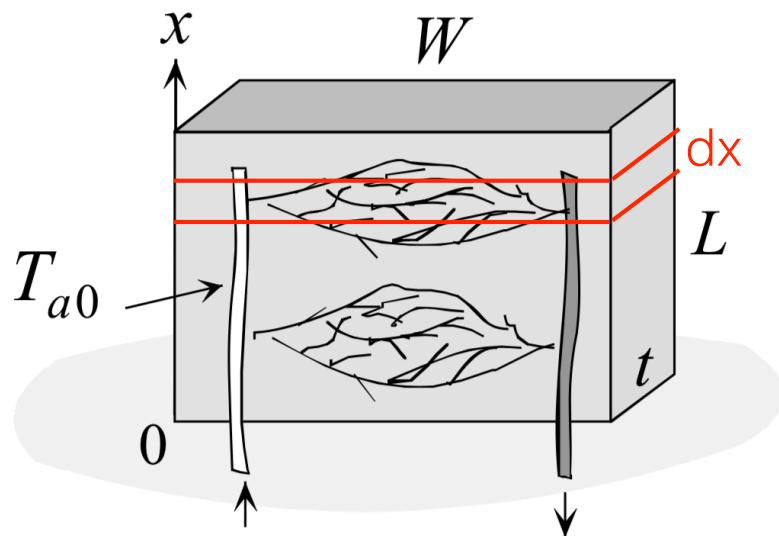
$$\frac{d^2\theta}{d\xi^2} - [m' + \beta]\theta + m' = 0 \quad m' = \frac{2h(W+t)L^2}{kWt} \quad \beta = \frac{\dot{w}_b\rho_b c_b L^2}{k}$$

$$\theta = \frac{T - T_{a0}}{T_\infty - T_{a0}}$$

$$\xi = \frac{x}{L}$$

*Farlow, J.O., Thompson, C.V., and Rosner, D.E., "Plates of the Dinosaur Stegosaurus: Forced Convection Heat Loss Fins?", Science, vol. 192, pp.1123-1125, 1976.

Problema #10.13



$$A_C = Wt$$

$$dA_s = Pdx$$

$$P = 2(W+t)$$

$$d\forall = Wt \cdot dx$$

Balanço de energia:

$$q_x - q_{x+dx} - dq_{conv} + dq_{blood} = 0$$

$$dq_{conv} = h dA_s (T - T_\infty)$$

$$dq_{blood} = \dot{w}_b d\forall \rho_b c_b (T_{a0} - T)$$



Balanço de energia: $q_x - q_{x+dx} - dq_{conv} + dq_{blood} = 0$

Usando uma série de Taylor truncada:

$$q_x - \cancel{q_x} + \frac{\cancel{dq_x}}{\cancel{dx}} dx - hP(T - T_\infty)dx + \dot{w}_b W t \rho_b c_b (T_{a0} - T)dx = 0$$

Usando a lei de Fourier:

$$-\frac{d}{dx} \left(-k A_c \frac{dT}{dx} \right) dx - hP(T - T_\infty)dx + \dot{w}_b W t \rho_b c_b (T_{a0} - T)dx = 0$$

Dedução



$$-\frac{d}{dx} \left(-kA_c \frac{dT}{dx} \right) dx - hP(T - T_\infty) dx + \dot{w}_b W t \rho_b c_b (T_{a0} - T) dx = 0$$

$$kWt \frac{d^2 T}{dx^2} - 2h(W+t)(T - T_\infty) + \dot{w}_b W t \rho_b c_b (T_{a0} - T) = 0$$

$$\frac{d^2 T}{dx^2} - \frac{2h(W+t)}{kWt} (T - T_\infty) + \frac{\dot{w}_b \rho_b c_b}{k} (T_{a0} - T) = 0$$

Dedução



$$\frac{d^2T}{dx^2} - \frac{2h(W+t)}{kWt}(T - T_{\infty}) + \frac{\dot{w}_b \rho_b c_b}{k}(T_{a0} - T) = 0$$

$$\frac{d^2T}{dx^2} - \left[\frac{2h(W+t)}{kWt} + \frac{\dot{w}_b \rho_b c_b}{k} \right] T + \frac{2h(W+t)}{kWt} T_{\infty} + \frac{\dot{w}_b \rho_b c_b}{k} T_{a0} = 0$$

$$\frac{d^2T}{dx^2} - \left[\frac{2h(W+t)}{kWt} + \frac{\dot{w}_b \rho_b c_b}{k} \right] (T - T_{a0}) + \frac{2h(W+t)}{kWt} T_{\infty} - \frac{2h(W+t)}{kWt} T_{a0} = 0$$

$$\frac{d^2T}{dx^2} - \left[\frac{2h(W+t)}{kWt} + \frac{\dot{w}_b \rho_b c_b}{k} \right] (T - T_{a0}) + \frac{2h(W+t)}{kWt} (T_{\infty} - T_{a0}) = 0$$

