

26/03/2020

①

$$\nabla^2 \phi = 0, \quad \vec{v} = \nabla \phi$$

Far-field  $\Rightarrow$  Perturbation velocity vanishes

$$\lim_{\vec{r} \rightarrow \infty} \vec{v} = 0$$

one is left with undisturbed flow

Body velocity  $\vec{U}$

fluid has induced velocity  $\vec{v}$

Lab. Frame  $\Rightarrow$  inertial

$$F(\vec{x}, t) \Big|_B = 0 \quad \text{Level Surface: } \hat{n} \Big|_B = \frac{\nabla F}{\|\nabla F\|} \Big|_B$$

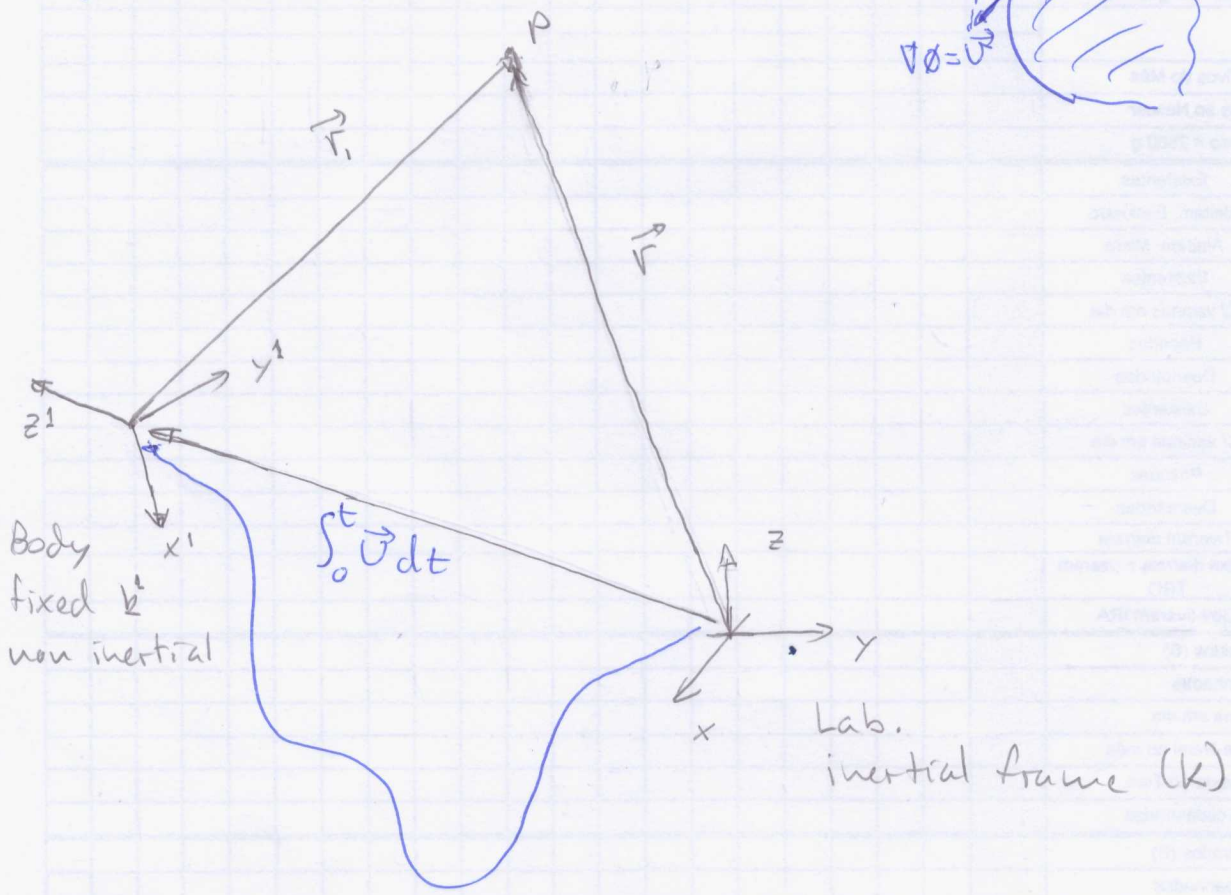
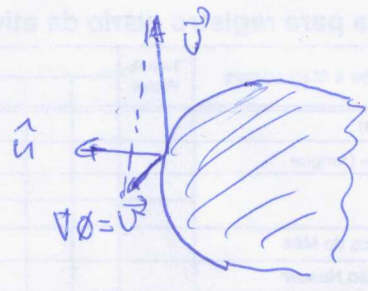
$$\text{Lagrange: } \frac{DF}{Dt} = 0$$

$$\text{Euler: } \frac{\partial F}{\partial t} + \nabla \phi \cdot \nabla F = 0$$

$$\frac{DF}{Dt} \Big|_B = 0 \Rightarrow \frac{\partial F}{\partial x^i} \frac{\partial x^i}{\partial t} + \nabla \phi \cdot \nabla F = 0$$

$\vec{U}$

$$\boxed{[\nabla\phi \cdot \hat{n}]_B = [\vec{v} \cdot \hat{n}]_B}$$



$$P(\vec{r}, t) = P_{\infty} - \rho \left[ \frac{d\phi}{dt} + \frac{\|\nabla\phi\|^2}{2} \right]$$

$$\vec{r}^{(1)} = \vec{r} - \int_0^t \vec{v}(z) dz ; t_1 = t$$

$$\begin{cases} \phi_1(\vec{r}^1, t_1) = \phi(\vec{r}, t) \\ F_1(\vec{r}^1, t_1) = F(\vec{r}, t) \\ P_1(\vec{r}^1, t_1) = P(\vec{r}, t) \end{cases}$$

Scalar functions

Let's assume that at the

③

time we are considering now, at this moment, both frames coincide:

$$t_1 = t$$

$$\nabla_1(\dots) = \nabla(\dots) ; \quad \nabla_1^2(\dots) = \nabla^2(\dots) ; \quad \frac{\partial t}{\partial t_1} = 1$$

$$\frac{\partial(\dots)}{\partial t_1} = \frac{\partial(\dots)}{\partial t} + U \cdot \nabla(\dots) \Rightarrow \frac{\partial(\dots)}{\partial t} = \frac{\partial(\dots)}{\partial t_1} - \vec{U} \cdot \nabla_1(\dots)$$

$$P_{\infty} - P = \rho \left[ \frac{\partial \phi}{\partial t_1} - \vec{U} \cdot \nabla_1 \phi + \frac{\|\nabla_1 \phi\|^2}{2} \right]$$

$$\boxed{\frac{P_{\infty} - P}{\rho} = \frac{\partial \phi}{\partial t} - \vec{U} \cdot \vec{q}_1 + \frac{\|\vec{q}_1\|^2}{2}}$$

$$C_p = \frac{-2}{U_{\infty}^2} \left[ \frac{\partial \phi}{\partial t_1} - \vec{U} \cdot \vec{q}_1 + \frac{\|\vec{q}_1\|^2}{2} \right]$$

$$\vec{F} = - \iint_{S_B} p \hat{n} ds = \iint_{S_B} \rho \frac{\partial \phi}{\partial t} \hat{n} ds + \iint_{S_B} \rho \left[ \frac{q^2}{2} - \vec{U} \cdot \vec{q} \right] \hat{n} ds$$

$$\vec{F} = \frac{\partial}{\partial t} \iint_{S_B} \rho \phi \hat{n} ds + \iint_{S_B} \rho \left[ \frac{q^2}{2} - \vec{U} \cdot \vec{q} \right] \hat{n} ds$$

$$\begin{aligned} \vec{U} \times (\hat{n} \times \vec{q}) &= (\vec{U} \cdot \vec{q}) \hat{n} - (\vec{U} \cdot \hat{n}) \vec{q} \\ &= (\vec{U} \cdot \vec{q}) \hat{n} - (\vec{q} \cdot \hat{n}) \vec{q} \end{aligned}$$

Pure translation

$$\vec{F} = \frac{\partial}{\partial t} \iint_{S_B} \rho \phi \hat{n} ds + \iint_{S_B} \rho \left[ \frac{q^2}{2} \hat{n} - (\vec{q} \cdot \hat{n}) \vec{q} \right] ds - \rho \vec{U} \times \iint_{S_B} (\hat{n} \times \vec{q}) ds$$

$$\iint_{S_B} \left[ \frac{(\vec{q} \cdot \vec{q}) \hat{n} - (\vec{q} \cdot \hat{n}) \vec{q}}{2} \right] ds + \iint_{\Sigma} \left[ \frac{(\vec{q} \cdot \vec{q}) \hat{n} - (\vec{q} \cdot \hat{n}) \vec{q}}{2} \right] ds =$$

$\Sigma$   
 far field  
 $\vec{r} \rightarrow \infty$

$\rightarrow$  vanishes as  
 $\lim_{\vec{r} \rightarrow \infty} \vec{q} = 0$

$$= \iint_{\mathcal{D}} [\vec{q} \cdot \nabla \vec{q} - \vec{q} \cdot \nabla \vec{q}] d\theta = 0$$

$\mathcal{D}$   
 Flow

$$\oint_{S_B} \left[ \frac{q^2 \hat{u}}{2} - (\vec{q} \cdot \hat{u}) \vec{q} \right] ds = 0$$

$$\vec{F} = \frac{d}{dt} \oint_{S_B} \rho \hat{u} ds - \int_{S_B} \vec{u} \times (\hat{u} \times \vec{q}) ds$$

D'Alembert's Paradox

$$\phi = \phi_1 + \phi_2 + \phi_3$$

$$\nabla^2 \phi = 0 \Rightarrow \nabla^2 \phi_{\underline{i}} = 0 \quad \underline{i} = 1, 2, 3$$

$$\nabla^2 \phi_{\underline{i}} = 0 ; \nabla \phi_{\underline{i}} \cdot \hat{n}_{\mathcal{B}} = (U_{\underline{i}} n_{\underline{i}})_{\mathcal{B}}$$

no summation convention

Furthermore, we define unitary potentials,  $\psi_i$ , of the form:

$$\phi_{\underline{i}} = U_{\underline{i}} \psi_{\underline{i}} \Rightarrow \nabla^2 \psi_{\underline{i}} = 0$$

$$\nabla \psi_{\underline{i}} \cdot \hat{n} = \frac{\partial \psi_{\underline{i}}}{\partial n} = U_{\underline{i}} \quad \text{on } S_{\mathcal{B}}$$

$$\phi = U_1 \psi_1 + U_2 \psi_2 + U_3 \psi_3 = \vec{U} \cdot \hat{u}$$

↳ General translating motion.

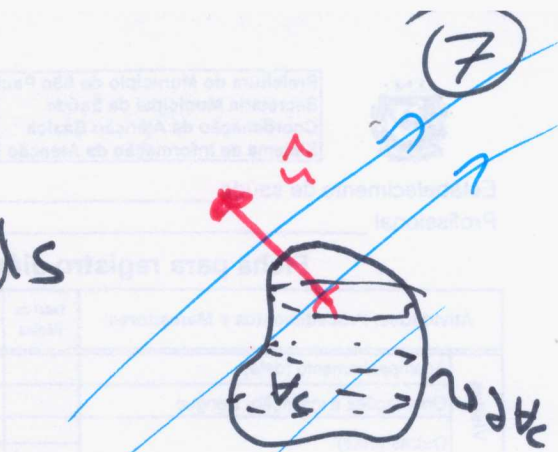
$$\vec{F}_e = \frac{d}{dt} \left( m_{\mathcal{B}} \vec{U} - \oint_{S_{\mathcal{B}}} \rho \hat{u} ds \right) = (m \delta_{ik} + m_{ik}) \frac{dU_k}{dt}$$

$$m_{ik} = m_{ki} = - \oint_{S_{\mathcal{B}}} \rho \psi_k n_i ds = - \oint_{S_{\mathcal{B}}} \rho \psi_k \frac{\partial \psi_i}{\partial n} ds$$

# T. Gauss

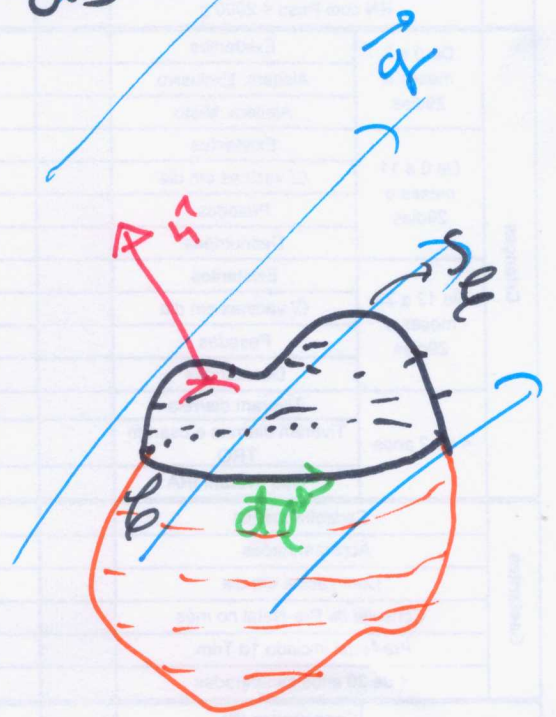
$$\oiint_{\partial V} \vec{q} \cdot \hat{n} \, ds = \iiint_V \nabla \cdot \vec{q} \, ds$$

$$\oiint_{\partial V} \hat{n} \times \vec{q} \, ds = \iiint_V \nabla \times \vec{q} \, ds$$



## Stokes Theorem:

$$\oint_C \vec{q} \cdot d\vec{l} = \iint_{S_C} (\nabla \times \vec{q}) \cdot \hat{n} \, ds$$



## Circulation definition:

$$\Gamma \equiv \oint_C \vec{q} \cdot d\vec{l} = \iint_{S_C} (\nabla \times \vec{q}) \cdot \hat{n} \, ds$$

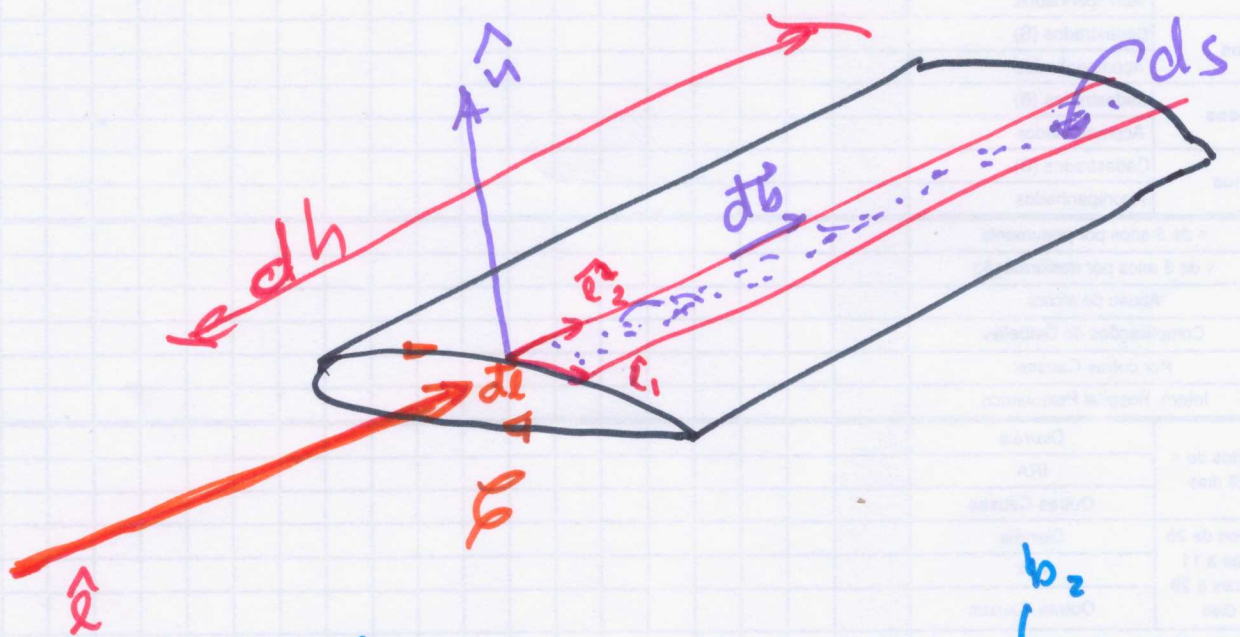
notice that through Gauss' Theorem this is related to  $\oiint \hat{n} \times \vec{q} \, ds$

$$\vec{\Gamma} = \frac{d}{dt} \iint_{S_D} \rho \vec{v} \cdot \hat{n} ds - \rho \vec{U} \times \iint_{S_B} (\hat{n} \times \vec{q}) ds$$

$$\vec{I} = \iint_{S_B} (\hat{n} \times \vec{q}) ds$$

$$\hat{e} \cdot \vec{I} = \hat{e} \cdot \iint_{S_B} (\hat{n} \times \vec{q}) ds = \int_{h_1}^{h_2} \left[ \oint \vec{q} \cdot d\vec{l} \right] dh =$$

$$= \int_{h_1}^{h_2} \Gamma_e(h) dh$$



$$\rho \vec{U} \times \iint \hat{n} \times \vec{q} ds = \rho \vec{U} \times \int \Gamma(b) db$$



(16/04/2020)

1

$$z = x + iy \quad i = \sqrt{-1}$$

$$e^x = \sum_{k=0}^{\infty} \frac{x^k}{k!} \Rightarrow e^{iy} = \sum_{k=0}^{\infty} \frac{(iy)^k}{k!}$$

$$e^{iy} = \sum_{k=0}^{\infty} \frac{i^{2k} y^{2k}}{(2k)!} + \sum_{k=0}^{\infty} \frac{i^{(2k+1)} y^{2k+1}}{(2k+1)!}$$

$$= \sum_{k=0}^{\infty} \frac{(-1)^k y^{2k}}{(2k)!} + i \sum_{k=0}^{\infty} \frac{(-1)^k y^{2k+1}}{(2k+1)!}$$

$$e^{iy} = \cos(y) + i \sin(y)$$

$$z = r e^{i\theta} = r (\cos\theta + i \sin\theta)$$

$$r = |z| = \sqrt{x^2 + y^2}$$

$$\theta = \arg(z)$$

## Analytic Functions

$$f(z) = u(x, y) + i v(x, y)$$

Cauchy - Riemann  
Conditions

$$\left\{ \begin{array}{l} \frac{\partial u}{\partial x} = \frac{\partial v}{\partial y} \\ \frac{\partial u}{\partial y} = -\frac{\partial v}{\partial x} \end{array} \right.$$

$$f'(z) = u_x + i v_x$$

$$f'(z) = v_y - i u_y$$

$$f(z) = u(x, y) + i v(x, y)$$

$$\frac{\partial^2 u}{\partial x^2} = \frac{\partial^2 v}{\partial y \partial x}$$

$$\frac{\partial^2 u}{\partial y^2} = -\frac{\partial^2 v}{\partial x \partial y}$$

Similarly:

$$\frac{\partial^2 v}{\partial x^2} + \frac{\partial^2 v}{\partial y^2} = 0 \Rightarrow \nabla^2 v = 0$$

Cauchy - Riemann in polar form:

$$x = r \cos \theta$$

$$y = r \sin \theta$$

$$\frac{\partial u}{\partial r} = \frac{1}{r} \frac{\partial v}{\partial \theta}$$

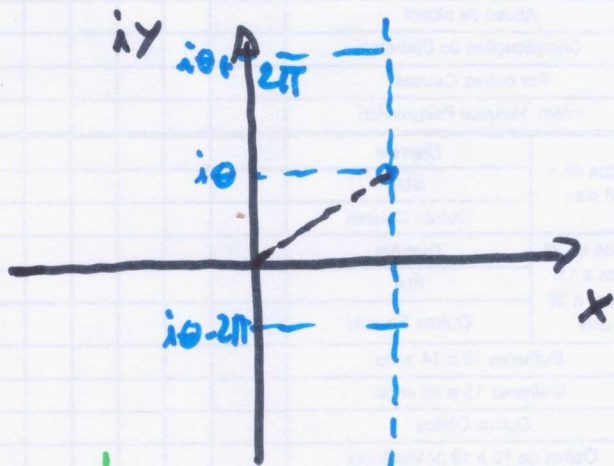
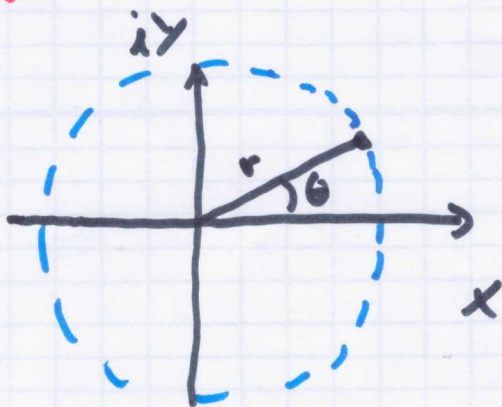
$$\frac{1}{r} \frac{\partial u}{\partial \theta} = -\frac{\partial v}{\partial r}$$

$$f(z) = u(r, \theta) + i v(r, \theta)$$

$$\frac{df}{dz} = f'(z) = e^{-i\theta} \left( \frac{\partial u}{\partial r} + i \frac{\partial v}{\partial r} \right)$$

$\exp(z) = \exp(z \pm k2\pi i) \Rightarrow$  Periodic

$\log(z) \equiv \ln(r) + i(\theta \pm 2k\pi) \Rightarrow$  Multi-valued



$$\exp[\log(z)] = z$$

$$\bullet \log[\exp(z)] = z \pm i2k\pi$$

## Cylindrical Coordinates

$$\nabla(\dots) = \frac{\partial(\dots)}{\partial r} \hat{\lambda}_r + \frac{1}{r} \frac{\partial(\dots)}{\partial \theta} \hat{\lambda}_\theta + \frac{\partial(\dots)}{\partial z} \hat{\lambda}_z$$

$$\nabla^2 \phi = \frac{1}{r} \frac{\partial}{\partial r} \left( r \frac{\partial \phi}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 \phi}{\partial \theta^2} + \frac{\partial^2 \phi}{\partial z^2} = 0$$

## Spherical Coordinates:

$$\nabla(\dots) = \frac{\partial(\dots)}{\partial r} \hat{\lambda}_r + \frac{1}{r} \frac{\partial(\dots)}{\partial \theta} \hat{\lambda}_\theta + \frac{1}{r \sin \theta} \frac{\partial(\dots)}{\partial \phi}$$

$$\nabla^2 \phi = \frac{1}{r^2} \frac{\partial}{\partial r} \left( r^2 \frac{\partial \phi}{\partial r} \right) + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left( \sin \theta \frac{\partial \phi}{\partial \theta} \right) +$$

$$+ \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 \phi}{\partial \phi^2} = 0$$

# Point Source: (3-D)

4

$$\phi = -\frac{\sigma}{4\pi r}$$

$$\vec{r} = (x, y, z)^T$$

$$r = \|\vec{r}\|$$

$\sigma \Rightarrow$  intensity

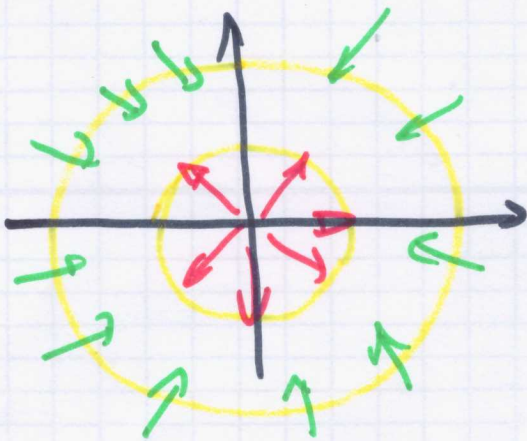
Laplace eq.

$$\frac{1}{r^2} \frac{\partial}{\partial r} \left( \frac{r^2 \sigma}{4\pi r^2} \right) = 0 \quad \text{okay}$$

$$\vec{q} = -\frac{\sigma}{4\pi} \nabla \left( \frac{1}{r} \right) = \frac{\sigma \vec{r}}{4\pi r^3}$$

