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Cruising flights (review)

Flight performance

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Model

Equilibrium

$$\sum F_x = 0$$

$$\sum F_z = 0$$



$$T - D = 0$$

$$L - W = 0$$

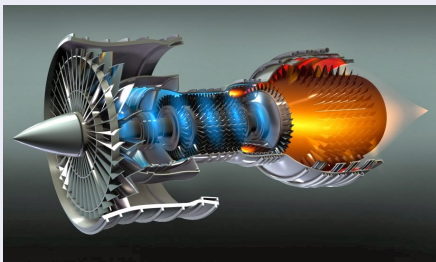
Considerations:

- No accelerations
- Leveled flight
- Trimmed flight
- Weight variation comes only from fuel consumption

Kinematics

$$\frac{dx}{dt} = V$$

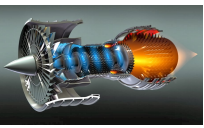
Consumption



$$\frac{dW}{dt} = -cT$$



$$\frac{dW}{dt} = -\frac{\hat{c} P}{\hat{k} \eta_P}$$



Important relations

Velocities

$$V = \left\{ \frac{T}{S} \frac{1}{\rho C_{D0}} \left[1 \pm \sqrt{1 - \frac{1}{E_m (T/W)^2}} \right] \right\}^{1/2}$$

$$V^4 - \frac{2\hat{k}\eta_P}{\rho} \frac{P_e}{W} \frac{W}{S} V + 4k \left(\frac{W}{S} \right)^2 \frac{1}{\rho^2 C_{D,0}^2} = 0$$

Thrust / power required

$$T_r = \frac{1}{2} \rho V^2 S C_{D0} + 2Sk \left(\frac{W}{S} \right)^2 \frac{1}{\rho V^2}$$

$$P_r = \frac{1}{2} \rho S C_{D0} V^3 + 2Sk \left(\frac{W}{S} \right)^2 \frac{1}{\rho V}$$

Range

$$x = -\frac{1}{c} \int_{W_1}^{W_2} V \left(\frac{C_L}{C_D} \right) \frac{1}{W} dW$$

$$x = -\frac{\hat{k}\eta_P}{\hat{c}} \int_{W_1}^{W_2} \left(\frac{C_L}{C_D} \right) \frac{1}{W} dW$$

Endurance

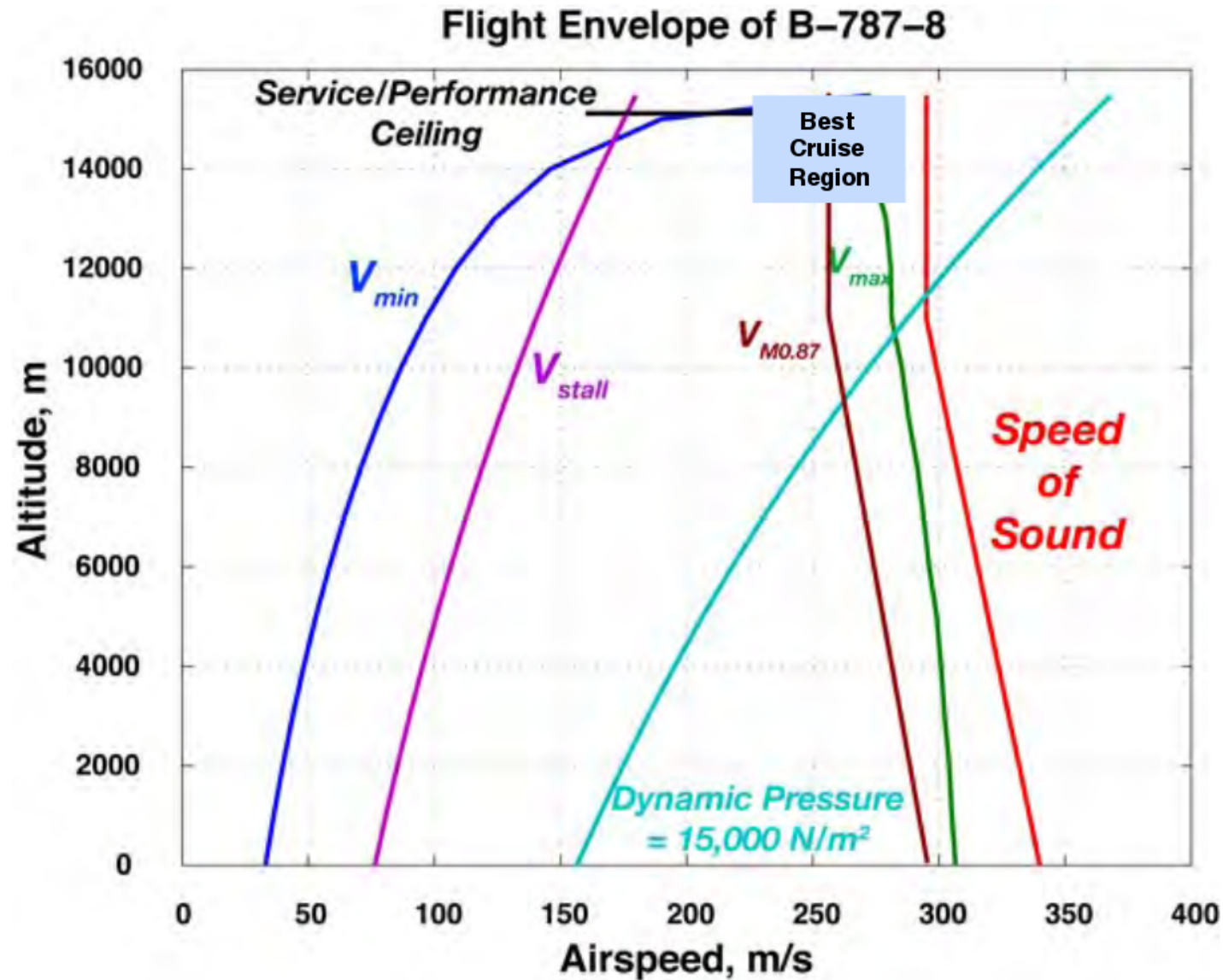
$$t = -\frac{1}{c} \int_{W_1}^{W_2} \left(\frac{C_L}{C_D} \right) \frac{1}{W} dW$$

