

Curva de Retenção

Modelos de Ajuste

Gardner (1958)

Brooks & Corey (1966)

Van Genuchten (1980)

Fredlund & Xing (1994)

Objetivo

- A curva de retenção é utilizada nas análises de fluxo em meio não saturado e a sua forma matemática (equações de ajuste) facilitam este uso.
- A curva de retenção é usada para a obtenção da função de permeabilidade dos solos não saturados.
- Tratando-se das funções de permeabilidade, tanto as equações empíricas como os modelos estatísticos fazem uso dos parâmetros das equações de ajuste das curvas de retenção.

Gardner (1958)

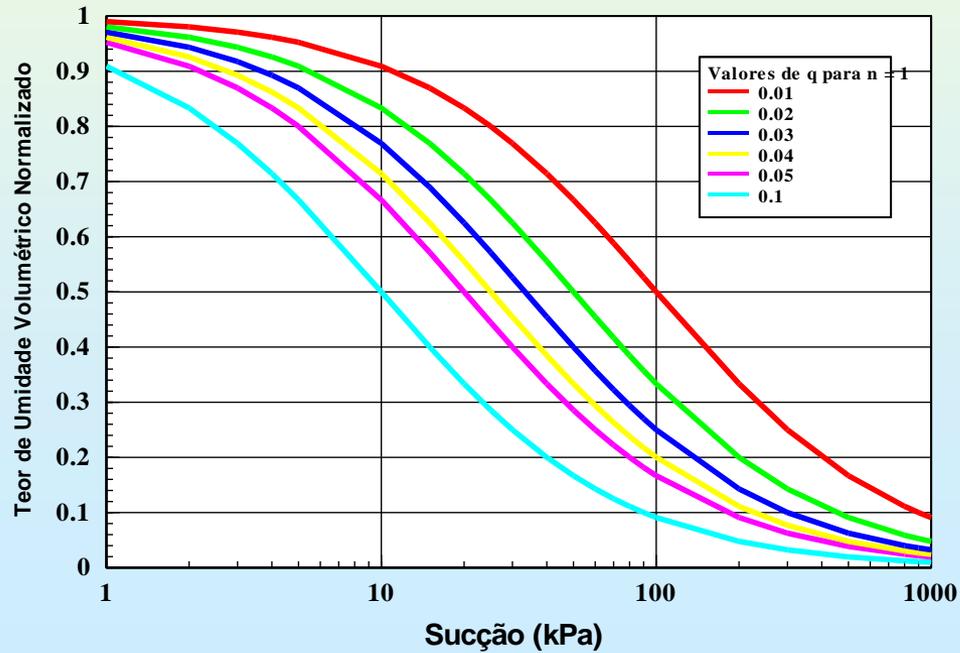
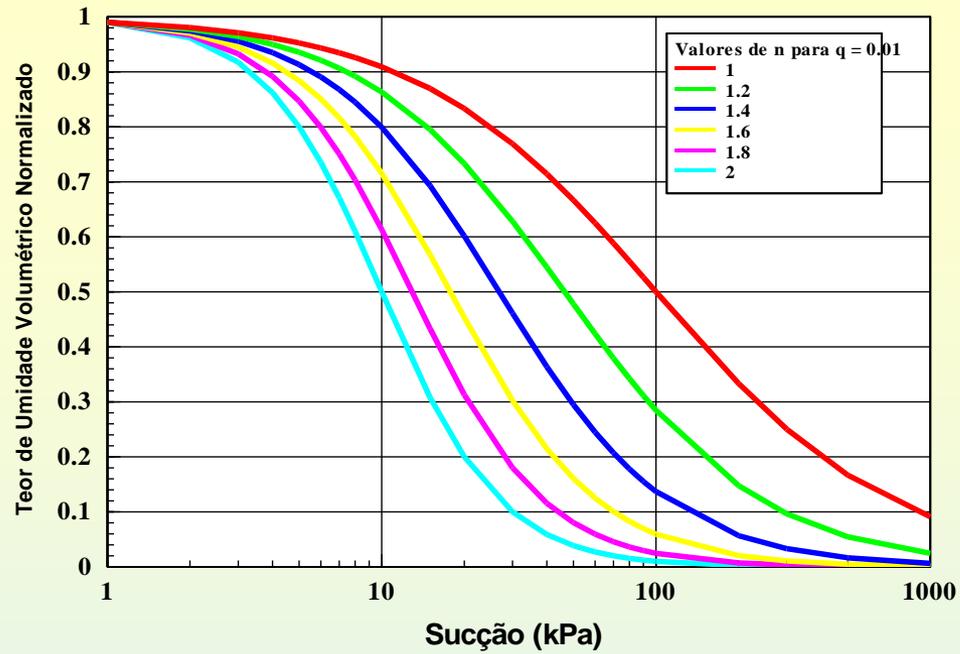
$$\Theta = \frac{1}{1 + q\psi^n}$$

q – parâmetro de ajuste relacionado com sucção de entrada de ar

n - parâmetro de ajuste relacionado com a inclinação no ponto de inflecção da curva de retenção

Gardner (1958)