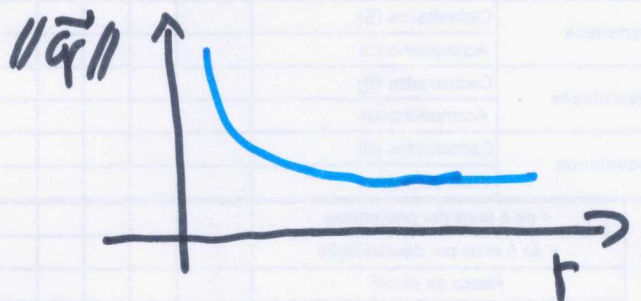
$$r \neq 0 \quad (r > 0)$$

$$\vec{q} = (q_r, q_\theta, q_\phi)^T \Rightarrow \left( \frac{\sigma}{4\pi r^2}, 0, 0 \right)^T$$

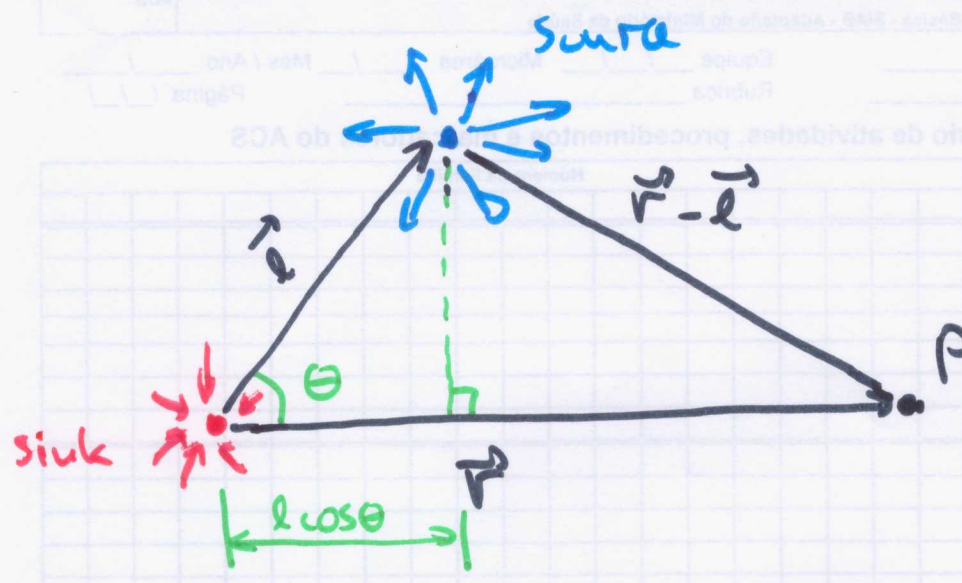


$\sigma > 0 \Rightarrow$  source

$\sigma < 0 \Rightarrow$  sink



# Doublet.



$$\Phi_p = \frac{\sigma}{4\pi} \left( \frac{1}{\|r\|} - \frac{1}{\|r-l\|} \right)$$

limit where  
 $l \rightarrow 0$  ;  $\|l\| = d$   
 $\sigma \rightarrow \infty$   
 and  $\sigma l \rightarrow \mu$

$$\Phi = \lim_{\substack{l \rightarrow 0 \\ \sigma \rightarrow \infty \\ \sigma l \rightarrow \mu}} \frac{\sigma}{4\pi} \left( \frac{\|r-l\| - \|r\|}{\|r\| \|r-l\|} \right) = ?$$

$$\lim_{l \rightarrow 0} \|r\| \|r-l\| = r^2 \quad \text{and} \quad \lim_{l \rightarrow 0} \{ \|r-l\| - \|r\| \} = -l \cos \theta$$

$$\|r-l\|^2 = \|r\|^2 + \|l\|^2 - 2\|r\|\|l\|\cos \theta$$

$$\|r\| = r, \quad \|l\| = l$$

$$\|r-l\|^2 - \|r\|^2 = l^2 - 2rl \cos \theta$$

$$\|r-l\| - \|r\| = \frac{l^2 - 2rl \cos \theta}{\|r-l\| + \|r\|}$$

$$\|r-l\| - \|r\| \approx -2rl \cos \theta = -\mu \cos \theta$$

$$\lim_{\substack{l \rightarrow 0 \\ \sigma \rightarrow \infty \\ \sigma l \rightarrow \mu}} \Phi_p = \lim_{\substack{q \rightarrow 0 \\ \tau \rightarrow \infty \\ \sigma l \rightarrow \mu}} - \frac{\sigma l \cos \theta}{4\pi r^2} = - \frac{\mu \cos \theta}{4\pi r^2}$$

$$\Phi_{\text{Dipole}} = - \frac{\mu \cos \theta}{4\pi r^2} = - \frac{\vec{\mu} \cdot \vec{r}}{4\pi r^3}$$

$$\vec{\mu} \cdot \vec{r} = \mu r \cos \theta$$

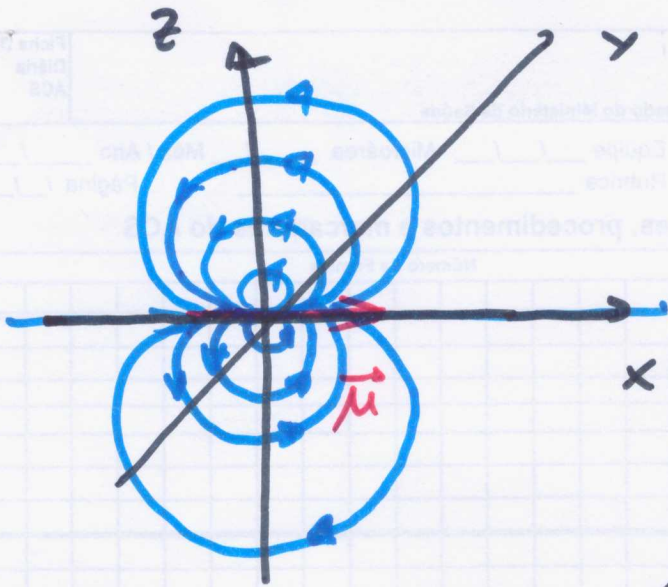
$$\nabla^2 \Phi = \frac{1}{r^2} \frac{\partial}{\partial r} \left( \frac{r^2 \mu \cos \theta}{2\pi r^3} \right) + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left( \frac{\sin^2 \theta \mu}{4\pi r^2} \right) =$$

$$[\sin^2 \theta]' = 2 \sin \theta \cos \theta$$

$$- \frac{\mu \cos \theta}{2\pi r^4} + \frac{\mu \cos \theta}{2\pi r^4} = 0$$

$$q_r = \frac{\partial \Phi}{\partial r} = \frac{\mu \cos \theta}{2\pi r^3} ; \quad q_\theta = \frac{1}{r} \frac{\partial \Phi}{\partial \theta} = \frac{\mu \sin \theta}{4\pi r^3}$$

$$q_\varphi = \frac{1}{r \sin \theta} \frac{\partial \Phi}{\partial \varphi} = 0$$



7

Poly nomials

$$\Phi = Ax + By + Cz$$

( $\rightarrow$  1st order

$$\left\{ \begin{aligned} u = \frac{\partial \Phi}{\partial x} &= A = U_{\infty} \\ v = \frac{\partial \Phi}{\partial y} &= B = V_{\infty} \\ w = \frac{\partial \Phi}{\partial z} &= C = W_{\infty} \end{aligned} \right.$$

$$\Phi = Ax^2 + By^2 + Cz^2 \Rightarrow \nabla^2 \Phi = A + B + C = 0$$

$\Rightarrow$  for  $B=0$ ,  $A = -C$

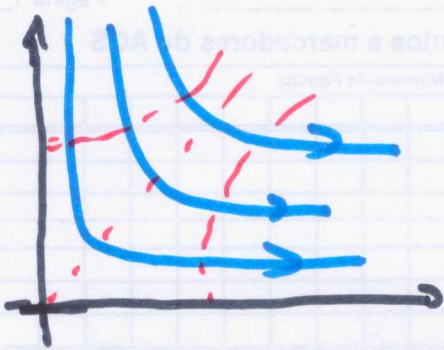
$$\Phi = A(x^2 - z^2) \Rightarrow \left\{ \begin{aligned} u &= 2Ax \\ v &= 0 \\ w &= -2Az \end{aligned} \right.$$

~~\*~~

Stream line function: }  $\vec{q} \times d\vec{l} = 0$   
 Stream line element:  $d\vec{l}$

Streamline equation:  $\boxed{dx = \frac{dy}{u} = \frac{dz}{w}}$

$$\frac{dx}{2Ax} = \frac{dz}{-2Az} \Rightarrow xz = \text{constant} \quad \text{along streamlines} \quad \textcircled{8}$$



Corner Flow

2-D source : Cylindrical / polar coordinates

$$q_\theta = 0$$

$$\text{Vorticity: } \omega_z = -\frac{1}{r} \left( \frac{\partial(rq_\theta)}{\partial r} - \frac{\partial(q_r)}{\partial \theta} \right) =$$

$$= \frac{1}{r} \frac{\partial(q_r)}{\partial \theta} = 0 \Rightarrow q_r(r)$$

$$\text{Continuity: } \nabla \cdot \vec{q} = \frac{1}{r} \frac{\partial(rq_r)}{\partial r} = 0 \Rightarrow r \cdot q_r = \text{ct.}$$

$$r \cdot q_r = \frac{Q}{2\pi} = \frac{\sigma}{2\pi}$$

$$Q \Rightarrow \text{Volumetric flow rate: } Q = \sigma = \int_0^{2\pi} q_r r d\theta = 2\pi q_r r$$

$$\left. \begin{aligned} q_r &= \frac{\partial \phi}{\partial r} = \frac{\sigma}{2\pi r} \\ q_\theta &= \frac{1}{r} \frac{\partial \phi}{\partial \theta} = 0 \end{aligned} \right\} \begin{aligned} \phi &= \frac{\sigma \ln(r)}{2\pi} + C \\ \phi &= \frac{\sigma}{2\pi} \ln(r) \end{aligned}$$



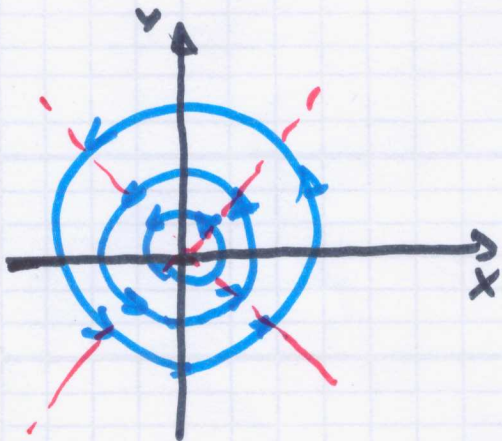
# 2-D Doublet (similar reasoning)

$\vec{\mu} = (\mu, 0) \Rightarrow$

$$\Phi = -\frac{\mu \cdot \vec{r}}{2\pi r^2}$$

$$\left\{ \begin{aligned} \Phi(r, \theta) &= -\frac{\mu \cos \theta}{2\pi r} \\ q_r &= \frac{\partial \Phi}{\partial r} = \frac{\mu \cos \theta}{2\pi r^2} \\ q_\theta &= \frac{1}{r} \frac{\partial \Phi}{\partial \theta} = \frac{\mu \sin \theta}{2\pi r^2} \end{aligned} \right.$$

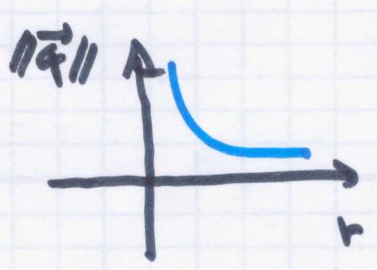
## Vortex (2-D point vortex)



the "real thing"  
 $\|\vec{q}\|$

A graph showing the velocity magnitude  $\|\vec{q}\|$  on the vertical axis versus radius  $r$  on the horizontal axis. A blue curve starts at a high value for small  $r$  and decreases as  $r$  increases, following a  $1/r$  relationship. A vertical line is drawn at a radius  $r_0$ .

$r_0$   
 scales with "viscosity"  
 Kolmogorov



The vorticity is zero everywhere, except for a single point, at the origin in this particular case.

$$\omega_z = -\frac{1}{r} \left[ \frac{\partial(rq_\theta)}{\partial r} - \frac{\partial q_r}{\partial \theta} \right] = -\frac{1}{r} \frac{\partial(rq_\theta)}{\partial r} = 0$$

$$\Gamma q_\theta = A$$

$$\Gamma \rightarrow \infty \Rightarrow q_\theta \rightarrow 0$$

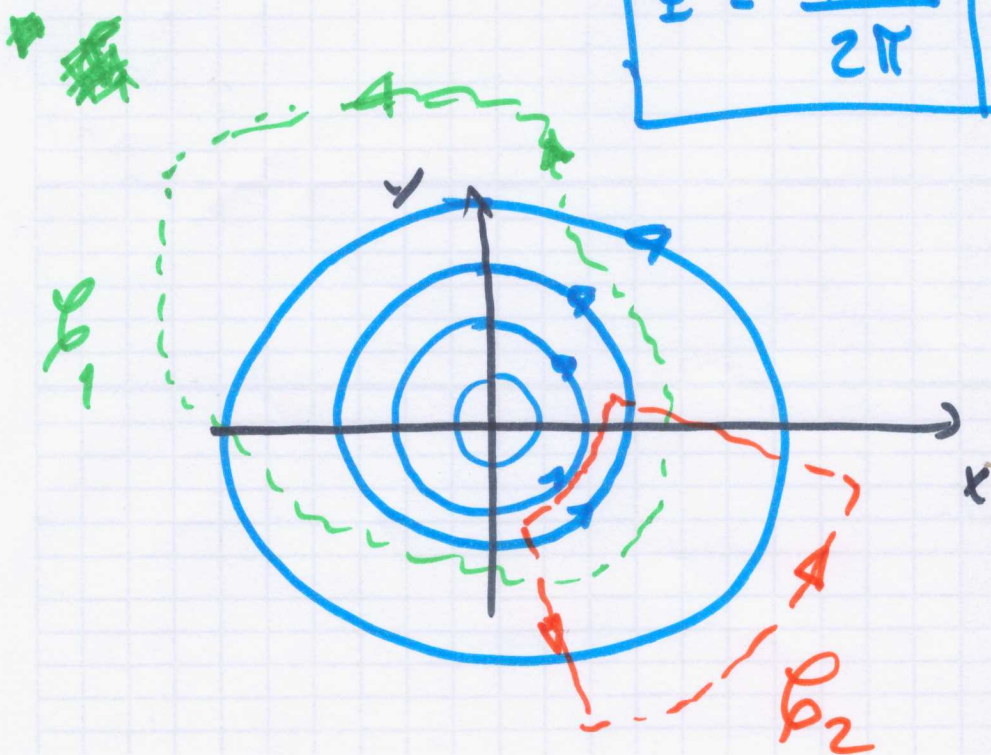
$$\Gamma = \oint \vec{q} \cdot d\vec{l} = \int_0^{2\pi} q_\theta \cdot r \cdot d\theta = 2\pi A$$

circle with radius "r" center at the origin and oriented counter-clockwise (positive)

$$A = \frac{\Gamma}{2\pi}$$

$$\left\{ \begin{array}{l} q_r = 0 \\ q_\theta = \frac{\Gamma}{2\pi r} \end{array} \right\} \Rightarrow \phi = \int q_\theta \cdot r \cdot d\theta + c$$
  
$$\phi = \frac{\Gamma \theta}{2\pi} + c$$

$$\boxed{\phi = \frac{\Gamma \theta}{2\pi}}$$



$$\oint \vec{q} \cdot d\vec{l} = \Gamma$$

$$\oint \vec{q} \cdot d\vec{l} = 0$$

# Complex Potential: (2-D)

$$F(z) \equiv \underbrace{\Phi(x,y)}_{\text{Potential function}} + i \underbrace{\Psi(x,y)}_{\text{Stream function}}$$

C.R.  $\therefore \Phi_{,x} = \Psi_{,y} = u$   
 $\Phi_{,y} = -\Psi_{,x} = v$

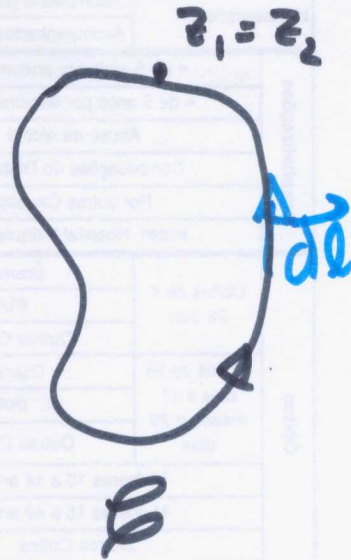
$$F'(z) = \frac{dF}{dz} = \Phi_{,x} + i \Psi_{,x} = \Psi_{,y} - i \Phi_{,y} = u - iv$$

$$F'(z) = u - iv = \overline{U(z)} \equiv W \text{ complex velocity}$$

$$\frac{dF}{dz} = u - iv = W = \overline{U}$$

$$\Gamma = \oint_C \overline{q} \cdot d\vec{l} = \oint_C u dx + v dy = \oint_C d\Phi$$

$$Q = \oint_C (u dy - v dx) = \oint_C d\Psi$$



$$\oint_C f w(z) dz = \oint_C (u - iv)(dx + i dy) =$$

$$= \oint_C (u dx + v dy) + i \oint_C (u dy - v dx) =$$

$$= \oint_C d\Phi + i \oint_C d\psi = \Gamma + i Q$$

$$\oint_C f w dz = \Gamma + i Q = F(z_2) - F(z_1)$$

$$\nabla \phi = \vec{u} \parallel \psi \mid \text{constant}$$

$$\nabla \psi = \vec{u} \perp \phi \mid \text{constant}$$

$$\psi \perp \phi$$

$$\nabla \phi \perp \nabla \psi$$

Flow	$F(z)$	$W(z)$
Uniform	$Az$	$A \in \mathbb{C}$

Corner of Angle $\theta = \frac{\pi}{n}$	$Az^n$	$A_n z^{n-1}$
---	--------	---------------

Source at $z=0$ $Q = 2\pi A$ $A \in \mathbb{R}$	$A \log(z)$ $\frac{Q}{2\pi} \log(z)$	$\frac{A}{z}$ $\frac{Q}{2\pi z}$
---	---	-------------------------------------

Vortex at $z=0$ $\Gamma$	$-\frac{i\Gamma}{2\pi} \log(z)$	$\frac{i\Gamma}{2\pi z}$
--------------------------------	---------------------------------	--------------------------

Doublet at $z=0$ $\vec{\mu} // \hat{x}$ direction $\mu$	$-\frac{\mu}{2\pi z^2}$	$\frac{\mu}{2\pi z^2}$
--	-------------------------	------------------------

(16/04/2020)

(1)

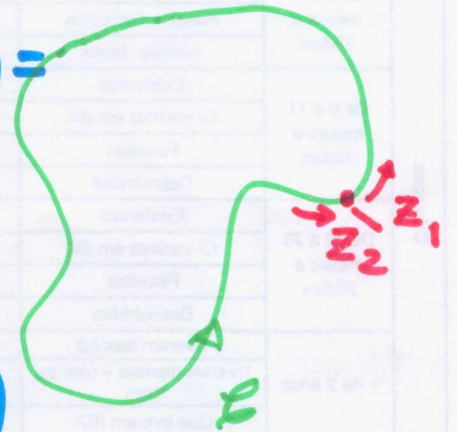
$$\left\{ \begin{array}{l} u = \frac{\partial \phi}{\partial x} = \frac{\partial \psi}{\partial y} \\ v = \frac{\partial \phi}{\partial y} = -\frac{\partial \psi}{\partial x} \end{array} \right. \quad \begin{array}{l} F = \Phi + i\Psi \\ \frac{dF}{dz} = W = u - iv \\ U = \bar{W} = u + iv \end{array}$$

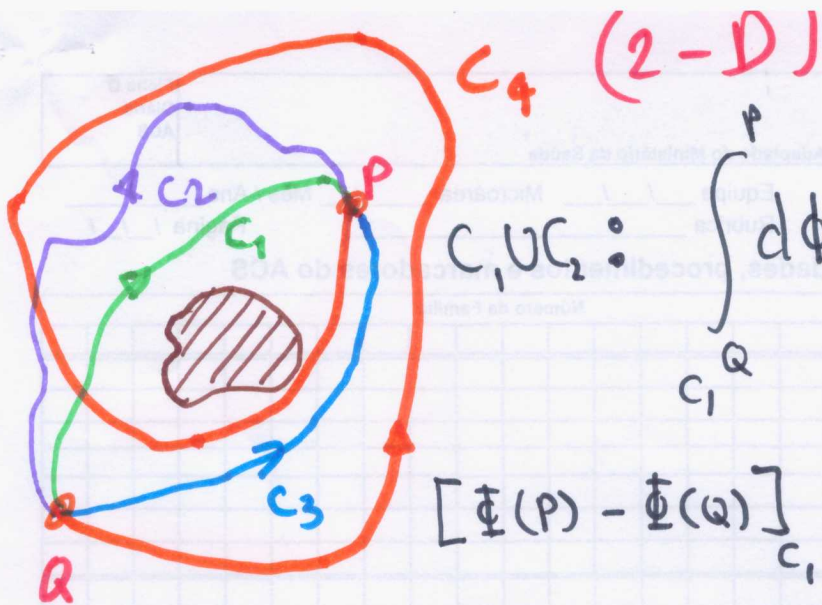
$$\oint_{\Gamma} w(z) dz = \oint_{\Gamma} (u - iv)(dx + iy) =$$

$$= \oint_{\Gamma} (u dx + v dy) + i \oint_{\Gamma} (u dy - v dx)$$

$$= \oint_{\Gamma} d\phi + i \oint_{\Gamma} d\psi = \Gamma + i Q.$$

$$\Gamma + i Q = \oint_{\Gamma} w(z) dz = F(z_2) - F(z_1)$$





$$C_1 \cup C_2 : \int_{C_1}^P d\phi - \int_{C_2}^P = 0$$

$$[\Phi(P) - \Phi(Q)]_{C_1} = [\Phi(P) - \Phi(Q)]_{C_2}$$

$$\int_{C_3}^P d\phi - \int_{C_1}^P d\phi = \Gamma \Rightarrow \begin{cases} [\Phi(P) - \Phi(Q)]_{C_3} - [\Phi(P) - \Phi(Q)]_{C_1} = \Gamma \\ [\Phi(P) - \Phi(Q)]_{C_4} - [\Phi(P) - \Phi(Q)]_{C_3} = \Gamma \end{cases}$$

$C_4 \cup C_3 \Rightarrow$  (red)       $C_3 \cup C_1$  (blue)       $C_4 \cup C_1$  (purple)

---


$$[\Phi(P) - \Phi(Q)]_{C_4} - [\Phi(P) - \Phi(Q)]_{C_1} = 2\Gamma$$

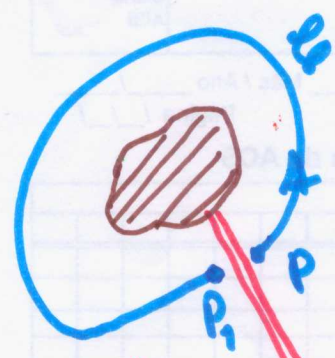
Then, on taking Q as a reference point, we can write:

$$[\Phi(P)_{C_4} - \Phi(P)_{C_1}] = 2\Gamma + [\Phi(Q)_{C_4} - \Phi(Q)_{C_1}]$$

Reference Point  $\Rightarrow \Phi(Q)_{C_4} = \Phi(Q)_{C_1}$

therefore, we get:

$$\Phi(P)_{C_4} - \Phi(P)_{C_1} = 2\Gamma$$



$$\lim_{P \rightarrow P_1} \int_P^{P_1} d\Phi = \lim_{P \rightarrow P_1} [\Phi(P) - \Phi(P_1)] = \Gamma$$

$\infty$  branch cut.

