

Fadiga de Materiais Estruturais: Fundamentos e Aplicações

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AGENDA

1. *Motivação (Motivation)*
2. *Modos de Falha (Failures Modes)*
3. *Falhas Estruturais por Fadiga (Fatigue Failures)*
4. *Metodologias para Avaliação da Vida à Fadiga (Fatigue Methodologies)*
 - *Carregamento Constante (Constant Amplitude Loading)*
 - $S-N$ } *Initiation*
 - $\epsilon-N$ }
 - $da/dN-\Delta K$ (*Propagation*)

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AGENDA

4. Metodologias para Avaliação da Vida à Fadiga (Fatigue Methodologies)

- Carregamento Constante (Constant Amplitude)
 - S-N
 - ϵ -N
 - $da/dN-\Delta K$
- Efeitos de Entalhes (Notches)
- Carregamento Variável (Variable Amplitude Loading)
 - Contagem de Ciclos (Cycle Counting)
 - Acúmulo de Dano (Damage Summing Methods)
 - Efeitos da Sequência (Sequence Effects)
- Juntas Soldadas (Welded Joints)
- Fadiga Multiaxial (Multiaxial Fatigue)

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O Curso



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AGENDA

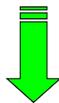
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Motivação

- *Fatores de Segurança Possuem Base Empírica*
- *Cálculo de estruturas é feito com base na experiência previa*



Danos e Defeitos Comprometem a Integridade Estrutural!

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Motivação

- **Integridade Estrutural**

Considera-se que uma estrutura está **íntegra** quando pode suportar os carregamentos de operação com uma probabilidade mínima de falha durante o tempo de vida útil.

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Motivação

- **Integridade Estrutural**

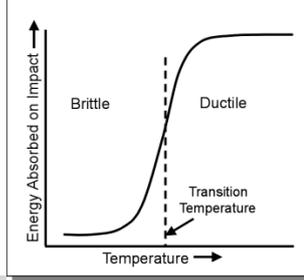
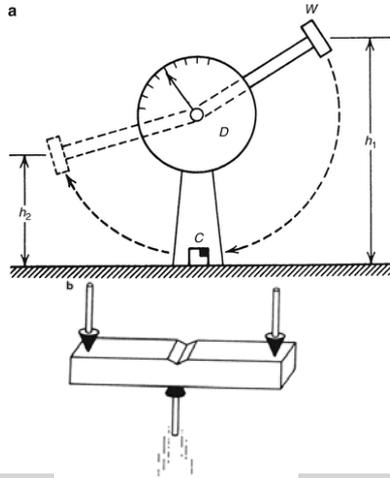
Considera-se que uma estrutura está íntegra quando pode suportar os carregamentos de operação com uma probabilidade mínima de falha durante o tempo de vida útil.

- Uma falha impede que uma estrutura ou componente cumpra su função estrutural.
- As falhas podem ser **catastróficas** ou **não**

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Navio Titanic

Temperatura de Transição Dúctil-Frágil



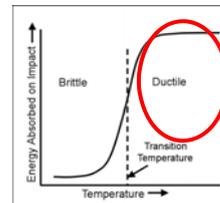
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Navio Titanic

| | C | Mn | P | S | Si | Mn:S |
|--------------|------|------|-------|-------|-------|--------|
| Aço Titanic | 0.21 | 0.47 | 0.045 | 0.069 | 0.017 | 6.8:1 |
| Aço ASTM A36 | 0.20 | 0.55 | 0.012 | 0.037 | 0.007 | 14.9:1 |

| | σ_{ys} (MPa) | σ_T (MPa) | Elong. (%) |
|--------------|---------------------|------------------|------------|
| Aço Titanic | 193 | 417 | 29 |
| Aço ASTM A36 | 235 | 460 | 22 |

| | T_{Tr} (°C) @ 20 J |
|----------------------------|----------------------|
| Aço Titanic (Longitudinal) | 32 |
| Aço Titanic (Transversal) | 56 |
| Aço ASTM A36 | -27 |



Temperatura de Transição Elevada ←



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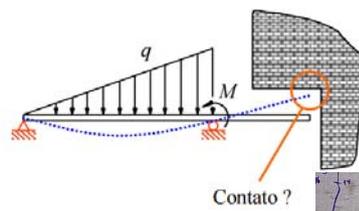
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Modos de Falha

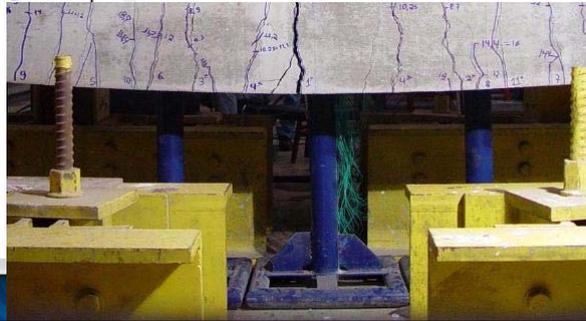
- Deformação excessiva
- Escoamento / Colapso Plástico
- Fadiga
- Fratura
- Flambagem
- Corrosão
- Creep

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Deformação



Normas: limitam deslocamentos máximos.

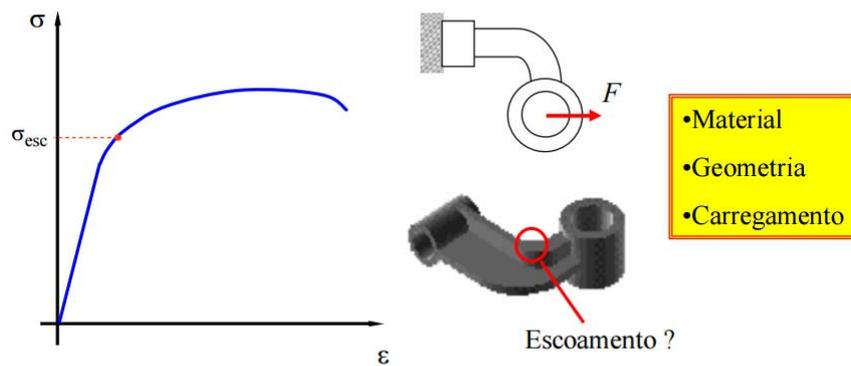


Deformação Excessiva



Escoamento

Escoamento à temperatura ambiente

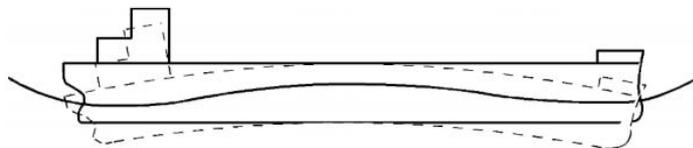


➔ Projeta-se para que as tensões nos pontos críticos não ultrapassem σ_{esc} .