$$\Theta = \frac{1}{1 + q\psi^n}$$

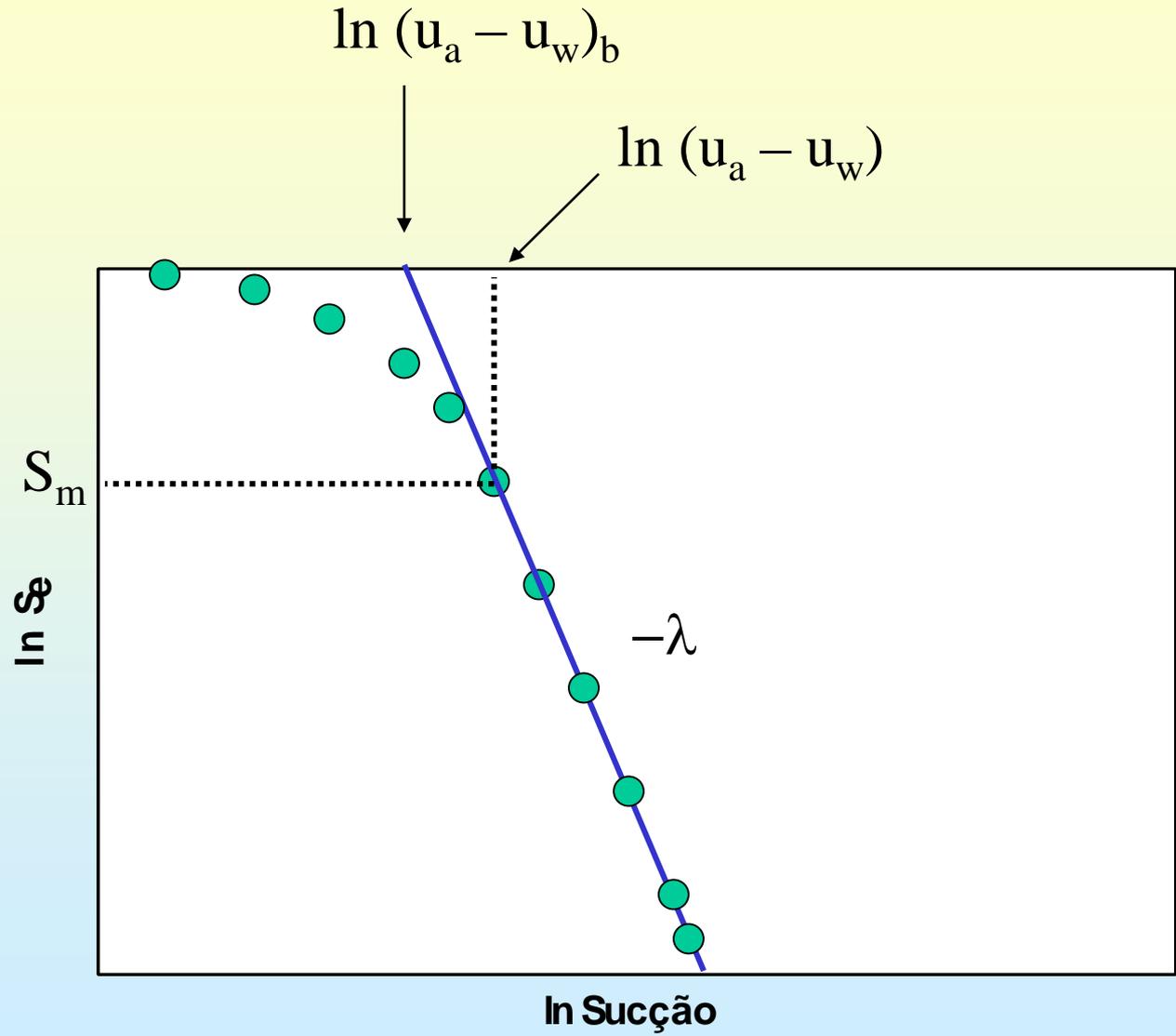


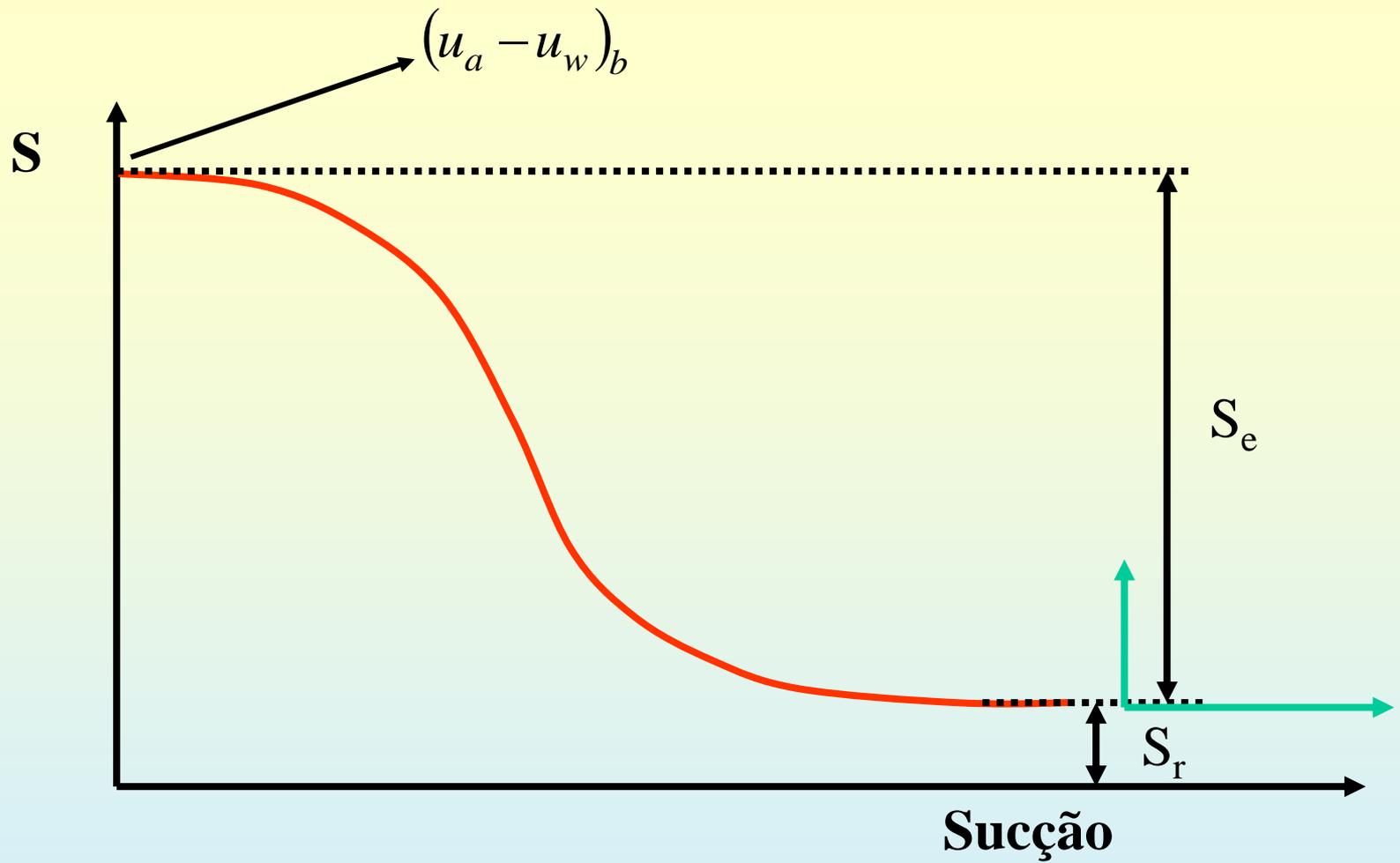
Brooks & Corey (1966)

$$S_e = \frac{S - S_r}{1 - S_r} = \left(\frac{(u_a - u_w)_b}{(u_a - u_w)} \right)^\lambda \quad \text{para } (u_a - u_w) \geq (u_a - u_w)_b$$

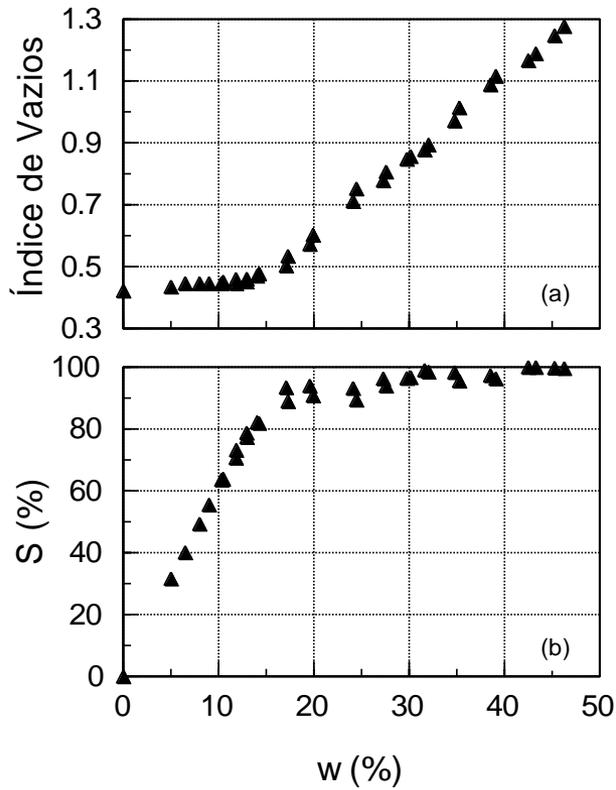
- Brooks & Corey observaram que se fossem omitidos os dados para graus de saturação maiores que aproximadamente 85% os dados se apresentavam alinhados em uma reta, quando plotados em termos de $\log S_e$ e \log da sucção.
- O valor de S_r tem papel importante no ajuste. Em geral este valor é determinado de modo a fornecer o melhor ajuste.
- Inicialmente obtida para rochas porosas
- Aplicável a solos homogêneos
- Os parâmetros são obtidos por ajuste ao dados de sucção e saturação.

$$S_e = \frac{S - S_r}{1 - S_r} = \left(\frac{(u_a - u_w)_b}{(u_a - u_w)} \right)^\lambda \text{ para } (u_a - u_w) \geq (u_a - u_w)_b$$