$$F(z) = U_\infty z + \frac{A}{z} = U_\infty(x + iy) + \frac{A}{r} e^{-i\theta}$$

$$= \left( U_\infty x + \frac{A}{r} \cos\theta \right) + i \left( U_\infty y - \frac{A}{r} \sin\theta \right)$$

$$= \Phi + i\Psi$$

$\Psi = 0$  at the circle:  $\Psi = U_\infty y - \frac{A}{r} \sin\theta = 0$

$$\Psi = U_\infty r \sin\theta - \frac{A}{r} \sin\theta = 0$$

$$U_\infty r^2 = A$$

$$r = + \sqrt{\frac{A}{U_\infty}} = + \sqrt{\frac{\mu}{2\pi U_\infty}}$$

$$\mu = 2\pi A$$



# Cylinder with Magnus effect.

④

$$F(z) = U_{\infty} z + \frac{A}{z} - i\Gamma \log\left(\frac{z}{a}\right) =$$

$$= U_{\infty} z + \frac{\mu}{2\pi z} + \frac{i\Gamma}{2\pi} \log\left(\frac{z}{a}\right) \quad \text{where } a \in \mathbb{R}$$

$$F(z) = \left[ U_{\infty} x + \frac{\mu}{2\pi r} \cos\theta - \frac{\Gamma}{2\pi} (\theta \pm 2k\pi) \right] +$$

$$+ i \left[ U_{\infty} y - \frac{\mu \sin\theta}{2\pi r} + \frac{\Gamma}{2\pi} \ln\left(\frac{r}{a}\right) \right] = \Phi + i\Psi$$

$$\Psi = 0 \Rightarrow \text{wall} \Rightarrow \Psi = U_{\infty} a \sin\theta - \mu \sin\theta + \frac{\Gamma}{2\pi} \ln\left(\frac{a}{a}\right)$$

( $r=a$ )

$$\Psi = 0 \Rightarrow a = + \sqrt{\frac{\mu}{2\pi U_{\infty}}}$$

same as before

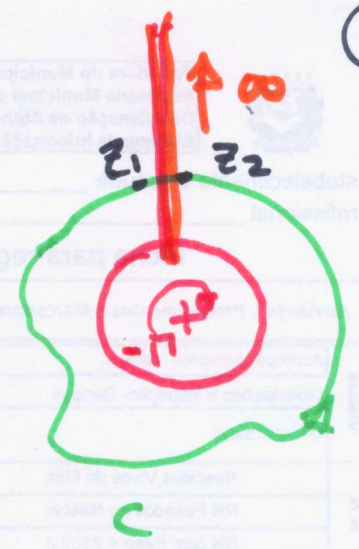
Kutta-Joukowski Theorem:

$$\vec{F} = \rho \vec{U} \times \int_{b_1}^{b_2} \vec{F}(b) dt_b \Rightarrow \vec{L} = \rho U_{\infty} \Gamma$$

$$W = \frac{dF}{dz} = U_\infty - \frac{\mu}{2\pi z^2} + \frac{i\Gamma a}{2\pi z}$$

$$W = U_\infty - \frac{\mu e^{-i2\theta}}{2\pi r^2} + \frac{i\Gamma a e^{-i\theta}}{2\pi r}$$

$$U = \bar{W} = U_\infty - \frac{\mu e^{i2\theta}}{2\pi r^2} - \frac{i\Gamma a e^{i\theta}}{2\pi r}$$



$$z_1 = x + iy \equiv z_2$$

$$\begin{cases} z_1 = R e^{i\theta} \\ z_2 = R e^{i(\theta + 2\pi)} \end{cases}$$

Circulation  $\Gamma$ :

$$\Gamma_T + iQ_T = \oint_C W(z) dz = F(z_2) - F(z_1) = \frac{i\Gamma}{2\pi} \left[ \log\left(\frac{z_2}{a}\right) - \log\left(\frac{z_1}{a}\right) \right]$$

$$= \frac{i\Gamma}{2\pi} \log\left(\frac{z_2}{z_1}\right) = \frac{i\Gamma}{2\pi} \left\{ \ln\left(\frac{R}{R}\right) + i(\theta + 2\pi - \theta) \right\}$$

$$= \frac{i\Gamma}{2\pi} \{ i2\pi(1) \} = -\Gamma \Rightarrow \Gamma_T + iQ_T = -\Gamma + i0$$

Laurent Series:

$$f(z) = \sum_{n=0}^{\infty} a_n (z-z_0)^n + \sum_{n=1}^{\infty} \frac{b_n}{(z-z_0)^n} = \sum_{n=-\infty}^{\infty} c_n (z-z_0)^n$$

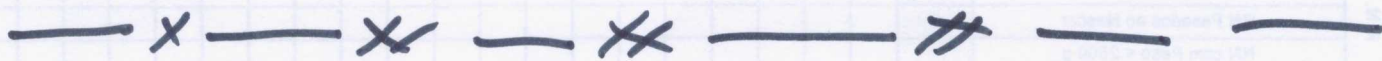
$$R_1 < |z - z_0| < R_2$$

$$c_n = \frac{1}{2\pi i} \oint_C \frac{f(z) dz}{(z-z_0)^{n+1}} \quad \forall n \in \mathbb{Z}$$

two important cases:

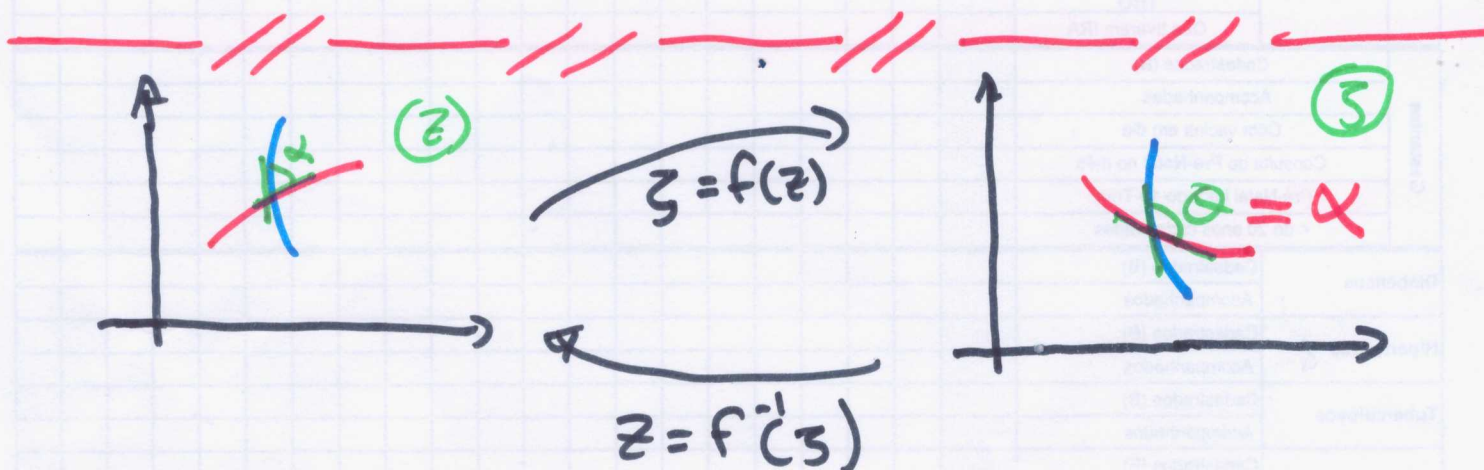
$$[z^{-1}]' = -z^{-2} \implies \int z^{-2} dz = -\frac{1}{z}$$

$$[z^{-2}]' = -2z^{-3} \implies \int z^{-3} dz = -\frac{1}{2z^2}$$



$$W(z) = A_0 + \frac{A_1}{z} + \dots = \sum_{n=0}^{\infty} \frac{A_n}{z^n}$$

$$F(z) = A_0 z + A_1 \log(z) - \sum_{n=2}^{\infty} \frac{A_n}{(n-1)z^{(n-1)}} + C$$



$$\delta z = \frac{d\zeta}{dz} \delta z \implies \delta \zeta = \frac{df}{dz} \delta z$$

$$\left\{ \begin{aligned} |\delta \zeta| &= \left| \frac{df}{dz} \right| \cdot |\delta z| \implies \text{local isotropic stretching} \\ \arg(\delta \zeta) &= \arg\left(\frac{df}{dz}\right) + \arg(\delta z) \end{aligned} \right.$$

Conformal Mapping  
Preserves local angles

local isotropic and finite rotation.

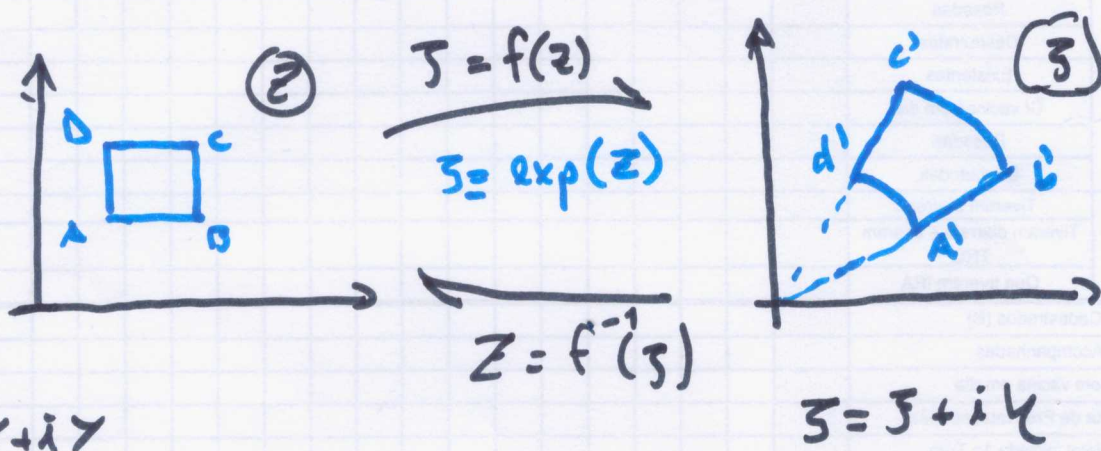
(23/04/2020)

①

$$W(z) = A_0 + \frac{A_1}{z} + \dots = \sum_{n=0}^{\infty} \frac{A_n}{z^n}$$

$$F(z) = A_0 z + A_1 \log(z) - \sum_{n=2}^{\infty} \frac{A_n}{(n-1)z^{(n-1)}} + \dots$$

Conformal Mapping flows:



$$\left. \begin{array}{l} \zeta = \zeta(x, y) \\ \eta = \eta(x, y) \end{array} \right\} \Rightarrow \zeta = F(z) \Leftrightarrow z = F^{-1}(\zeta) = \begin{cases} x = x(\zeta, \eta) \\ y = y(\zeta, \eta) \end{cases}$$

$$F(z) = \Phi(x, y) + i\Psi(x, y) = \Phi(\zeta, \eta) + i\Psi(\zeta, \eta) \Rightarrow F(\zeta)$$

Scalar Function.

$$J = \begin{vmatrix} \zeta_{,x} & \zeta_{,y} \\ \eta_{,x} & \eta_{,y} \end{vmatrix} = (\zeta_{,xx})^2 + (\zeta_{,yy})^2 = (\eta_{,xx})^2 + (\eta_{,yy})^2 = \left| \frac{d\zeta}{dz} \right|^2 \in \mathbb{C} \rightarrow \mathbb{R}$$

So, whenever and wherever  $J \neq 0$ , we are good.

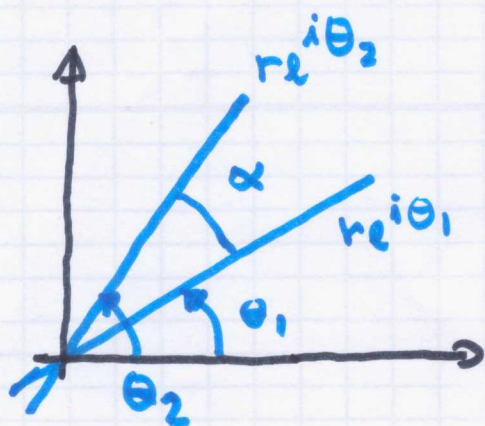
$$\frac{dF}{dz} = \frac{dF}{d\zeta} \frac{d\zeta}{dz} \iff \frac{dF}{d\zeta} = \frac{dF}{dz} \frac{1}{(d\zeta/dz)}$$

$$\nabla_{xy}^2 (\dots) = \underbrace{\left| \frac{d\zeta}{dz} \right|^2}_{(J)} \nabla_{\zeta\eta}^2 (\dots)$$

$$\frac{dz}{d\zeta} = \frac{1}{d\zeta/dz} ; \quad \tilde{W}(\zeta) = W[z(\zeta)] \frac{dz}{d\zeta}$$

At a critical point of the transformation,  $\frac{d\zeta}{dz} = 0 \iff \frac{dz}{d\zeta} = \infty$

Therefore, we try to keep those points out of the region of interest, so as not to get  $\tilde{W}(\zeta) \rightarrow \infty$ . Unless we know that  $W(z) = 0$  there: stagnation point.



$$\left. \begin{array}{l} \theta_2 - \theta_1 = \alpha \\ \zeta = z^n \end{array} \right\} \begin{array}{l} \delta\zeta = n z^{n-1} \delta z \\ \zeta_1 = r^n e^{i(n\theta_1)} \\ \zeta_2 = r^n e^{i(n\theta_2)} \end{array}$$

$\alpha \xrightarrow{f(z)} n\alpha$   
 $(z) \qquad (\zeta)$

$$\Gamma_{\zeta} + i Q_{\zeta} = \oint_{C_{\zeta}} \tilde{w}(\zeta) d\zeta = \oint_{C_{\zeta}} \frac{w(z)}{\left(\frac{d\zeta}{dz}\right)} \frac{d\zeta}{dz} dz =$$

$$= \int_{C_z} w(z) dz = \Gamma + i Q$$

The requirement for uniform flow at  $z = \infty$ , further imposes the condition:

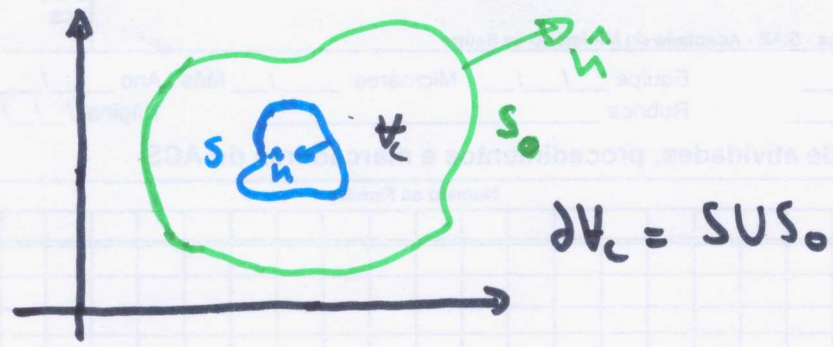
$$\zeta = \infty \Rightarrow \begin{cases} z = \zeta = \infty \\ \left. \frac{dz}{d\zeta} \right|_{\zeta = \infty} = 1 \end{cases}$$

$$z(\zeta) = \zeta + \sum_{n=2}^{\infty} \frac{C_n}{\zeta^n} \Rightarrow \frac{dz}{d\zeta} = 1 - \sum_{n=1}^{\infty} \frac{n C_n}{\zeta^{(n+1)}}$$

### Blazius Relations for steady 2-D Flows

$$X - i Y = i \frac{\rho}{2} \oint_{C_0} [w(z)]^2 dz$$

$$M = -\frac{\rho}{2} \operatorname{Re} \left\{ \oint_{C_0} [w(z)]^2 z dz \right\}$$



$$\sum \vec{F} = \iiint_{\mathcal{V}_c} \frac{\partial}{\partial t} (\rho \vec{U}) dV + \iint_{S_0} \rho \vec{U} (\vec{U} \cdot \hat{n}) ds + \iint_S \rho \vec{U} (\vec{U} \cdot \hat{n}) ds +$$

$$+ \iint_{S_0} p \hat{n} ds + \iint_S p \hat{n} ds$$

Force interaction between fluid and body

Bernoulli:

$$p = p_T - \frac{\rho U^2}{2} - \frac{\rho \partial \Phi}{\partial t}$$

$\rightarrow$  far field

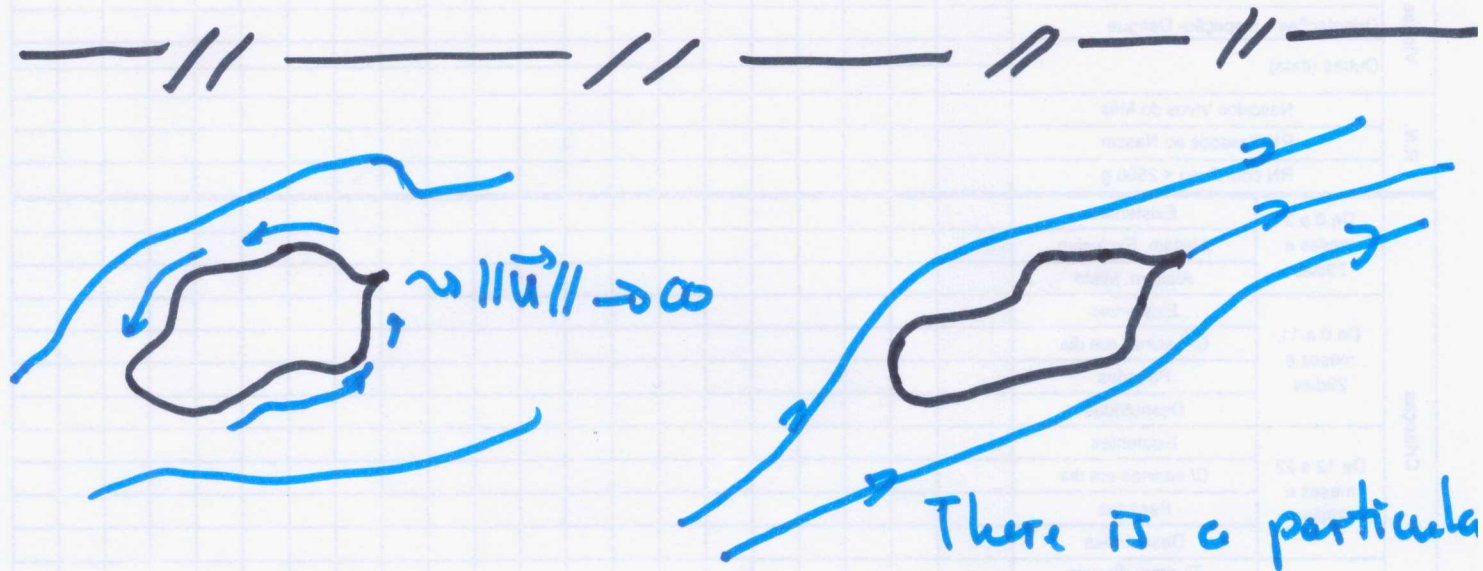
$\rightarrow$  constant

$$\iint_S p \hat{n} ds = \vec{F} = - \iint_{\mathcal{V}_c} \frac{\partial \vec{U}}{\partial t} - \iint_{S_0} \rho \vec{U} (\vec{U} \cdot \hat{n}) ds + \iint_{S_0} \frac{\rho U^2}{2} \hat{n} ds$$

$$\sum \vec{M} = \iiint_{\mathcal{V}_c} \frac{\partial}{\partial t} (\rho \vec{r} \times \vec{U}) dV + \iint_{S_0} \rho \vec{r} \times \vec{U} (\vec{U} \cdot \hat{n}) ds + \iint_S \rho \vec{r} \times \vec{U} (\vec{U} \cdot \hat{n}) ds +$$

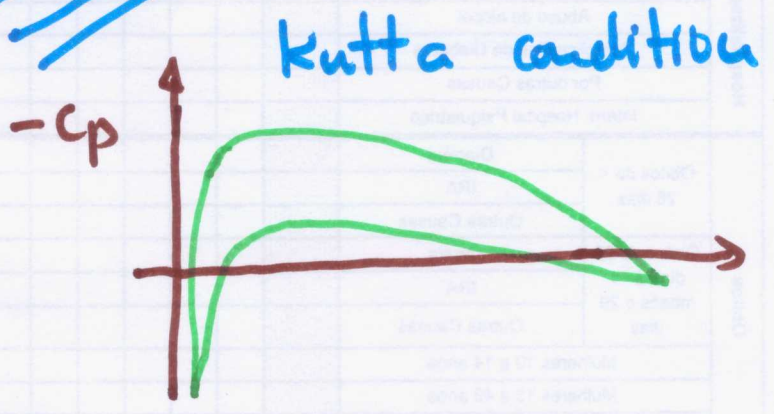
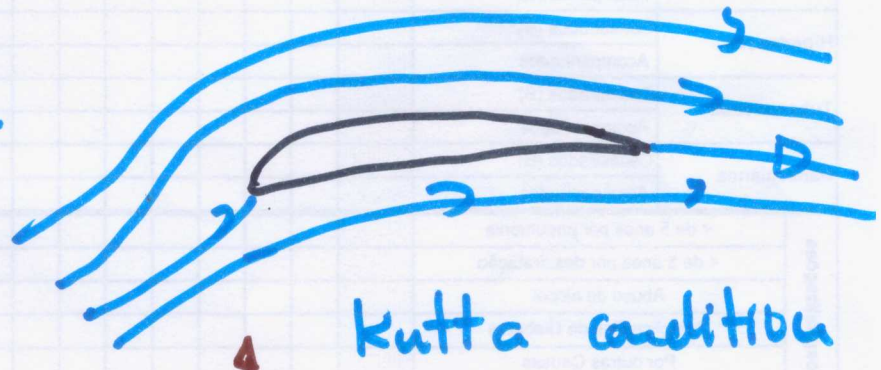
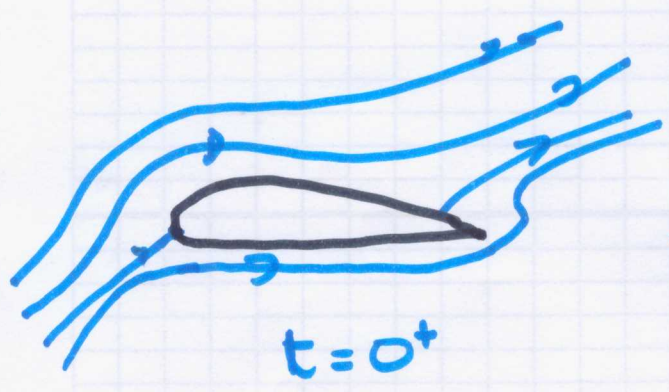
$$+ \iint_{S_0} \vec{r} \times \hat{n} p ds + \iint_S \vec{r} \times \hat{n} p ds$$

$$\iint_S \vec{r} \times \hat{n} P ds = \vec{M} = - \iint_{S_0} \vec{r} \times \vec{U} (\vec{U} \cdot \hat{n}) ds + \iint_{S_0} \vec{r} \times \hat{n} \frac{\rho U^2}{2} ds$$



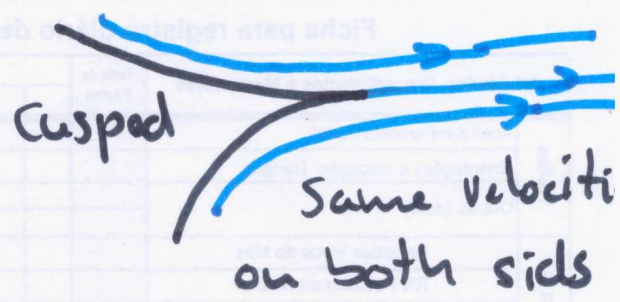
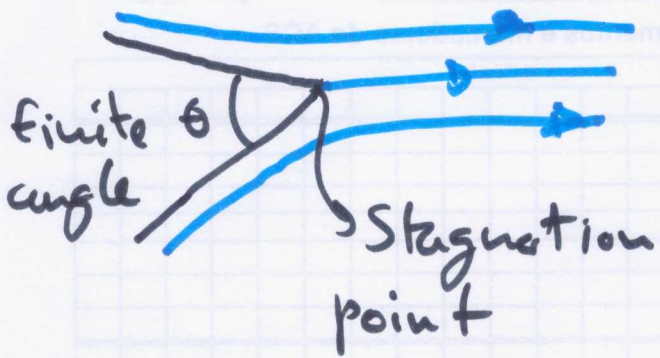
it cancels the "tangent" component at that point.