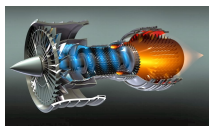
$$t = -\frac{\hat{k}\eta_P}{\hat{c}} \int_{W_1}^{W_2} \left(\frac{C_L}{C_D} \right) \frac{1}{VW} dW$$

Jet

Piston-prop

Flight envelope





Range

Cruise-fuel weight consumption $\xi = \frac{\Delta W_f}{W_1}$

Case: constant altitude and constant lift coefficient

$$x_{h-C_L} = \frac{2V_1 E}{c} \left(1 - \sqrt{1 - \xi}\right)$$

$$x_{h-C_L} = \frac{\hat{k}\eta_P E}{\hat{c}} \ln \left(\frac{1}{1 - \xi} \right)$$

Case: constant velocity and constant lift coefficient

$$x_{V-C_L} = \frac{V_1 E}{c} \ln \left(\frac{1}{1 - \xi} \right)$$

$$x_{V-C_L} = \frac{\hat{k}\eta_P E}{\hat{c}} \ln \left(\frac{1}{1 - \xi} \right)$$

Case: constant velocity and constant height

$$x_{V-h} = \frac{2V_1 E_m}{c} \tan^{-1} \left[\frac{E_1 \xi}{2E_m (1 - kC_{L,1} E_1 \xi)} \right]$$

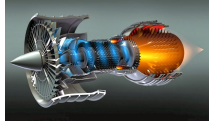
$$x_{V-h} = \frac{2\hat{k}\eta_P E_m}{\hat{c}} \tan^{-1} \left[\frac{E_1 \xi}{2E_m (1 - kC_{L,1} E_1 \xi)} \right]$$

Conclusions

$$\left(\frac{C_L^{0.5}}{C_D} \right)_{max}$$

$$\left(M \frac{L}{D} \right)_{max}$$

$$\left(\frac{C_L}{C_D} \right)_{max}$$



Endurance



Case: constant altitude and constant lift coefficient

$$t_{h-C_L} = \frac{E_1}{c} \ln \left(\frac{1}{1-\xi} \right)$$

$$t_{h-C_L} = \frac{2\hat{k}\eta_P E}{\hat{c}V_1} \left(\frac{1}{\sqrt{1-\xi}} - 1 \right)$$

Case: constant velocity and constant lift coefficient

$$t_{V-C_L} = \frac{E_1}{c} \ln \left(\frac{1}{1-\xi} \right)$$

$$t_{V-C_L} = \frac{\hat{k}\eta_P E}{\hat{c}V} \ln \left(\frac{1}{1-\xi} \right)$$