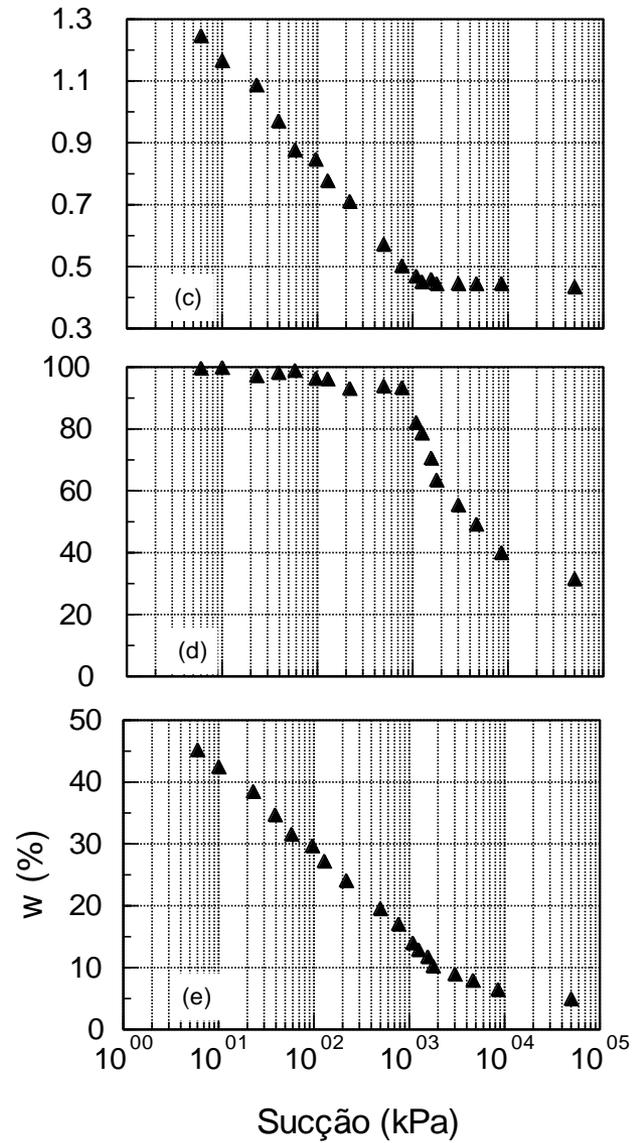


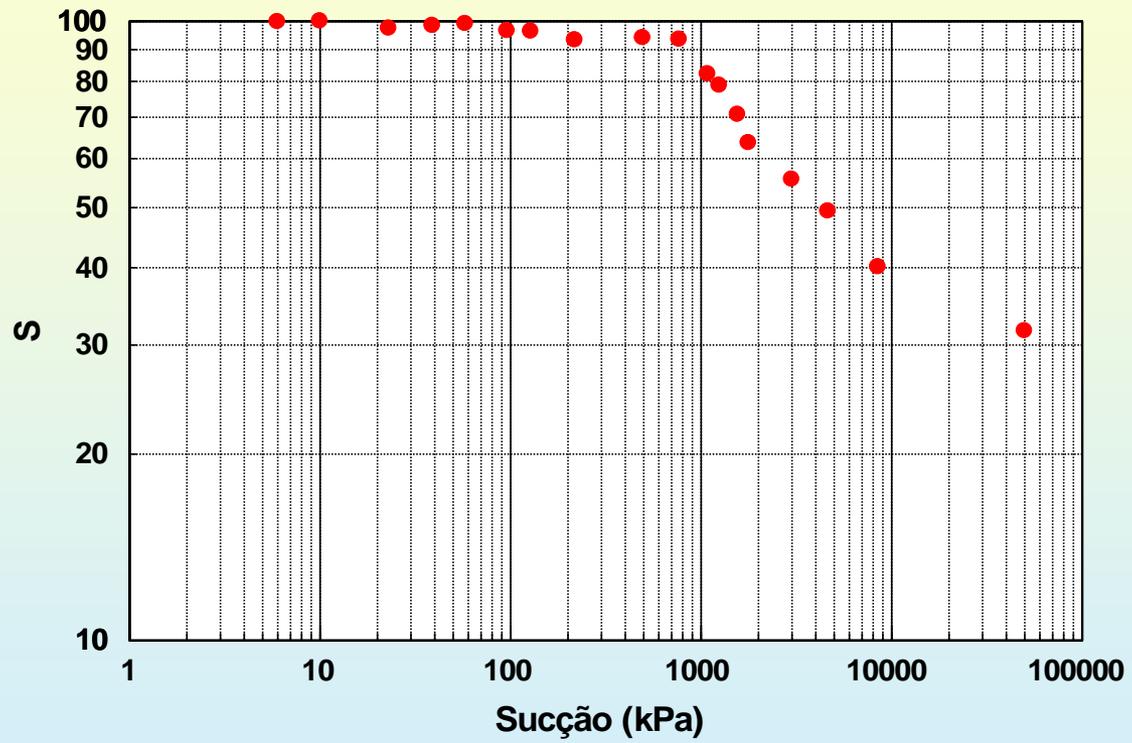


$$S_e = \frac{S - S_r}{1 - S_r} = \left(\frac{(u_a - u_w)_b}{(u_a - u_w)} \right)^\lambda$$



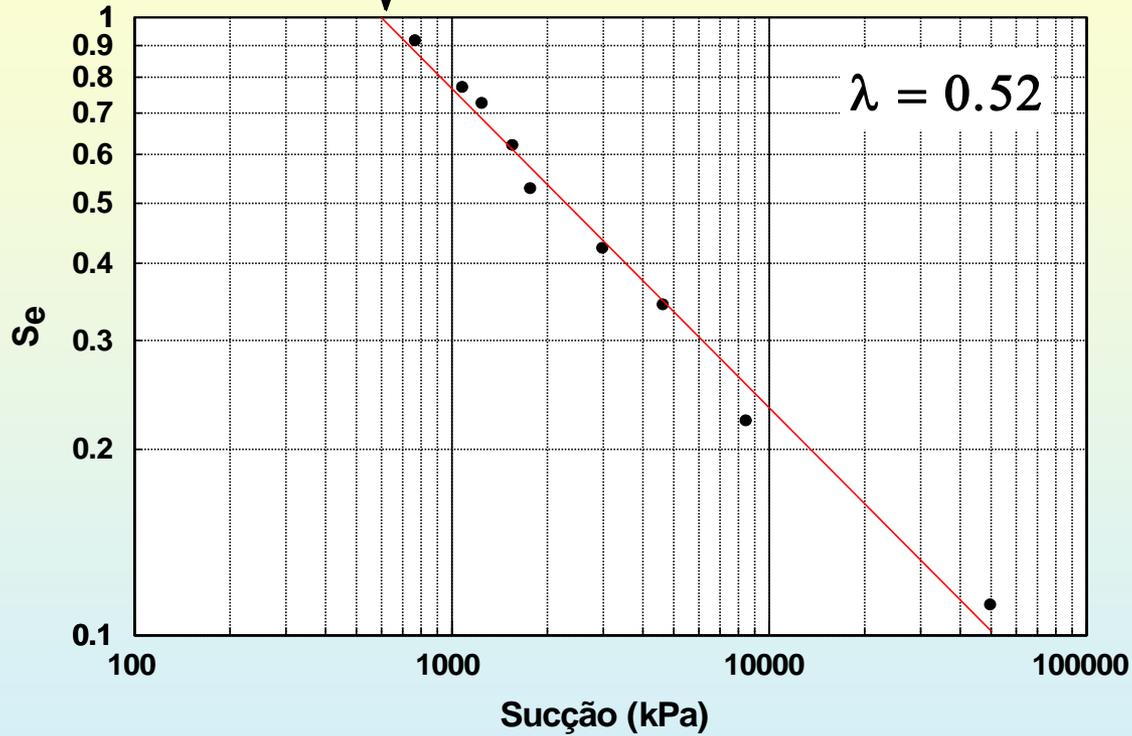
Argila de Londres (lama)
 ▲ EXEMPLO





$$(u_a - u_w)_b = 595 \text{ kPa}$$

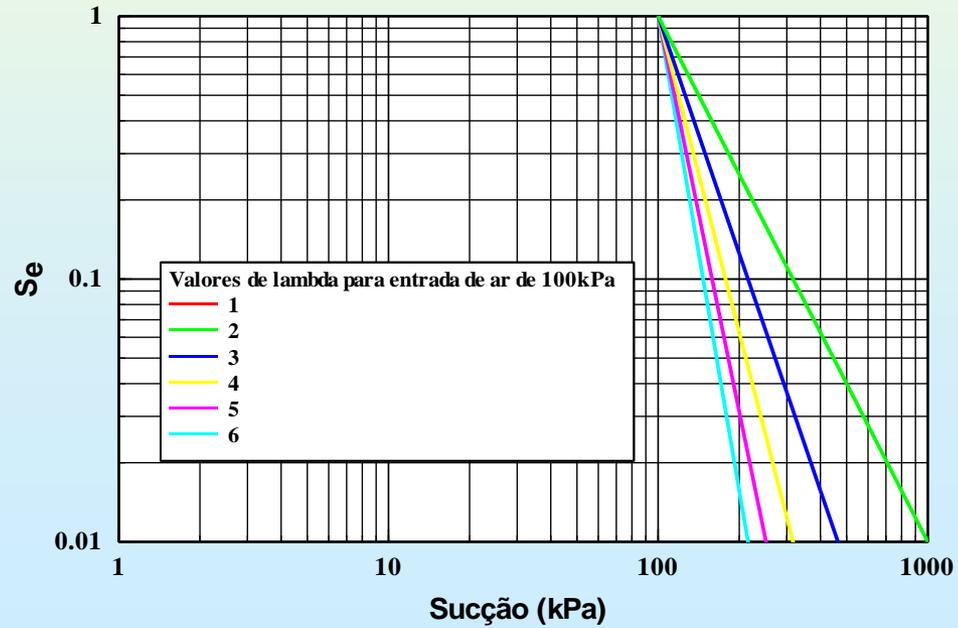
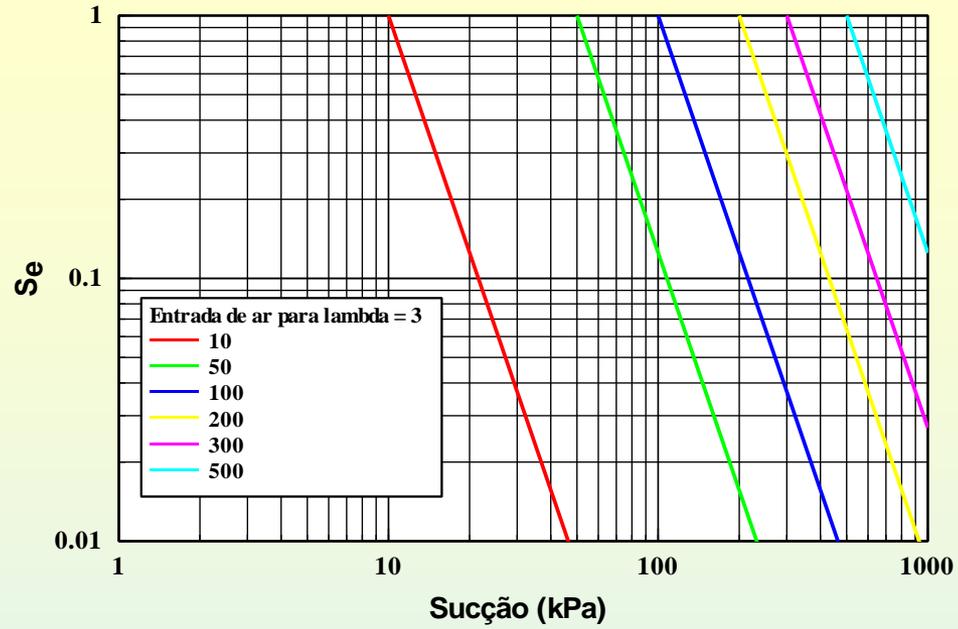
$$S_r = 23\%$$