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Fadiga

Hogging (Alquebramento)



Sagging (Tosamento)

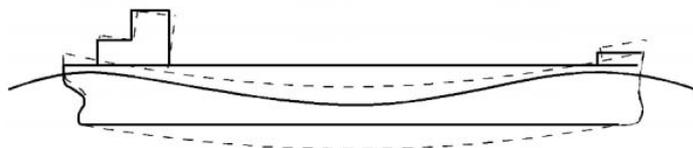
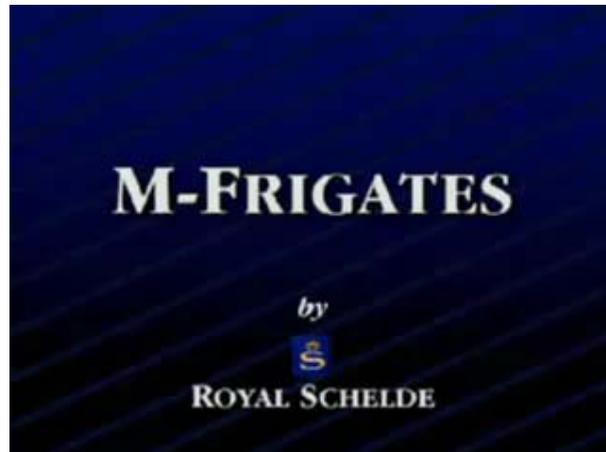


Fig. 2.2.1 Vertical bending due to waves

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Fadiga



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Fadiga



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Fratura Frágil



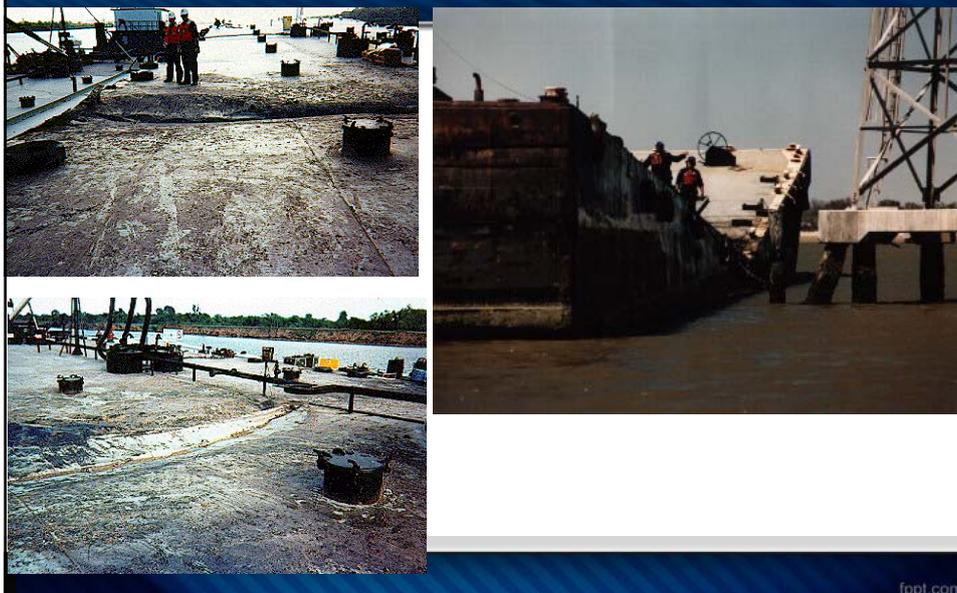
ano 2000

Figure 1. Forward section of the FLARE [1].

Falha acontece mesmo sob tensões menores que o limite de escoamento

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Flambagem “Viga-Navio”



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Fratura

ano 2000



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Oscilação auto-excitada(Ressonância)



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Modo de Falha Combinado

$$1+1 = ?$$



$$1+1 < 1$$

$$1+1 > 1$$



Incertezas nas Cargas



Somewhere out there

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Cargas Ocasionais (Impacto)



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Incertezas nas Cargas



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Incertezas nas Cargas



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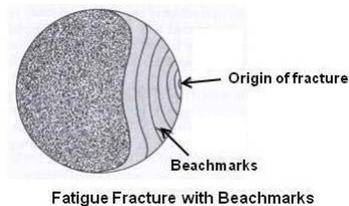
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Falhas Fadiga

- A **FADIGA** representa mais de 50% de todas as falhas mecânicas reportadas na literatura.
- *Efeito cumulativo de Danos (Microestruturais) devido à ação cíclica de Esforços.*



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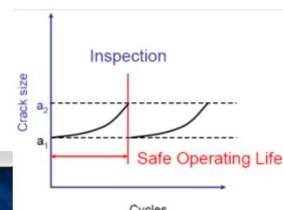
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Falhas Catastróficas

- Custos devido à problemas da fadiga/fratura nos EUA \$119 Bilhões 4% PIB (1980)



Estimativas da vida à fadiga muito conservadoras implica em **altos custos** de **construção/manutenção/inspeção**.



Plataforma semi-submersível Alexander Kielland



•1980 nas águas do
Mar do Norte

- Fadiga da junta soldada
circunferencial no
contraventamento D-6



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Fadiga em Plataforma

27 March, 1980, 18:30
Ekofisk Oil Field, North Sea

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Fadiga em Navios



Falhas Catastróficas por Fadiga



- CUSTOS?
- RESPONSABILIDADES ? Civil , Penal !
- IMPACTO NA NATUREZA?

FADIGA

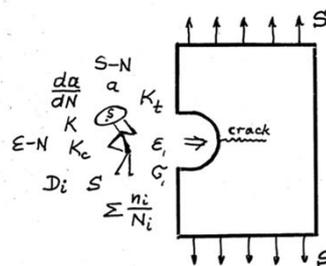
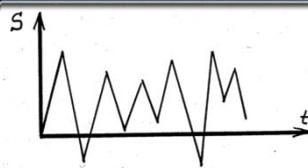
- O que é?
- Quando e porquê acontece?
- Como é avaliada a resistência à Fadiga dado um carregamento cíclico?
- Como é caracterizada a resistência à Fadiga de um material?



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FADIGA – O que é?