Case: constant velocity and constant height

$$t_{V-h} = \frac{2E_m}{c} \tan^{-1} \left[\frac{E_1\xi}{2E_m(1-kC_{L,1}E_1\xi)} \right]$$

$$t_{V-h} = \frac{2\hat{k}\eta_P E_m}{\hat{c}V} \tan^{-1} \left[\frac{E_1\xi}{2E_m(1-kC_{L,1}E_1\xi)} \right]$$

Conclusions

$$\left(\frac{C_L}{C_D} \right)_{max}$$

$$\left(\frac{C_L^{3/2}}{C_D} \right)_{max}$$

Important relations

$$C_D = C_{D0} + kC_L^2$$

$$C_L = C_{L\alpha}(\alpha - \alpha_{L=0})$$

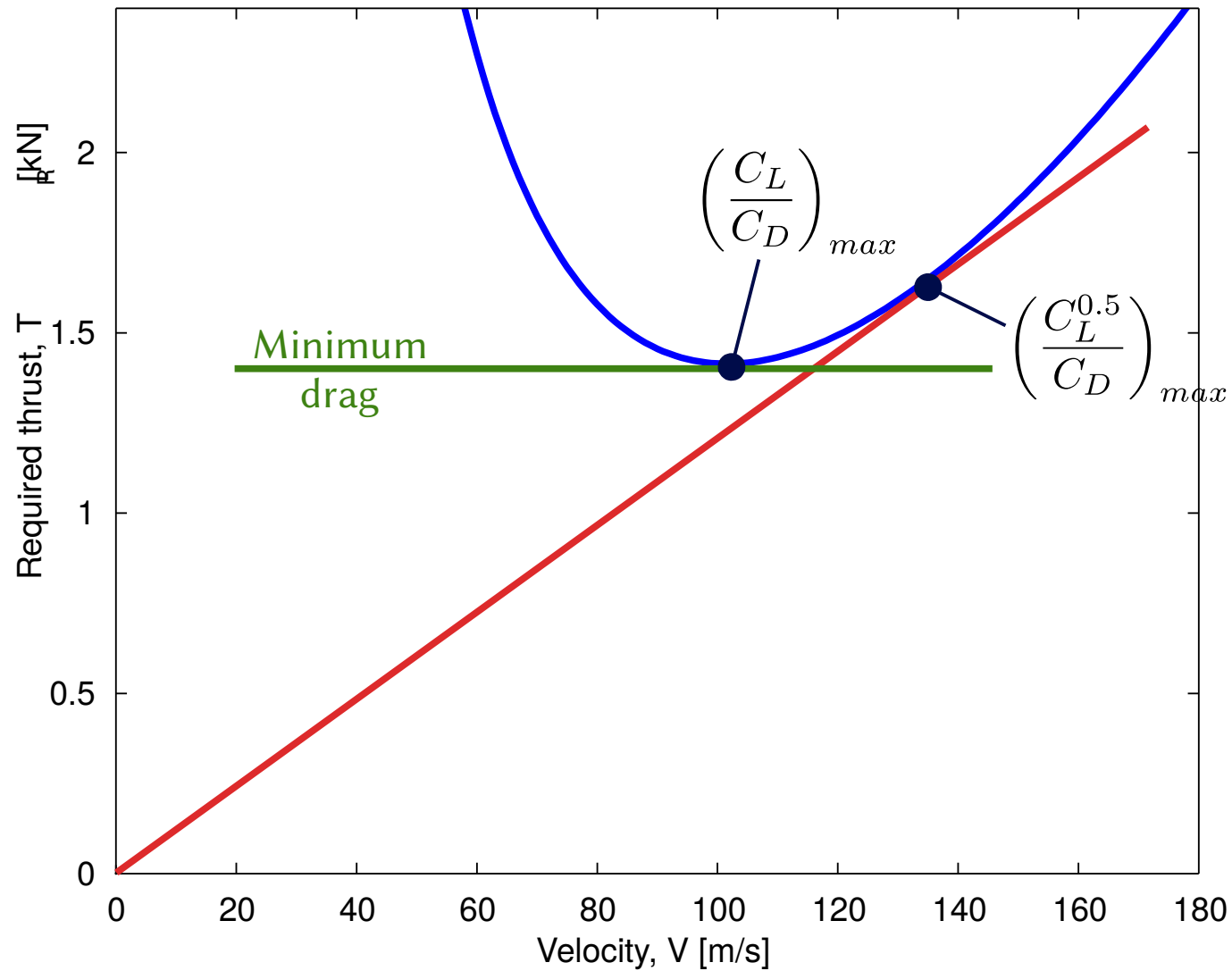
$$\left(\frac{C_L}{C_D}\right)_{max} \rightarrow C_L = \left(\frac{C_{D0}}{k}\right)^{1/2}; \quad C_D = 2C_{D0}$$

$$\left(\frac{C_L^{0.5}}{C_D}\right)_{max} \rightarrow C_L = \left(\frac{C_{D0}}{3k}\right)^{1/2}; \quad C_D = \frac{4C_{D0}}{3}$$

