

# **Curva de Retenção**

## **Modelos de Ajuste**

**Gardner (1958)**

**Brooks & Corey (1966)**

**Van Genutchen (1980)**

**Fredlund & Xing (1994)**

# Objetivo

- A curva de retenção é utilizada nas análises de fluxo em meio não saturado e a sua forma matemática (equações de ajuste) facilitam este uso.
- A curva de retenção é usada para a obtenção da função de permeabilidade dos solos não saturados.
- Tratando-se das funções de permeabilidade, tanto as equações empíricas como os modelos estatísticos fazem uso dos parâmetros das equações de ajuste das curvas de retenção.

## Gardner (1958)

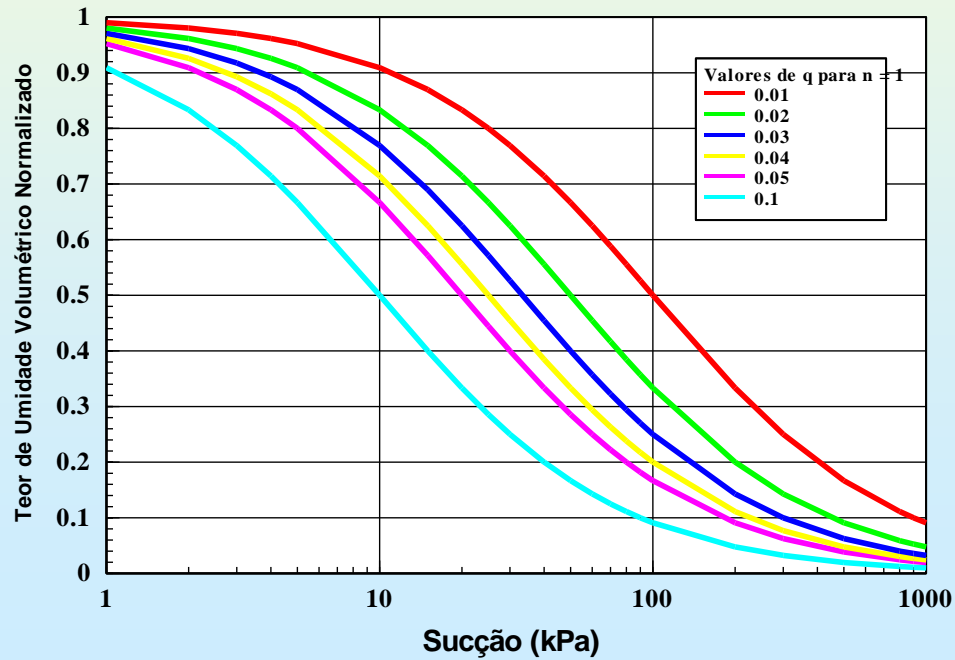
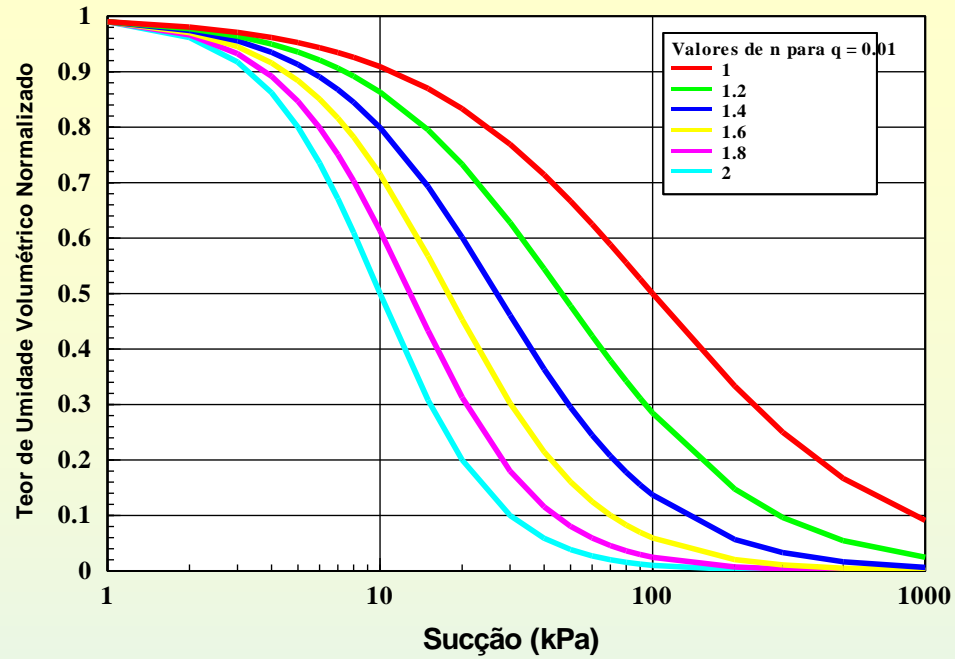
$$\Theta = \frac{1}{1 + q\psi^n}$$