$N_i = ?$

$N_p = ?$

$N_T =$

?

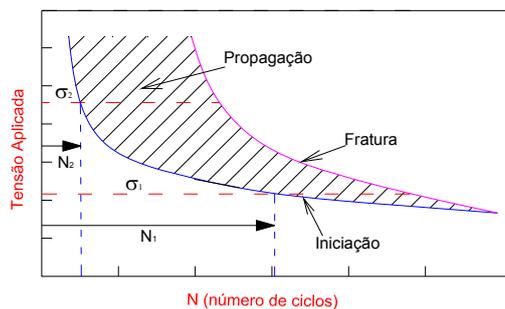
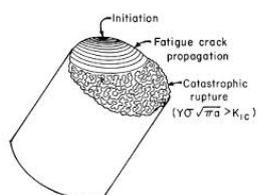
Fadiga mecânica é o fenômeno de **dano** progressivo de materiais sujeitos a esforços **cíclicos** (ΔP , ΔM , ΔT).

26

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Objetivos do Estudo da Fadiga

- Estimativas acuradas do tempo de iniciação de uma trinca (N_i)
- As correspondentes taxas de propagação de trinca (da/dN)

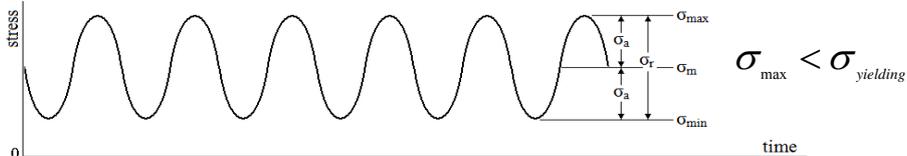


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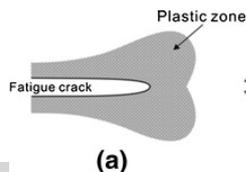
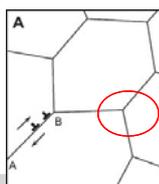
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Quando Aconteça Fadiga

✓ Esforços Alternados



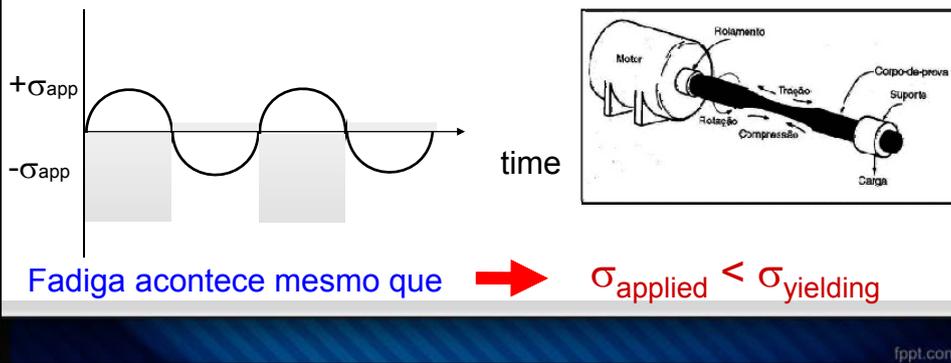
✓ Deformação Plástica Localizada (Processo Irreversível)



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DEFINIÇÃO FADIGA

- **Fadiga mecânica** é o fenômeno de **dano** progressivo de materiais sujeitos a esforços **cíclicos** (ΔP , ΔM , ΔT).

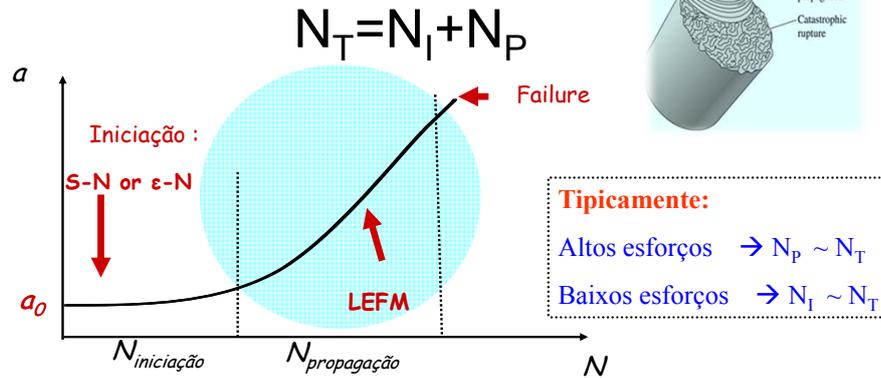


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Avaliação da Vida à Fadiga

Vida à fadiga de um componente:



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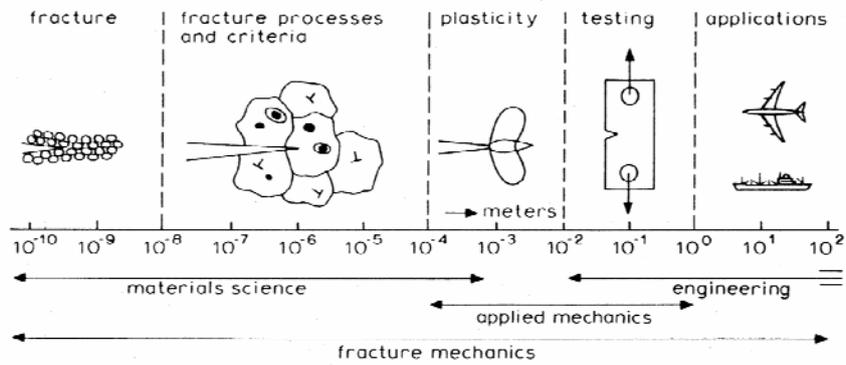
Iniciação de Trincas

- Duas metodologias
 - S x N (Alto ciclo)
 - ϵ x N (Baixo ciclo)
- Caracterizada por:
 - Deformação plástica altamente localizada
 - Fenômeno de superfície
 - Processo estocástico

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The Broad Field of Fracture Mechanics/Fatigue

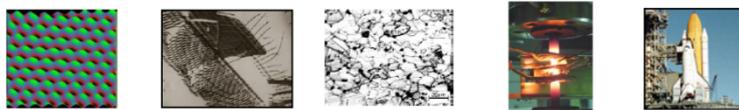


(from Ewalds & Wanhil, ref.3)

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The Broad Field of Fracture Mechanics/Fatigue