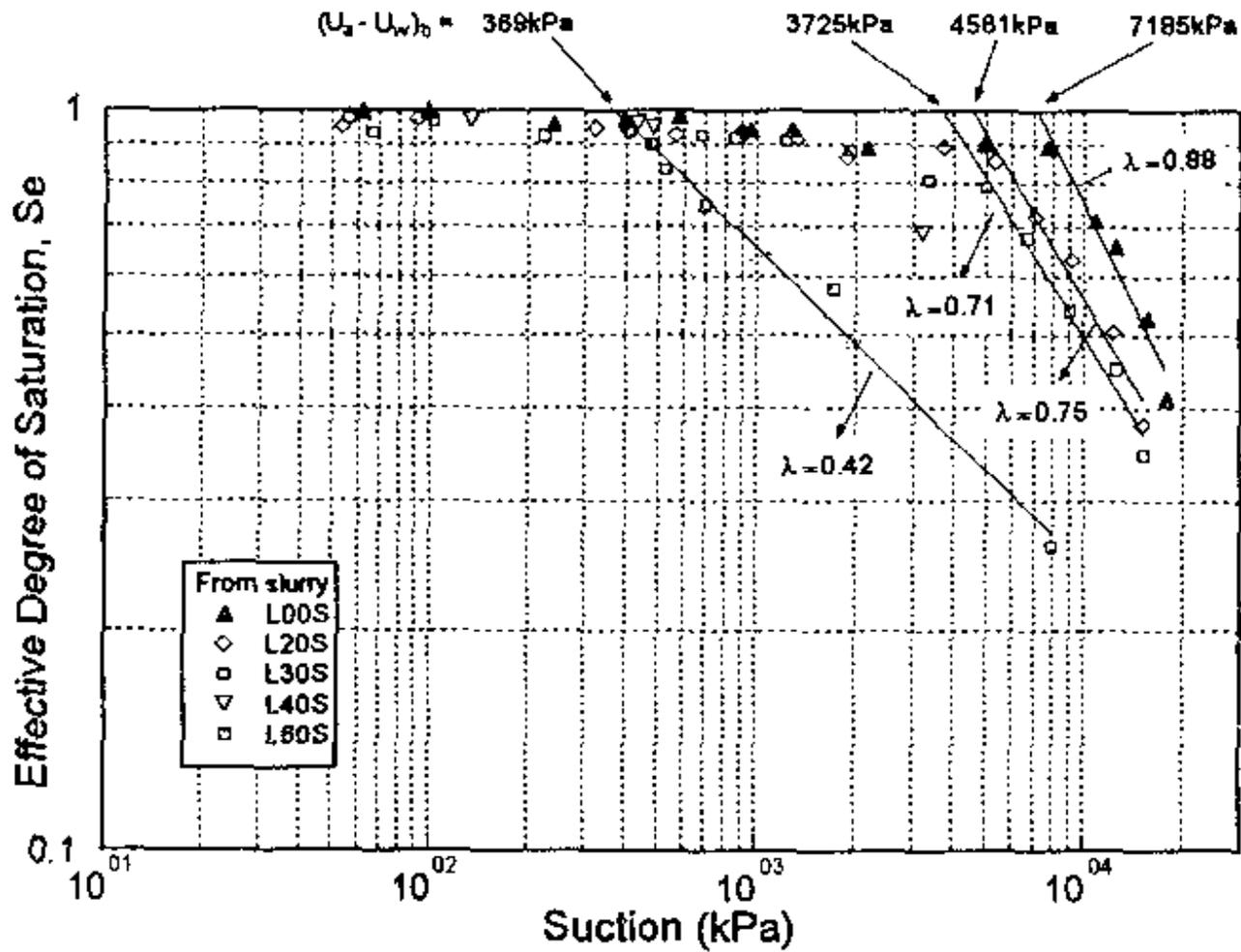


$$S_e = \frac{S - S_r}{1 - S_r} = \left(\frac{(u_a - u_w)_b}{(u_a - u_w)} \right)^\lambda$$

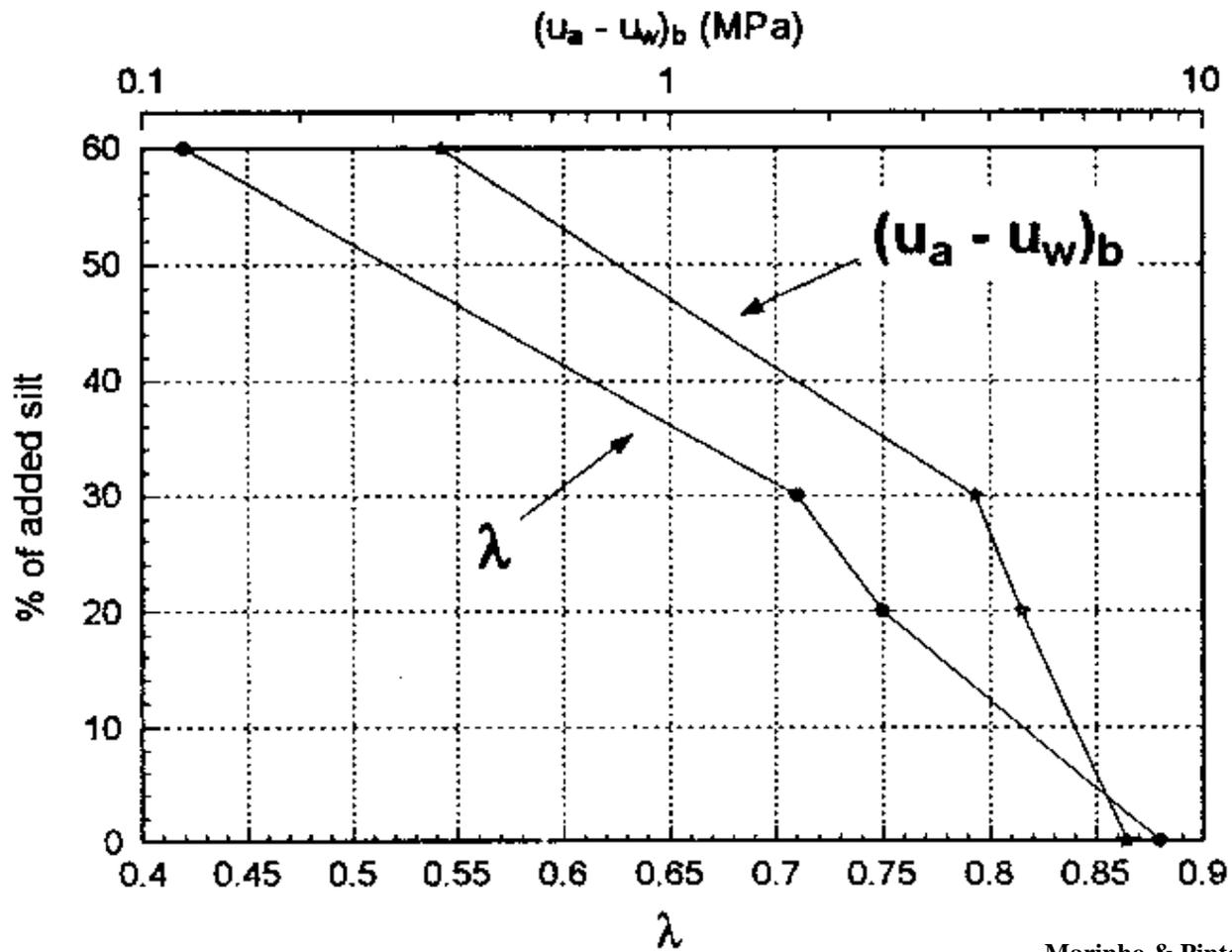
Brooks & Corey (1966)

$$S_e = \frac{S - S_r}{1 - S_r} = \left(\frac{(u_a - u_w)_b}{(u_a - u_w)} \right)^\lambda$$





Marinho & Pinto (1997)



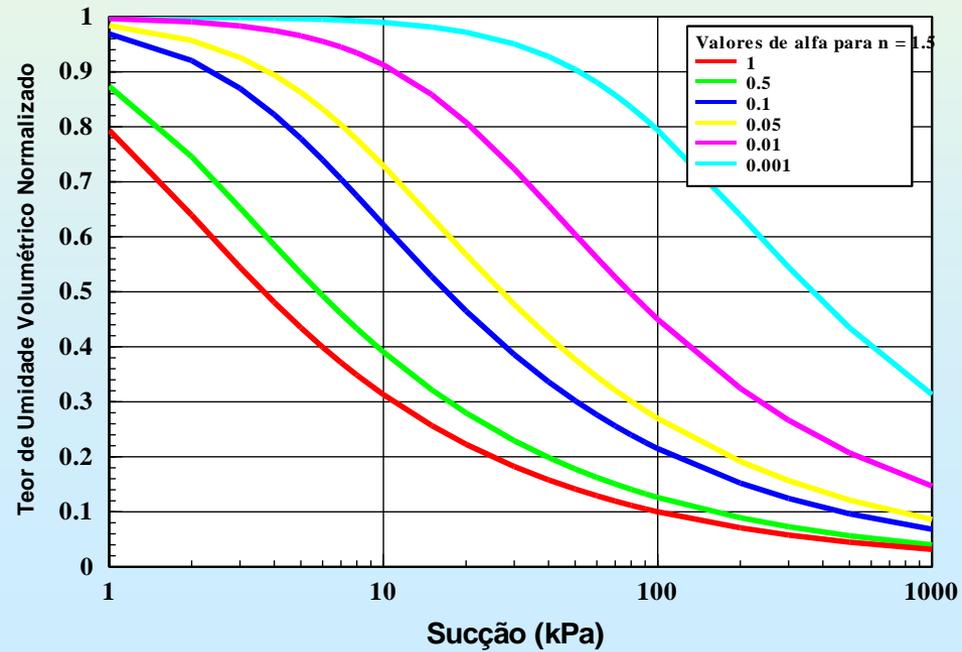
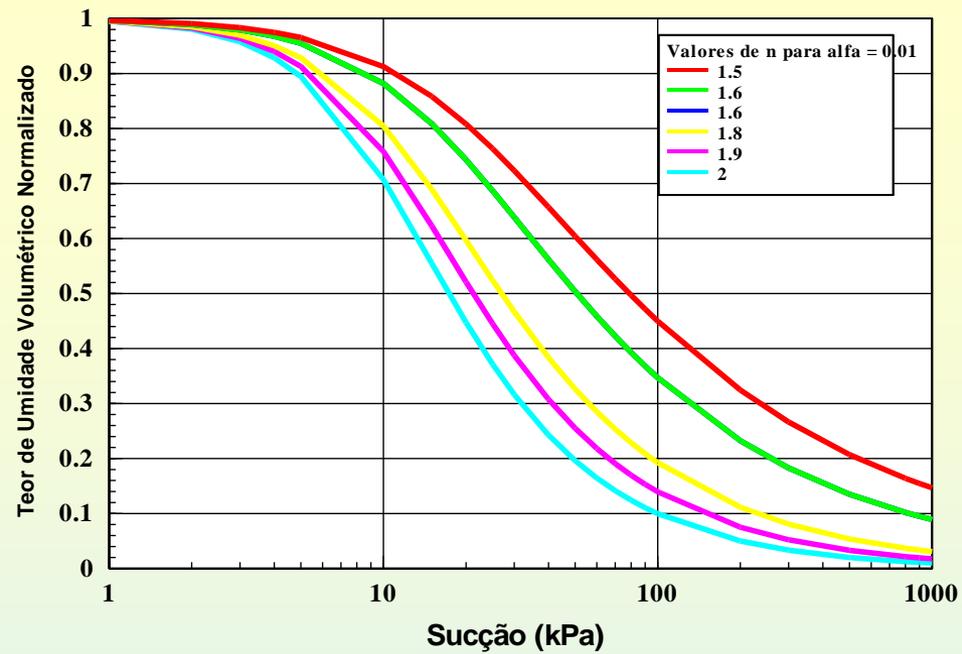
Marinho & Pinto (1997)