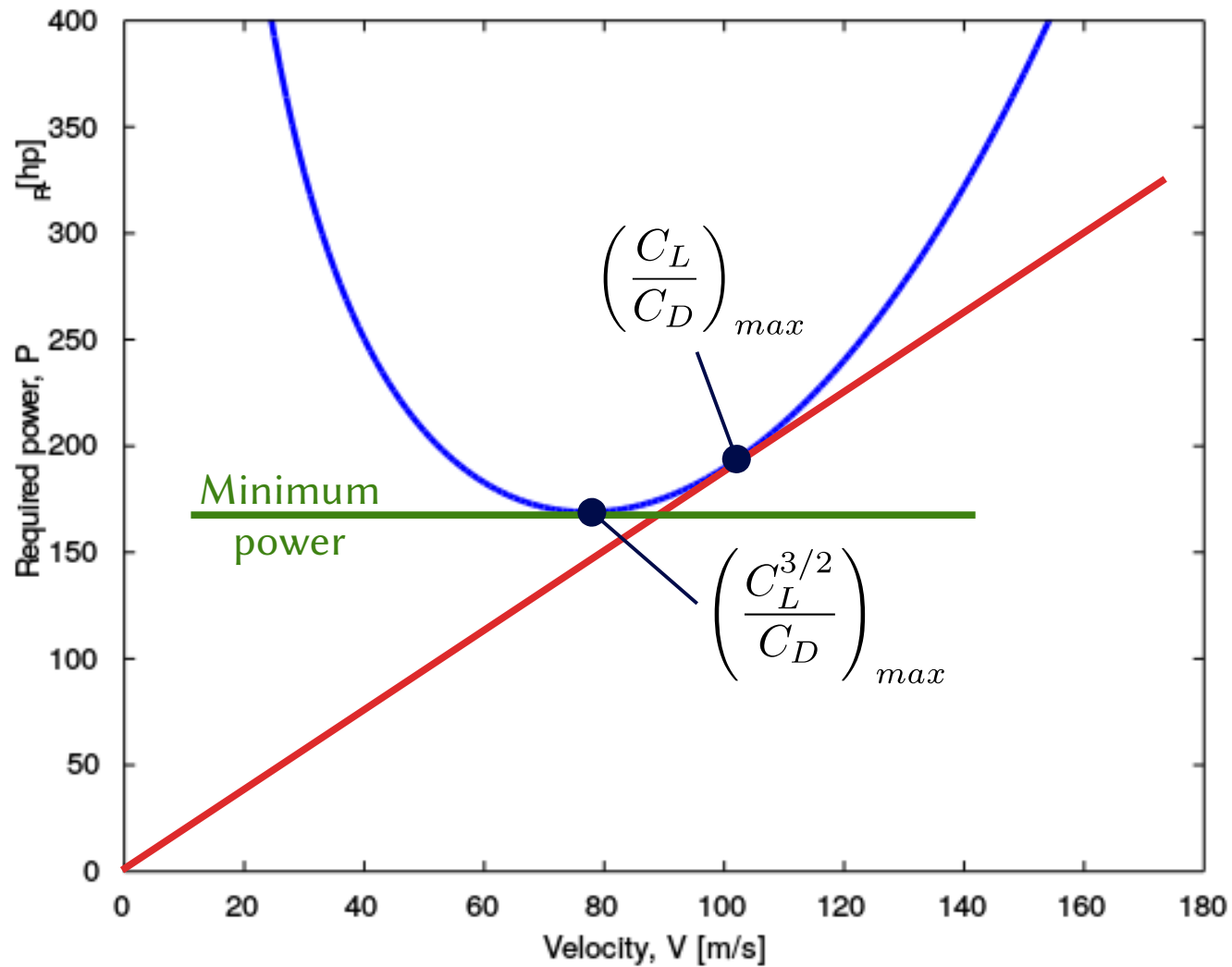
$$\left(\frac{C_L^{1.5}}{C_D}\right)_{max} \rightarrow C_L = \left(\frac{3C_{D0}}{k}\right)^{1/2}; \quad C_D = 4C_{D0}$$

$$\left(\frac{C_L^3}{C_D^2}\right)_{max} \rightarrow C_L = \left(\frac{3C_{D0}}{k}\right)^{1/2}; \quad C_D = 4C_{D0}$$