Adimensionlização



$$\frac{d^2T}{dx^2} - \left[\frac{2h(W+t)}{kWt} + \frac{\dot{w}_b \rho_b c_b}{k} \right] (T - T_{a0}) + \frac{2h(W+t)}{kWt} (T_\infty - T_{a0}) = 0$$

$$\theta = \frac{T - T_{a0}}{T_\infty - T_{a0}} \quad \Rightarrow d^2\theta = \frac{d^2T}{T_\infty - T_{a0}} \quad \Rightarrow d^2T = (T_\infty - T_{a0}) d^2\theta$$

$$\xi = \frac{x}{L} \quad \Rightarrow d\xi = \frac{dx}{L} \quad \Rightarrow dx^2 = L^2 d\xi^2$$

$$\frac{T_\infty - T_{a0}}{L^2} \frac{d^2\theta}{d\xi^2} - \left[\frac{2h(W+t)}{kWt} + \frac{\dot{w}_b \rho_b c_b}{k} \right] \theta (T_\infty - T_{a0}) + \frac{2h(W+t)}{kWt} (T_\infty - T_{a0}) = 0$$

Adimensionlização



$$\frac{T_{\infty} - T_{a0}}{L^2} \frac{d^2\theta}{d\xi^2} - \left[\frac{2h(W+t)}{kWt} + \frac{\dot{w}_b \rho_b c_b}{k} \right] \theta (T_{\infty} - T_{a0}) + \frac{2h(W+t)}{kWt} (T_{\infty} - T_{a0}) = 0$$

$$\frac{d^2\theta}{d\xi^2} - \left[\frac{2h(W+t)L^2}{kWt} + \frac{\dot{w}_b \rho_b c_b L^2}{k} \right] \theta + \frac{2h(W+t)L^2}{kWt} = 0$$

$$\frac{d^2\theta}{d\xi^2} - [m' + \beta] \theta + m' = 0$$

$$m' = \frac{2h(W+t)L^2}{kWt}$$

$$\beta = \frac{\dot{w}_b \rho_b c_b L^2}{k}$$



$$\frac{d^2\theta}{d\xi^2} - [m' + \beta]\theta + m' = 0$$

Condições de contorno:

$$T(x=0) = T_{a0} \Rightarrow \theta_b(\xi=0) = 0$$

$$-kA_c \frac{dT}{dx} \Big|_{x=L} = 0 \Rightarrow \frac{d\theta}{d\xi} \Big|_{\xi=1} = 0 \quad A_c \ll A_s$$



$$\frac{d^2\theta}{d\xi^2} - [m' + \beta]\theta + m' = 0$$

Definindo: $m^2 = m' + \beta$

$$\frac{d^2\theta}{d\xi^2} - m^2\theta + m' = 0$$

$$\theta' = \theta - \frac{m'}{m^2}$$

$$\theta = \theta' + \frac{m'}{m^2}$$

$$\frac{d^2\theta'}{d\xi^2} - m^2\theta' = 0$$

Equação homogênea:

$$\frac{d^2\theta'}{d\xi^2} - m^2\theta' = 0$$

$$\theta' = C_1 \operatorname{senh}(m\xi) + C_2 \cosh(m\xi)$$

ou

$$\theta' = C_3 e^{m\xi} + C_4 e^{-m\xi}$$



$$\frac{d^2\theta'}{dx^2} - m^2 \theta' = 0 \quad \theta = \theta' + \frac{m'}{m^2}$$

Condições de contorno:

$$\theta_b(\xi = 0) = 0 \Rightarrow \theta'_b(\xi = 0) = -\frac{m'}{m^2}$$

$$\left. \frac{d\theta}{dx} \right|_{\xi=1} = 0 \Rightarrow \left. \frac{d\theta'}{dx} \right|_{\xi=1} = 0$$

Solução particular



Partimos da solução:

$$\theta' = C_1 \operatorname{senh}(m\xi) + C_2 \cosh(m\xi) \quad (1)$$

Aplicaremos as condições de contorno:

$$\theta'_b(\xi = 0) = -\frac{m'}{m^2} \Rightarrow C_2 = \theta'_b$$

$$\left. \frac{d\theta'}{dx} \right|_{\xi=1} = 0 \Rightarrow C_1 m \cosh(m) + C_2 m \operatorname{senh}(m) = 0$$