There is a particular value of  $P$  that makes the flow leave the discontinuity smoothly





# T.E.

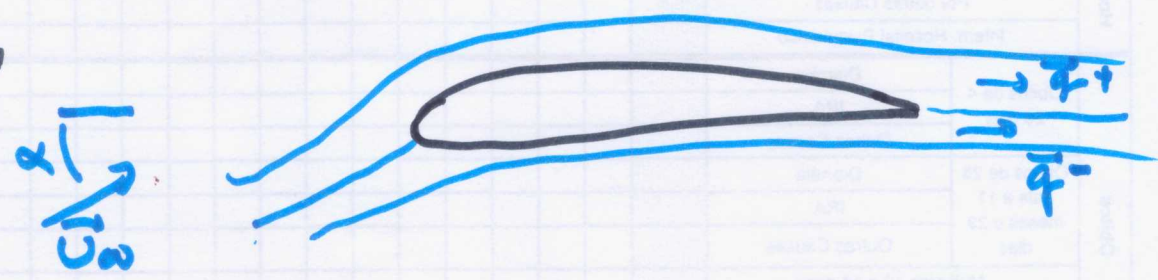


Steady discontinuities must meet the conditions

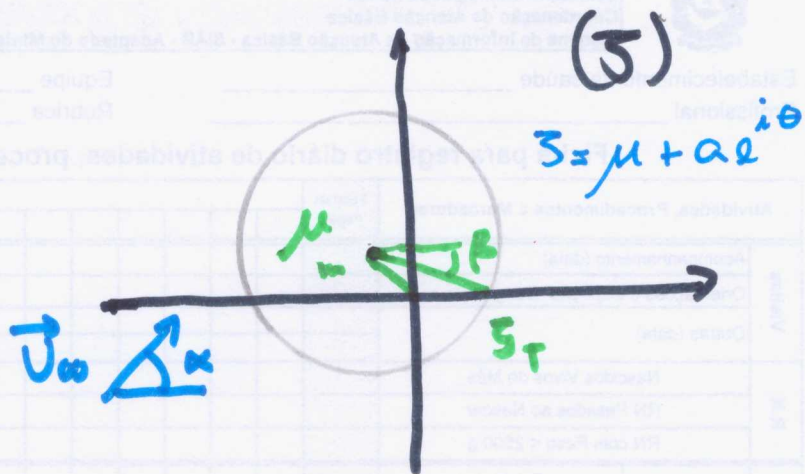
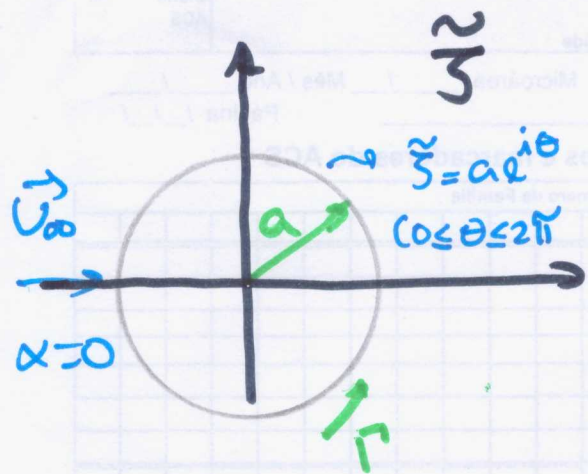
$$p^+ = p^- \quad \text{and} \quad \vec{V}^+ \cdot \hat{n} = \vec{V}^- \cdot \hat{n}$$

Bernoulli:  $p^+ + \frac{\rho(u^+)^2}{2} = p_0 = p^- + \frac{\rho(u^-)^2}{2} \Rightarrow \|\vec{U}^-\| = \|\vec{U}^+\|$

2-D Flow



$$\|\vec{U}_\infty + \vec{q}^+\| = \|\vec{U}_\infty + \vec{q}^-\| \Rightarrow \text{2-D flow } \vec{q}^- = \vec{q}^+$$



$$F(\tilde{z}) = U_\infty \tilde{z} + \frac{U_\infty a^2}{\tilde{z}} + \frac{i\Gamma}{2\pi} \log\left(\frac{\tilde{z}}{a}\right)$$

$$z = \tilde{z} e^{i\alpha} + \mu \Rightarrow \tilde{z} = (z - \mu) e^{-i\alpha}$$

$$\mu = m e^{i\delta}, \quad z_T = \mu + a e^{-i\beta}$$

$$F(z) = U_\infty (z - \mu) e^{-i\alpha} + \frac{U_\infty a^2 e^{i\alpha}}{(z - \mu)} + \frac{i\Gamma}{2\pi} \log\left(\frac{z - \mu}{a e^{i\alpha}}\right)$$

Kutta condition:

$$W(z) \Big|_{z_T} = W(z) \Big|_{z_T} \frac{1}{\left(\frac{dz}{d\tilde{z}}\right)_{z_T}}$$

$$\begin{cases} W(z_T) = 0 \\ \frac{dz}{d\tilde{z}} \Big|_{z_T} = 0 \end{cases}$$

$$W(z) = \frac{dF}{dz} = U_{\infty} e^{-i\alpha} - \frac{U_{\infty} a^2 e^{i\alpha}}{(z-\mu)^2} + \frac{i\Gamma}{2\pi} \frac{a e^{i\alpha}}{(z-\mu)} \frac{1}{a e^{i\alpha}} \quad (8)$$

$$W(z) = U_{\infty} e^{-i\alpha} + \frac{i\Gamma}{2\pi(z-\mu)} - \frac{U_{\infty} a^2 e^{i\alpha}}{(z-\mu)^2}$$

Then for the Kutta condition to hold, we need

$$W(z_r) = 0 \quad \Rightarrow \quad (z_r - \mu) = a e^{-i\beta}$$

On imposing this condition, we get

$$\Gamma = 4\pi a U_{\infty} \sin(\alpha + \beta)$$

Transformation:  $z = \zeta + \frac{(\zeta_r)^2}{\zeta}$

$\zeta_r$  is real ( $\zeta_r \in \mathbb{R}$ )

(30/04/20)

1

Kutta Condition  $w(z_T) = 0$

Critical Point of Joukowski transformation

$$\Gamma = 4\pi a U_\infty \sin(\alpha + \beta)$$

$$L = \rho U_\infty \Gamma = 4\pi \rho U_\infty^2 a \sin(\alpha + \beta)$$

$$C_L = 8\pi \left(\frac{a}{c}\right) \sin(\alpha + \beta) \quad \Leftarrow \quad C_L = \frac{L}{\frac{1}{2} \rho U_\infty^2 c}$$

$c = \text{chord.}$



For Joukowski airfoils:  $c \cong 4a$

$$C_L = 2\pi \sin(\alpha + \beta) \Rightarrow$$

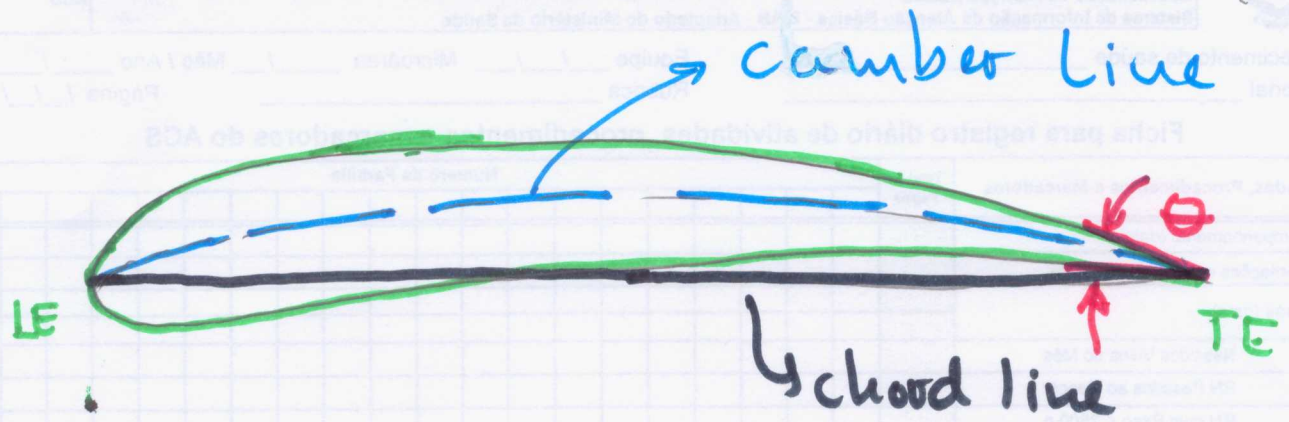
$$C_L \cong 2\pi(\alpha + \beta)$$

$\alpha$  and  $\beta$  in radians.

$$\text{for } \alpha = -\beta \Rightarrow C_L = 0 \Rightarrow$$

$$\alpha_0 = \alpha \Big|_{L=0} = -\beta$$





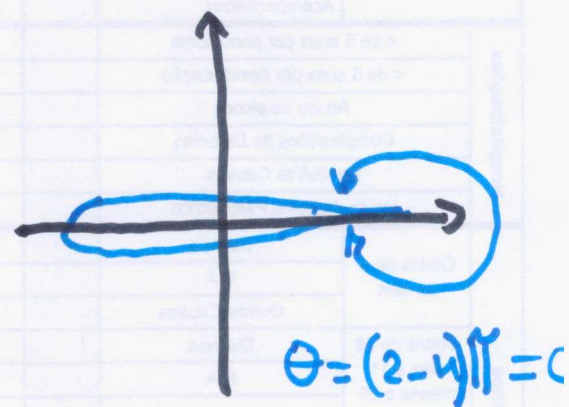
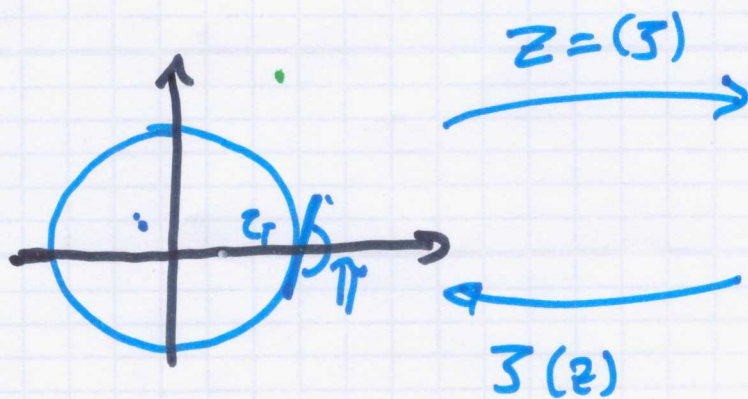
Joukowski transformation

$$TE: z_t = \zeta_T = C \in \mathbb{R}$$

$$z = \zeta + \frac{c^2}{\zeta}$$

$$\frac{dz}{d\zeta} = 1 - \frac{c^2}{\zeta^2} \Rightarrow \left. \frac{dz}{d\zeta} \right|_{\zeta_T} = 1 - \frac{c^2}{\zeta_T^2} = 0$$

$$\frac{d^2z}{d\zeta^2} = \frac{2c^2}{\zeta^3} \Rightarrow \left. \frac{d^2z}{d\zeta^2} \right|_{\zeta_T} = \frac{2}{\zeta_T} \neq 0 \Rightarrow \boxed{n=2}$$



Cuspid T.E.

$$\boxed{\theta = 0}$$

$$\theta = (2-n)\pi = 0$$

# Joukowski Airfoil:

$$C_l = 2\pi(\alpha + \beta) \quad , \quad \alpha_0 = -\beta$$

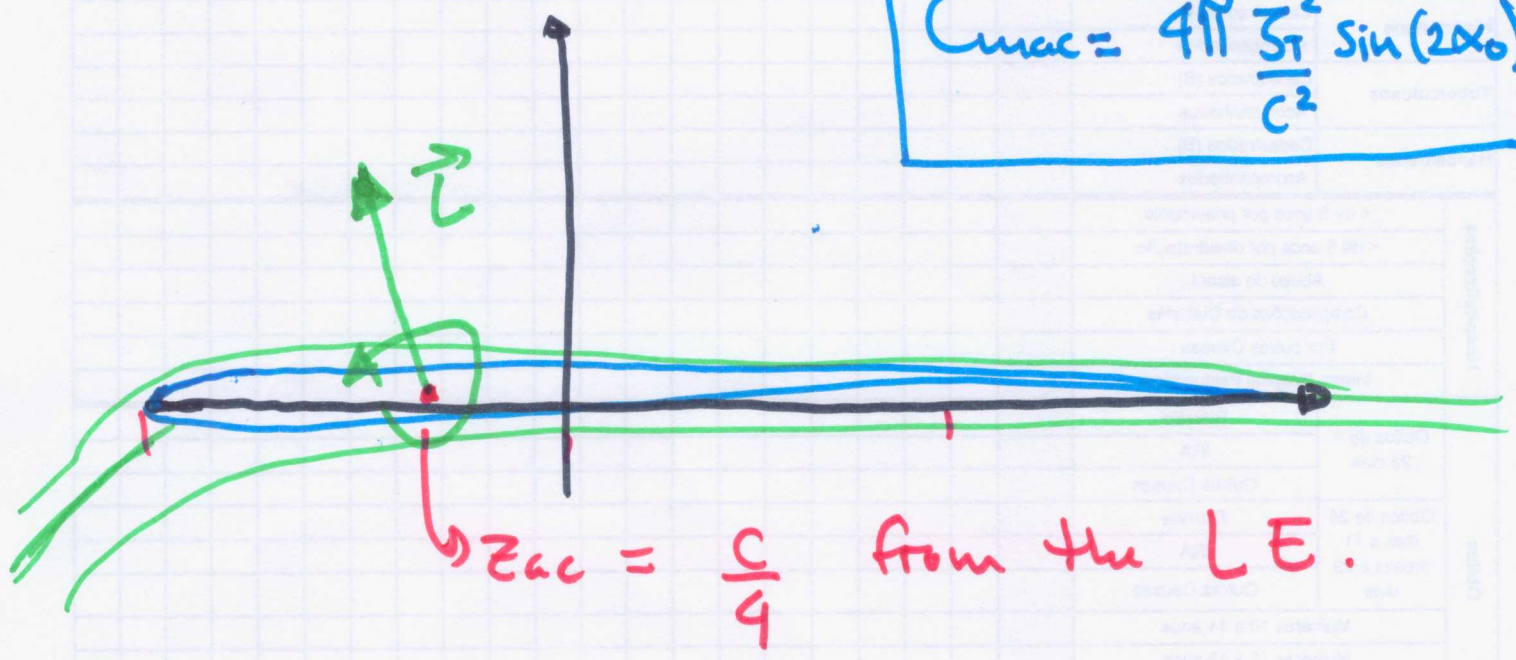
Aerodynamic Center coordinate

$$z_{Ac} \equiv \mu - \frac{\gamma_T^2}{a} e^{i\beta} \quad ; \quad \mu = m e^{i\delta}$$

$$M_{Ac} = -2\pi \rho U_\infty^2 \gamma_T^2 \sin(2\beta)$$

For thin airfoils,  $z_{Ac}$  is very close to the quarter-chord point

$$C_{mac} = 4\pi \frac{\gamma_T^2}{c^2} \sin(2\alpha_0)$$



# Katz and Plotkin, Low speed

## Aerodynamics.

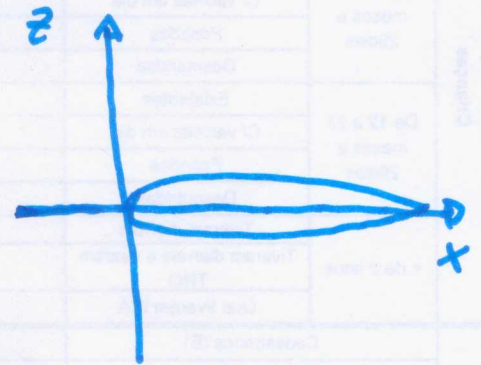
### Chapter 5

### Small disturbance Flow over 2-D airfoils.

wing upper and lower surfaces

$$z = \eta_u(x, y)$$

$$z = \eta_l(x, y)$$



thickness function:

$$\eta_T = \frac{1}{2}(\eta_u - \eta_l)$$

camber function:

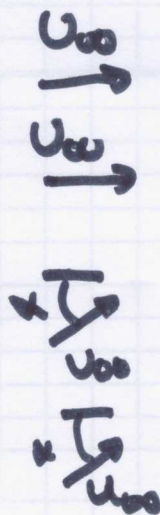
$$\eta_c = \frac{1}{2}(\eta_u + \eta_l)$$

$$\eta_u = \eta_c + \eta_T$$

$$\eta_l = \eta_c - \eta_T$$

Superimposing

solutions:



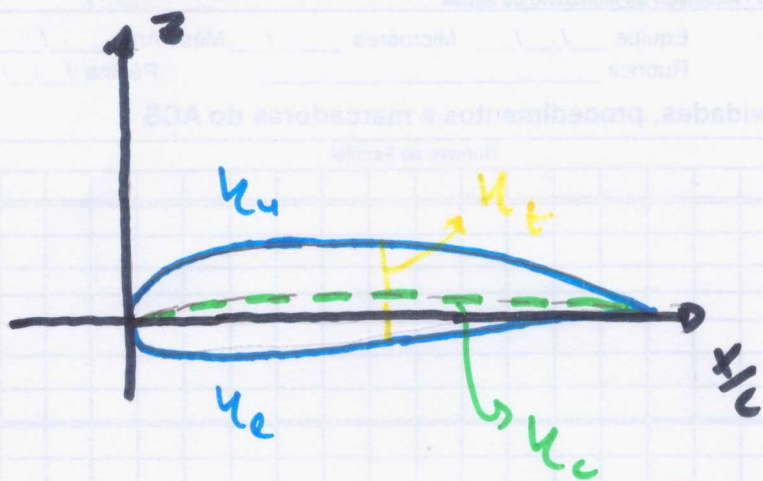
thickness  $\Phi_1$

camber  $\Phi_2$

flat plate at a.o.a.  $\alpha$   $\Phi_3$

$$\eta = \Phi_1 + \Phi_2 + \Phi_3$$

$$z = \eta(x, y) \Rightarrow F(x, y, z) = z - \eta(x, y) = 0 \quad (5)$$



outward normal

$$\hat{n} = \frac{\nabla F}{\|\nabla F\|}$$

$$\hat{n} = \frac{1}{\|\nabla F\|} \left( -\frac{\partial \eta}{\partial x}, -\frac{\partial \eta}{\partial y}, 1 \right)$$

upward surface

on the lower side, simply

$$\hat{n}_l = -\hat{n}$$

Velocity potential:

$$\Phi = W_\infty z + U_\infty x + \phi$$

Wall B.c.

$$F(x, y, z) = z - \eta(x, y) = 0$$

$$\nabla \Phi \cdot \hat{n} = \nabla \Phi \cdot \frac{\nabla F}{\|\nabla F\|} = 0$$

$$\frac{\partial \Phi}{\partial z} \cdot \frac{\partial \Phi}{\partial z} = \frac{\partial \eta}{\partial x} \left( U_\infty + \frac{\partial \Phi}{\partial x} \right) + \frac{\partial \eta}{\partial y} \frac{\partial \Phi}{\partial y} - W_\infty$$

$$\vec{Q}_\infty = (U_\infty, V_\infty, W_\infty), \quad \|\vec{Q}_\infty\| = Q_\infty$$

$$\frac{|\partial_x \phi|}{Q_\infty}, \frac{|\partial_y \phi|}{Q_\infty}, \frac{|\partial_z \phi|}{Q_\infty} \ll 1$$

Slender body hypothesis:  $|\partial_x \eta|, |\partial_y \eta| \ll 1$   
Fails at L.E.



$$V_{\infty} = 0$$

$$\left| \frac{W_{\infty}}{U_{\infty}} \right| = \tan \alpha = \alpha \ll 1 :$$

$$W_{\infty} \approx Q_{\infty} \alpha$$

$$U_{\infty} \approx Q_{\infty}$$

$$(\partial_x \psi)(\partial_x \Phi) \approx 0$$

$$(\partial_y \psi)(\partial_y \Phi) \approx 0$$

We are left with:

$$\left. \frac{\partial \Phi}{\partial z} \right|_{(x, y, \eta)} = Q_{\infty} \left( \frac{\partial \eta}{\partial x} - \alpha \right)$$

### Taylor Series expansion ( $|\eta| \ll 1$ )

$$\left. \frac{\partial \Phi}{\partial z} \right|_{(x, y, z=\eta)} = \frac{\partial \Phi}{\partial z}(x, y, 0) + \eta \frac{\partial^2 \Phi}{\partial z^2}(x, y, 0) + O(\eta^3)$$

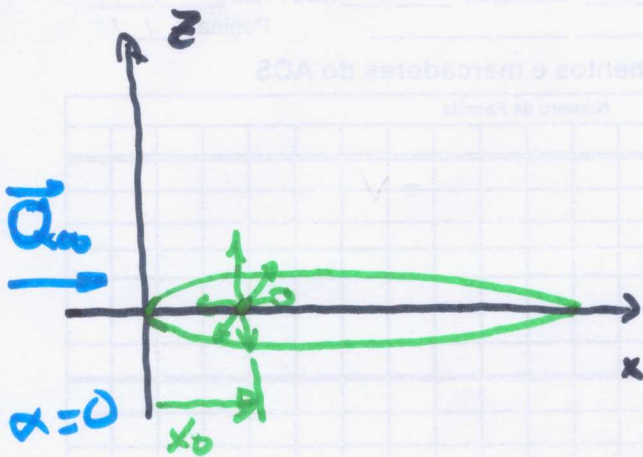
For very thin wings:  $|\eta| \ll 1$ , we

make:

$$\boxed{\frac{\partial \Phi}{\partial z}(x, y, 0) = Q_{\infty} \left( \frac{\partial \eta}{\partial x} - \alpha \right)}$$

(07/05/2020)

①



$$\nabla^2 \Phi = 0$$

$$w(x, 0^\pm) = \pm Q_\infty \frac{d\psi_t}{dx}$$

$$\Phi = \frac{\sigma_0}{2\pi} \ln(r), \quad r = \sqrt{(x-x_0)^2 + z^2} \Rightarrow \vec{q} \Rightarrow q_r = \frac{\sigma_0}{2\pi r}$$