Atoms Dislocations Crystals Specimens Structures



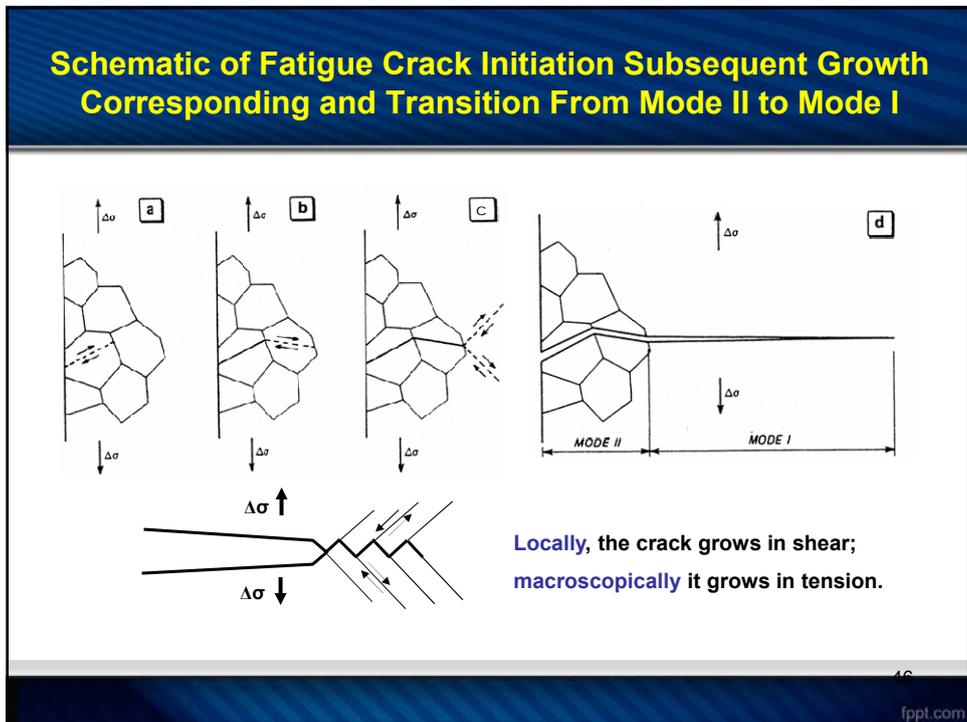
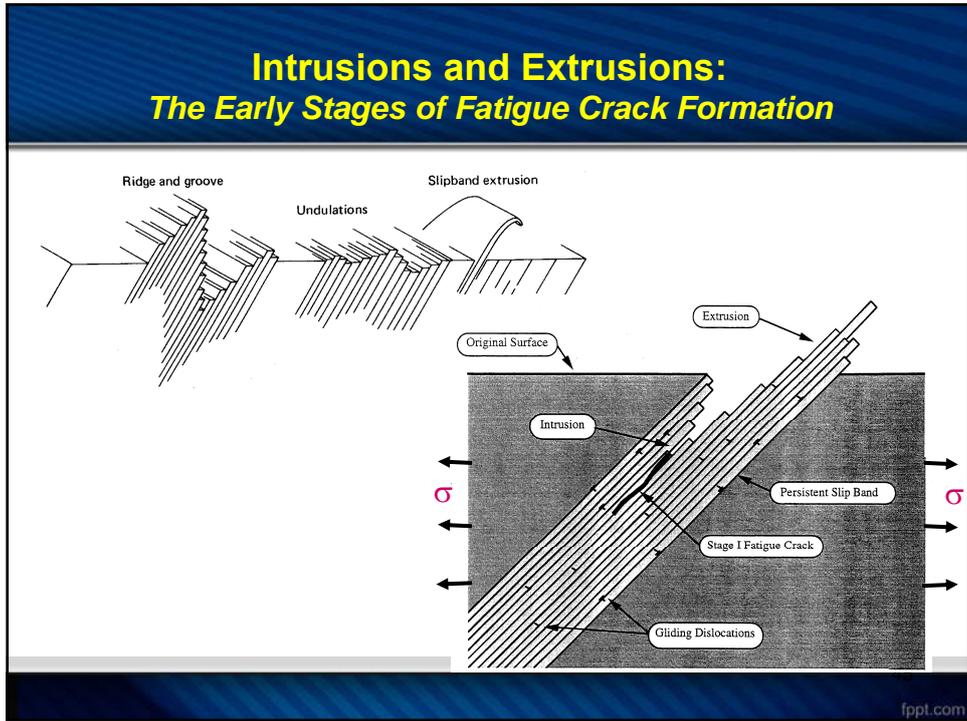
10^{-10} 10^{-8} 10^{-6} 10^{-4} 10^{-2} 10^0 10^2

Understand the physics on this scale

Model the physics on this scale

Use the models on this scale

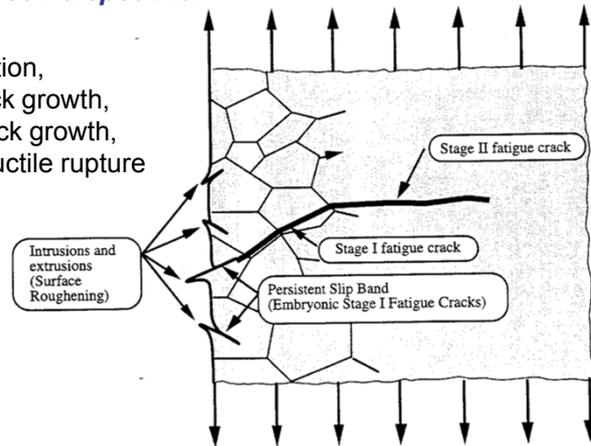
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The Process of Fatigue

The Materials Science Perspective:

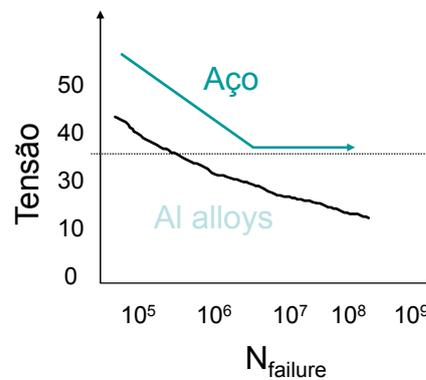
- Cyclic slip,
- Fatigue crack initiation,
- Stage I fatigue crack growth,
- Stage II fatigue crack growth,
- Brittle fracture or ductile rupture