Van Genuchten (1980)

$$S_e = \frac{S - S_r}{1 - S_r} = \left(\frac{1}{1 + \alpha(u_a - u_w)^n} \right)^m$$

Van Genuchten (1980)

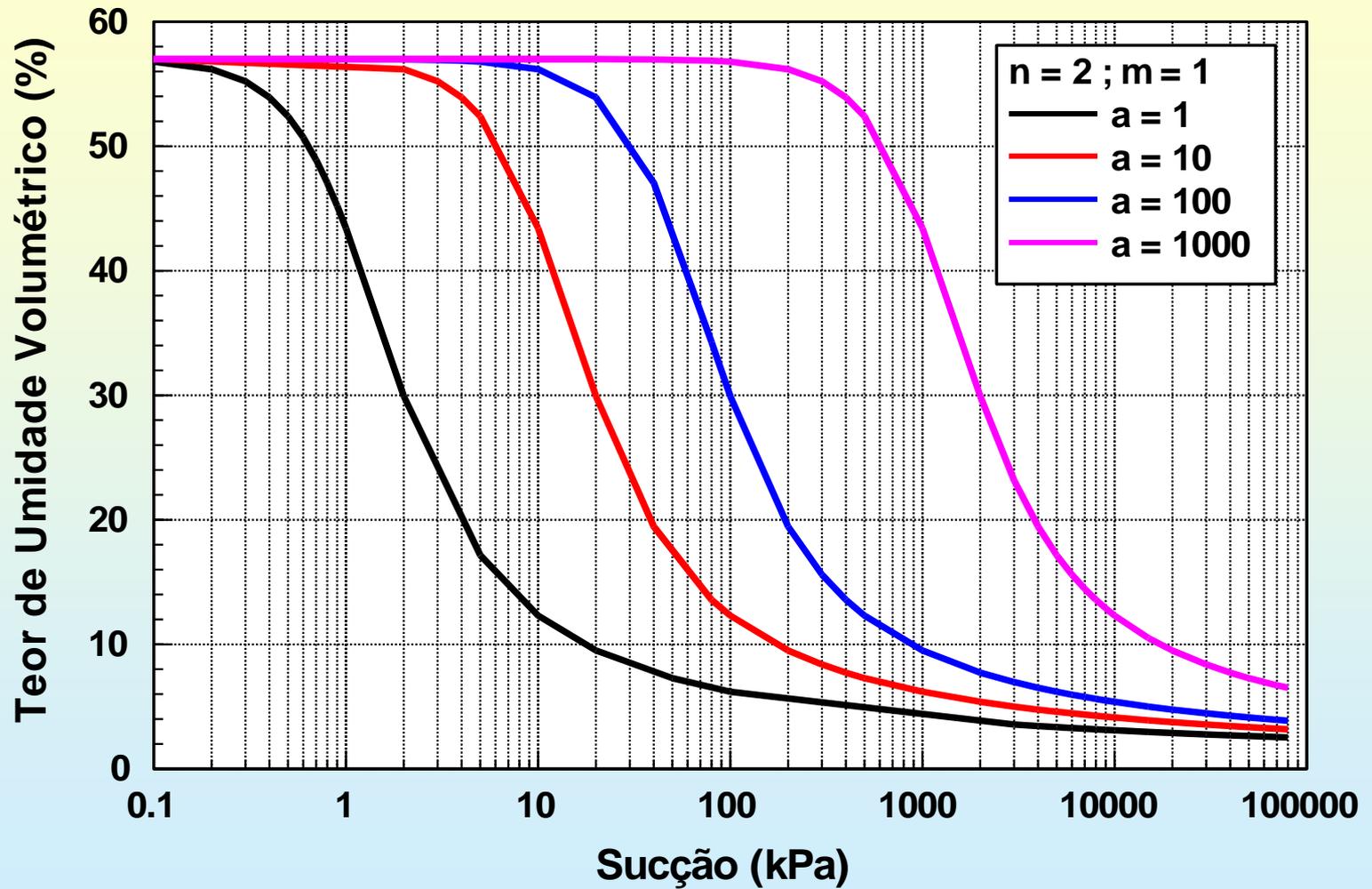
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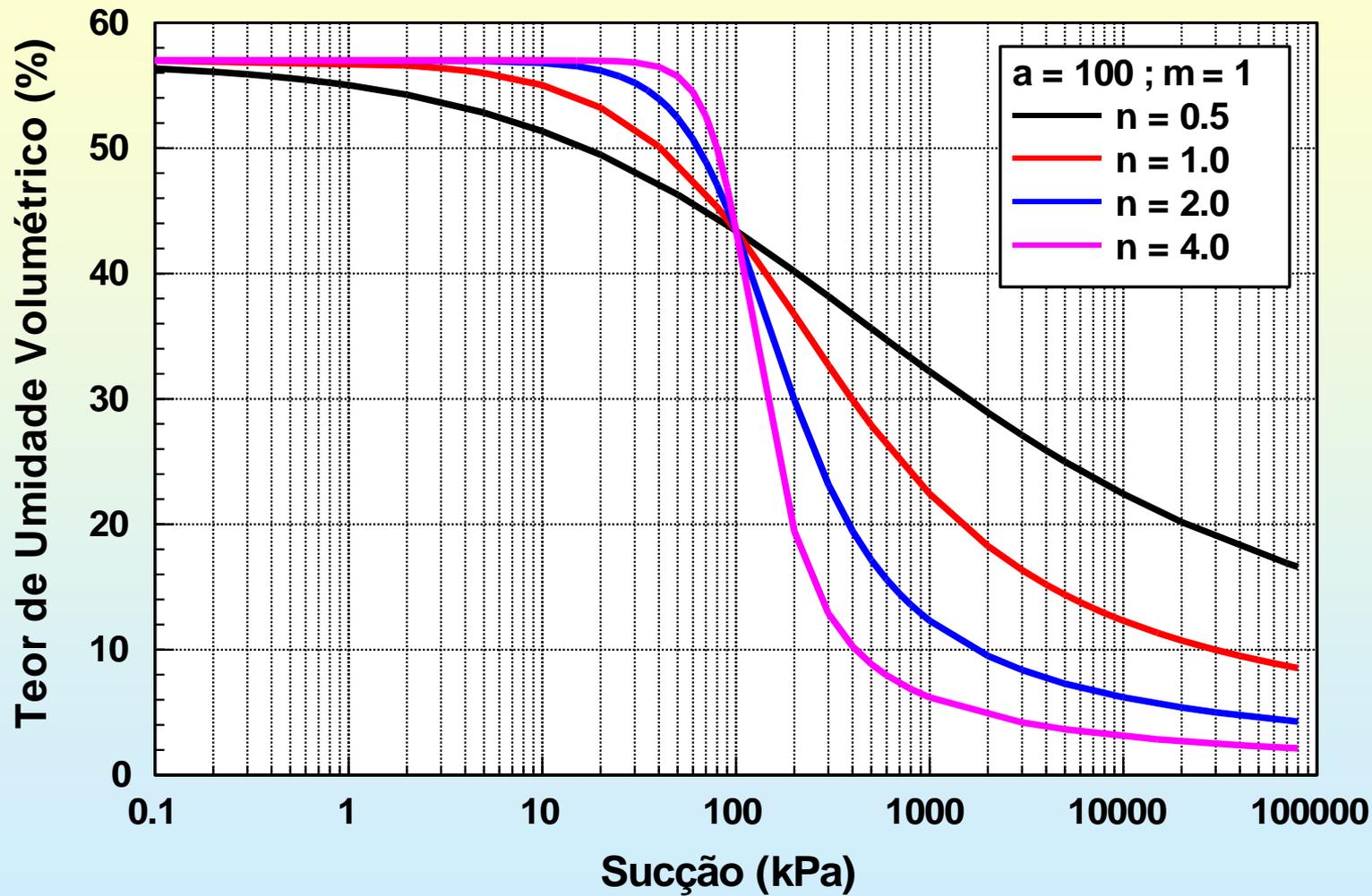