**q** – parâmetro de ajuste relacionado com sucção de entrada de ar

**n** - parâmetro de ajuste relacionado com a inclinação no ponto de inflecção da curva de retenção

# Gardner (1958)

$$\Theta = \frac{1}{1 + q\psi^n}$$

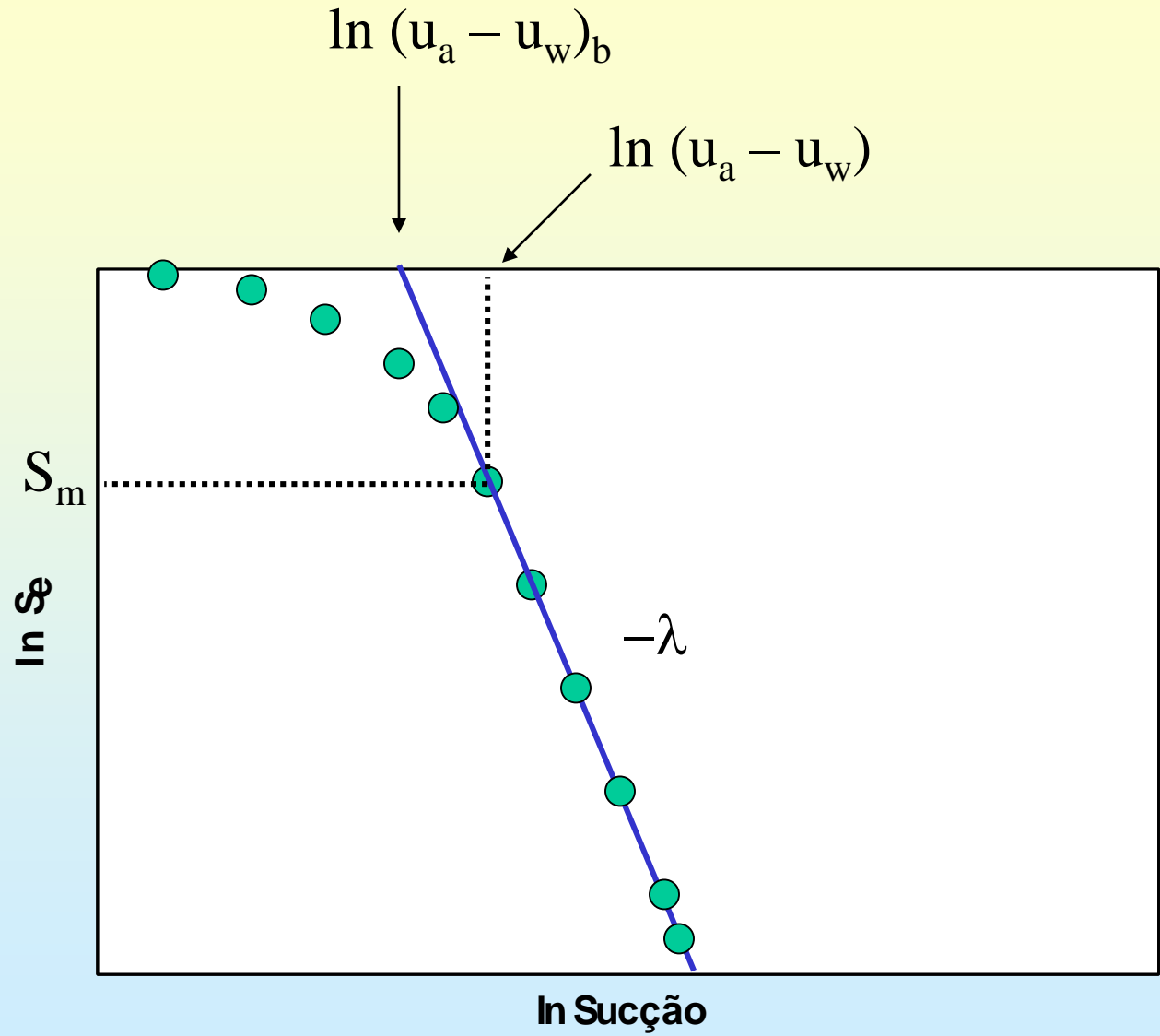


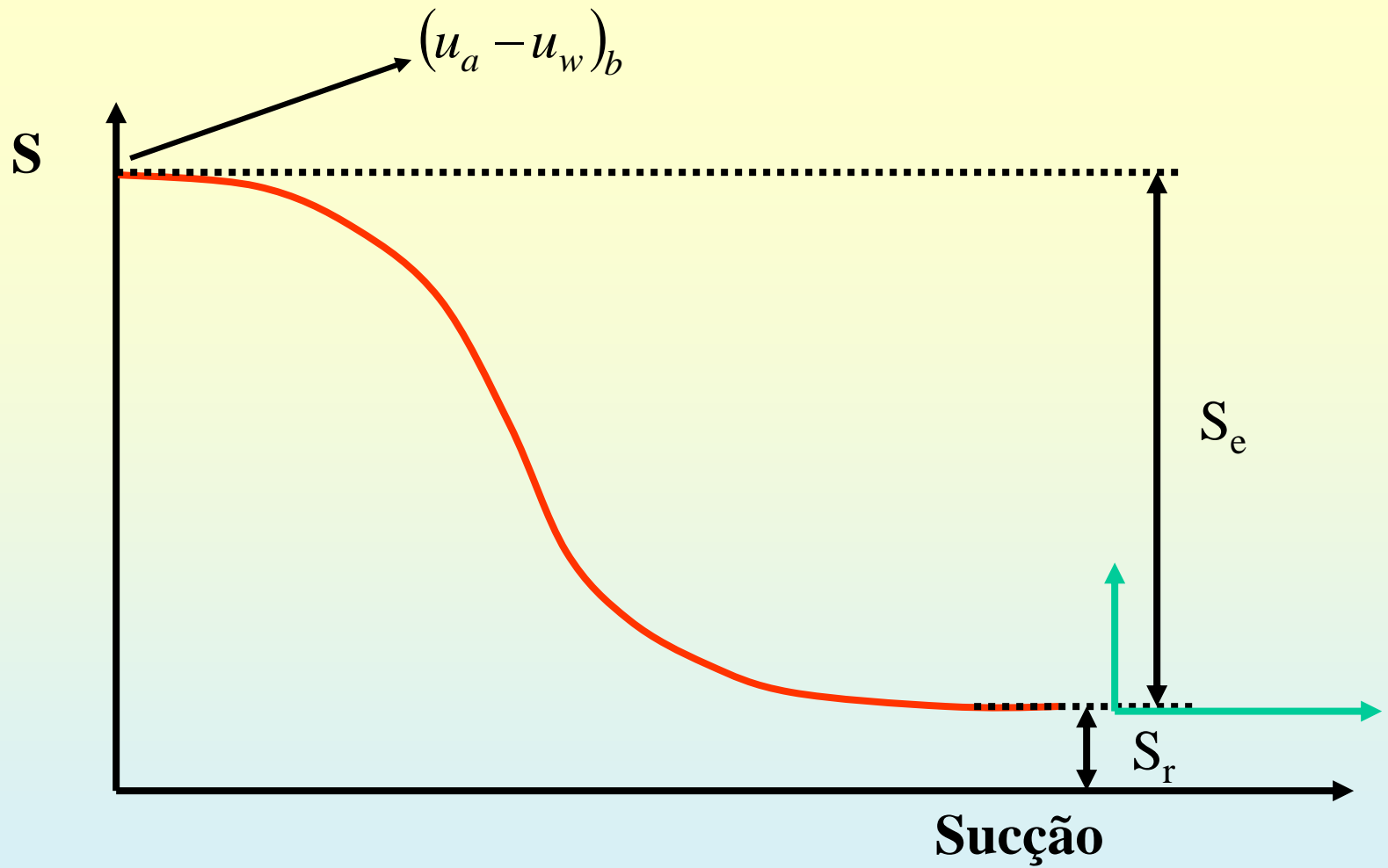
## Brooks & Corey (1966)

$$S_e = \frac{S - S_r}{1 - S_r} = \left( \frac{(u_a - u_w)_b}{(u_a - u_w)} \right)^\lambda \quad \text{para } (u_a - u_w) \geq (u_a - u_w)_b$$

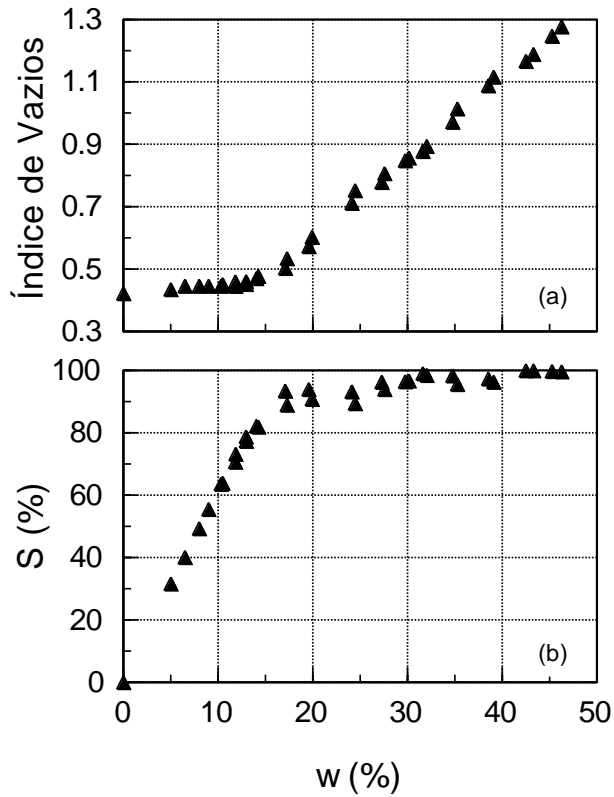
- Brooks & Corey observaram que se fossem omitidos os dados para graus de saturação maiores que aproximadamente 85% os dados se apresentavam alinhados em uma reta, quando plotados em termos de  $\log S_e$  e  $\log$  da sucção.
- O valor de  $S_r$  tem papel importante no ajuste. Em geral este valor é determinado de modo a fornecer o melhor ajuste.
- Inicialmente obtida para rochas porosas
- Aplicável a solos homogêneos
- Os parâmetros são obtidos por ajuste ao dados de sucção e saturação.

$$S_e = \frac{S - S_r}{1 - S_r} = \left( \frac{(u_a - u_w)_b}{(u_a - u_w)} \right)^\lambda \text{ para } (u_a - u_w) \geq (u_a - u_w)_b$$