Combinando as duas condições de contorno:

$$\Rightarrow C_1 \cosh(m) + \theta'_b \operatorname{senh}(m) = 0$$

$$\Rightarrow C_1 = -\theta'_b \tanh(m)$$

Solução particular



Substituindo em (1): $\theta' = -\theta'_b \tanh(m) \operatorname{senh}(m\xi) + \theta'_b \cosh(m\xi)$

$$\frac{\theta'}{\theta'_b} = -\frac{\operatorname{senh}(m)}{\cosh(m)} \operatorname{senh}(m\xi) + \cosh(m\xi)$$

$$\frac{\theta'}{\theta'_b} = \frac{\cosh(m) \cosh(m\xi) - \operatorname{senh}(m) \operatorname{senh}(m\xi)}{\cosh(m)}$$

Nossa solução fica:

$$\boxed{\frac{\theta'}{\theta'_b} = \frac{\cosh[m(1-\xi)]}{\cosh(m)}}$$

$$\cosh(x-y) = \cosh(x) \cosh(y) - \operatorname{senh}(x) \operatorname{senh}(y)$$

Perfil de temperatura adimensional



$$\frac{\theta'}{\theta'_b} = \frac{\cosh[m(1-\xi)]}{\cosh(m)}$$

$$\theta = \theta' + \frac{m'}{m^2}$$

$$\theta'_b = -\frac{m'}{m^2}$$

$$\frac{\theta - \frac{m'}{m^2}}{-\frac{m'}{m^2}} = \frac{\cosh[m(1-\xi)]}{\cosh(m)} \quad \rightarrow \quad \theta = \frac{m'}{m^2} - \frac{m'}{m^2} \frac{\cosh[m(1-\xi)]}{\cosh(m)}$$

$$m^2 = m' + \beta$$

$$\theta = \frac{T - T_{a0}}{T_\infty - T_{a0}}$$



$$\theta = \frac{m'}{m' + \beta} \left\{ 1 - \frac{\cosh[\sqrt{m' + \beta}(1-\xi)]}{\cosh(\sqrt{m' + \beta})} \right\}$$

Perfil de temperatura adimensional



$$\theta = \frac{m'}{m' + \beta} \left\{ 1 - \frac{\cosh \left[\sqrt{m' + \beta} (1 - \xi) \right]}{\cosh \left(\sqrt{m' + \beta} \right)} \right\}$$

$$\theta = \frac{T - T_{a0}}{T_\infty - T_{a0}}$$

$$m' = \frac{2h(W+t)L^2}{kWt}$$

$$\xi = \frac{x}{L}$$

$$\beta = \frac{\dot{w}_b \rho_b c_b L^2}{k}$$

Calor total transferido



Vamos calcular o calor total transferido a partir da aleta:

$$q_a = -kA_c \frac{dT}{dx} \Big|_{x=0} = -\frac{kWt}{L} (T_\infty - T_{a0}) \frac{d\theta'}{d\xi} \Big|_{\xi=0}$$

$$\frac{\theta'}{\theta'_b} = \frac{\cosh m(1-\xi)}{\cosh(m)}$$

$$q_a = -\frac{kWt}{L} (T_\infty - T_{a0}) \left[-\theta'_b m \frac{\sinh m(1-\xi)}{\cosh(m)} \right]_{\xi=0}$$

$$q_a = \frac{kWt}{L} (T_\infty - T_{a0}) \theta'_b m \frac{\sinh(m)}{\cosh(m)}$$

$$q_a = \frac{kWt}{L} (T_\infty - T_{a0}) \theta'_b m \tanh(m)$$

Calor total transferido



$$q_a = \frac{kWt}{L} (T_{\infty} - T_{a0}) \theta'_b m \tanh(m)$$

$$\theta'_b = -\frac{m'}{m^2} \quad \rightarrow \quad q_a = -\frac{kWt}{L} (T_{\infty} - T_{a0}) \frac{m'}{m^2} \sqrt{m' + \beta} \tanh(\sqrt{m' + \beta})$$

$$m^2 = m' + \beta \quad \rightarrow \quad q_a = \frac{kWt}{L} (T_{a0} - T_{\infty}) \frac{m'}{m^2} \sqrt{m' + \beta} \tanh(\sqrt{m' + \beta})$$

$$q_a = \frac{kWt}{L} (T_{a0} - T_{\infty}) \frac{m'}{\sqrt{m' + \beta}} \tanh(\sqrt{m' + \beta})$$