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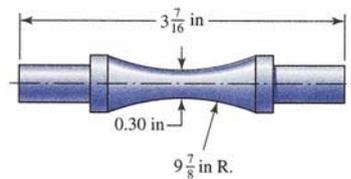
Curvas S-N

- Fadiga de alto ciclo
- Tensão aplicada $\Delta\sigma$
 $\sigma_{\text{applied}} < \sim 2/3 \sigma_{\text{yield}}$
- Tensões são **nominalmente** elásticas.
- Localmente o material deforma plasticamente



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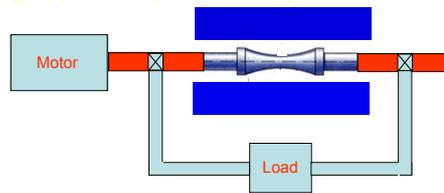
Avaliação Convencional das Propriedades S-N



Superfície Polida

Momento Fletor Constante

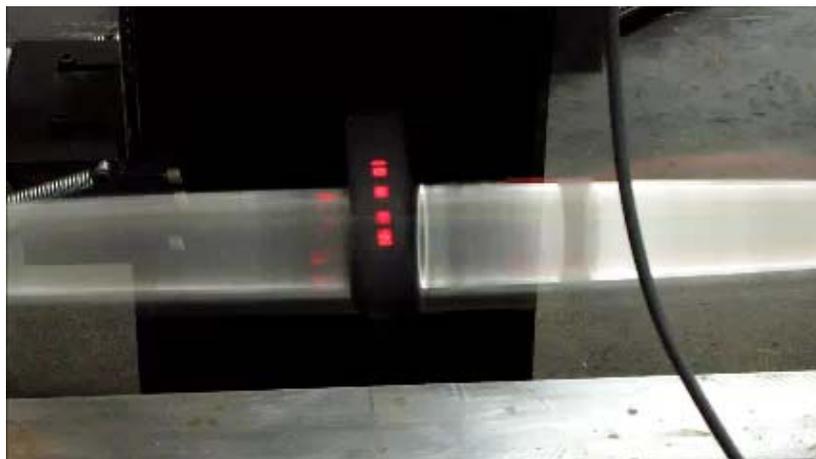
Typical testing apparatus, pure bending



Rotating beam machine – applies fully reverse bending stress

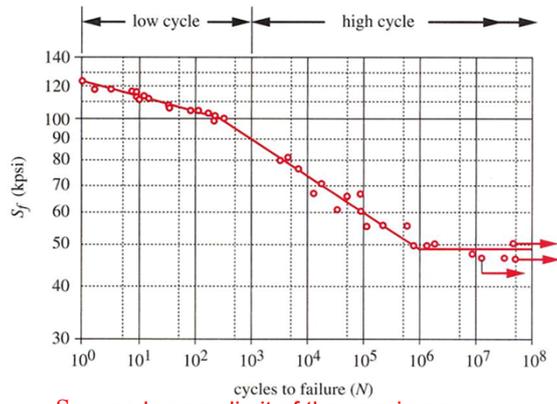
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Avaliação Convencional das Propriedades S-N



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Typical S-N curve

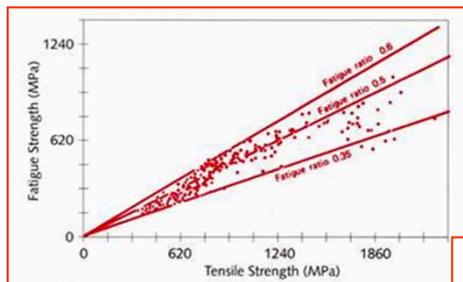


S_e = endurance limit of the specimen

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Relationship Between Endurance Limit and Ultimate Strength

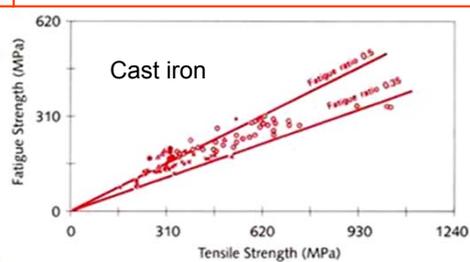


Steel

$$S'_e = \begin{cases} 0.5S_{ut} & S_{ut} \leq 200 \text{ ksi (1400 MPa)} \\ 100 \text{ ksi} & S_{ut} > 200 \text{ ksi} \\ 700 \text{ MPa} & S_{ut} > 1400 \text{ MPa} \end{cases}$$

Cast iron

$$S'_e = \begin{cases} 0.4S_{ut} & S_{ut} < 60 \text{ ksi (400 MPa)} \\ 24 \text{ ksi} & S_{ut} \geq 60 \text{ ksi} \\ 160 \text{ MPa} & S_{ut} < 400 \text{ MPa} \end{cases}$$



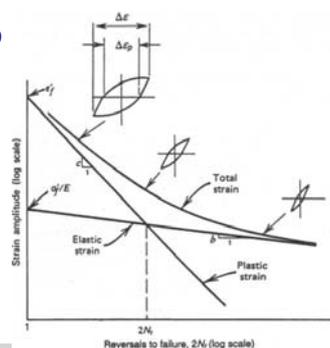
Cast iron

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Curvas ϵ -N

Fadiga de baixo ciclo

- Carregamento aplicado produz deformações plásticas $\Rightarrow \Delta\epsilon_{\text{total}} > \epsilon_{\text{escoamento}}$
 - $\Delta\epsilon_{\text{total}} = \Delta\epsilon_{\text{elásticas}} + \Delta\epsilon_{\text{plásticas}}$
- Entalhes
- Descontinuidades



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Curvas ϵ -N

- Fadiga de baixo ciclo

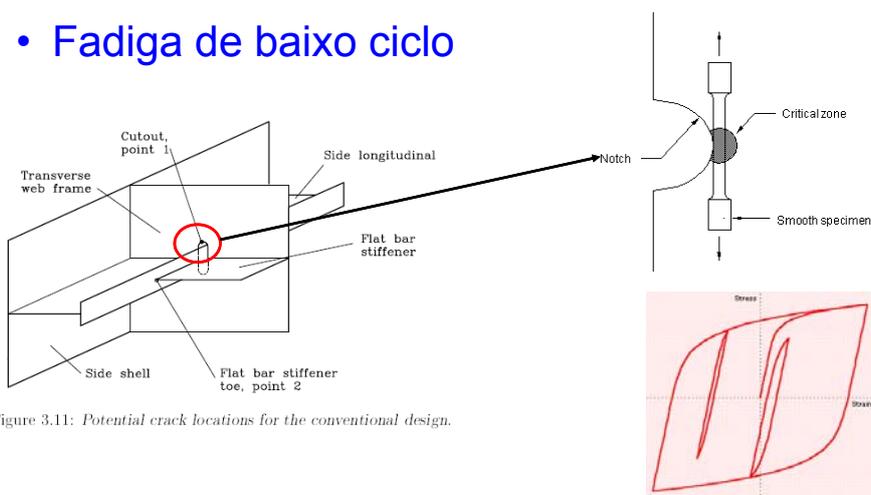


Figure 3.11: Potential crack locations for the conventional design.