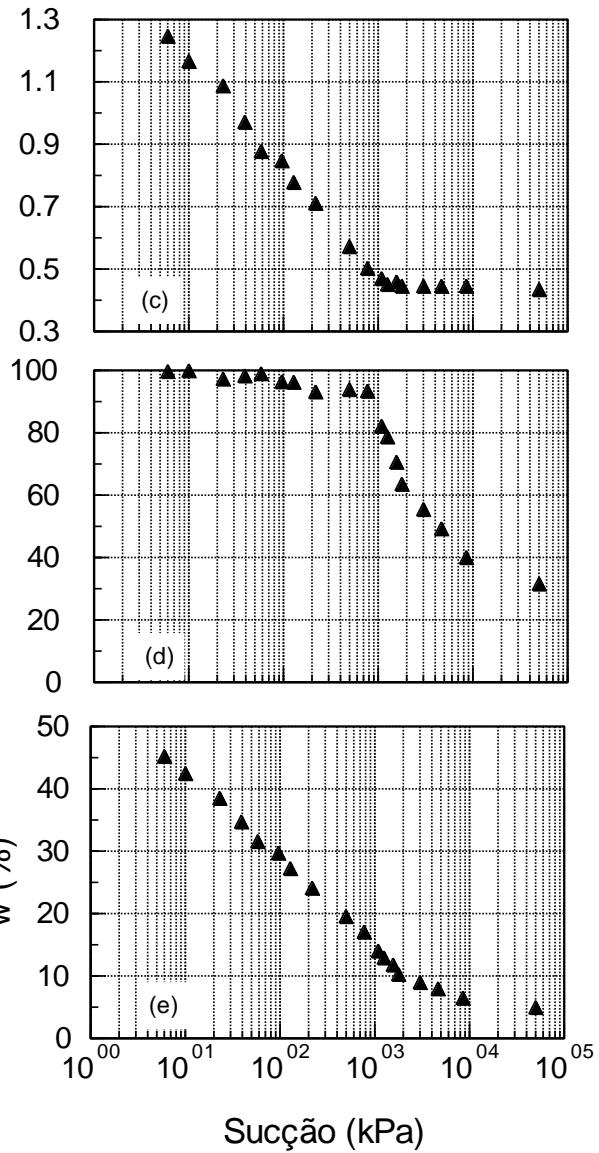




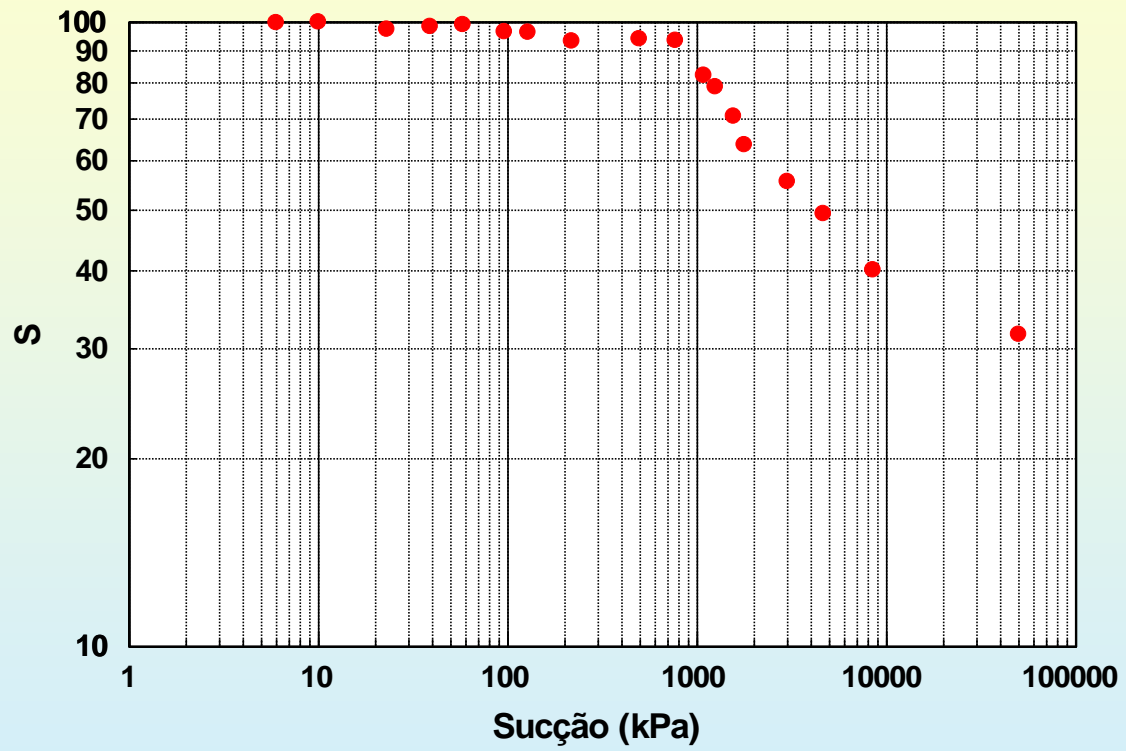
$$S_e = \frac{S - S_r}{1 - S_r} = \left( \frac{(u_a - u_w)_b}{(u_a - u_w)} \right)^\lambda$$



Argila de Londres (lama)  
 ▲ EXEMPLO

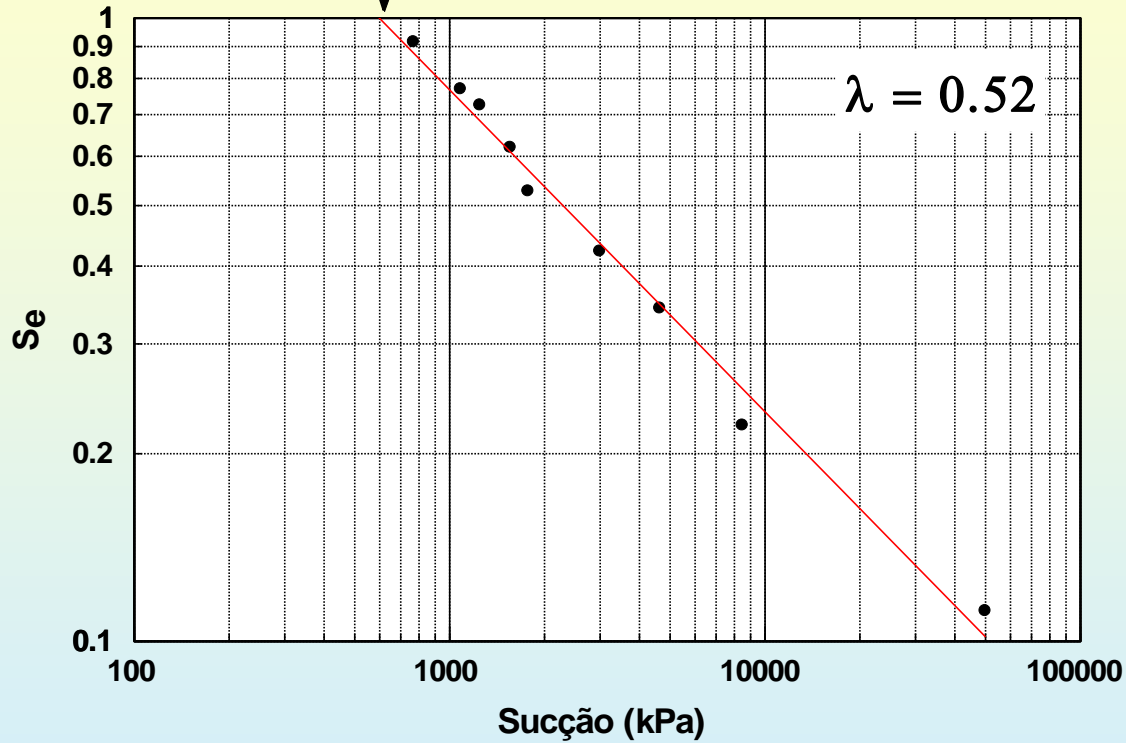






$$(u_a - u_w)_b = 595 \text{ kPa}$$

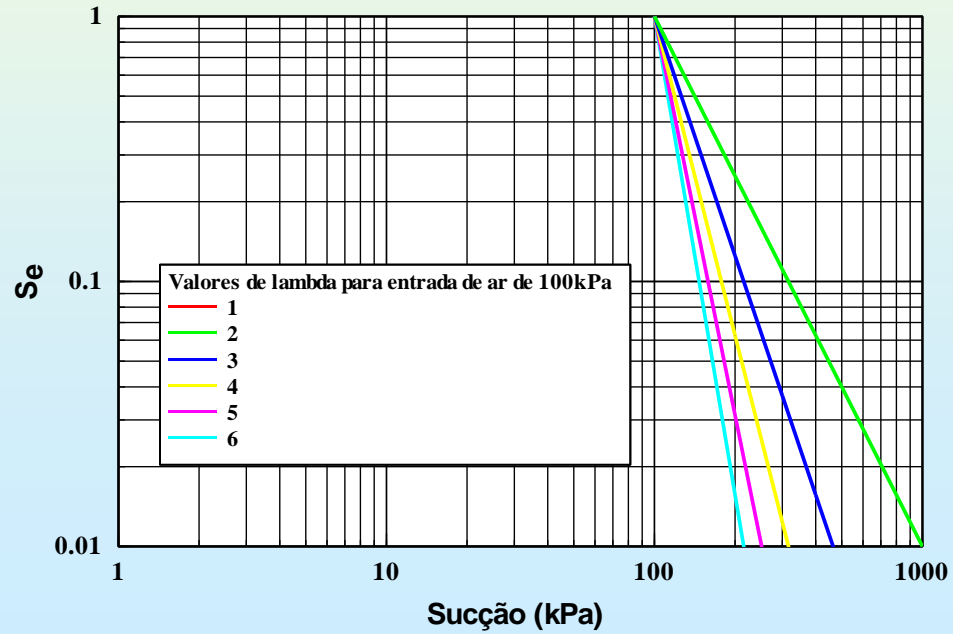
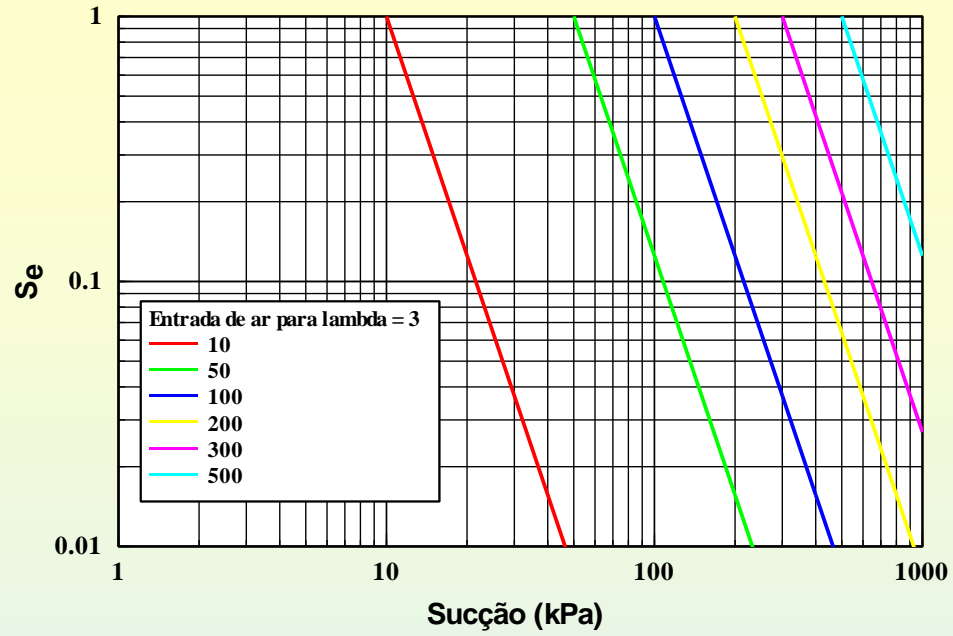
$$S_r = 23\%$$