Source/sink distribution:

$$\Phi(x, z) = \frac{1}{2\pi} \int_0^c \sigma(x_0) \ln[\sqrt{(x-x_0)^2 + z^2}] dx_0$$

$$u(x, z) = \frac{1}{2\pi} \int_0^c \sigma(x_0) \frac{(x-x_0)}{(x-x_0)^2 + z^2} dx_0$$

$$w(x, z) = \frac{1}{2\pi} \int_0^c \sigma(x_0) \frac{z}{(x-x_0)^2 + z^2} dx_0$$

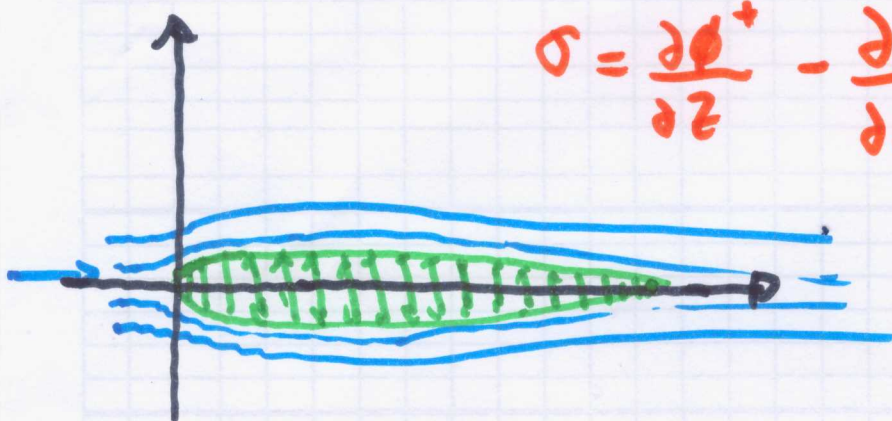
$$\lim_{z \rightarrow 0^+} \frac{1}{2\pi} \int_{x_{LE}}^{x_{TE}} \frac{\sigma(x_0) z dx_0}{(x-x_0)^2 + z^2} = \lim_{z \rightarrow 0^+} \frac{\sigma(x)}{2\pi} \int_{-\infty}^{\infty} \frac{z dx_0}{(x-x_0)^2 + z^2} = w(x)$$

$$\lambda \equiv (x - x_0)/z ; \quad d\lambda = -dx_0/z$$

$$W(x, 0^+) = \lim_{z \rightarrow 0^+} \frac{\Gamma(x)}{2\pi} \int_{-\infty}^{\infty} \frac{d\lambda}{1 + \lambda^2} = \frac{\Gamma(x)}{2\pi} \tan^{-1}(\lambda) \Big|_{-\infty}^{\infty}$$

$$W(x, 0^+) = \frac{\Gamma(x)}{2} \Rightarrow W(x, 0^+) = \frac{\partial \phi(x, 0^+)}{\partial z} = \pm \frac{\Gamma(x)}{2}$$

$$W^+ - W^- = \Gamma(x) \quad \text{for } x_{LE} \leq x \leq x_{TE} \quad \text{and } z \rightarrow 0^+$$



$$\sigma = \frac{\partial \phi^+}{\partial z} - \frac{\partial \phi^-}{\partial z}$$

$$\Gamma(x) = 2Q_{\infty} \frac{d\psi_t}{dx}$$

$$\phi(x, z) = \frac{Q_{\infty}}{\pi} \int_0^c \frac{d\psi_t(x_0)}{dx} \ln \left[ \sqrt{(x-x_0)^2 + z^2} \right] dx_0$$

$$\psi(x, z) = \frac{Q_{\infty}}{\pi} \int_0^c \frac{d\psi_t(x_0)}{dx} \frac{(x-x_0)}{(x-x_0)^2 + z^2} dx_0$$

$$W(x, z) = \frac{Q_{\infty}}{\pi} \int_0^c \frac{d\psi_t(x_0)}{dx} \frac{z}{(x-x_0)^2 + z^2} dx_0$$

$$C_p = -\frac{2u'}{U_\infty} = -\frac{2u'}{Q_{00}}$$

$$\boxed{\alpha = 0}$$

$$\vec{F} = - \int_0^c P \cdot \hat{n} ds$$

In the most general case, we'd have:  $F = z - y(x, y)$

$$\hat{n} = \frac{1}{\|\nabla F\|} \left( -\frac{\partial F}{\partial x}, -\frac{\partial F}{\partial y}, 1 \right)$$

Then we would scale  $F(x, y, z)$ , so as to make  $\|\nabla F\| = 1$  on  $F(x, y, z) = 0$

and that would lead to

$$F_x = \oint_w \left[ P_u \frac{\partial \psi_u}{\partial x} - P_e \frac{\partial \psi_e}{\partial x} \right] dx dy$$

$$F_y = \oint_w \left[ P_u \frac{\partial \psi_u}{\partial y} - P_e \frac{\partial \psi_e}{\partial y} \right] dx dy$$

$$F_z = \oint_w (P_e - P_u) dx dy$$

$$D = F_x \cos \alpha + F_z \sin \alpha \cong F_x + F_z \alpha$$

$$L = -F_x \sin \alpha + F_z \cos \alpha \cong F_z - F_x \alpha$$

$$C_p = - \frac{2U(x,0)}{Q_{\infty}}$$

$$C_p = - \frac{2}{\rho} \int_0^c \frac{d\eta_f(x_0)}{dx} \frac{1}{(x-x_0)} dx_0$$

$\alpha = 0$

$$L = F_z = \int_0^c (P_u - P_s) dx_0 = 0$$

$(C_{p_u} - C_{p_s}) = 0$  for  $\forall x \in [0, c]$   
owing to symmetry

Hence the symmetric thickness distribution does not contribute to Lift.

How about drag:

$$D = 2 \int_0^c P_u \frac{d\eta_f}{dx} dx = -2\rho \frac{Q_{\infty}^2}{\rho} \int_0^c \int_0^c \frac{\eta'_f(x_0) \eta'_f(x)}{(x-x_0)} dx_0 dx$$

$$\Delta = \int_0^c \eta'_f(x_0) \left[ \int_0^c \frac{\eta'_f(x)}{(x-x_0)} dx \right] dx_0 = - \int_0^c \eta'_f(x) \left[ \int_0^c \frac{\eta'_f(x_0)}{(x_0-x)} dx_0 \right] dx$$

$$\Delta = \int_0^c \eta'_f(x_0) I(x_0) dx_0 = - \int_0^c \eta'_f(x) I(x) dx$$

$$\Delta = 0$$

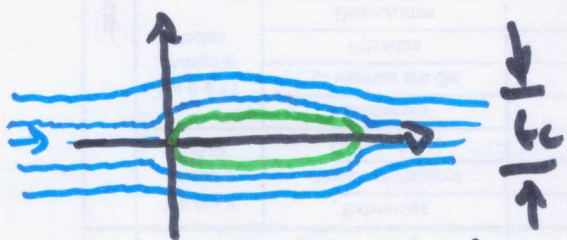
Therefore, the symmetric thickness distribution does not contribute to Lift, nor to Drag, neither does it contribute to the pitching moment, owing to its symmetry. (5)

Glauert Integral:

$$\int_0^\pi \frac{\cos(n\theta_0) d\theta_0}{\cos\theta_0 - \cos\theta} = \frac{\pi \sin(n\theta)}{\sin\theta}$$

$$n = 0, 1, 2, \dots$$

Flow past an ellipse at zero a.o.a. ( $\alpha = 0$ )



Max thickness:  $t_c$

$$x = \frac{c}{2}(1 - \cos\theta) \Rightarrow dx = \frac{c}{2} \sin\theta d\theta$$

$$\frac{x}{c} = \tilde{x} = \frac{1 - \cos\theta}{2} \Rightarrow d\tilde{x} = \frac{\sin\theta d\theta}{2}$$

$$\text{Contour of the ellipse: } \frac{(x - \frac{c}{2})^2}{(\frac{c}{2})^2} + \frac{y^2}{(\frac{t_c}{2})^2} = 1$$

$$\eta(x) = z$$

$$\eta = \pm t \sqrt{x(c-x)}$$

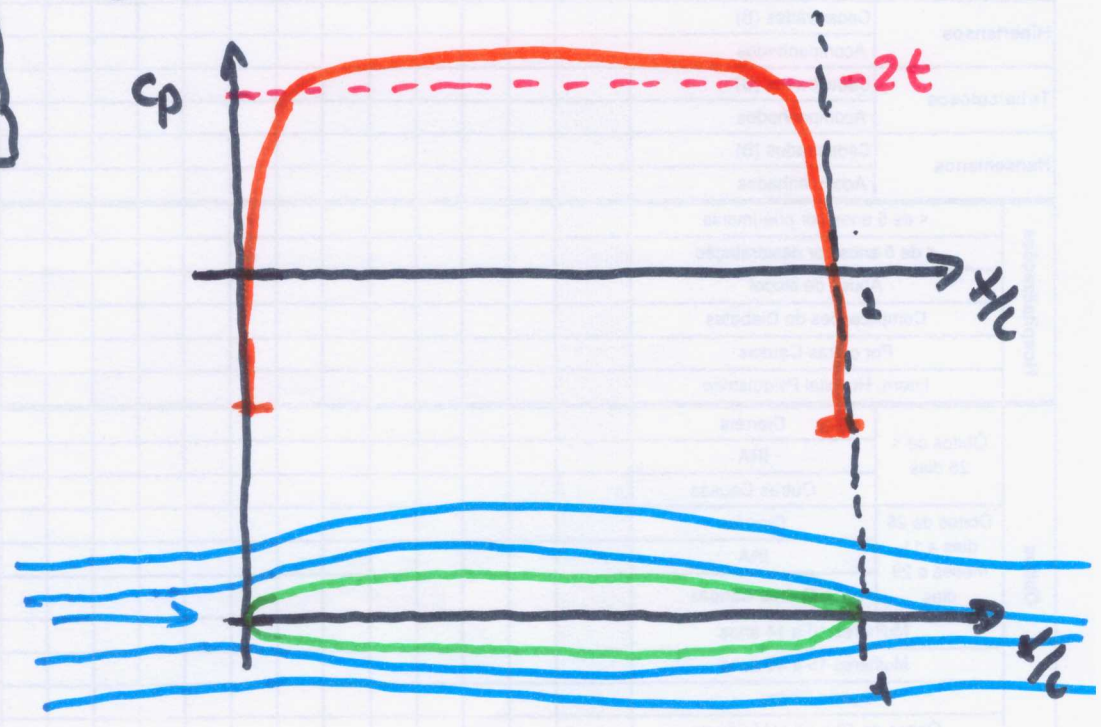
$$\frac{d\eta}{dx} = \pm \frac{t}{2} \frac{c-2x}{\sqrt{x(c-x)}}$$

then, and only then, we cast  $\frac{d\eta}{dx}$  in terms of  $\theta$  :

$$\frac{d\eta_{\pm}}{dx} = \frac{t}{2} \frac{c - c(1 - \cos\theta)}{\sqrt{\frac{c}{2}(1 - \cos\theta) \left[ c - \frac{c}{2}(1 - \cos\theta) \right]}} = t \frac{\cos\theta}{\sin\theta}$$

$$u(x,0) = \frac{t Q_{\infty}}{\pi} \int_0^{\pi} \frac{\cos\theta_0}{\cos\theta_0 - \cos\theta} d\theta_0 = t Q_{\infty}$$

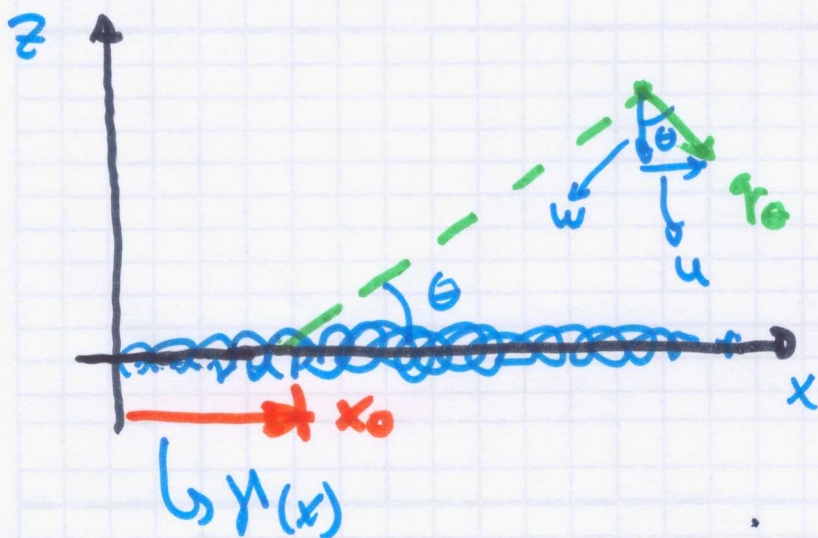
$$C_p = -2t$$



# The Lift Problem — zero thickness airfoil at an a.o.a ( $\alpha \neq 0$ )

(7)

$$\frac{\partial \phi}{\partial z}(x, 0^\pm) = Q_\infty \left( \frac{d\gamma_c}{dx} - \alpha \right)$$



$$\Phi_{h(x)} = -\frac{\gamma(x_0)}{2\pi} \theta$$

$$\Phi \Big|_{r(x_0)} = -\frac{\gamma(x_0)}{2\pi} \tan^{-1} \left( \frac{z}{x-x_0} \right)$$

$$q_\theta = -\frac{\gamma_0}{2\pi}, \quad q_r = 0$$

$$r = \sqrt{(x-x_0)^2 + z^2}$$

$$u = \frac{\partial \Phi}{\partial x} = \frac{\gamma_0}{2\pi} \frac{z}{(x-x_0)^2 + z^2}$$

$$w = \frac{\partial \Phi}{\partial z} = -\frac{\gamma_0}{2\pi} \frac{(x-x_0)}{(x-x_0)^2 + z^2}$$

$$\text{at } z=0 \Rightarrow w = -\frac{\gamma_0}{2\pi(x-x_0)}$$

$$\Phi(x, z) = -\frac{1}{2\pi} \int_0^c \gamma(x_0) \tan^{-1} \left( \frac{z}{x-x_0} \right) dx_0$$

$$u(x, z) = \frac{1}{2\pi} \int_0^c \gamma(x_0) \frac{z}{(x-x_0)^2 + z^2} dx_0 \quad \Bigg| \quad w(x, z) = -\frac{1}{2\pi} \int_0^c \gamma(x_0) \frac{(x-x_0)}{(x-x_0)^2 + z^2} dx_0$$



A function like:  $f(x) = \frac{z}{\pi [(x-x_0)^2 + z^2]}$

behaves as a Dirac delta in the limit

$$\lim_{z \rightarrow 0} \int_{-\infty}^{\infty} g(x) f(x, z) dx = \int_{-\infty}^{\infty} g(x) \delta(x-x_0) = g(x_0)$$

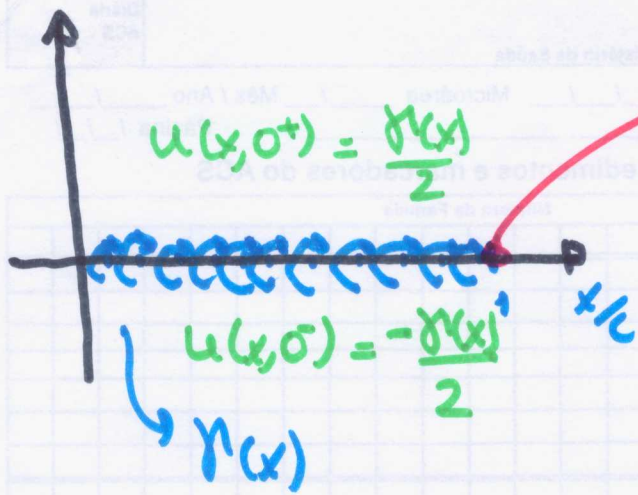
$$g(x) \in C_c^\infty$$

↳ infinitely differentiable with compact support ( $g \neq 0$  over a finite interval over the x axis)

$$u(x, 0^\pm) = \pm \lim_{z \rightarrow 0} \frac{1}{2\pi} \int_{-\infty}^{\infty} \delta(x_0) \frac{z}{(x-x_0)^2 + z^2} dx_0 = \pm \frac{\delta'(x) \pi}{2\pi}$$

$$u(x, 0^\pm) = \pm \frac{\delta'(x)}{2}$$

$$w(x, 0) = - \frac{1}{2\pi} \int_0^c \frac{\delta'(x_0) dx_0}{(x-x_0)}$$



9

T.E.  $\gamma\left(\frac{x}{c}=1\right) = 0$   
 Kutta condition

$$\frac{\partial \phi(x, 0)}{\partial z} = w(x, 0) = Q_{\infty} \left( \frac{d\psi_c}{dx} - \alpha \right)$$

$$-\frac{1}{2\pi} \int_0^c \gamma(x_0) \frac{dx_0}{(x-x_0)} = Q_{\infty} \left( \frac{d\psi_c}{dx} - \alpha \right)$$

$\forall x \mid 0 < x < c$

$$C_p = -\frac{2u'}{Q_{\infty}} \Rightarrow C_p = \mp \frac{\gamma}{Q_{\infty}} \Rightarrow \Delta C_p = \frac{2\gamma}{Q_{\infty}}$$

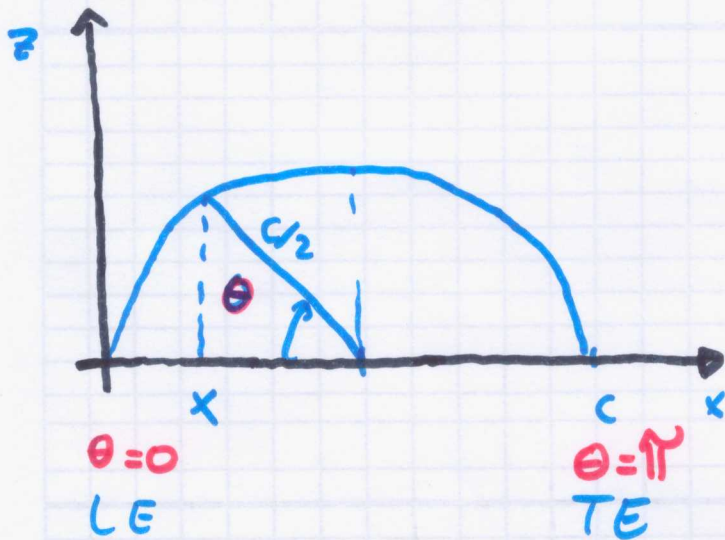
$$\Delta C_p \Big|_{T.E} = 0 \Rightarrow \gamma\left(\frac{x}{c}=1\right) = 0 \Rightarrow \underline{\underline{\text{Kutta}}}$$

14/05/2020

1

$$\Delta C_p = \frac{2\Gamma}{Q_\infty} \Rightarrow \Delta P = P_i - P_u = \rho Q_\infty \gamma(x)$$

$$L = \rho Q_\infty \Gamma \Leftarrow \Gamma \int_0^c \gamma(x) dx$$



$$x = \frac{c}{2} (1 - \cos\theta)$$

$$0 \leq \theta \leq \pi$$

$$dx = \frac{c}{2} \sin\theta d\theta$$

$$\theta = \cos^{-1} \left( 1 - 2\frac{x}{c} \right)$$

$$-\frac{1}{2\pi} \int_0^\pi \gamma(\theta_0) \frac{\sin\theta_0 d\theta_0}{(\cos\theta - \cos\theta_0)} = Q_\infty \left[ \frac{d\psi_c(\theta)}{dx} - \alpha \right]$$

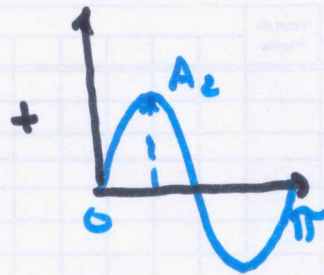
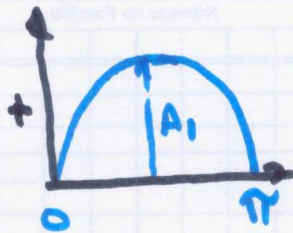
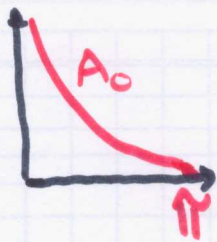
Kutta condition:  $\gamma(\pi) = 0$

$$\sum_{n=1}^{\infty} A_n \sin(n\theta)$$

We need an additional term to capture the leading edge suction peak.

$$A_0 \cot\left(\frac{\theta}{2}\right) = A_0 \frac{1 + \cos\theta}{\sin\theta}$$

$$f(\theta) = 2Q_{\infty} \left[ A_0 \frac{(1 + \cos\theta)}{\sin\theta} + \sum_{n=1}^{\infty} A_n \sin(n\theta) \right]$$



+ ...

$$-\frac{1}{2\pi} \int_0^{\pi} 2Q_{\infty} \left[ A_0 \frac{(1 + \cos\theta_0)}{\sin\theta_0} + \sum_{n=1}^{\infty} A_n \sin(n\theta_0) \right] \frac{\sin\theta_0 d\theta_0}{(\cos\theta_0 - \cos\theta)} =$$

$$= Q_{\infty} \left[ \frac{d\psi_c(\theta)}{dx} - \alpha \right]$$

Reminder of Glauert's integral:

$$\int_0^{\pi} \frac{\cos(n\theta_0) d\theta_0}{\cos\theta_0 - \cos\theta} = \frac{\pi \sin(n\theta)}{\sin\theta} ; n = 0, 1, 2, \dots$$

$$-\frac{1}{\pi} A_0 \int_0^{\pi} \frac{\cos(0\theta_0) + \cos\theta_0}{\cos\theta_0 - \cos\theta} d\theta_0 = -\frac{A_0}{\pi} (0 + \pi) = -A_0$$

$$\sin(n\theta_0) \sin\theta_0 = \frac{1}{2} [\cos[(n-1)\theta_0] - \cos[(n+1)\theta_0]]$$

$$n = 1, 2, 3 \dots$$

$$-\frac{1}{\pi} \int_0^{\pi} \frac{A_n \sin(n\theta_0) \sin\theta_0}{\cos\theta_0 - \cos\theta} d\theta_0 = -\frac{A_n}{2\pi} \int_0^{\pi} \frac{[\cos[(n-1)\theta_0] - \cos[(n+1)\theta_0]] d\theta_0}{\cos\theta_0 - \cos\theta}$$

$$-A_0 + \sum_{n=1}^{\infty} A_n \cos(n\theta) = \frac{d\psi_c(\theta)}{dx} - \alpha$$

$$A_0 = \alpha - \frac{1}{\pi} \int_0^{\pi} \frac{d\psi_c(\theta)}{dx} d\theta \quad ; \quad n=0$$

$$A_n = \frac{2}{\pi} \int_0^{\pi} \frac{d\psi_c(\theta)}{dx} \cos(n\theta) d\theta \quad ; \quad n=1, 2, 3, \dots$$

$$\psi(\theta) = 2Q_{\infty} \left[ \frac{A_0(1 + \cos\theta)}{\sin\theta} + \sum_{n=1}^{\infty} A_n \sin(n\theta) \right]$$

$$x = \frac{c}{2} (1 - \cos\theta) \quad , \quad \begin{cases} x=0 \Rightarrow \theta=0 \Rightarrow LE \\ x=c \Rightarrow \theta=\pi \Rightarrow TE \end{cases} \quad \left| \begin{array}{l} \text{Kutta} \\ \psi(\pi) = 0 \end{array} \right.$$

$$dx = \frac{c}{2} \sin\theta d\theta$$

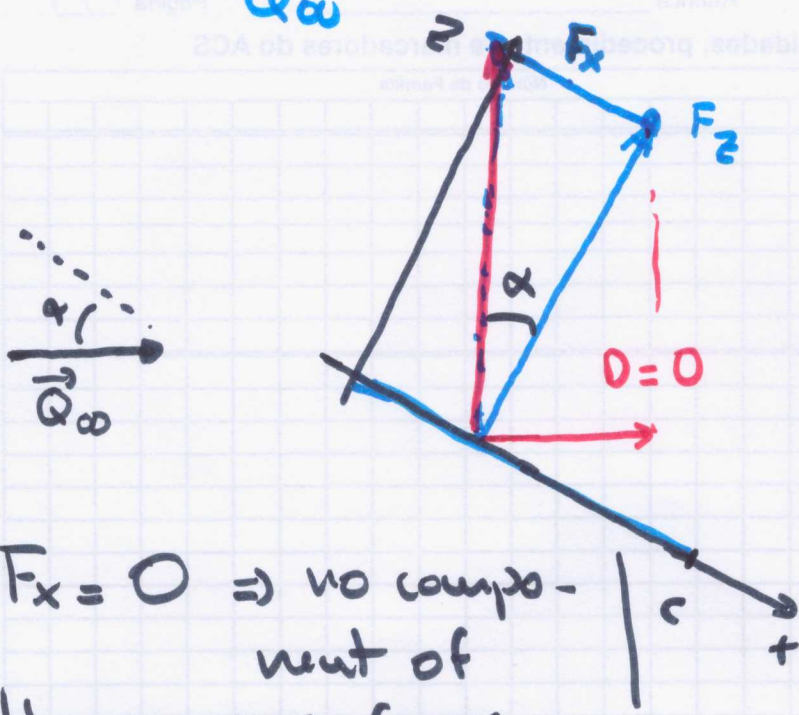
$$w(\theta) = Q_{\infty} \left( \frac{d\psi_c(\theta)}{dx} - \alpha \right) \Rightarrow \frac{w}{Q_{\infty}} = -A_0 + \sum_{n=1}^{\infty} A_n \cos(n\theta)$$

(downwash)

- 1)  $A_0$  is the only coefficient that depends on  $\alpha$
- 2)  $A_0$  gives a constant contribution to downwash.

$$\Delta C_p = \frac{2\gamma}{Q_\infty} \Rightarrow \Delta P(x) = \rho Q_\infty \gamma(x)$$

$$\alpha \ll 1$$



$$F_z = \int_0^c \Delta P(x) dx = \int_0^c \rho Q_\infty \gamma(x) dx$$

$$F_z = \rho Q_\infty \Gamma$$

$F_x = 0 \Rightarrow$  no component of the pressure forces (which act in the normal direction) along the chord.