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Low Cycle Fatigue

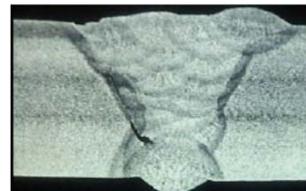
- Overloads
- ↓
- Plastic Deformation
- ↓
- Strain Life Analysis



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Propagação de Trinca

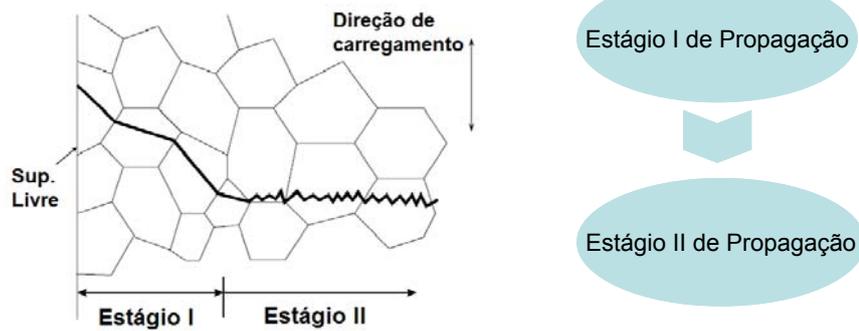
Contudo... para estruturas soldadas: $N_T \sim N_P$



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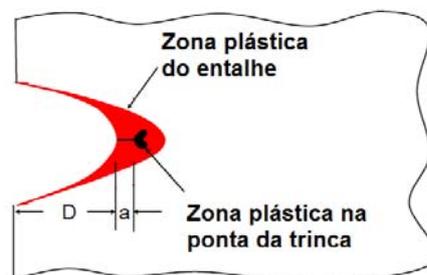
Propagação de Trinca



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Propagação de Trinca

• Estágio I



• Tamanho (a) ~ 2-4 grãos (D)

• Fortemente influenciada pela microestrutura

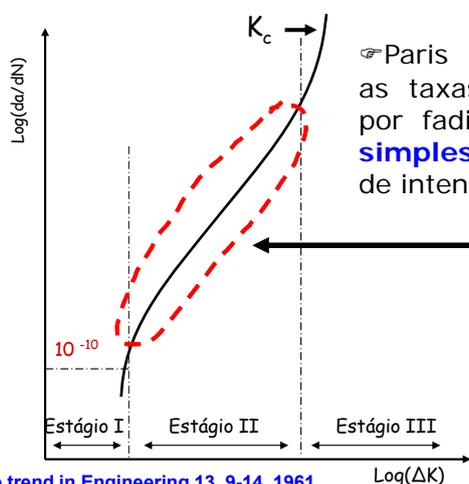
• Planos de escorregamento

• Nível de tensão

• Plasticidade na ponta da trinca

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Propagação de Trincas (Estágio II)



Paris (1961) propus caracterizar as taxas de crescimento de trinca por fadiga - em forma **elegante** e **simples** - por meio do fator elástico de intensidade de tensões K :

$$\frac{da}{dN} = C(\Delta K)^m$$

$$\Delta K = \xi \Delta \varepsilon_{ij}$$

$$\xi = \left(\frac{E\sqrt{2\pi r}}{f_{ij}(\theta)} \right)$$

The trend in Engineering 13, 9-14, 1961

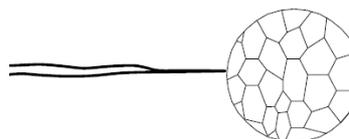
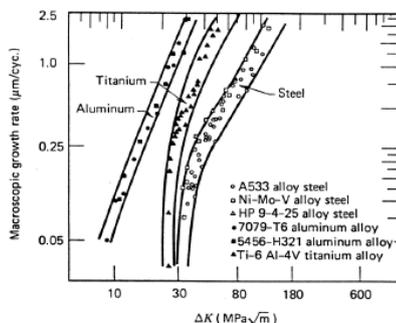
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Propagação de Trincas (Estágio II)

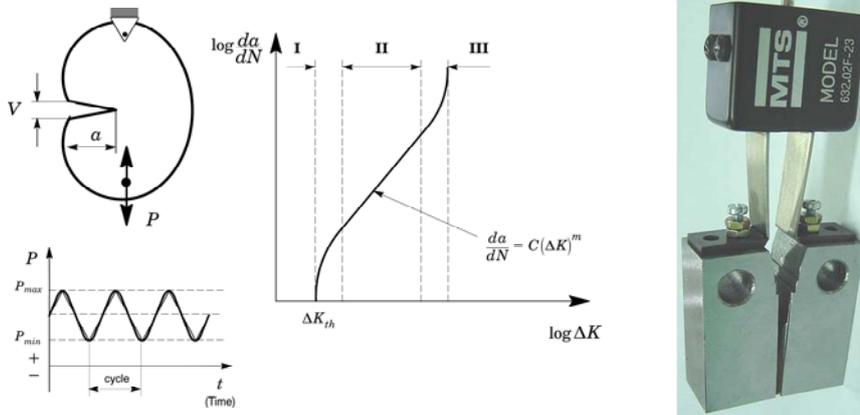
- Pouca influencia da resistência do material

- Zona plástica \gg microestrutura do material (pouca influência da microestrutura)