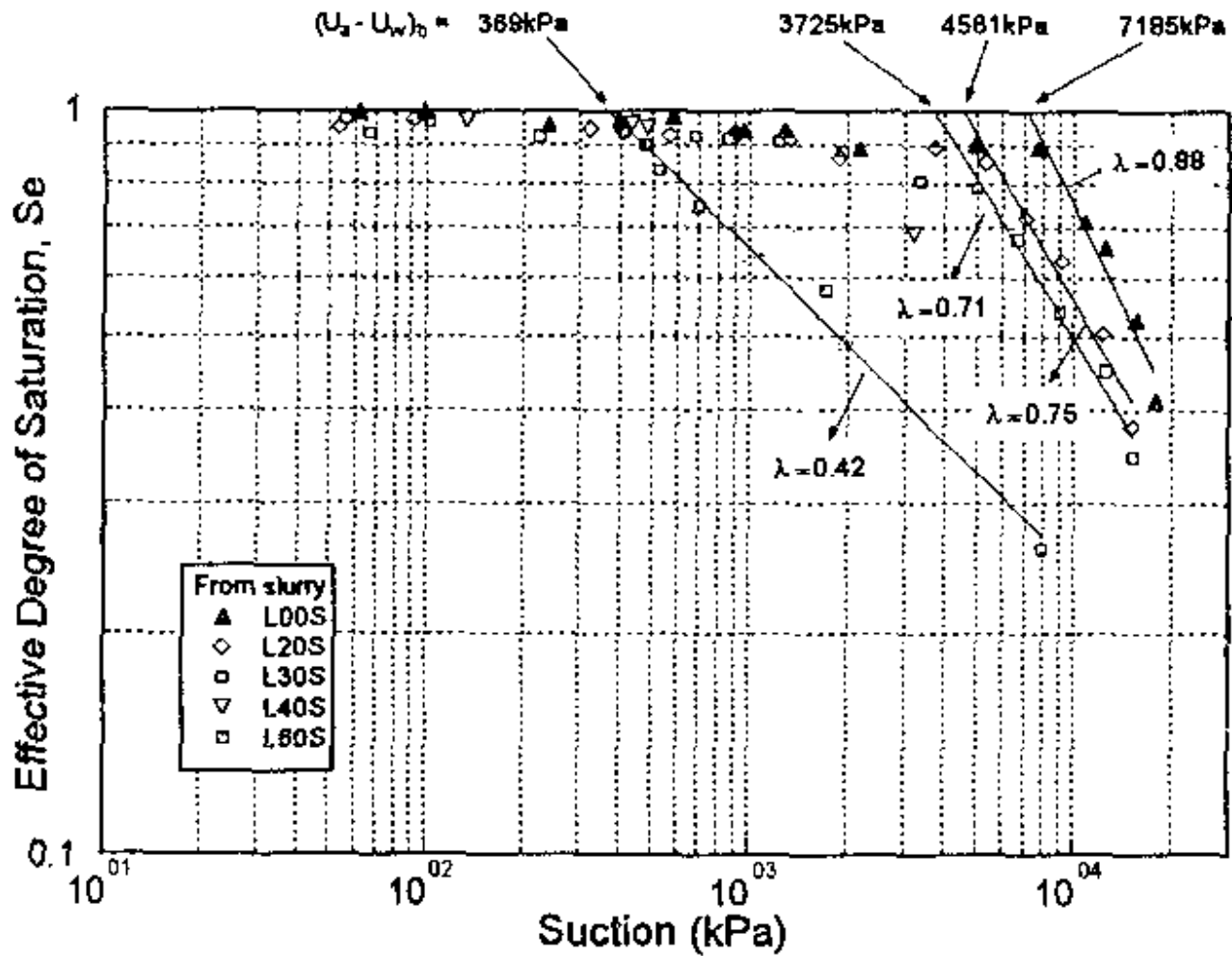


$$S_e = \frac{S - S_r}{1 - S_r} = \left( \frac{(u_a - u_w)_b}{(u_a - u_w)} \right)^\lambda$$

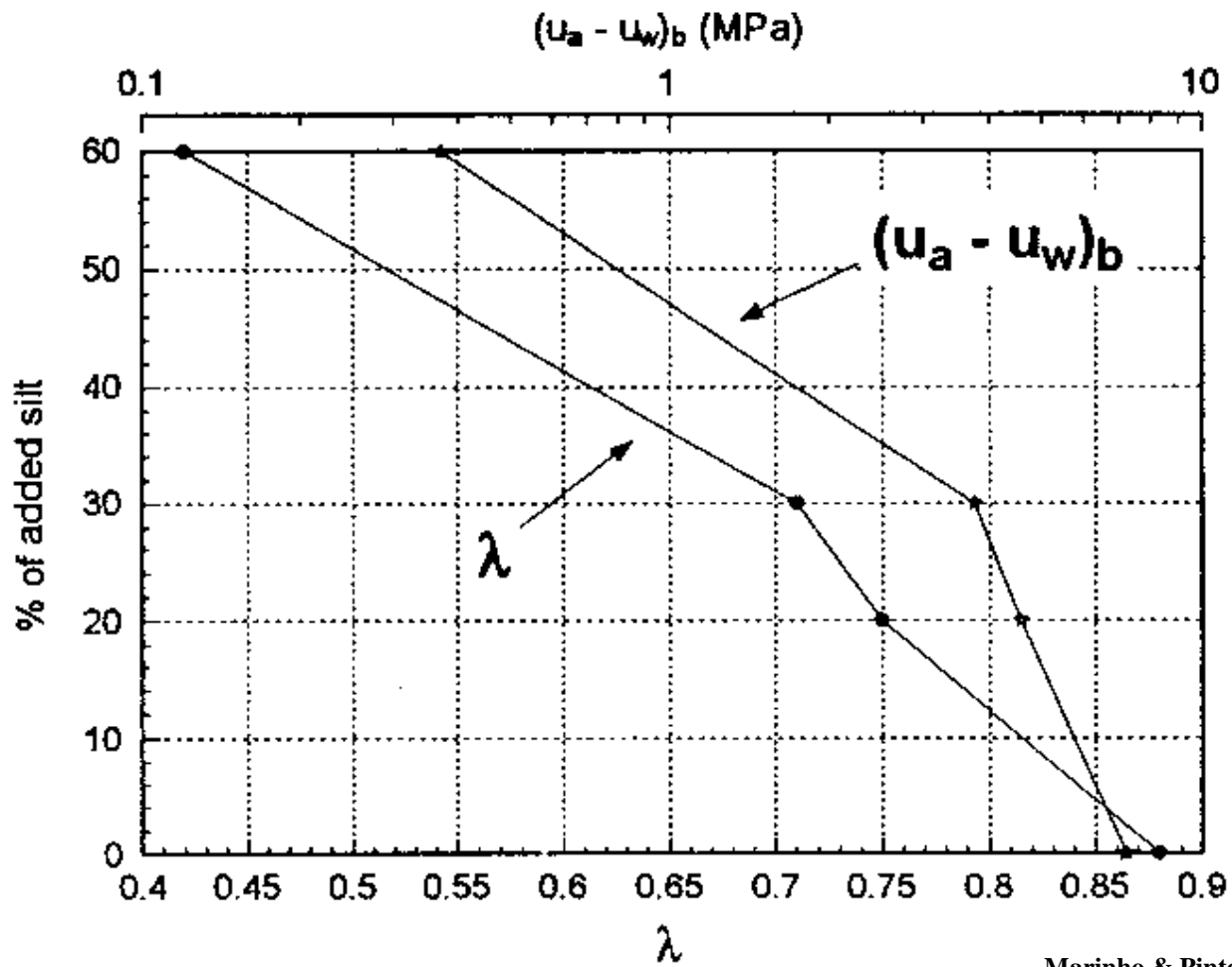
# Brooks & Corey (1966)

$$S_e = \frac{S - S_r}{1 - S_r} = \left( \frac{(u_a - u_w)_b}{(u_a - u_w)} \right)^\lambda$$





Marinho & Pinto (1997)



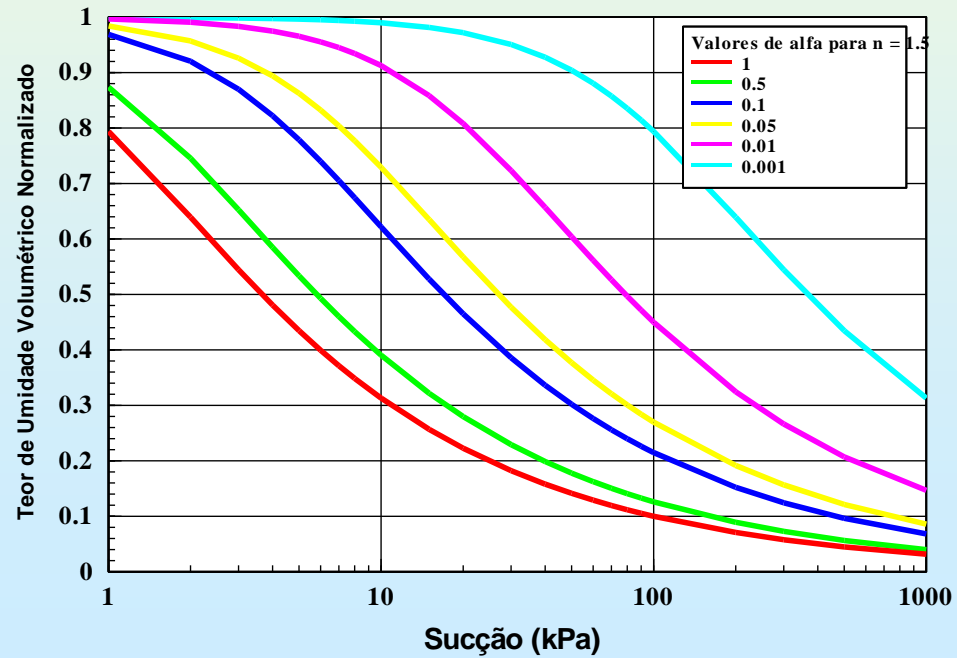
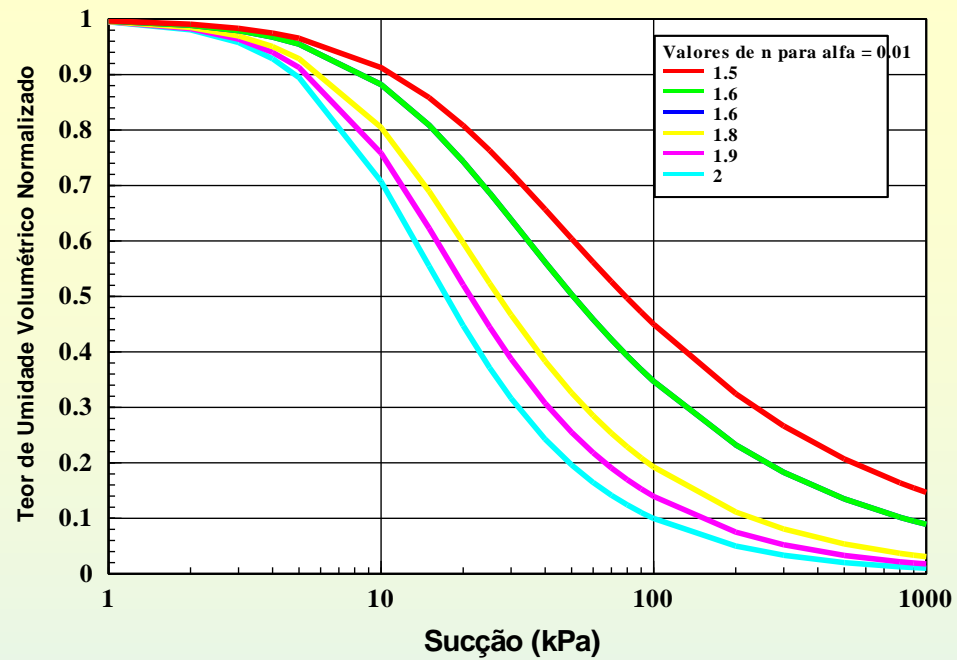
Marinho & Pinto (1997)