$L \cos \alpha = F_z$

$$L = F_z = \rho Q_\infty \Gamma$$

As a result of this, we would get

$$D = F_z \sin \alpha \approx F_z \alpha \Rightarrow \text{Problem } \frac{D}{c}$$

From Kutta-Joukowski theorem, we expect

$$L = \rho Q_\infty \Gamma, \text{ but } D = 0$$

However, one can show that as the curvature radius of the L.E. goes to zero along with (local) thickness, the L.E. becomes a singularity with infinite acceleration of the flow.

Hence there appears a suction force there.

And this suction force amounts to exactly

$$F_{xLE} = -\rho Q_{\infty} \Gamma \alpha$$

therefore, the end result for the Net Drag becomes:

$$D = \rho Q_{\infty} \Gamma \alpha - \rho Q_{\infty} \Gamma \alpha = 0$$

So we get the expected result  $\begin{cases} L = \rho Q_{\infty} \Gamma \\ D = 0 \end{cases}$



### Forces and Moments.

$$\Gamma = \int_0^c \gamma(x) dx = \int_0^{\pi} \gamma(\theta) \frac{c}{2} \sin \theta d\theta$$

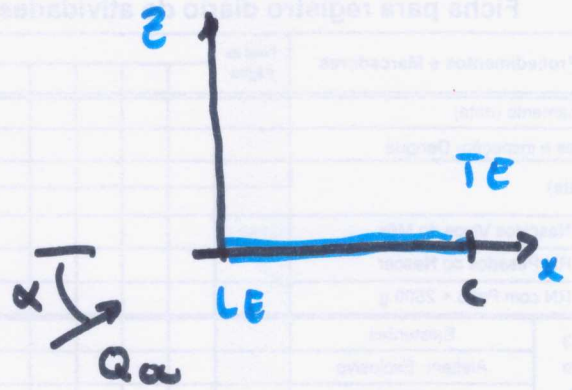
$$\Gamma = 2Q_{\infty} \int_0^{\pi} \left[ A_0 \frac{(1 + \cos \theta)}{\sin \theta} + \sum_{n=1}^{\infty} A_n \sin(n\theta) \right] \frac{c}{2} \sin \theta d\theta$$

$$\int_0^{\pi} (1 + \cos \theta) d\theta = \pi$$

$$\int_0^{\pi} \sin(n\theta) \sin(\theta) d\theta = \begin{cases} \pi/2 & n=1 \\ 0 & n \neq 1 \end{cases}$$

$$\Gamma = Q_\infty c \pi \left( A_0 + \frac{A_1}{2} \right) \Rightarrow L = \rho Q_\infty^2 c \pi \left( A_0 + \frac{A_1}{2} \right) \quad (6)$$

$$C_L = 2\pi \left( A_0 + \frac{A_1}{2} \right)$$



Pitching moment:

1) with respect to the L.E.  $\Rightarrow$  origin

$$M_0 = - \int_0^c \Delta P x dx = \rho Q_\infty \int_0^\pi \gamma(\theta) \frac{c^2}{4} (1 - \cos\theta) \sin\theta d\theta =$$

$$= -\rho Q_\infty \left[ \frac{c}{2} \int_0^\pi \gamma(\theta) \frac{c}{2} \sin\theta d\theta - \frac{c^2}{4} \int_0^\pi \gamma(\theta) \cos\theta \sin\theta d\theta \right]$$

$$M_0 = -\frac{c}{2} L + \frac{\rho Q_\infty^2 c^2}{2} \left\{ A_0 \int_0^\pi (1 + \cos\theta) \cos\theta d\theta + \right.$$

$$\left. + \sum_{n=1}^{\infty} \frac{A_n}{2} \int_0^\pi \sin(n\theta) \sin(2\theta) d\theta \right\}$$

Only  $n=2$  survives this integral.



$$M_o = -\frac{cL}{2} + \frac{\rho Q_{\infty}^2 c^2}{2} \left\{ A_o \left[ \cancel{(\sin \theta)_0}^{\pi} + \int_0^{\pi} \cos^2 \theta d\theta \right] + \frac{A_2 \pi}{4} \right\} \quad (7)$$

$$M_o = -\frac{cL}{2} + \frac{\rho Q_{\infty}^2 c^2}{2} \left( \frac{A_o \pi}{2} + \frac{A_2 \pi}{4} \right)$$

$$M_o = -\frac{cL}{2} + \frac{\rho Q_{\infty}^2 c^2}{4} (A_o \pi + A_2 \pi)$$

$$\cos^2 \theta = \frac{\cos(2\theta) + 1}{2} \Rightarrow \int_0^{\pi} \cos^2 \theta d\theta = \frac{\pi}{2}$$

$$M_o = -\rho Q_{\infty}^2 \frac{c^2}{4} \pi (A_o + A_1 - \frac{A_2}{2})$$

$$A_o = \alpha - \frac{1}{\pi} \int_0^{\pi} \frac{d\psi_c(\theta)}{dx} d\theta \quad ; \quad A_n = \frac{2}{\pi} \int_0^{\pi} \frac{d\psi_c(\theta)}{dx} \cos(n\theta) d\theta$$

$$C_L = 2\pi (A_o + \frac{A_1}{2}) \Rightarrow C_L = 2\pi \left( \alpha - \frac{1}{2} \int_0^{\pi} \frac{d\psi_c(\theta)}{dx} d\theta + \frac{A_1}{2} \right)$$

↑  
A.A.A. Camber contribution  
(independent of  $\alpha$ )

$$C_{L0} = 2\pi (\alpha - \alpha_{L0})$$

$$\alpha_{L0} = -\frac{1}{\pi} \int_0^{\pi} \frac{d\psi_c(\theta)}{dx} (\cos \theta - 1) d\theta$$

$$C_{L\alpha} = \frac{dC_L}{d\alpha} = 2\pi$$

$$C_L = 2\pi(\alpha - \alpha_{0w})$$

$$C_L = 2\pi \left( A_0 + \frac{A_1}{2} \right)$$

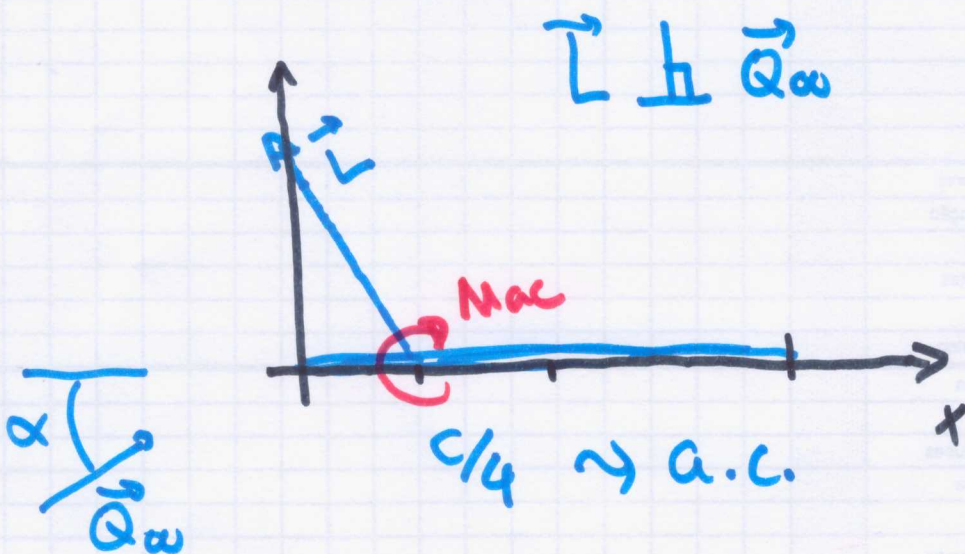
$$C_{M0} = \frac{M_0}{\frac{\rho Q_{\infty}^2}{2} c^2} = -\frac{\pi}{2} \left( A_0 + A_1 - \frac{A_2}{2} \right)$$

$$C_{M0} = -\frac{C_L}{4} + \frac{\pi}{4} (A_2 - A_1)$$

$C_{M_{c/4}}$

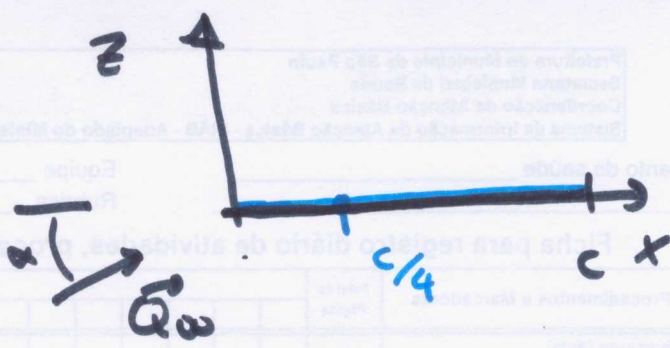
$$C_{M_{c/4}} = C_{Mac} = \frac{\pi}{4} (A_2 - A_1)$$

Pitching moment  
 sign convention  
 nose up  $\Rightarrow \oplus$   
 nose down  $\Rightarrow \ominus$



# Flat plate

$\alpha \neq 0$



$\psi_c(x) = 0 \quad \forall x \mid 0 \leq x \leq c$

$\frac{d\psi_c}{dx} = 0 \quad A_0 = \alpha$

$A_n = 0 \quad \forall n$

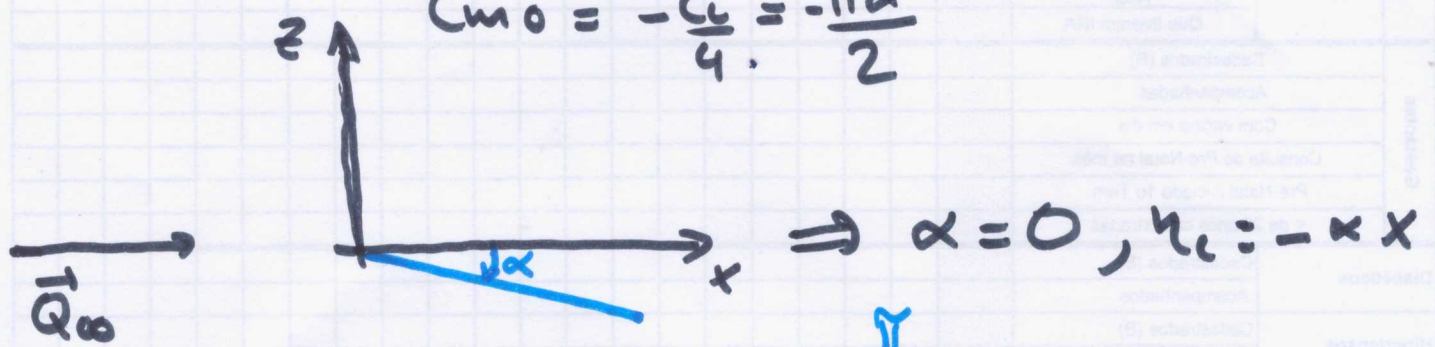
$A_0 = \alpha - \frac{1}{\pi} \int_0^\pi \frac{d\psi_c(\theta)}{dx} d\theta$

$A_n = \frac{2}{\pi} \int_0^\pi \frac{d\psi_c(\theta)}{dx} \cos(n\theta) d\theta$

$\Gamma = Q_\infty \pi c \alpha \quad C_L = 2\pi \alpha$

$C_{m,c} = 0$

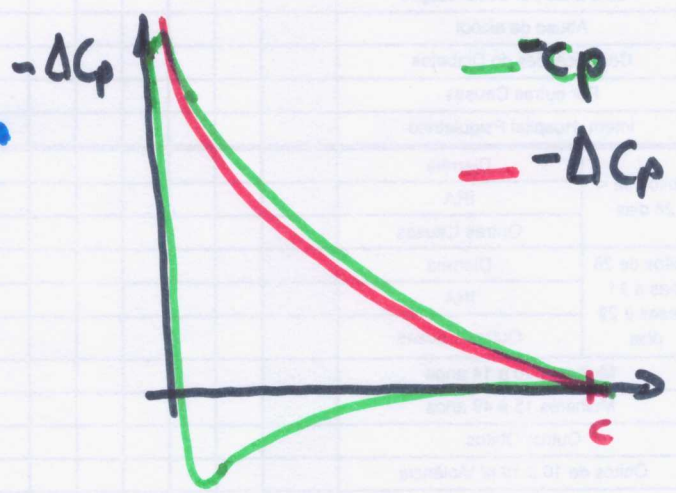
$C_{m,0} = -\frac{C_L}{4} = -\frac{\pi \alpha}{2}$



$\frac{d\psi_c}{dx} = -\alpha$

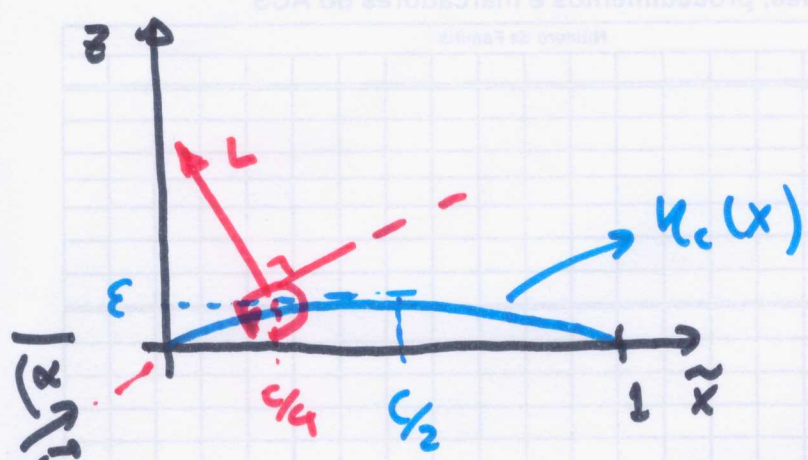
$A_0 = \alpha - \frac{1}{\pi} \int_0^\pi (-\alpha) d\theta = +\alpha$

$\Delta C_p = \frac{2\pi}{Q_\infty} = 4\alpha \frac{(1 + \cos\theta)}{\sin\theta \cot(\theta)}$



$$\eta_c(x) = 4\epsilon \frac{x}{c} \left[ 1 - \frac{x}{c} \right] = 4\epsilon \tilde{x}(1 - \tilde{x})$$

$(\epsilon \ll 1)$



$$\frac{d\eta_c}{dx} = 4\frac{\epsilon}{c} \left[ 1 - 2\frac{x}{c} \right]$$

$$\frac{d\eta_c(\theta)}{dx} = \frac{4\epsilon}{c} \cos\theta$$

$$\left. \begin{aligned} x &= \frac{c}{2} (1 - \cos\theta) \\ dx &= \frac{c}{2} \sin\theta d\theta \end{aligned} \right\}$$

$$A_0 = \alpha - \frac{1}{\pi} \int_0^\pi \frac{4\epsilon}{c} \cos\theta d\theta$$

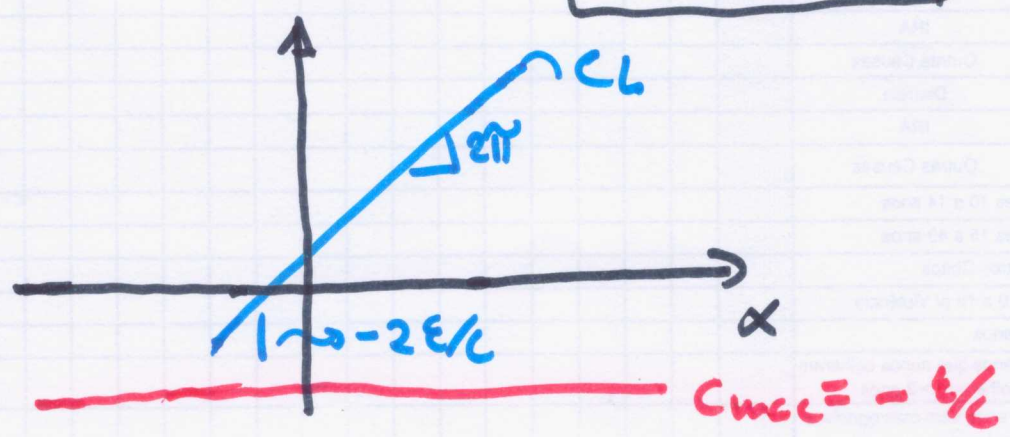
$$A_0 = \alpha$$

$$A_n = \frac{2}{\pi} \int_0^\pi \frac{4\epsilon}{c} \cos\theta (\cos(n\theta)) d\theta$$

$$A_1 = \frac{4\epsilon}{c}, \quad A_2 = A_3 = \dots = 0$$

$$C_L = 2\pi \left( \alpha + 2\frac{\epsilon}{c} \right) \Rightarrow \boxed{\alpha_{L0} = -\frac{2\epsilon}{c}}$$

$$C_{mac} = -\frac{\pi}{4} \frac{4\epsilon}{c} \Rightarrow \boxed{C_{mac} = -\frac{\epsilon}{c}}$$



28/05/2020

①

$$f(\theta) = 2Q_{\infty} \left[ A_0 \frac{1 + \cos\theta}{\sin\theta} + \sum_{n=1}^{\infty} A_n \sin(n\theta) \right]$$

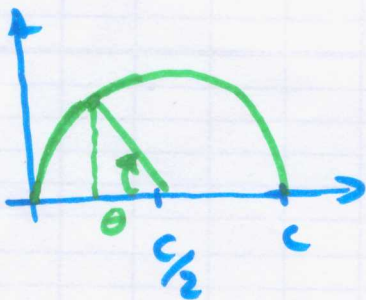
Kutta condition:  $f(\theta) \Big|_{\theta=\pi} = f(x) \Big|_{x=c} = 0$  (T.E.)

Glauert's Integral:  $\int_0^{\pi} \frac{\cos(n\theta_0) d\theta_0}{\cos\theta_0 - \cos\theta} = \frac{\pi \sin(n\theta)}{\sin\theta}$   
 $n = 0, 1, 2, \dots$

$$A_0 = \alpha - \frac{1}{\pi} \int_0^{\pi} \frac{d\psi_c(\theta)}{dx} d\theta \quad \left. \begin{array}{l} C_L = 2\pi(A_0 - A_{1/2}) \\ C_U = 2\pi(\alpha - \alpha_{L0}) \\ C_{mac} = \frac{\pi}{4}(A_2 - A_1) \end{array} \right\}$$

$$A_n = \frac{2}{\pi} \int_0^{\pi} \frac{d\psi_c(\theta)}{dx} \cos(n\theta) d\theta$$

$$x_{mac} = \frac{c}{4}, \quad \alpha_{L0} = -\frac{1}{\pi} \int_0^{\pi} \frac{d\psi_c(\theta)}{dx} [\cos\theta - 1] d\theta$$



$$x = \frac{c}{2} (1 - \cos\theta)$$

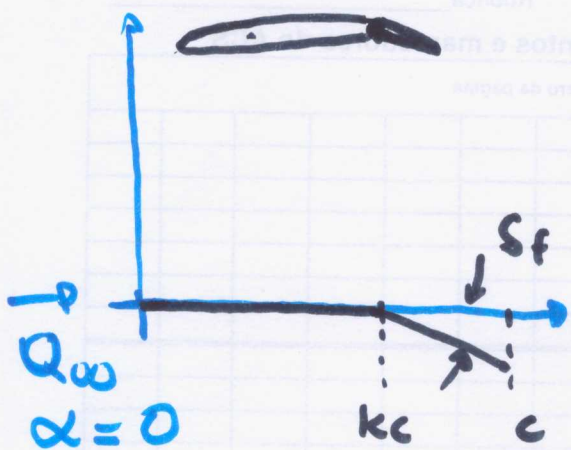
$$dx = \frac{c}{2} \sin\theta d\theta$$

$$0 \leq \theta \leq \pi$$

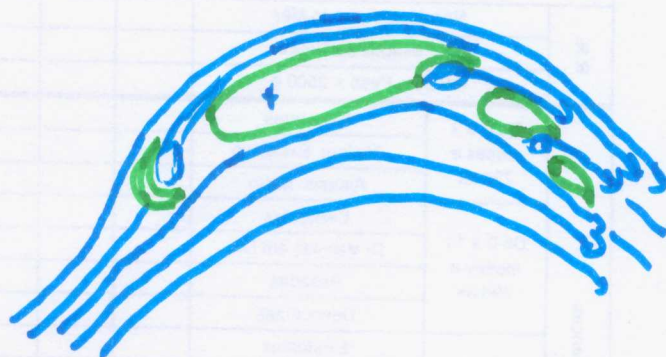
↑  
LE

↑  
TE

# Flapped Airfoil

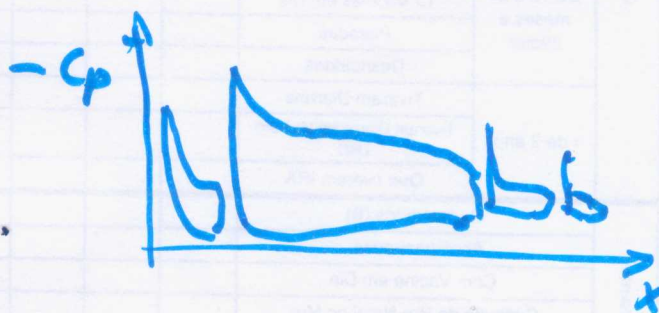


Not the same thing as Hyperlifting devices:



$$\delta_f \ll c$$

$$\alpha_{L0} = -\frac{1}{\pi} \int_0^\pi \frac{d\eta_c}{dx} (\cos\theta - 1) d\theta$$



Flap affects camber  $\eta_c$ :

the factor  $(\cos\theta - 1)$  is larger at  $\theta \approx \pi$  than it would be at  $\theta \approx 0$

$$\frac{d\eta_c}{dx} = 0 \quad \text{for} \quad 0 \leq x < k_c \quad \left| \begin{array}{l} k \in \mathbb{R} \\ 0 < k < 1 \end{array} \right.$$

$$\frac{d\eta_c}{dx} = -\delta_f \quad \text{for} \quad k_c < x \leq c$$

$$\theta_k \Rightarrow x = k_c = \frac{c}{2} (1 - \cos\theta_k)$$

$$1 - 2k = \cos\theta_k$$

$$\frac{dV_c(\theta)}{dx} = 0 \text{ for } 0 \leq \theta < \theta_k$$

$$\alpha_{L0} = -\frac{1}{\pi} \int_0^{\pi} \frac{dV_c(\theta)}{dx} (\cos\theta - 1) d\theta$$

$$= -\frac{\delta_f}{\pi} \int_0^{\pi} [\cos(\theta) - 1] d\theta = -\frac{\delta_f}{\pi} [\sin\theta - \theta]_0^{\pi}$$

$$\alpha_{L0} = \frac{\delta_f}{\pi} \left\{ \sin\theta_k + (\pi - \theta_k) \right\} \quad | \quad \theta_k \rightarrow \text{rad.}$$

On substituting the above result for its counterpart in the expressions for  $C_L$  and  $C_{mac}$ , we get:

$$\frac{dC_L}{d\delta_f} = [2(\pi - \theta_k) + 2\sin(\theta_k)] \Rightarrow \Delta C_L = \frac{dC_L}{d\delta_f} \delta_f$$

$$\frac{dC_{mac}}{d\delta_f} = \left[ \frac{\sin(2\theta_k)}{4} - \frac{\sin(\theta_k)}{2} \right] \Rightarrow \Delta C_{mac} = \frac{dC_{mac}}{d\delta_f} \delta_f$$

$$\frac{d\alpha_{L0}}{d\delta_f} = \frac{1}{\pi} [\sin(\theta_k) + (\pi - \theta_k)] \Rightarrow \Delta \alpha_{L0} = \frac{d\alpha_{L0}}{d\delta_f} \delta_f$$

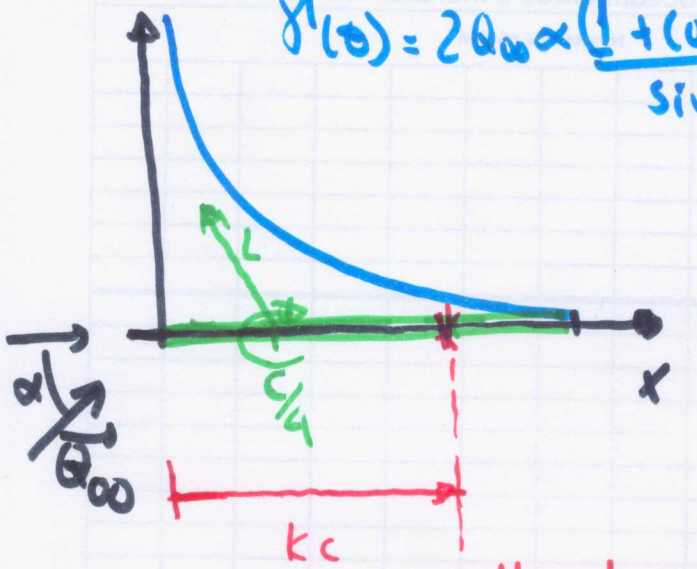
# Lumped - vortex element

$$\gamma(\theta) = 2Q_{\infty} \alpha \frac{(1 + \cos\theta)}{\sin\theta}$$

$$\Gamma = 2Q_{\infty} \alpha \int_0^{\pi} \frac{(1 + \cos\theta)}{\sin\theta} c \sin\theta d\theta$$

$$\Gamma = \pi c Q_{\infty} \alpha$$

$$w(x,0) = \frac{\gamma}{2\pi(x-x_0)} ; x \neq x_0$$



collocation point.