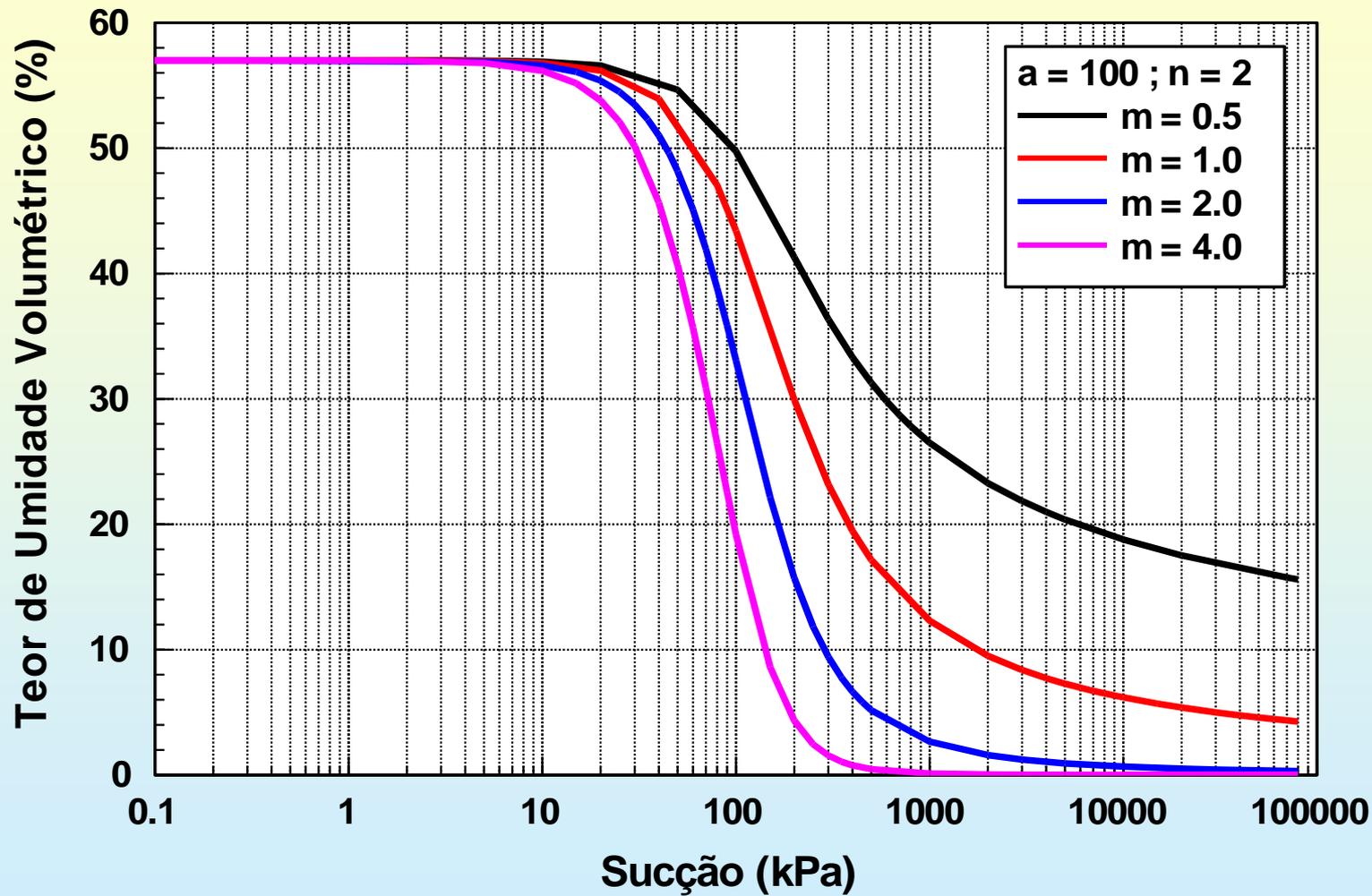
Fredlund & Xing (1994)

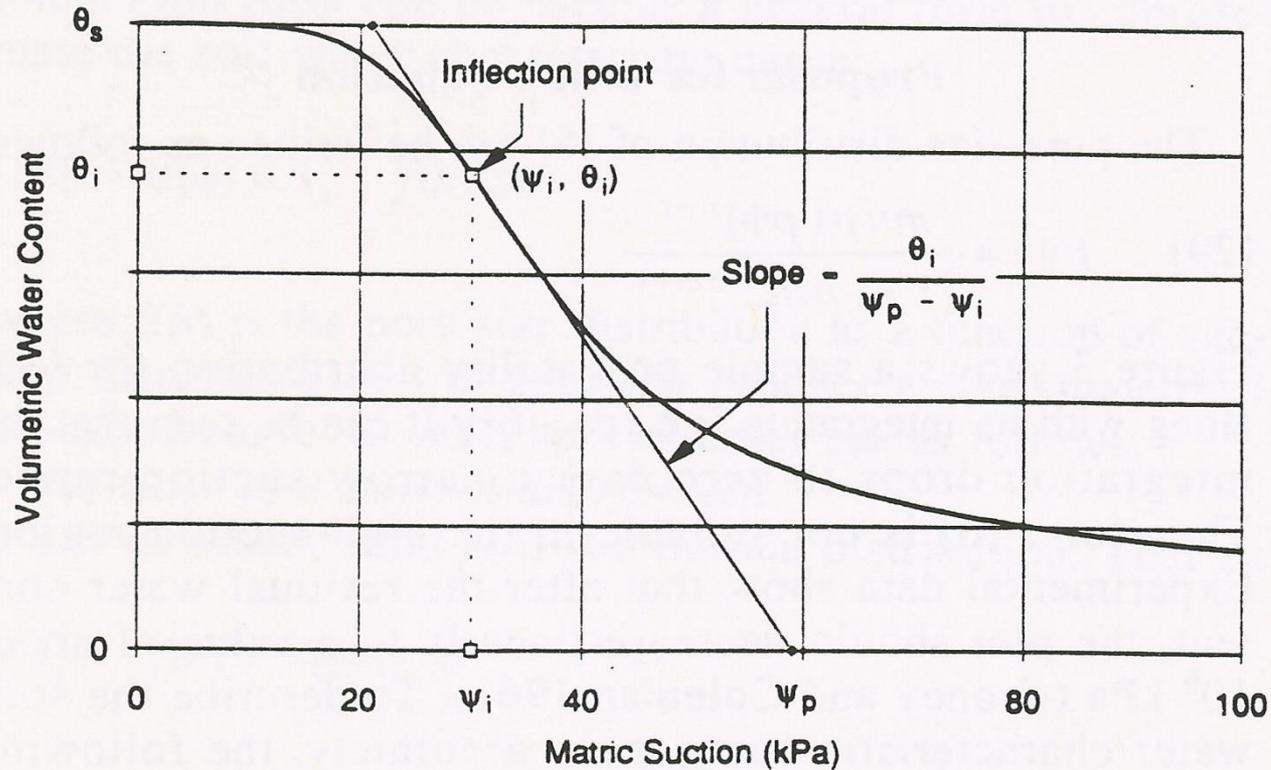
$$\theta = C(\psi) \frac{\theta_s}{\left\{ \ln \left[e + \left(\frac{\psi}{a} \right)^n \right] \right\}^m}$$

$$C(\psi) = 1 - \frac{\ln \left(1 + \frac{\psi}{\psi_r} \right)}{\ln \left[1 + \left(\frac{1000000}{\psi_r} \right) \right]}$$