## Van Genuchten (1980)

$$S_e = \frac{S - S_r}{1 - S_r} = \left( \frac{1}{1 + \alpha(u_a - u_w)^n} \right)^m$$

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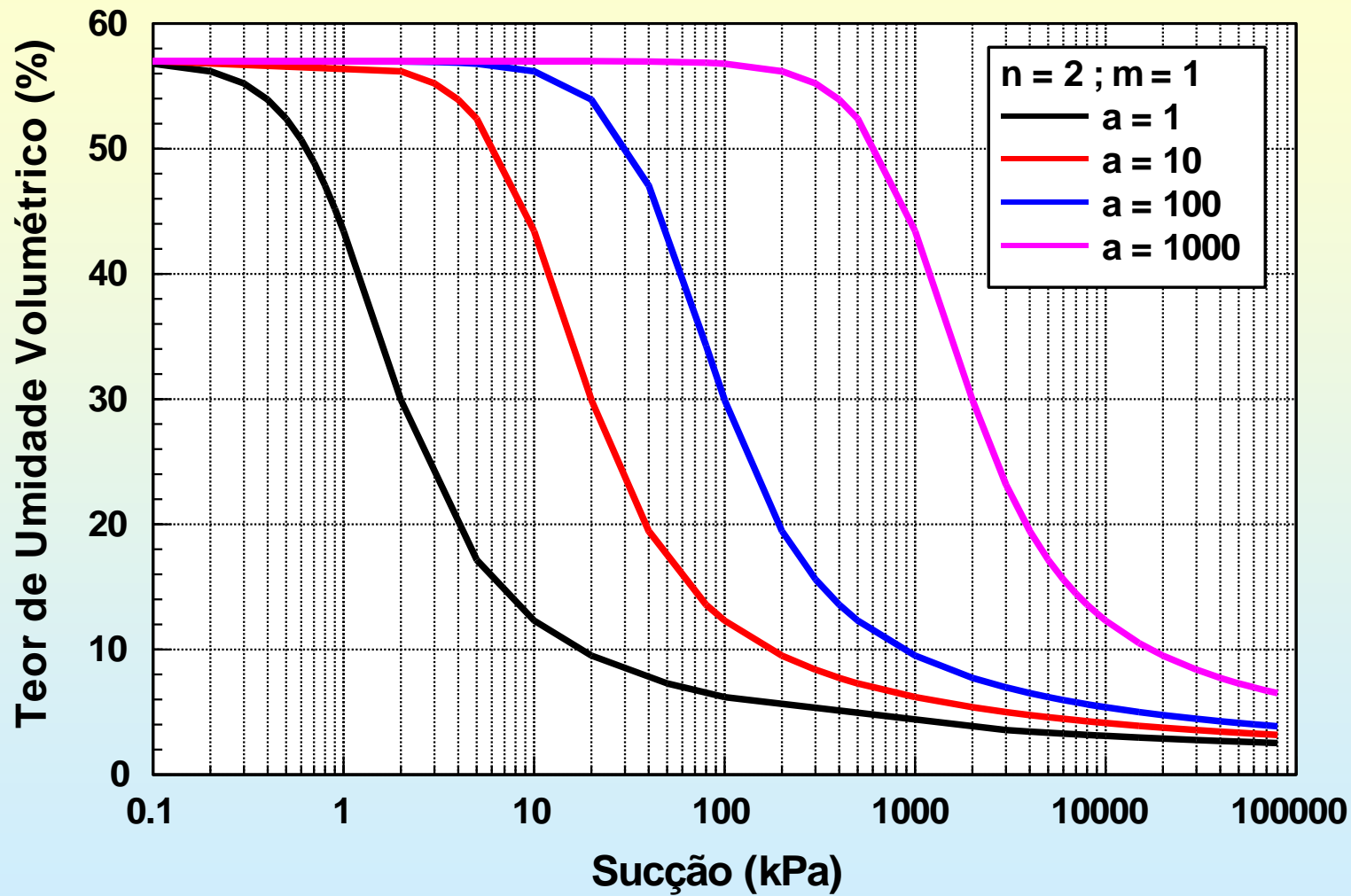


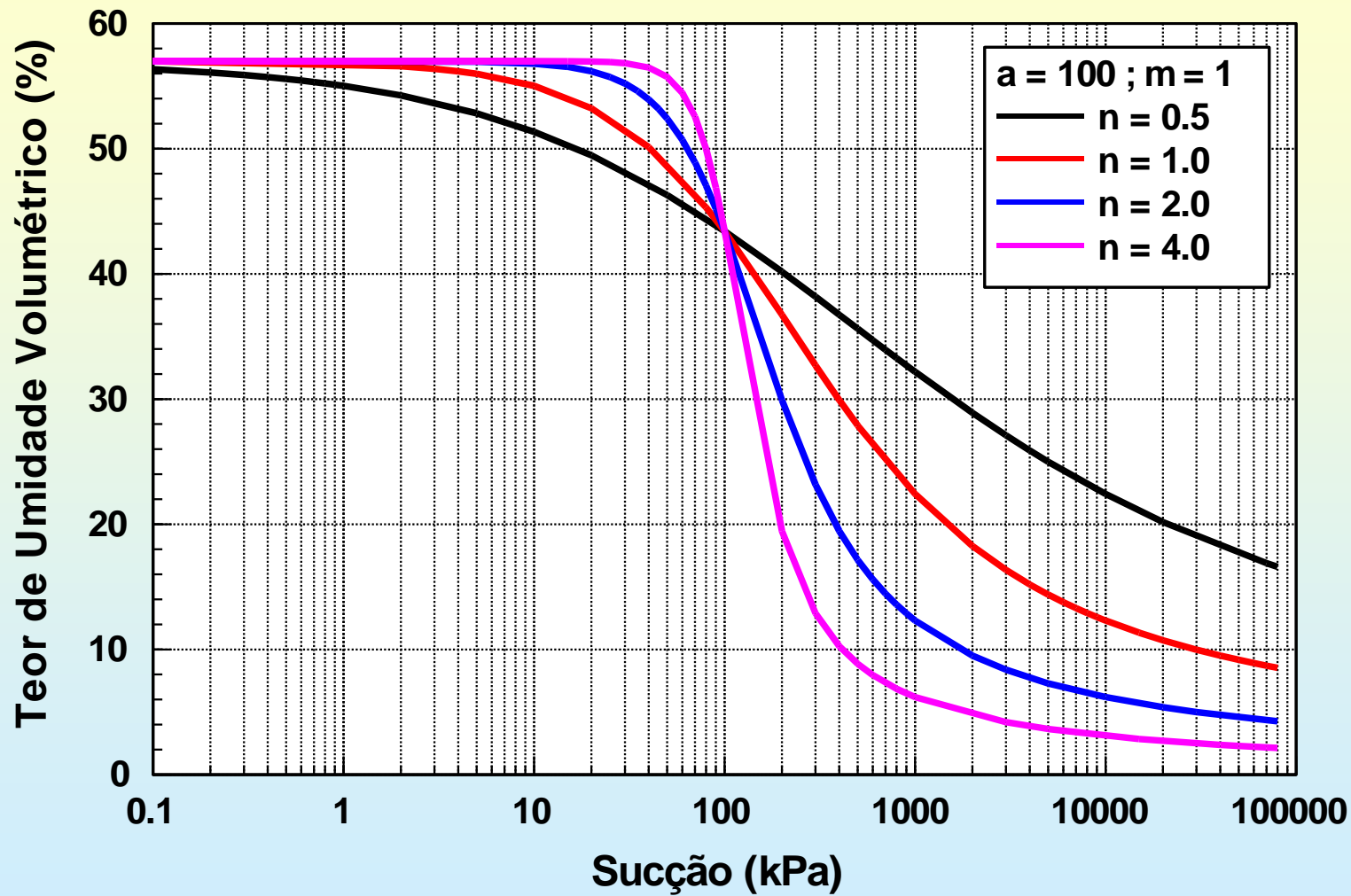
# Fredlund & Xing (1994)