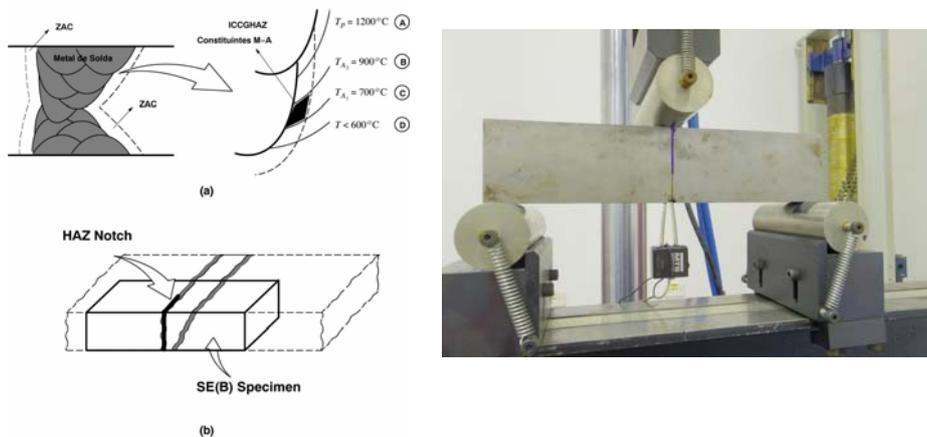
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Avaliação Convencional das Propriedades da/dN



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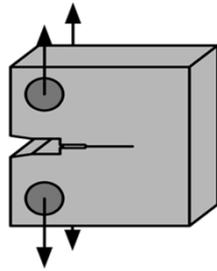
Avaliação Experimental de Fadiga



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Correlação Laboratório vs. Estrutura



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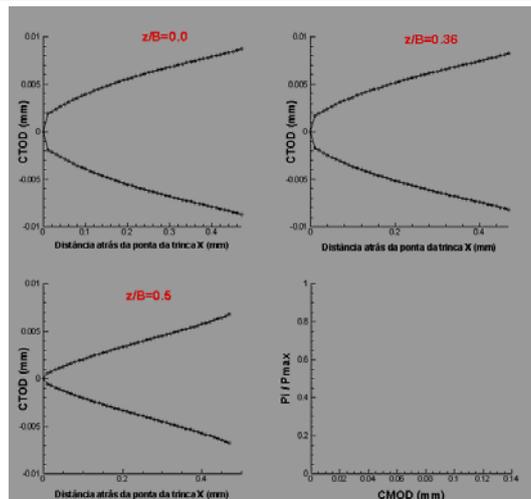
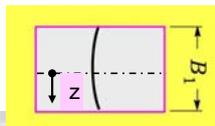
Análise Numérica de Fadiga

Força Motriz Efetiva

$$\Delta K_{eff} = f(P_{max}, P_o, a_j, t, W)$$

$$\frac{da}{dN} = C(\Delta K_{eff})^m$$

Fechamento Parcial da trinca



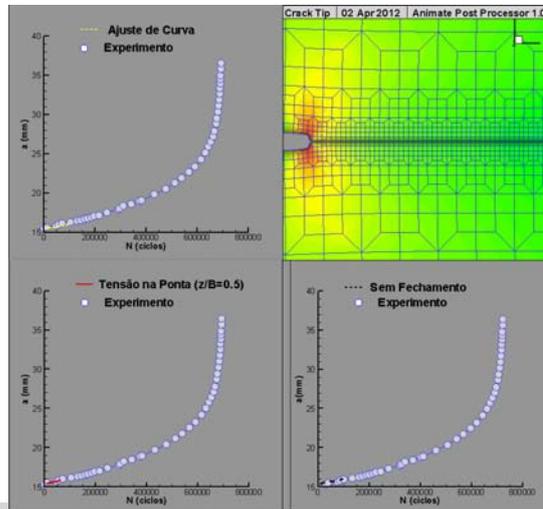
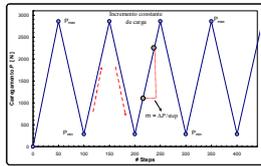
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Análise Numérica de Fadiga

Propagação de defeitos

$$N = \int_{a_i}^{a_f} \frac{da}{C(\Delta K_{eff})^m}$$

$$\Delta K_{eff} = f(P_{max}, P_o, a, t, W)$$



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AGENDA

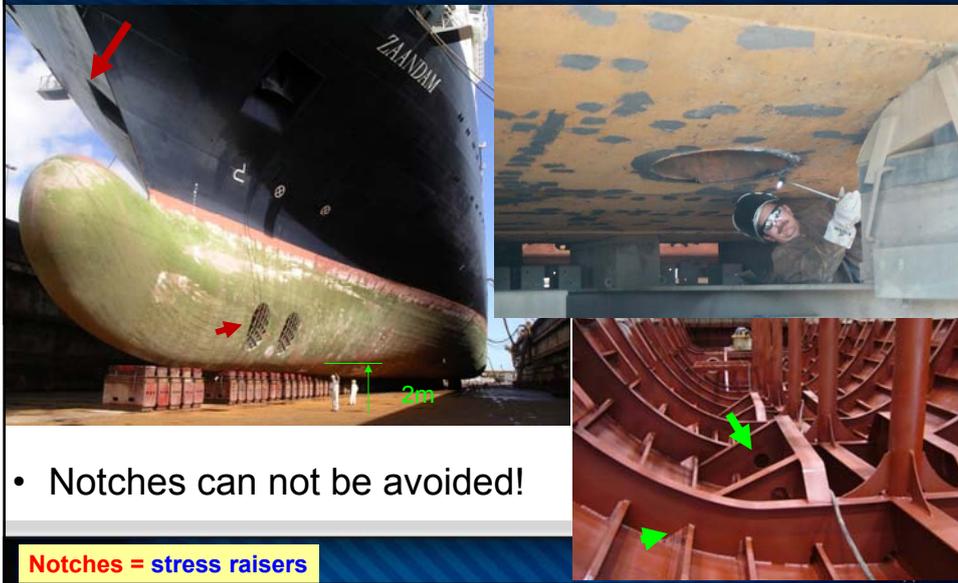
4. Metodologias para Avaliação da Vida à Fadiga (Fatigue Methodologies)

- Carregamento Constante (Constant Amplitude)
 - S-N
 - ϵ -N
 - da/dN - ΔK
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- Juntas Soldadas (Welded Joints)
- Fadiga Multiaxial (Multiaxial Fatigue)