Thrust required



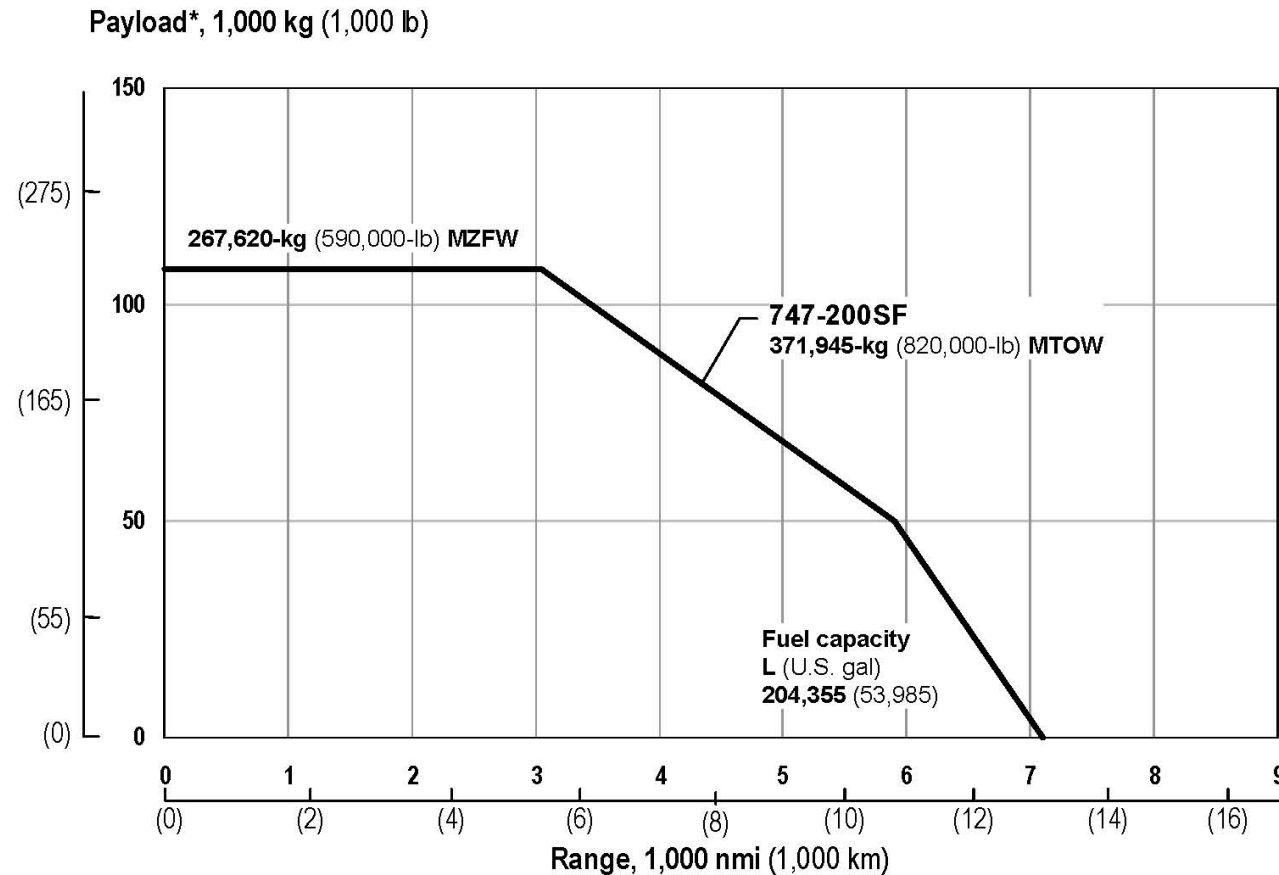
Power required



Payload vs. range

Boeing 747-200F/-200SF Payload-range capability

Pratt & Whitney JT9D-7Q and JT9D-7R4G2 engines*



*747-200F model.

Source: Boeing data.

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