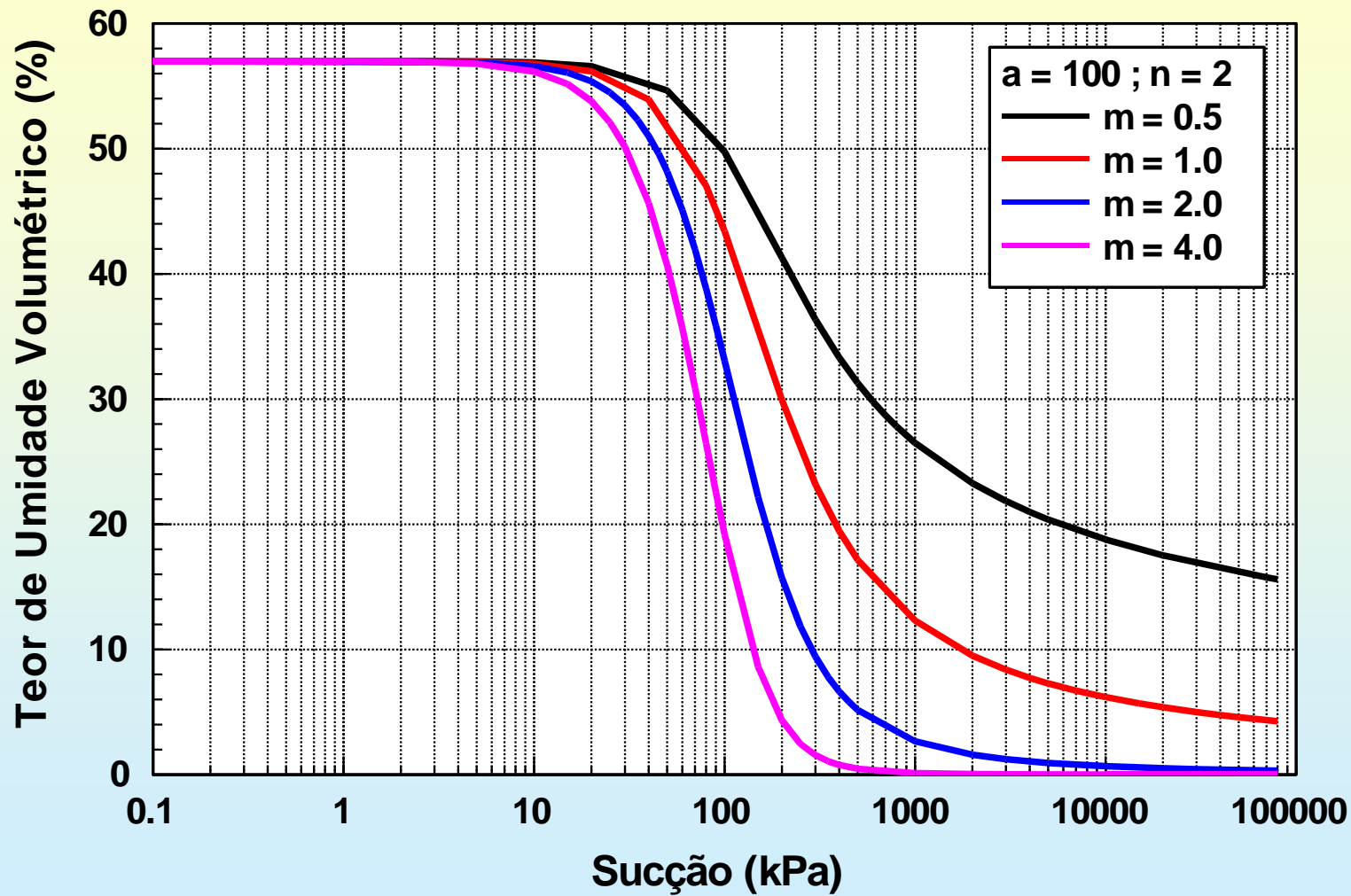
$$\theta = C(\psi) \frac{\theta_s}{\left\{ \ln \left[ e + \left( \frac{\psi}{a} \right)^n \right] \right\}^m}$$

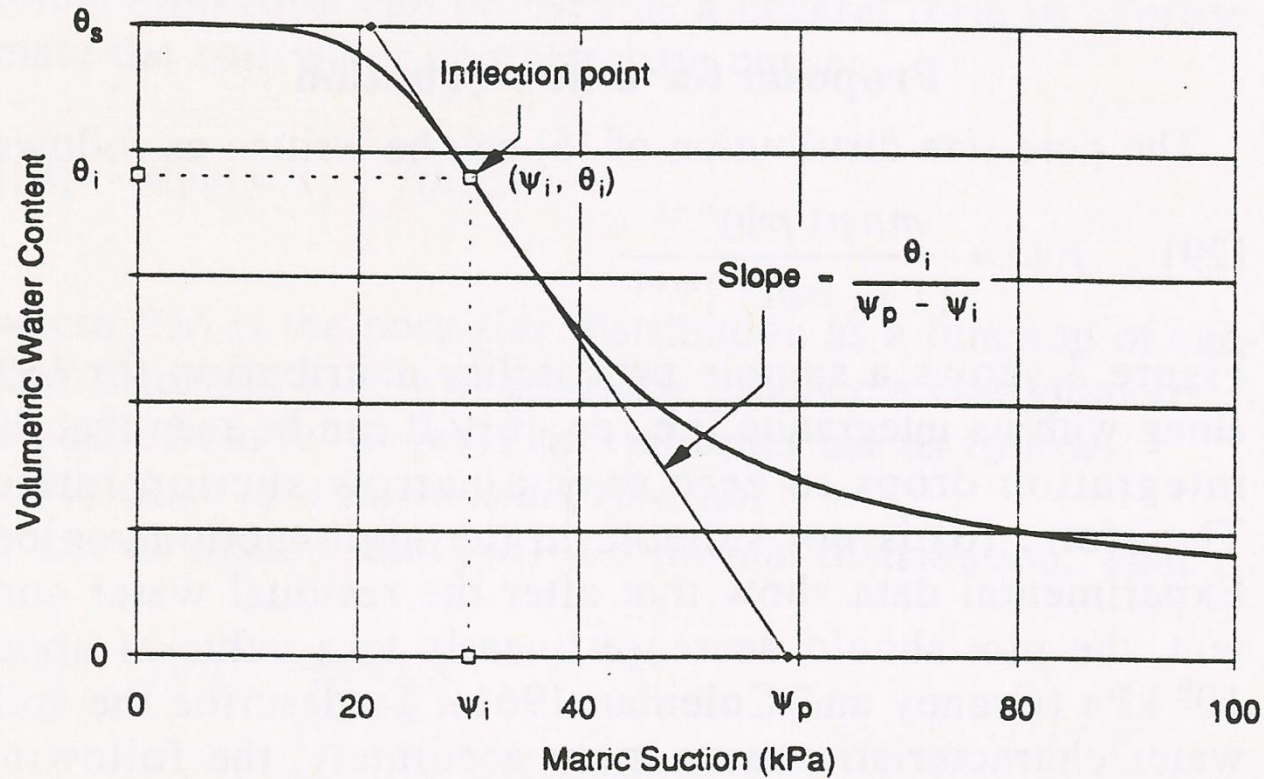
$$C(\psi) = 1 - \frac{\ln \left( 1 + \frac{\psi}{\psi_r} \right)}{\ln \left[ 1 + \left( \frac{1000000}{\psi_r} \right) \right]}$$











$$a = \psi_i$$

$$m = 3.67 \ln \left( \frac{\theta_s}{\theta_i} \right)$$

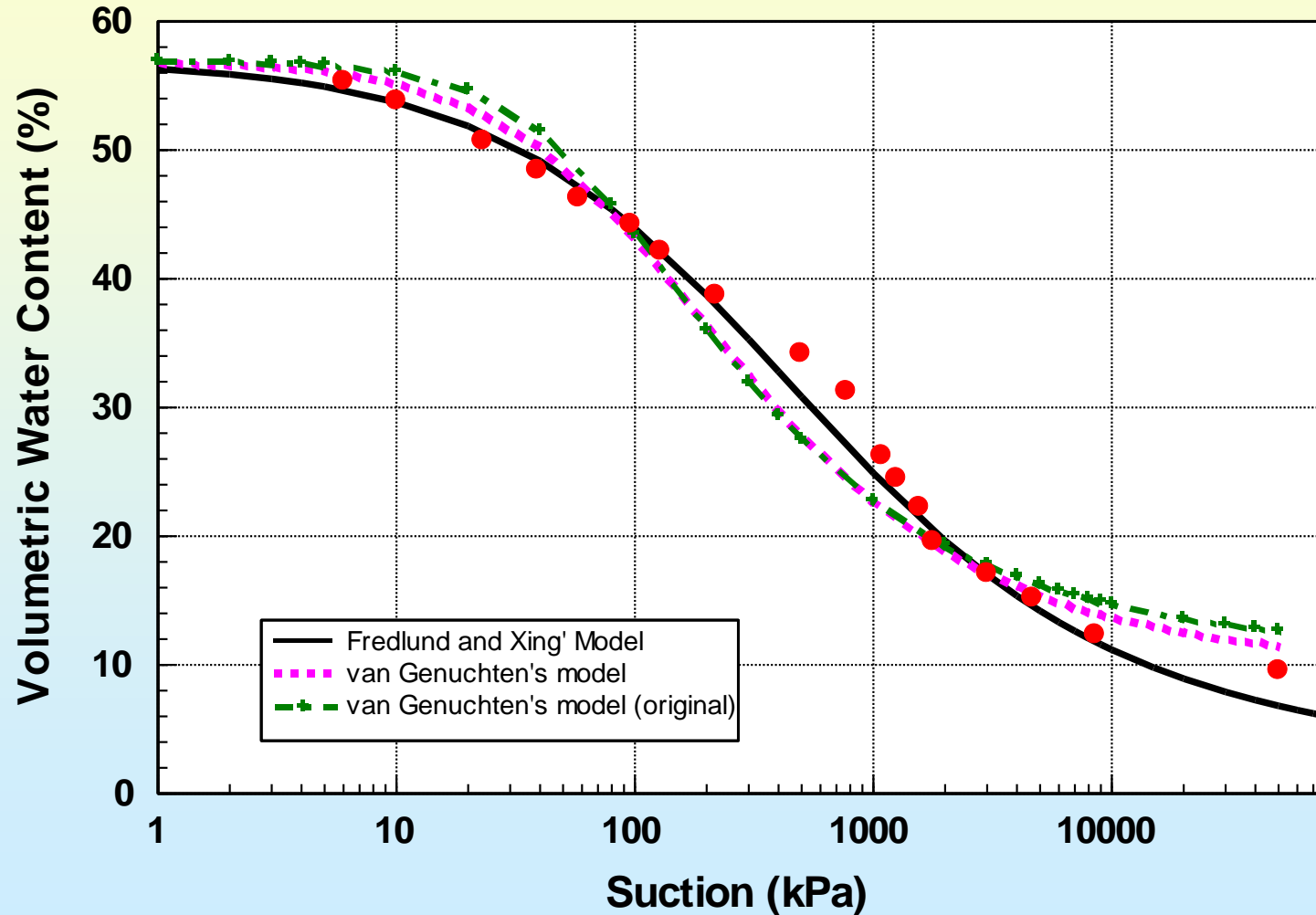
$$n = \frac{1.31^{m+1}}{m\theta_s} 3.72s\psi_i$$