Problema #10.22



Prolonged exposure to cold environment of elephants can result in frost bite on their ears. Model the elephant ear as a sheet of total surface area (two sides) A and uniform thickness δ . Assume uniform blood perfusion \dot{w}_b and uniform metabolic heat q_m''' . The ear loses heat by convection. The ambient temperature is T_∞ and the heat transfer coefficient is h . Using lumped capacity approximation and the Pennes model, show that the dimensionless transient heat equation is given by

Problema #10.22



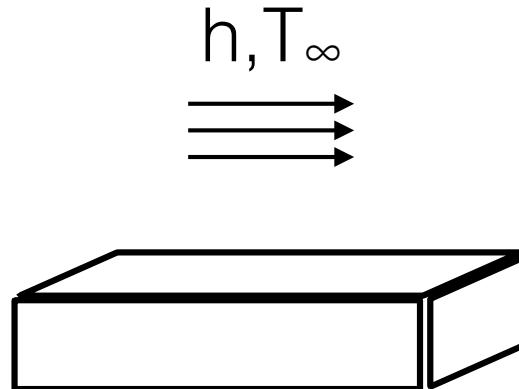
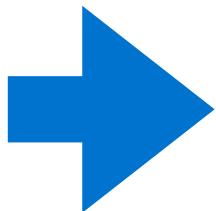
$$\frac{d\theta}{d\tau} = (1 + \gamma) - (1 + \beta)\theta ,$$

where

$$\theta = \frac{T - T_{a0}}{T_\infty - T_{a0}}, \quad \tau = \frac{2h}{\delta \rho c} t, \quad \beta = \frac{\dot{w}_b \rho_b c_b \delta}{2h}, \quad \gamma = \frac{q_m''' \delta}{2h(T_\infty - T_{a0})}.$$

Here ρ is tissue density and c tissue specific heat. The subscript b refers to blood. Determine the maximum time a zoo elephant can remain outdoors on a cold winter day without resulting in frost bite when the ambient temperature is lower than freezing temperature T_f . Assume that initially the ears are at uniform temperature T_i .

Balanço de energia



Balanço de energia: $M + q_{blood} - q_{conv} = mc \frac{dT}{dt}$

$$q_{conv} = hA(T - T_\infty)$$

$$q_{blood} = \dot{w}_b \nabla \rho_b c_b (T_{a0} - T) \quad \nabla = (A / 2) \delta$$

$$M = q_m'' \nabla$$

$$m = \rho \nabla$$



Balanço de energia: $M + q_{blood} - q_{conv} = mc \frac{dT}{dt}$

$$\rho \forall c \frac{dT}{dt} = q'''_m \forall + \dot{w}_b \forall \rho_b c_b (T_{a0} - T) - hA(T - T_\infty)$$

$$\rho c \frac{dT}{dt} = q'''_m + \dot{w}_b \rho_b c_b (T_{a0} - T) - \frac{2h}{\delta} (T - T_\infty)$$

Adimensionalização



$$\rho c \frac{dT}{dt} = q_m''' + \dot{w}_b \rho_b c_b (T_{a0} - T) - \frac{2h}{\delta} (T - T_\infty) = 0$$

$$\theta = \frac{T - T_{a0}}{T_\infty - T_{a0}} \rightarrow d\theta = \frac{dT}{T_\infty - T_{a0}} \rightarrow dT = (T_\infty - T_{a0}) d\theta$$

$$\tau = \frac{2h}{\delta\rho c} t \rightarrow d\tau = \frac{2h}{\delta\rho c} dt \rightarrow dt = \frac{\delta\rho c}{2h} d\tau$$

$$\rho c (T_\infty - T_{a0}) \frac{2h}{\delta\rho c} \frac{d\theta}{d\tau} = q_m''' + \dot{w}_b \rho_b c_b (T_{a0} - T) - \frac{2h}{\delta} (T - T_\infty) = 0$$

Adimensionalização



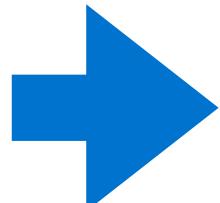
$$(T_{\infty} - T_{a0}) \frac{2h}{\delta} \frac{d\theta}{d\tau} = q_m''' + \dot{w}_b \rho_b c_b (T_{a0} - T) - \frac{2h}{\delta} (T - T_{\infty})$$

$$\theta = \frac{T - T_{a0}}{T_{\infty} - T_{a0}}$$

$$\frac{d\theta}{d\tau} = \frac{q_m''' \delta}{2h(T_{\infty} - T_{a0})} + \frac{\dot{w}_b \rho_b c_b \delta}{2h} \frac{(T_{a0} - T)}{(T_{\infty} - T_{a0})} - \frac{(T - T_{\infty})}{(T_{\infty} - T_{a0})}$$

$$\gamma = \frac{q_m''' \delta}{2h(T_{\infty} - T_{a0})}$$

$$\beta = \frac{\dot{w}_b \rho_b c_b \delta}{2h}$$



$$\frac{d\theta}{d\tau} = \gamma - \beta \theta - \frac{(T - T_{\infty})}{(T_{\infty} - T_{a0})}$$