$$a = \psi_i$$

$$m = 3.67 \ln \left(\frac{\theta_s}{\theta_i} \right)$$

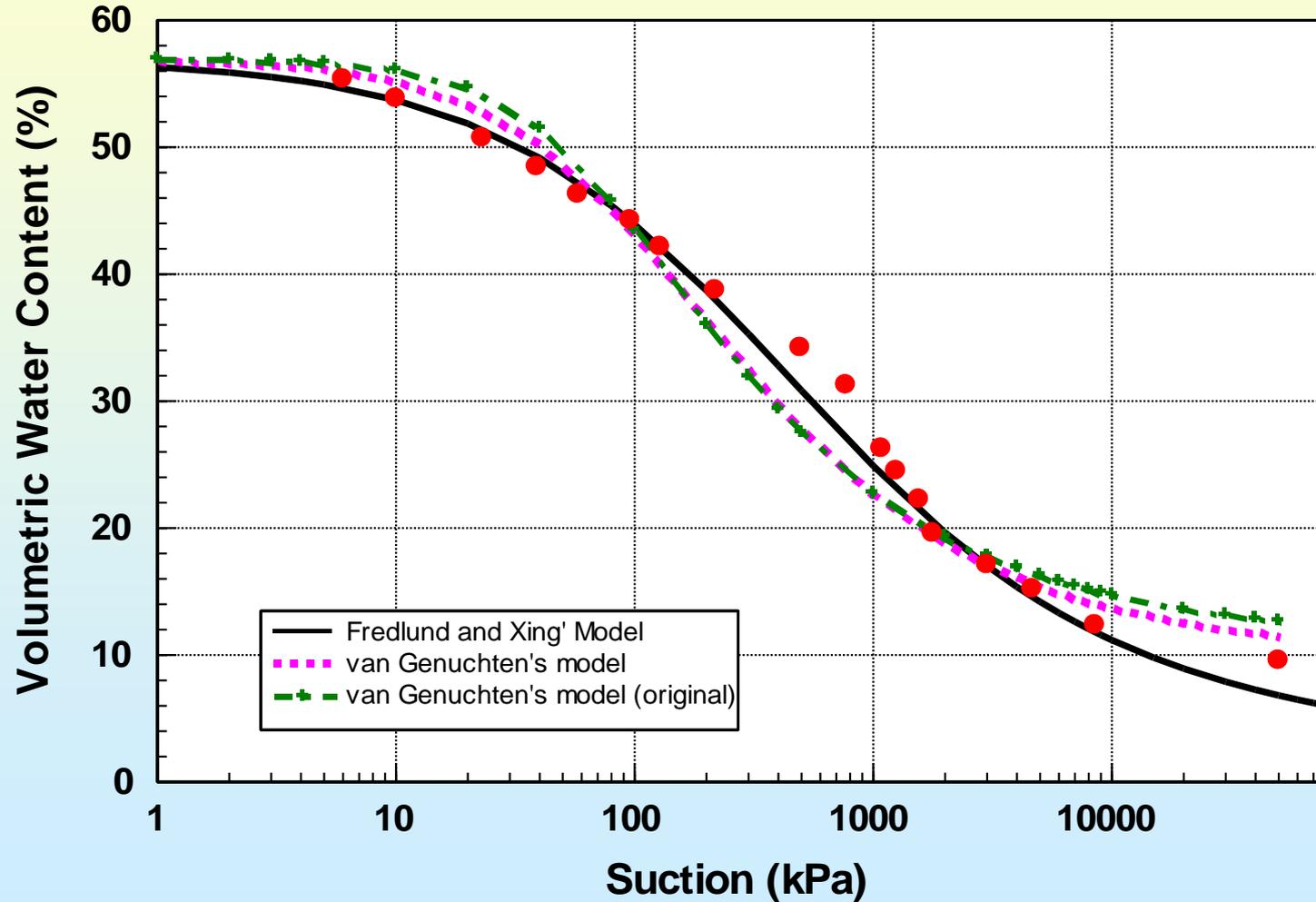
$$n = \frac{1.31^{m+1}}{m\theta_s} 3.72s\psi_i$$

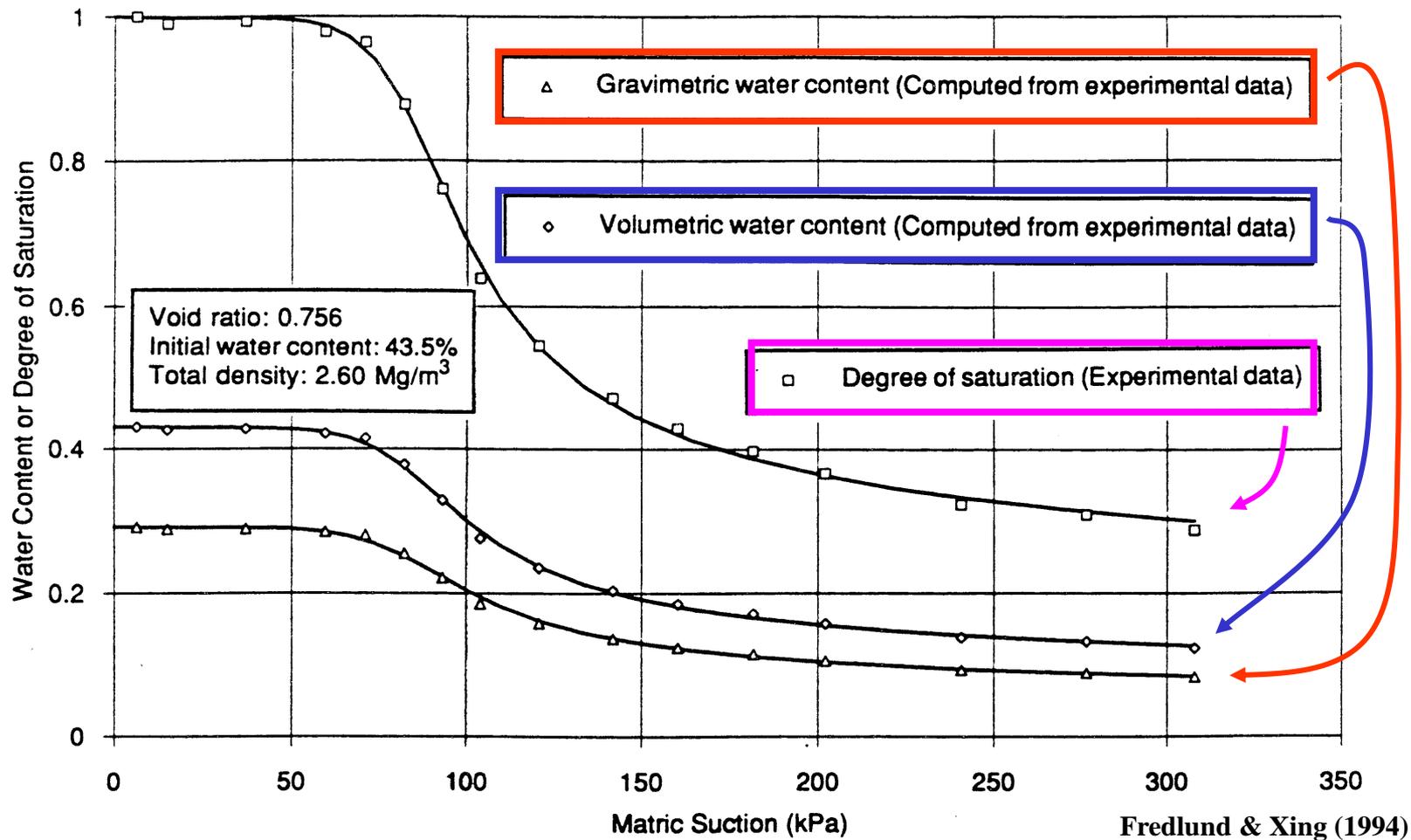
$$s = \frac{\theta_i}{\psi_p - \psi_i}$$

Fredlund and Xing' Model	
Saturated vol. water content (%)	57
a =	250
m =	1.6
n =	0.7

van Genuchten's model	
Teta r =	10
Teta m =	57
alfa =	0.01
m =	0.5
n =	1.1

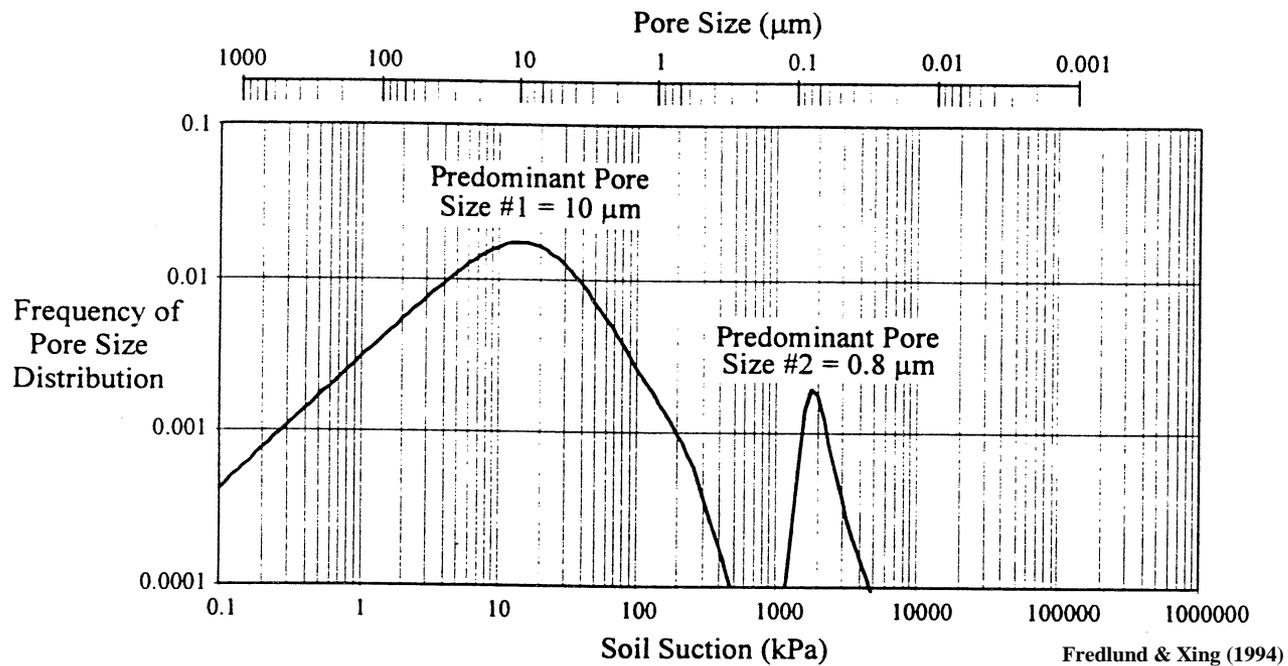
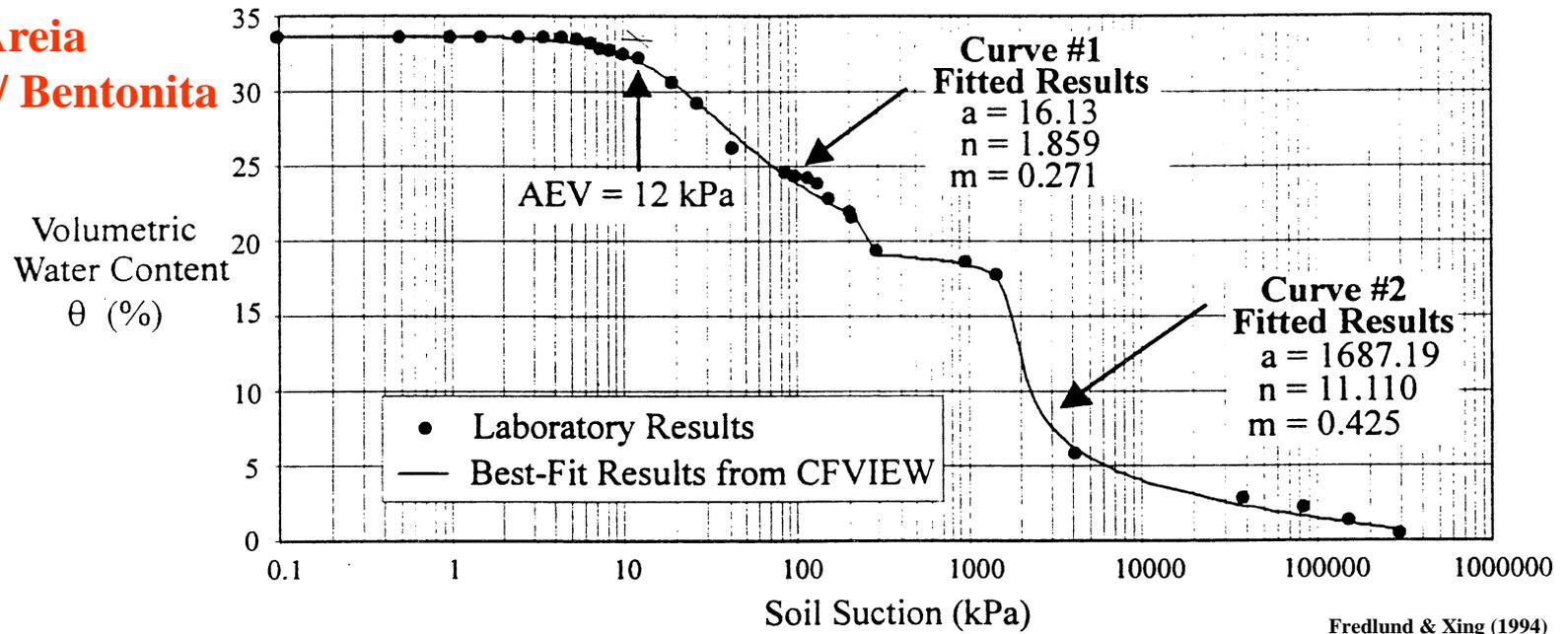
van Genuchten's model (original)	
Teta r =	11
Teta m =	57
alfa =	0.015
m = 1-1/n	0.333333
n =	1.5