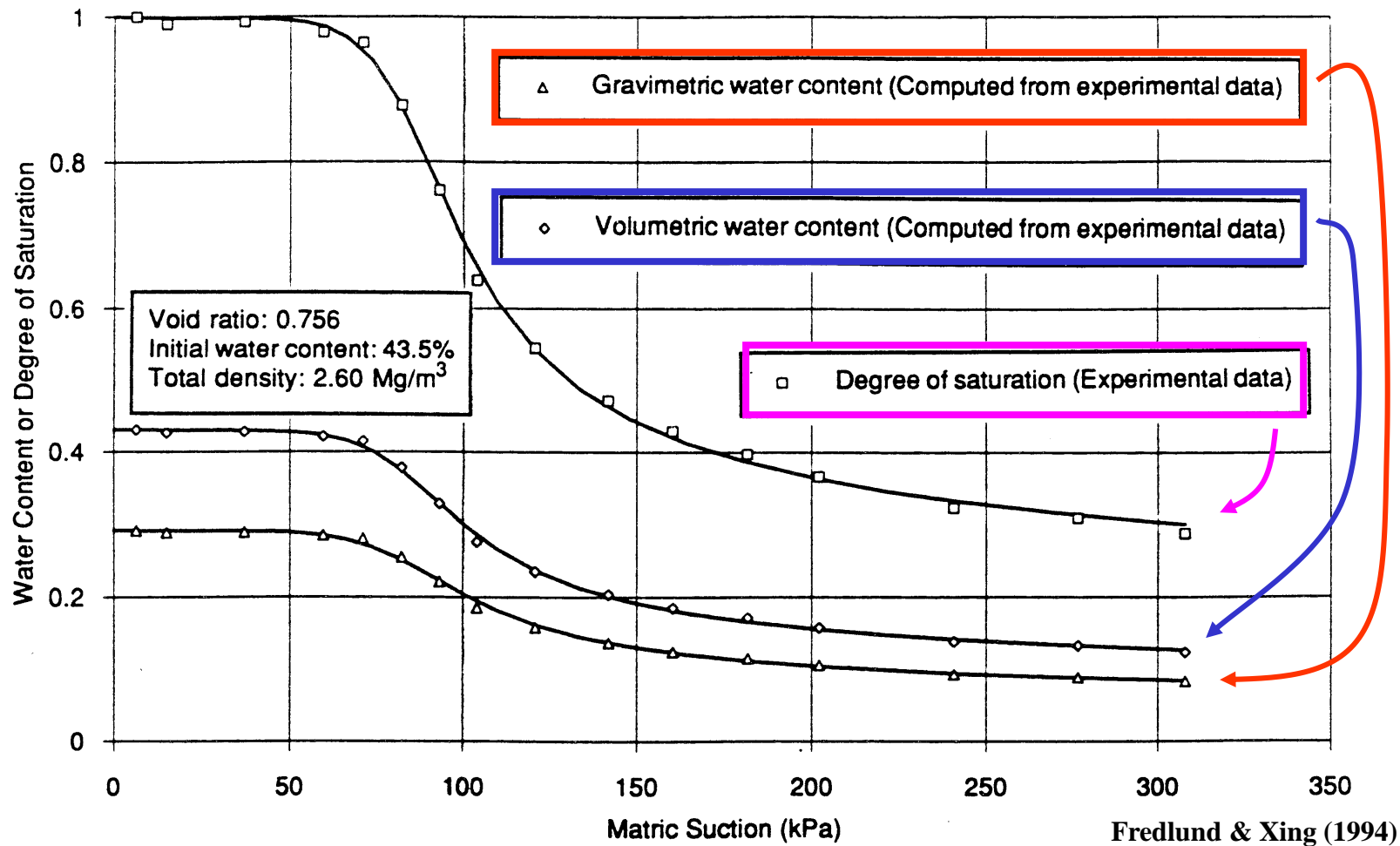
$$s = \frac{\theta_i}{\psi_p - \psi_i}$$

Fredlund and Xing' Model	
Saturated vol. water content (%)	57
a =	250
m =	1.6
n =	0.7

van Genuchten's model	
Teta r =	10
Teta m =	57
alfa =	0.01
m =	0.5
n =	1.1

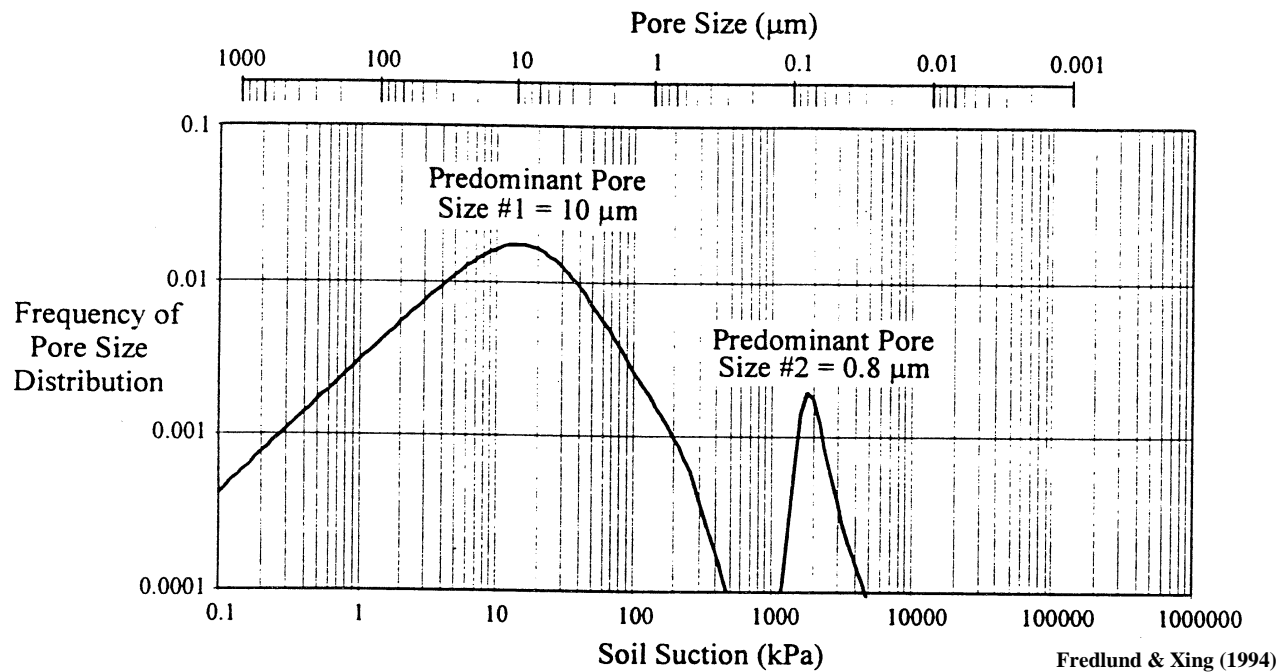
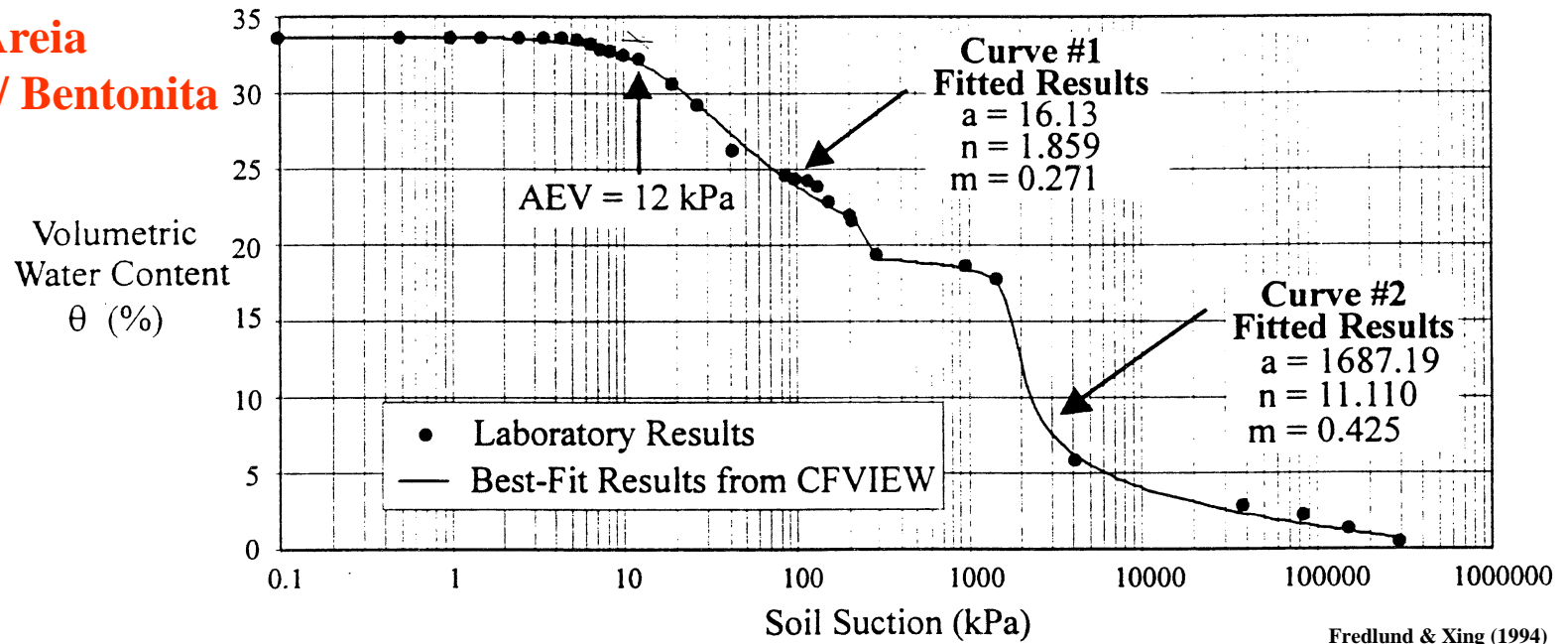
van Genuchten's model (original)	
Teta r =	11
Teta m =	57
alfa =	0.015
m = 1-1/n	0.333333
n =	1.5