Adimensionalização



$$\frac{d\theta}{d\tau} = \gamma - \beta\theta - \frac{(T - T_{\infty})}{(T_{\infty} - T_{a0})}$$

$$\theta = \frac{T - T_{a0}}{T_{\infty} - T_{a0}} \quad \tau = \frac{2h}{\delta\rho c} t$$

$$\frac{d\theta}{d\tau} = \gamma - \beta\theta - \frac{(\textcolor{red}{T} - T_{\infty}) - \textcolor{red}{T}_{a0} + T_{a0}}{(T_{\infty} - T_{a0})}$$

$$\frac{d\theta}{d\tau} = \gamma - \beta\theta - \frac{(\textcolor{red}{T} - \textcolor{red}{T}_{a0})}{(T_{\infty} - T_{a0})} - \frac{T_{a0} - T_{\infty}}{(T_{\infty} - T_{a0})}$$

$$\frac{d\theta}{d\tau} = \gamma - \beta\theta - \theta + 1$$

$$\boxed{\frac{d\theta}{d\tau} = (1 + \gamma) - (1 + \beta)\theta}$$

Equação diferencial



$$\frac{d\theta}{d\tau} = (1 + \gamma) - (1 + \beta)\theta$$

$$\theta = \frac{T - T_{a0}}{T_\infty - T_{a0}} \quad \tau = \frac{2h}{\delta\rho c} t$$

Condição inicial: $T(t=0) = T_i \rightarrow \theta(\tau=0) = \theta_i = \frac{T_i - T_{a0}}{T_\infty - T_{a0}}$

Solução (mudança de variável)



$$\frac{d\theta}{d\tau} = (1 + \gamma) - (1 + \beta)\theta$$

$$\theta = \frac{T - T_{a0}}{T_\infty - T_{a0}} \quad \tau = \frac{2h}{\delta\rho c} t$$

$$\theta(\tau = 0) = \theta_i = \frac{T_i - T_{a0}}{T_\infty - T_{a0}}$$

$$\theta' = \theta - \frac{1 + \gamma}{1 + \beta}$$



$$d\theta' = d\theta$$

$$\theta = \frac{1 + \gamma}{1 + \beta} + \theta'$$

$$\frac{d\theta'}{d\tau} = -(1 + \beta)\theta'$$

$$\theta'_i = \theta_i - \frac{1 + \gamma}{1 + \beta}$$

Solução (mudança de variável)



$$\frac{d\theta'}{d\tau} = -(1 + \beta)\theta' \quad \rightarrow \quad \frac{\theta'}{\theta_i} = e^{-(1+\beta)\tau}$$

$$\theta_i' = \theta_i - \frac{1 + \gamma}{1 + \beta} \quad \rightarrow \quad \frac{\theta - \frac{1 + \gamma}{1 + \beta}}{\theta_i - \frac{1 + \gamma}{1 + \beta}} = e^{-(1+\beta)\tau}$$

$$\theta = \frac{1 + \gamma}{1 + \beta} + \left[\theta_i - \frac{1 + \gamma}{1 + \beta} \right] e^{-(1+\beta)t} = \theta_i + \frac{1 + \gamma}{1 + \beta} \left[1 - e^{-(1+\beta)t} \right]$$

$$\theta = \frac{T - T_{a0}}{T_\infty - T_{a0}} \quad \rightarrow \quad \frac{T - T_{a0}}{T_\infty - T_{a0}} = \frac{T_i - T_{a0}}{T_\infty - T_{a0}} + \frac{1 + \gamma}{1 + \beta} \left[1 - e^{-(1+\beta)\tau} \right]$$

Solução (mudança de variável)



$$\frac{T - T_{a0}}{T_\infty - T_{a0}} = \frac{T_i - T_{a0}}{T_\infty - T_{a0}} + \frac{1 + \gamma}{1 + \beta} \left[1 - e^{-(1+\beta) \frac{2h}{\delta\rho c} t} \right]$$

$$\gamma = \frac{q_m''' \delta}{2h(T_\infty - T_{a0})}$$

$$\beta = \frac{\dot{w}_b \rho_b c_b \delta}{2h}$$