Now, for our lumped vortex,  $\gamma_0 = \Gamma$  and it sits at  $x = c/4$

To find out  $k_c$ , i.e. the point where tangency is met, we make:

$$w(k_c, 0) = \frac{-\Gamma}{2\pi c (k - 1/4)} = Q_{\infty} \left[ \frac{d\gamma}{dx} - \alpha \right]$$

$$\frac{-\Gamma}{2\pi c (k - 1/4)} = -Q_{\infty} \alpha ; \Gamma = \pi c Q_{\infty} \alpha$$

$$k = \frac{3}{4} \Rightarrow$$

$$k_c = x = \frac{3c}{4}$$

Collocation Point



# Generalized Kutta - Joukowski theorem

(Katz and Plotkin → P. 146-150)

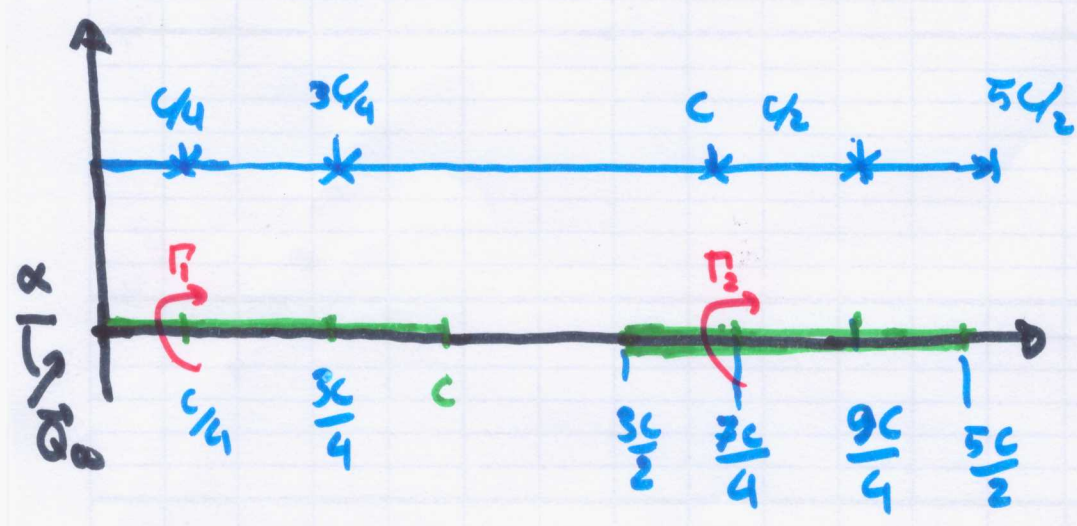
$$\text{Blazius: } x - iz = \frac{i\Gamma}{2c} \oint_C W^2 dz$$

$$L = \rho Q_{\infty} \Gamma \left( 1 + \frac{\vec{Q}_{\infty} \cdot \vec{q}_e}{Q_{\infty}^2} \right)$$

circulation of the vortex for which you are computing L

where  $\vec{q}_e$  is the velocity "induced" by other vortices at the airfoil vortex location

## Tandem Airfoils



on assuming that  $\alpha \ll 1$  the streamwise contribution "u" each vortex induces on the other is neglected. We are left with the vertical contribution only.

$$\omega_{1 \rightarrow 2} = -\frac{\Gamma_1}{2\pi c \left( \frac{3}{4} - \frac{1}{4} \right)} = -\frac{\Gamma_1}{3\pi c}$$

$$\omega_{2 \rightarrow 1} = -\frac{\Gamma_2}{2\pi c \left( \frac{1}{4} - \frac{3}{2} \right)} = +\frac{\Gamma_2}{3\pi c}$$

$$L_1 = \rho Q_{\infty} \Gamma_1 \left( 1 + \frac{\alpha \Gamma_2}{3\pi c} \right)$$

$$L_2 = \rho Q_{\infty} \Gamma_2 \left( 1 - \frac{\alpha \Gamma_1}{3\pi c Q_{\infty}} \right)$$

$$\vec{\omega} \cdot \vec{Q}_{\infty} = \omega Q_{\infty} \cos \alpha = \omega Q_{\infty} \alpha$$

tangency condition:

$$W = Q_{\infty} \left[ \frac{dV_c}{dx} - \alpha \right]$$

(Nett)

$$W_1 = -\frac{\Gamma_1}{2\pi(c/2)} + \frac{\Gamma_2}{2\pi c} + Q_{\infty} \alpha = 0$$

$$W_2 = -\frac{\Gamma_1}{2\pi 2c} + \frac{-\Gamma_2}{2\pi(c/2)} + Q_{\infty} \alpha = 0$$

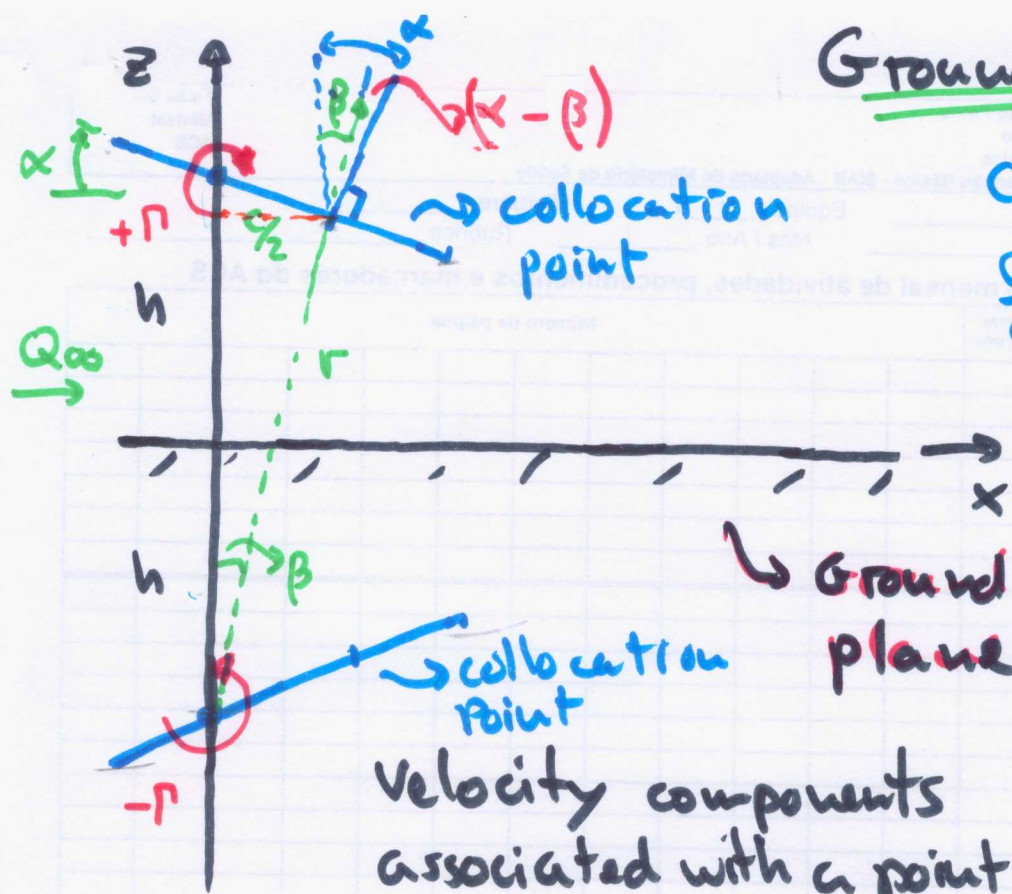
$$\Gamma_1 = \frac{4}{3} \pi c Q_{\infty} \alpha \quad ; \quad \Gamma_2 = \frac{2}{3} \pi c Q_{\infty} \alpha$$

$$C_{D1} = \frac{8\pi\alpha}{3} \left( 1 + \frac{2\alpha^2}{9} \right)$$

$$C_{D2} = \frac{4\pi\alpha}{3} \left( 1 - \frac{4\alpha^2}{9} \right)$$

# Ground Effect

(7)



Cosine Law

$$\frac{c^2}{4} = 4h^2 + r^2 - 2(2hr \cos \beta)$$

$$r \cos \beta = 2h - \frac{c}{2} \sin \alpha$$

Hence, we get:

$$r^2 = \frac{c^2}{4} + 4h^2 - 2hc \sin \alpha$$

Velocity components associated with a point vortex:

$$\begin{cases} u = \frac{\Gamma}{2\pi} \frac{(z-z_0)}{(z-z_0)^2 + (x-x_0)^2} \\ w = -\frac{\Gamma}{2\pi} \frac{(x-x_0)}{(z-z_0)^2 + (x-x_0)^2} \end{cases}$$

normal unit vector:  $\hat{n} = (\sin \alpha, \cos \alpha)^T \cong (x, 1)^T$

upper collocation point:  $x = \frac{c}{2} \cos \alpha, z = -\frac{c}{2} \sin \alpha$

"Induced" velocities:

at upper vortex:

$$\vec{q}_1 = \begin{pmatrix} -\frac{2\pi \cdot 2h}{(2h)^2} \\ +\frac{\Gamma}{2\pi} \frac{0}{(2h)^2} \end{pmatrix} = \begin{pmatrix} -\frac{\Gamma}{4\pi h} \\ 0 \end{pmatrix}$$

at upper collocation point

$$\vec{q}_{1c} = \frac{-\Gamma}{2\pi} \begin{pmatrix} \frac{2h - c \sin \alpha / 2}{r^2} \\ \frac{c \cos \alpha / 2}{r^2} \end{pmatrix}$$

$$r = \sqrt{4h^2 + \frac{c^2}{4} - 2ac \sin \alpha}$$

$$\|\vec{q}_{1c}\| = \frac{\Gamma}{2\pi r} ; \vec{q}_{1c} \cdot \hat{n} = \frac{\Gamma}{2\pi r} \cos(\beta - \alpha + \frac{\pi}{2})$$

(8)

$$\vec{q}_{1c} \cdot \hat{n} = -\frac{\Gamma}{2\pi r} \sin(\beta - \alpha) \rightsquigarrow \text{velocity that is induced by the lower vortex on the upper collocation point}$$

Velocity induced by the upper vortex on the upper collocation point is given by:

$$\vec{q}_{1c1} = -\Gamma/2\pi(c/2) = -\frac{\Gamma}{\pi c} \text{ to the plate.}$$

Tangency condition implies:

$$-\frac{\Gamma}{\pi c} + \vec{q}_{1c} \cdot \hat{n} + Q_{\infty} \alpha = 0$$

$$-\frac{\Gamma}{\pi c} - \frac{\Gamma}{2\pi r} \sin(\beta - \alpha) + Q_{\infty} \alpha = 0$$

$$\Gamma = \pi Q_{\infty} c \sin \alpha \left[ \frac{1 - (c/2h) \sin \alpha + (c^2/16h^2)}{1 - (c/4h) \sin \alpha} \right]$$

$$L = \beta Q_{\omega} \Gamma \left( 1 - \frac{\bar{Q}_{\omega} \cdot \vec{q}_c}{Q_{\omega}^2} \right)$$

$$L = \beta Q_{\omega} \Gamma \left( 1 - \frac{\Gamma}{4\pi Q_{\omega} h} \right)$$

Grand effect

on substituting the above result for  $\Gamma$ ,  
 and on taking it to the limit as  $c/h \rightarrow 0$ ,  
 we get

$$L = \pi \beta Q_{\omega}^2 c \sin \alpha \left[ 1 - \frac{c}{2h} \sin \alpha + \frac{c^2}{16h^2} (1 + \sin^2 \alpha) + \frac{O(c^3)}{h^3} \right]$$

04/06/2020

①

P.4.6 and P.4.7 (P. 222) Anderson's book :  
Fundamentals of Aerodynamics

NACA 4012

$$\tilde{\eta}_c \begin{cases} = 0.25(0.8\tilde{x} - \tilde{x}^2) & \text{for } 0 \leq \tilde{x} \leq 0.4 \\ = 0.111(0.2 + 0.8\tilde{x} - \tilde{x}^2) & \text{for } 0.4 \leq \tilde{x} \leq 1 \end{cases}$$

where  $\tilde{x} = x/c$  and  $\tilde{\eta}_c = \eta/c$

$$\tilde{x} = \frac{1 - \cos\theta}{2} ; d\tilde{x} = \frac{\sin\theta d\theta}{2} ; \begin{cases} \tilde{x} = 0 \Rightarrow \theta = 0 \\ \tilde{x} = 1 \Rightarrow \theta = \pi \end{cases}$$

$$A_0 = \alpha - \frac{1}{\pi} \int_0^\pi \eta'_c(\theta) d\theta \Rightarrow \alpha + \alpha_{L0}$$

$\underbrace{\hspace{10em}}_{+\alpha_{L0}}$

$$A_u = \frac{2}{\pi} \int_0^\pi \eta'_c(\theta) \cos(n\theta) d\theta \quad \left| \begin{array}{l} C_L = 2\pi(\alpha - \alpha_{L0}) \\ C_{mac} = \frac{\pi}{4}(A_2 - A_1) \\ \tilde{x}_{ac} = 1/4 \end{array} \right.$$

$$\eta'_c = \begin{cases} 0.25(0.8 - 2\tilde{x}) \Rightarrow 0.25(\cos\theta - 0.2) & 0 \leq \theta \leq \theta_s \\ 0.111(0.8 - 2\tilde{x}) \Rightarrow 0.111(\cos\theta - 0.2) & \theta_s \leq \theta \leq \pi \end{cases}$$

$$\cos(\theta_s) = 0.2 \Rightarrow \theta_s = 1.3694 \text{ rad}$$

$$I_0 = \int_a^b u'_i(\theta) d\theta = \int [\cos\theta - 0.2] d\theta = [\sin\theta]_a^b - [\theta]_a^b \quad (2)$$

$$I_1 = \int_a^b u'_i(\theta) \cos\theta d\theta = \int (\cos^2\theta - 0.2 \cos\theta) d\theta =$$

$$= \frac{1}{2} [\theta]_a^b + \frac{1}{4} [\sin(2\theta)]_a^b - \frac{2}{10} [\sin\theta]_a^b$$

$$I_2 = \int_a^b u'_i(\theta) \cos(2\theta) d\theta = \int (\cos\theta - 0.2) \cos(2\theta) d\theta =$$

$$= \frac{1}{6} [\sin(3\theta)]_a^b - 0.1 [\sin(2\theta)]_a^b + \frac{1}{2} [\sin(\theta)]_a^b$$

$$\alpha_{L0} = -\frac{1}{\pi} \left\{ 0.25 [I_1 - I_0]_{\theta_s}^{\theta_s} + 0.111 [I_1 - I_0]_{\theta_s}^{\pi} \right\}$$

$$\alpha_{L0} \cong -0.0724274 \text{ rd} \cong -4.15^\circ$$

$$C_2 = 2\pi (\alpha - \alpha_{L0}) \cong 2\pi (\alpha + 0.0724)$$

$$C_2 \Big|_{\alpha=3^\circ} = 0.784061$$

$$A_1 = \frac{2}{\pi} \left\{ 0.25 [I_1]_{\theta_s}^{\theta_s} + 0.111 [I_1]_{\theta_s}^{\pi} \right\} \cong 0.162921$$

$$A_2 = \frac{2}{\pi} \left\{ 0.25 [I_2]_{\theta_s}^{\theta_s} + 0.111 [I_2]_{\theta_s}^{\pi} \right\} \cong 0.0277447$$

$$C_{mac} \cong -0.106167$$

Circulation:

$$\Gamma \equiv \oint_C \vec{u} \cdot d\vec{\ell} = \iint_{S_C} (\nabla \times \vec{u}) \cdot \hat{n} \, dS = \iint_{S_C} \vec{\omega} \cdot \hat{n} \, dS$$

Stokes Theorem



$$\frac{D\vec{\omega}}{Dt} = \underbrace{\vec{\omega} \cdot \nabla \vec{u} - \vec{\omega} \nabla \cdot \vec{u}}_{\substack{\text{vorticity} \\ \text{distribution} \\ \text{remains}}} + \underbrace{\nabla T \times \nabla S - \frac{\nabla \rho}{\rho^2} \times \nabla Z + \nabla \times (\nabla \cdot \vec{z})}_{\substack{\text{sources have been} \\ \text{removed.}}}$$

Kelving-Helmholtz's Theorem.

$$\frac{D\Gamma}{Dt} = \oint_C \frac{D\vec{u}}{Dt} \cdot d\vec{\ell} = \oint_C \vec{f} \cdot d\vec{\ell} \Rightarrow \frac{D\Gamma}{Dt} = \oint_C \vec{g} \cdot d\vec{\ell} - \oint_C \frac{\nabla \rho}{\rho} \cdot d\vec{\ell} =$$

Therefore, we get:

$$\frac{D\Gamma}{Dt} = 0$$

Stokes Theorem implies these two integrals vanish. their kernels are irrotational.

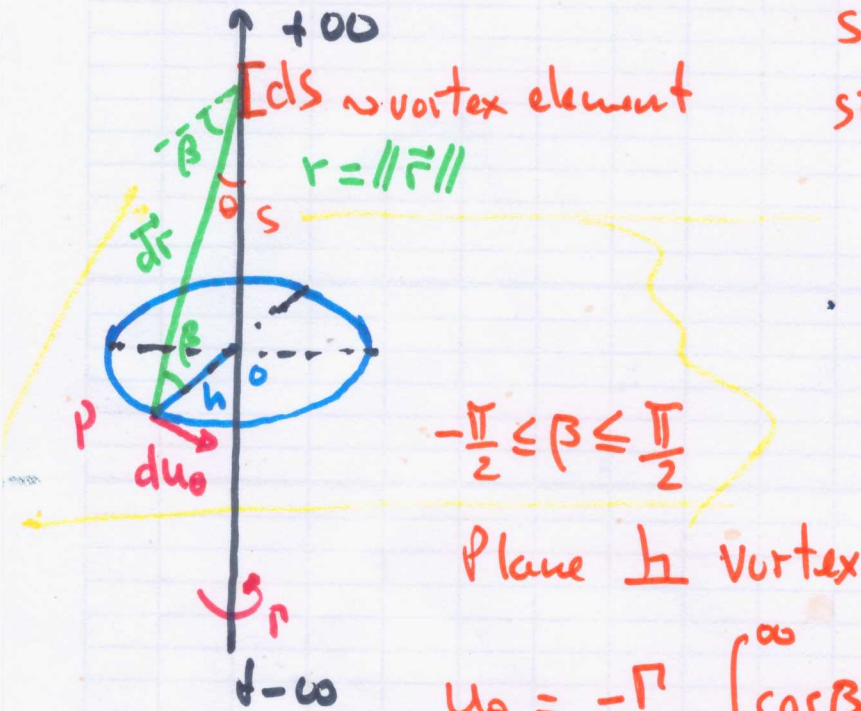


Reference:

Kuethe A.M. and Chow, C.Y. "Foundations of Aerodynamics Design". NY, J. Wiley, 1998  
5<sup>th</sup> ed.