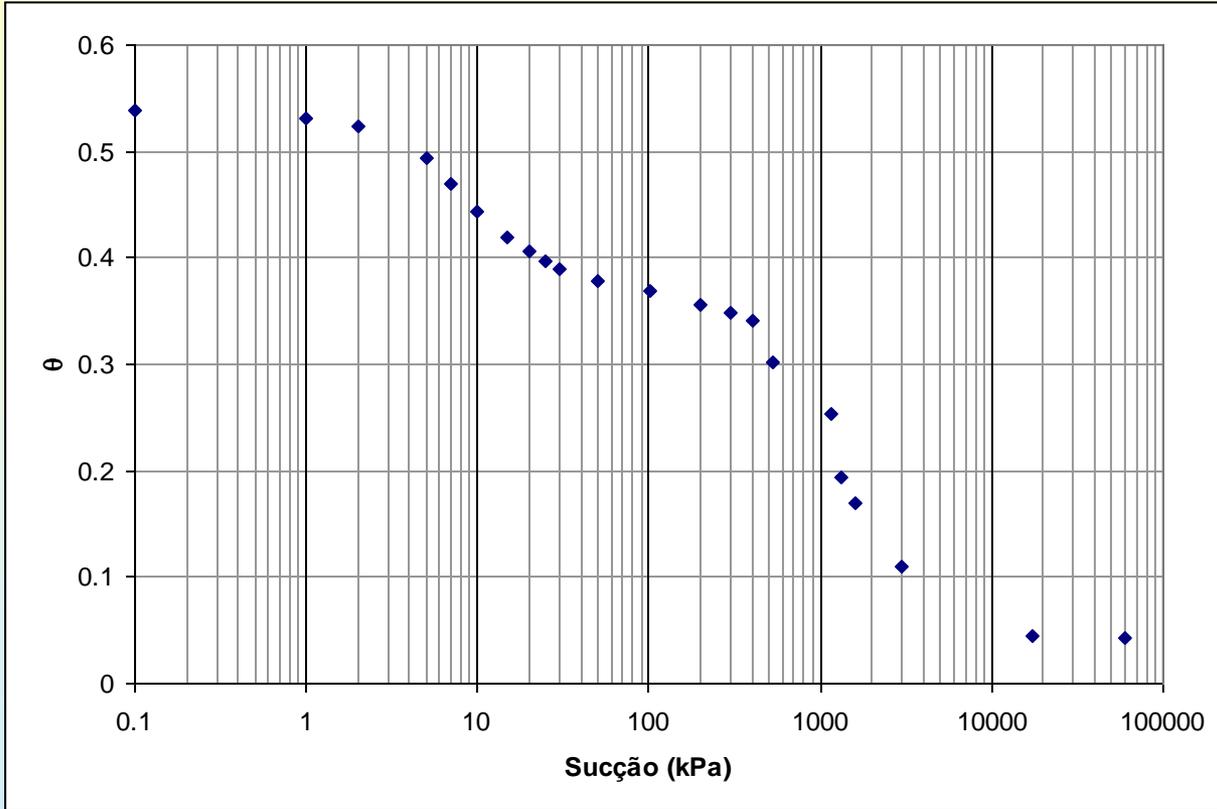


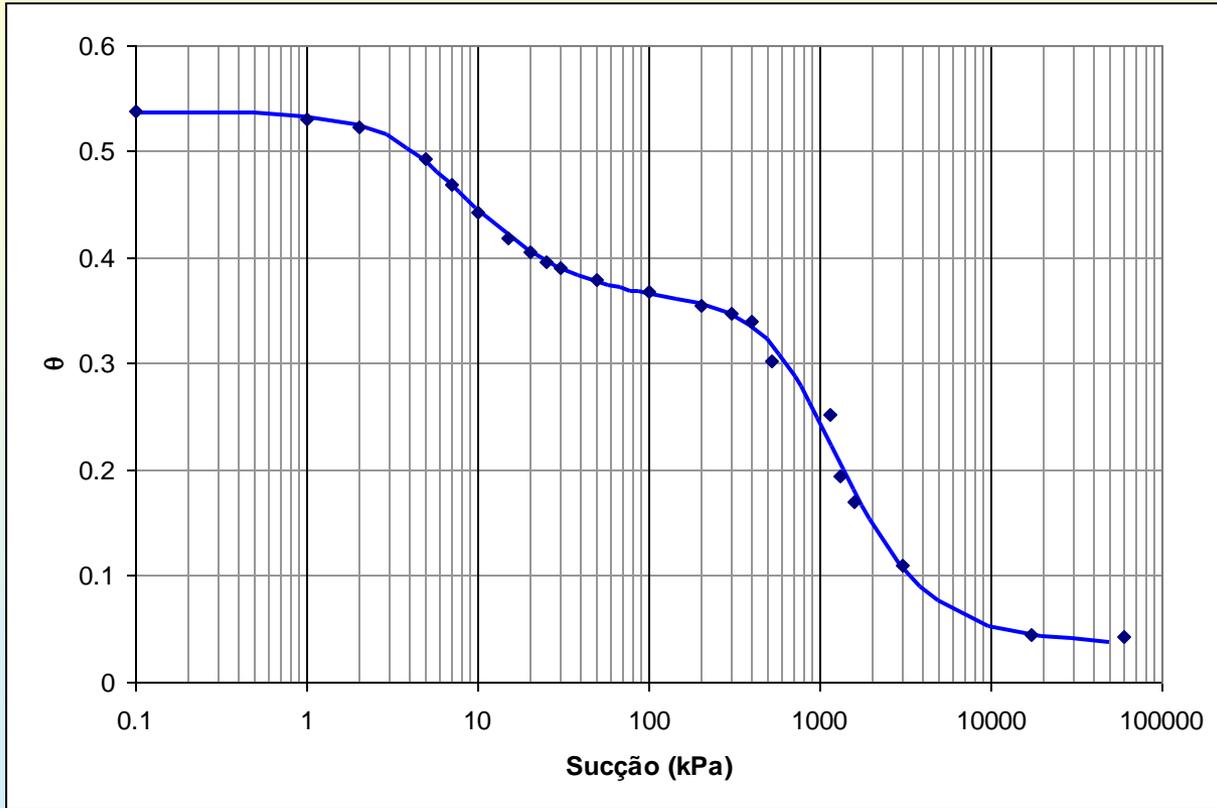


Dados de Brooks & Corey (1964)

Areia c/ Bentonita







Parâmetros de Ajuste

α_1	0.17699	1/kPa
n_1	1.95854	

α_2	0.00105	1/kPa
n_2	2.24122	

m_1	0.48942
w_1	0.36118

m_2	0.55381
w_2	0.63882

θ_s	0.53636
θ_R	0.03584