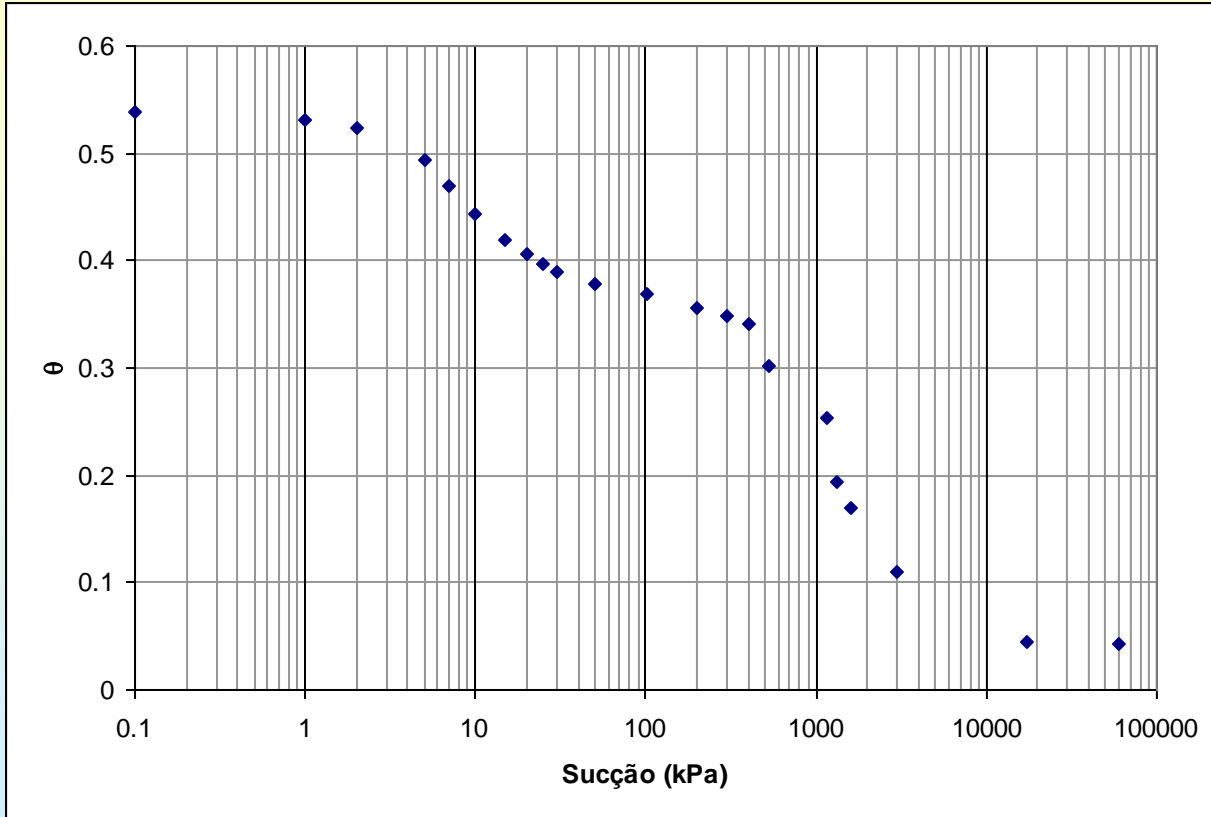




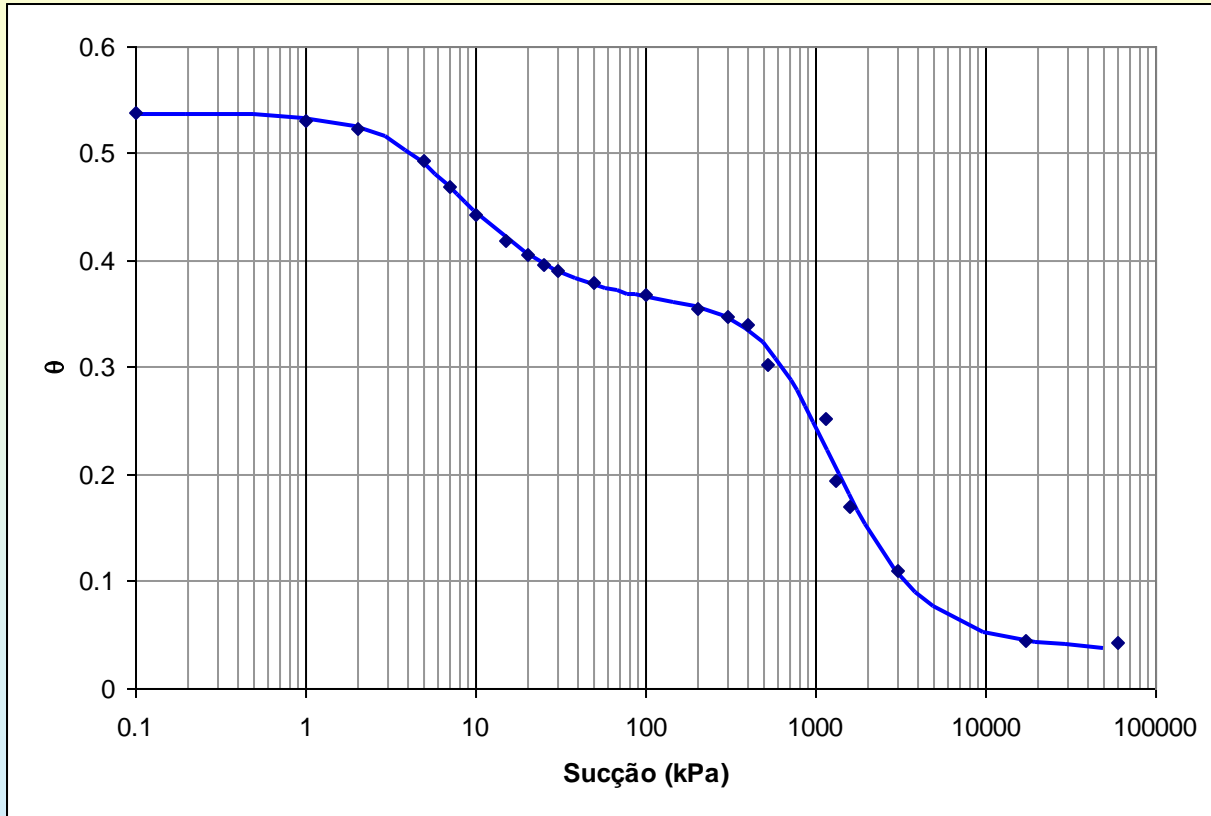
*Dados de Brooks & Corey (1964)*

# Areia c/ Bentonita









## Parâmetros de Ajuste

$\alpha_1$	0.17699	1/kPa
$n_1$	1.95854	

$\alpha_2$	0.00105	1/kPa
$n_2$	2.24122	

$m_1$	0.48942
$w_1$	0.36118

$m_2$	0.55381
$w_2$	0.63882

$\theta_s$	0.53636
$\theta_R$	0.03584