Chapter 6

straight vortex



$$\frac{h}{s} = \tan \theta \Rightarrow ds = -\frac{h d\theta}{\sin^2 \theta}$$

$$\sin \theta = \frac{h}{r} \Rightarrow r = \frac{h}{\sin \theta}$$

$$\beta + \theta = \frac{\pi}{2} \Rightarrow \cos \beta = \sin \theta$$

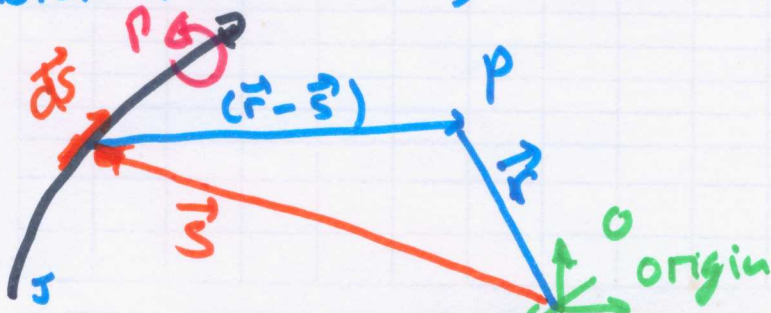
$$du_\theta = -\frac{\Gamma}{4\pi} \frac{\cos \beta ds}{r^2}$$

Plane  $h$  vortex

$$u_\theta = -\frac{\Gamma}{4\pi} \int_{-\infty}^{\infty} \frac{\cos \beta ds}{r^2} = -\frac{\Gamma}{4\pi} \int_{-\infty}^{\infty} \frac{\sin \theta ds}{r^2}$$

$$u_\theta = \frac{\Gamma}{4\pi} \int_0^\pi \frac{h \sin^3(\theta) d\theta}{h^2 \sin^2(\theta)} = \frac{\Gamma}{4\pi h} \int_0^\pi \sin \theta d\theta \Rightarrow \boxed{u_\theta = \frac{\Gamma}{2\pi h}}$$

Biot-Savart Law, General form:

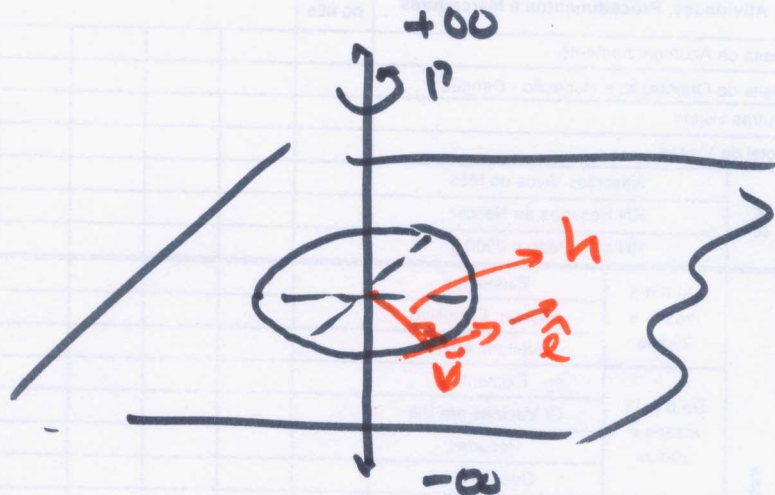


$$\vec{v}(\vec{r}) = \frac{\Gamma}{4\pi} \int \frac{d\vec{s} \times (\vec{r} - \vec{s})}{\|\vec{r} - \vec{s}\|^3}$$

infinite vortex filament: (straight)

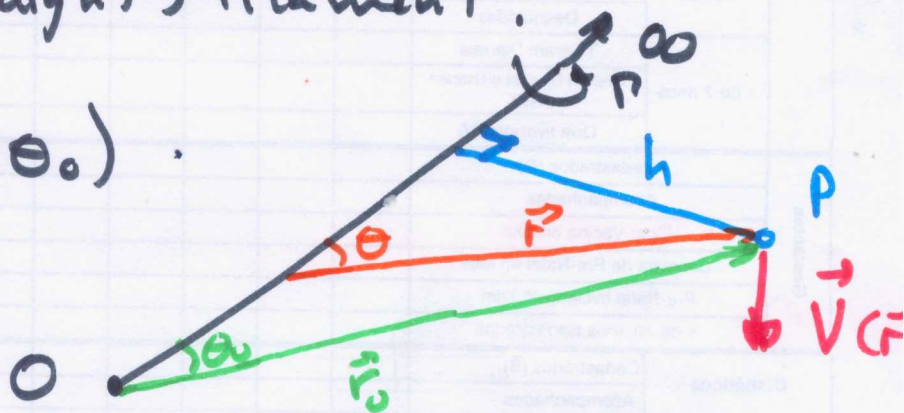
(5)

$$\vec{V}(\vec{r}) = \frac{\Gamma}{2\pi h} \hat{z} \quad \text{where the axis } \hat{z}$$



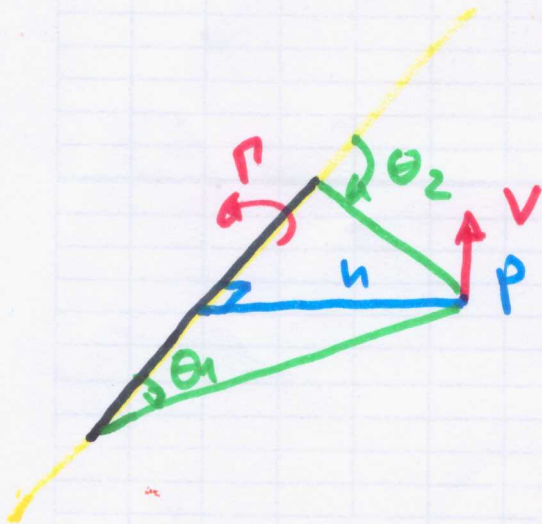
semi-infinite (straight) filament:

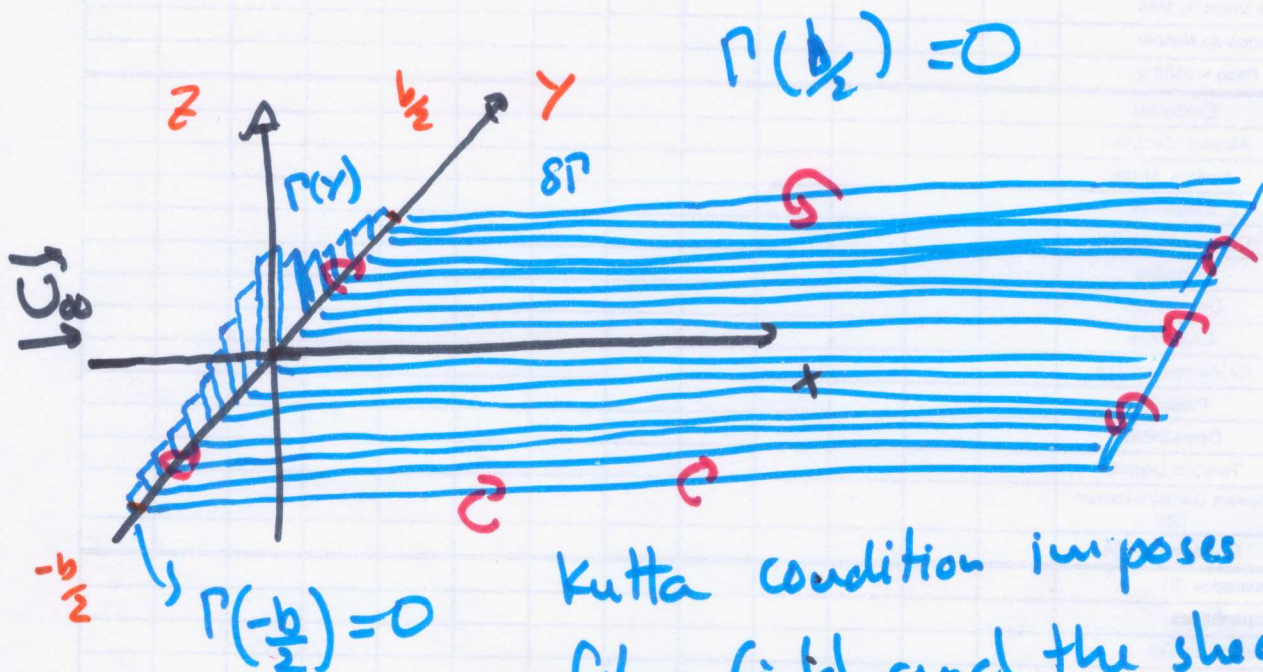
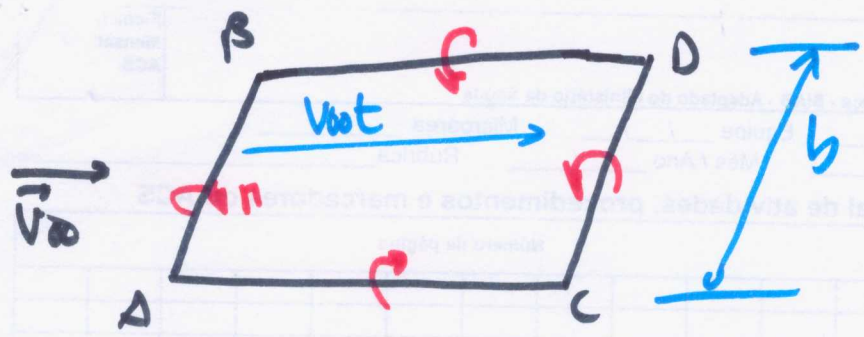
$$\vec{V}(\vec{r}) = \frac{\Gamma}{4\pi h} (2 + \cos \theta_0)$$



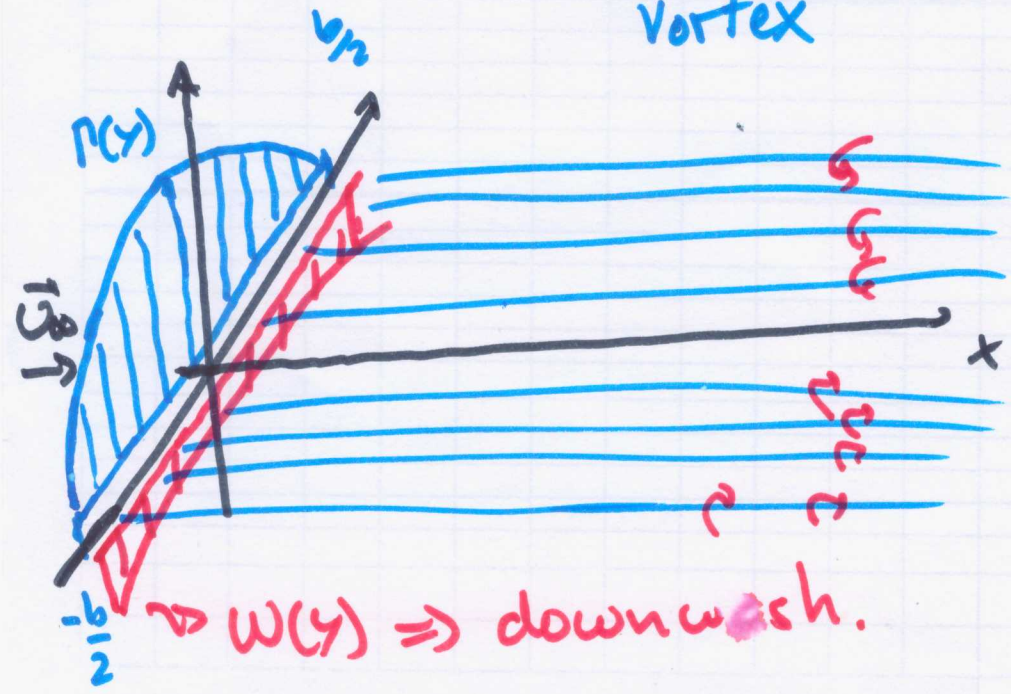
finite (straight) vortex filament:

$$\vec{V}(\vec{r}) = \frac{\Gamma}{4\pi h} (\cos \theta_1 - \cos \theta_2)$$



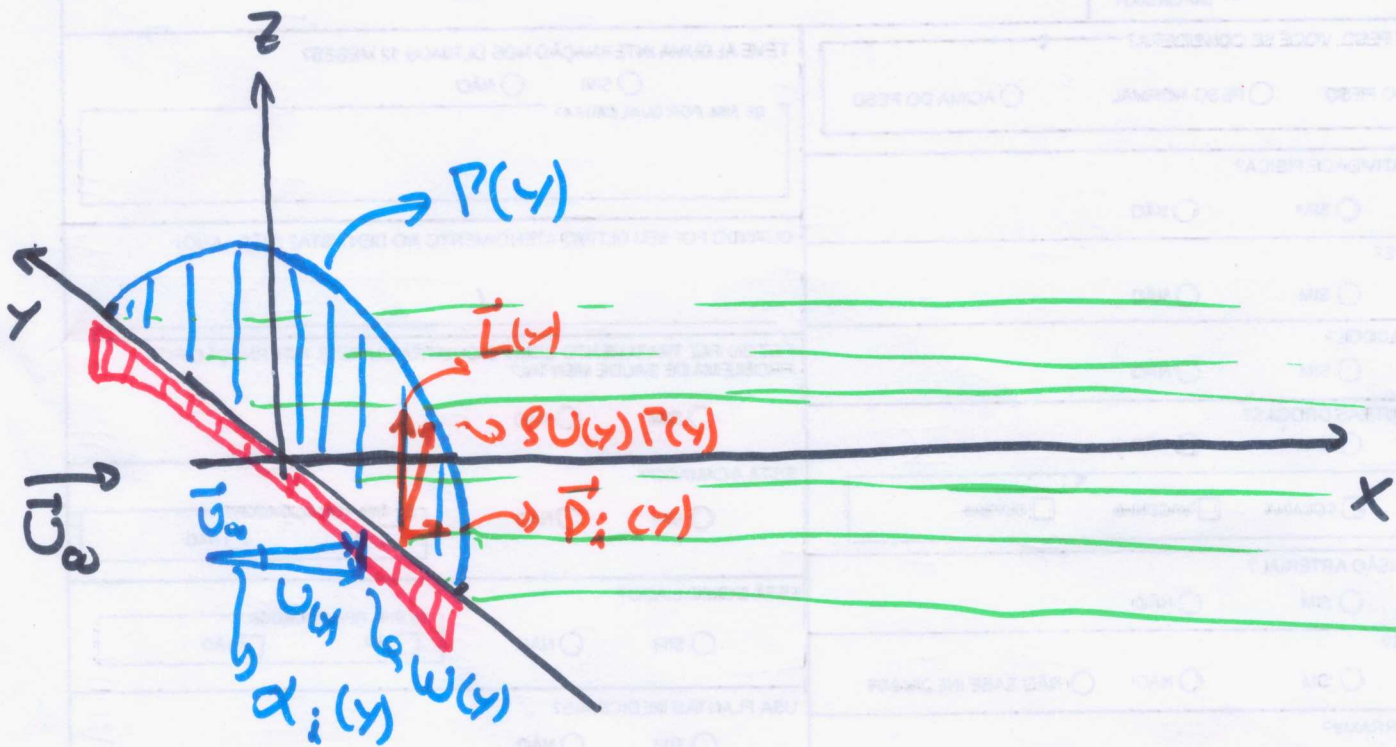


Kutta condition imposes smooth flow field and the shedding of the vortex sheet at the trailing edge. This sheet extends down to the starting vortex



18/06/2020

QUESTIONÁRIO AUTO-REVISÃO DE CONDIÇÕES / SITUAÇÕES DE SAÚDE



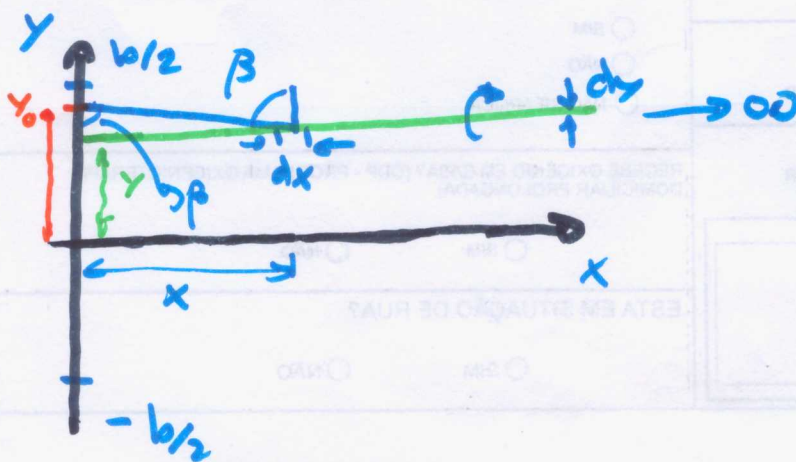
$$d\Gamma = \left( \frac{d\Gamma}{dy} \right) dy_{\text{wing}}$$

$$\alpha_i \approx \frac{w}{U_\infty}$$

induced angle of attack  $\Rightarrow \alpha_i = \tan^{-1} \left( \frac{w}{U_\infty} \right)$

$$L'(y) = \rho U(y) \Gamma \cos(\alpha_i) \approx \rho U(y) \Gamma(y) \approx \rho U_\infty \Gamma(y)$$

$$D'_i(y) = -\rho U(y) \Gamma \sin(\alpha_i) \approx -L' \alpha_i = -\rho w \Gamma(y)$$



$$dw_{x,y} = -\frac{d\Gamma}{4\pi} \frac{\cos\beta dx}{r^2}$$

$$dw_{x,y} = -\frac{d\Gamma}{4\pi h} (1 + \cos\theta_0)$$

$$\theta_0 = \frac{\pi}{2}, h = (y_0 - y)$$

$$dw_{x,y} = -\frac{d\Gamma}{4\pi (y_0 - y)}$$

$$d\omega_{y_0y} = -\frac{d\Gamma}{4\pi} \int_0^\infty \frac{\cos\beta dx}{r^2} = -\frac{d\Gamma}{4\pi} \frac{1}{(y_0 - y)}$$

$$\alpha_i(y_0) = \frac{\omega_i(y_0)}{U_\infty} = -\frac{1}{4\pi U_\infty} \int_{-b/2}^{b/2} \frac{(d\Gamma/dx)_{wing} dy}{(y_0 - y)}$$

2-D a.o.a:

$$\alpha = \alpha_G - \alpha_{L_0}$$

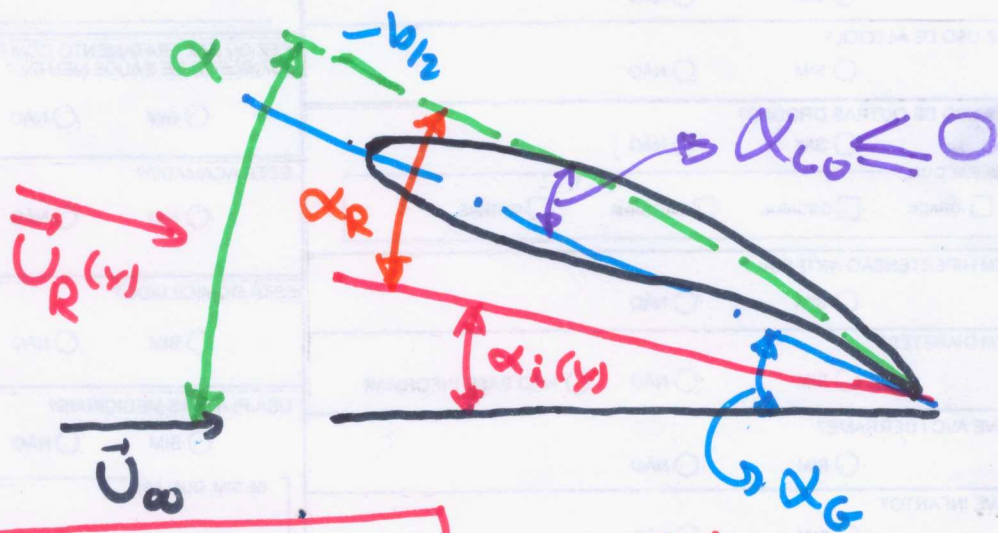
3D a.o.a

$$\alpha_R = \alpha(y) - \alpha_i(y)$$

$$\alpha_R = \alpha(y)$$

$$\alpha_R(y) = (\alpha_G - \alpha_{L_0}(y)) - \alpha_i(y)$$

$$\alpha_i(y) \geq 0$$



From the thin airfoil theory, we have:

$$\Gamma = \frac{1}{2} \frac{dc_c}{d\alpha} \alpha_R U_\infty c$$

↳ chord length

$$\frac{dc_c}{d\alpha} = a_0 = m_0 = 2\pi$$

$$\Gamma(y) = \frac{a_0}{2} c(y) U_\infty [\alpha(y) - \alpha_i(y)]$$

$$\Gamma(y) = \frac{a_0}{2} c(y) \left[ U_\infty \alpha(y) - \frac{1}{4\pi} \int_{-b/2}^{b/2} \frac{d\Gamma}{dy}(y) \frac{dy}{(y-y)} \right]$$

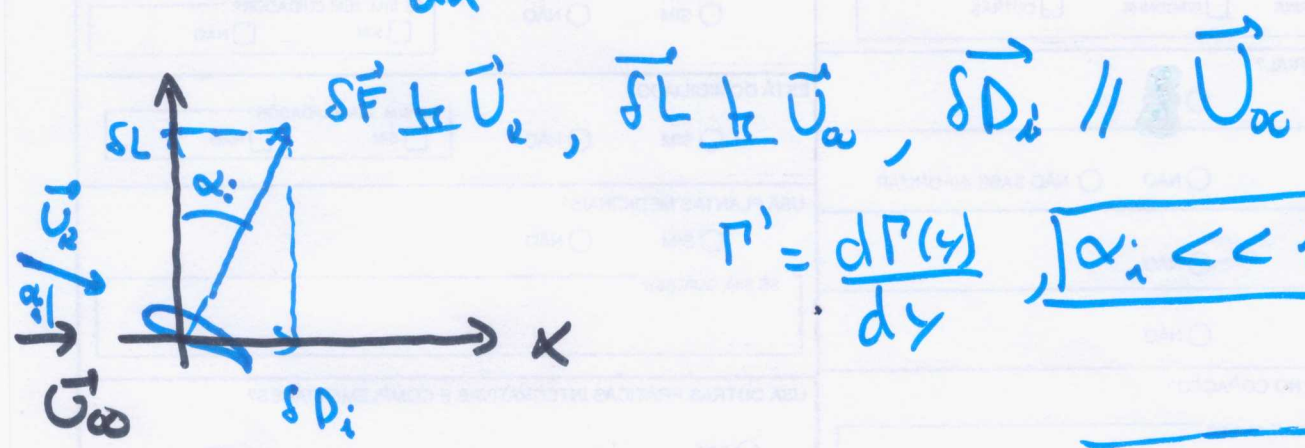
Fundamental equation of Prandtl's  
Lifting Line Theory

$$\Gamma(y) = \frac{a_0}{2} c(y) \left[ U_\infty \alpha(y) - \frac{1}{4\pi} \int_{-b/2}^{b/2} \frac{d\Gamma(x)}{dy} \frac{dx}{(y-x)} \right]$$

2.0 a.o.a.  $U_\infty \alpha_i(y)$

wing tips:  $\Gamma(-b/2) = \Gamma(b/2) = 0$

$$a_0 = c_{e\alpha} = \frac{dc_e}{d\alpha} = 2\pi$$



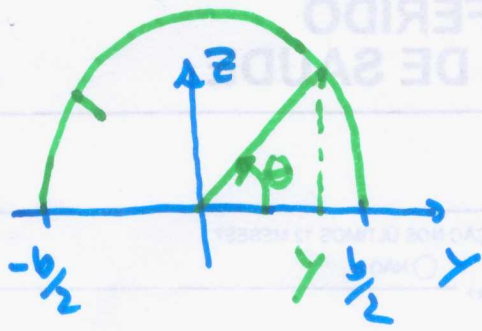
$$\Gamma' = \frac{d\Gamma(y)}{dy}, \quad |\alpha_i| \ll 1$$

$$\delta L = \rho U_\infty \Gamma'(y) dy \Rightarrow \delta F(y) \cos \alpha_i \Rightarrow \boxed{\delta L(y) \approx \delta F(y)}$$

$$\delta D_i(y) = \delta F(y) \sin \alpha_i \Rightarrow \delta D_i(y) = \delta L(y) \alpha_i(y)$$

$$\begin{cases} \delta L \approx \rho U_\infty \Gamma'(y) dy \\ \delta D_i \approx \rho U_\infty \Gamma'(y) \alpha_i(y) dy \end{cases}$$

$$w_i(y) = U_\infty \alpha_i(y)$$



$$y = \frac{b}{2} \cos \theta ; 0 \leq \theta \leq \pi$$

$$\int_0^\pi \frac{\cos(n\theta) d\theta}{\cos \theta - \cos \theta_0} = \frac{\pi \sin(n\theta_0)}{\sin(\theta_0)}$$

$$\Gamma(\theta) = 2b U_\infty \sum_{n=1}^{\infty} A_n \sin(n\theta)$$

$$W(\theta) = U_\infty \sum_{n=1}^{\infty} n A_n \frac{\sin(n\theta)}{\sin(\theta)} ; A_n = \frac{a_n}{b U_\infty (b/4)^n}$$

$$\mu(\theta) = \frac{C_{l\alpha}(\theta) C(\theta)}{4b}$$

$C_{l\alpha} = 2\pi$

Aspect Ratio:

$$AR = \frac{b^2}{S_w} \rightarrow \begin{matrix} \text{Wing span} \\ \text{Wing plan Area} \end{matrix}$$

$$\sum_{n=1}^{\infty} A_n \sin(n\theta) [n \mu(\theta) + \sin(\theta)] = \mu(\theta) \alpha(\theta) \sin(\theta)$$

$$C_L = \frac{L}{\frac{\rho U_\infty^2}{2} S_w} = \pi AR A_1$$

$\delta \geq 0$

$$C_{Di} = \frac{D_i}{\frac{\rho U_\infty^2}{2} S_w} = \frac{C_i^2}{\pi AR} (1 + \delta) ; \delta = \sum_{n=2}^{\infty} n \left( \frac{A_n}{A_1} \right)^2$$

$$C_{mR} = \frac{M_R}{\frac{\rho U_\infty^2}{2} S_w \bar{c}} = -\frac{\pi}{4} (AR^2) A_2 \quad (\text{Roll})$$

$$C_{my} = \frac{M_y}{\frac{\rho U_\infty^2}{2} S_w \bar{c}} = \frac{\pi}{4} (AR^2) \sum_{n=1}^{\infty} (2n+1) A_n A_{n+1} \quad (Yaw)$$

Let's assume a situation where only  $A_1 \neq 0$  and  $A_k = 0 \forall k > 1$

$$C_L = \pi AR A_1, C_{Di} = \frac{C_L^2}{\pi AR} (\delta=0), C_{mz} = C_{my} = 0$$

For an elliptic loaded wing, we have

$$\Gamma(\theta) = \Gamma_0 \sin \theta, \quad \Gamma(y) = \Gamma_0 \sqrt{1 - \left(\frac{2y}{b}\right)^2}$$

$$A_1 = \frac{\Gamma_0}{2bU_\infty}$$