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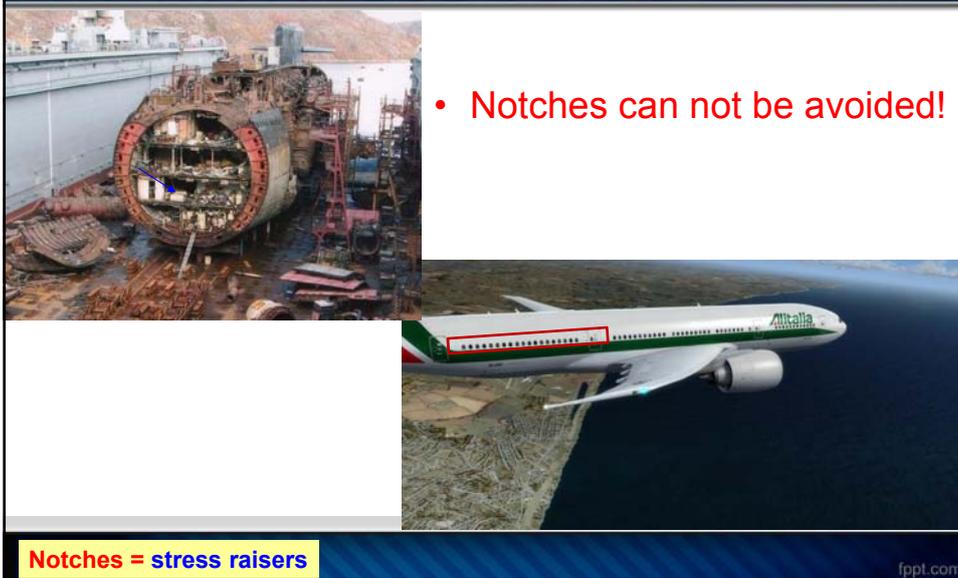
Opening (Notch)



- Notches can not be avoided!

Notches = stress raisers

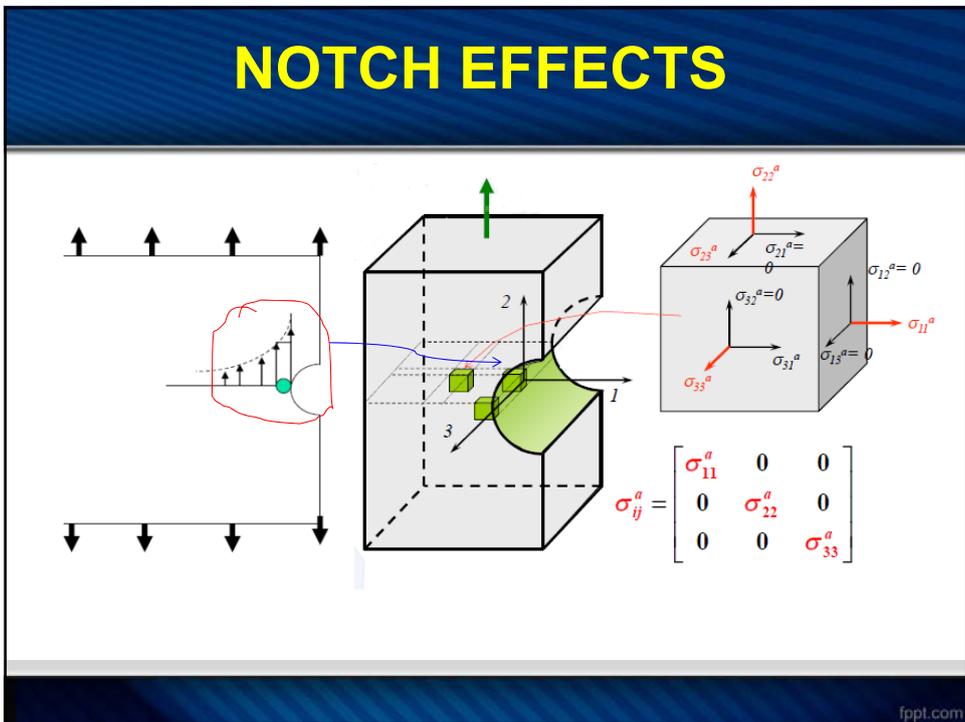
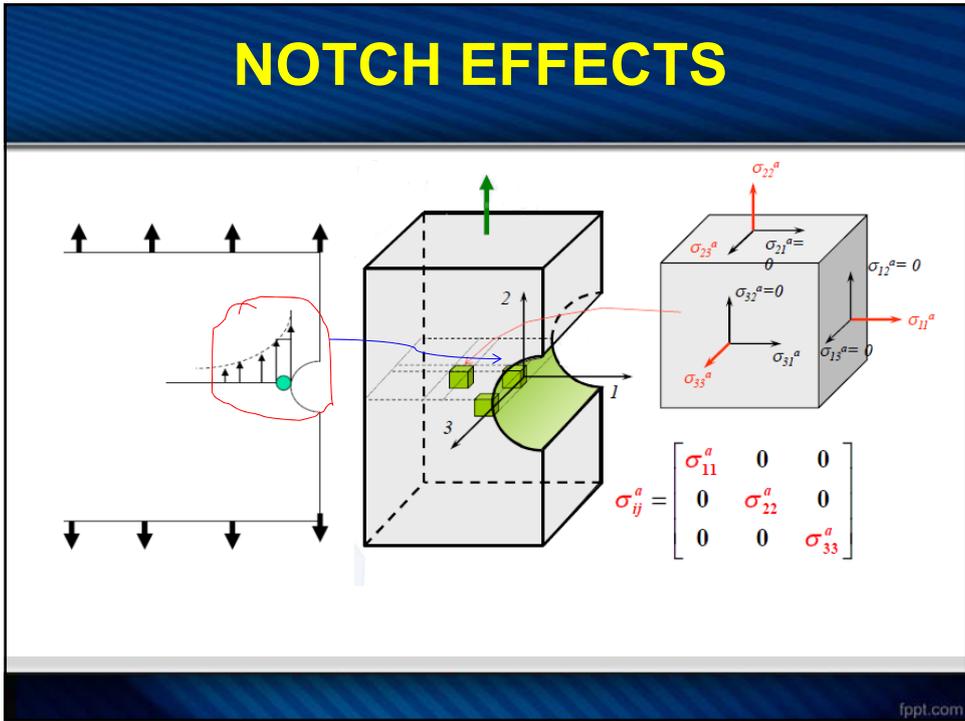
Entalhes (Notches)



- Notches can not be avoided!

Notches = stress raisers

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NOTCH EFFECTS

$$\sigma_n = \frac{F}{A_{net}}$$

and

$$\sigma_{peak} = K_t \sigma_n$$

NOTCH EFFECTS

For tension $\lambda = 0$ and $\theta = 90$

stress

$\frac{\sigma_\theta}{\sigma}$

$\frac{\sigma_r}{\sigma}$

$\frac{a}{r}$

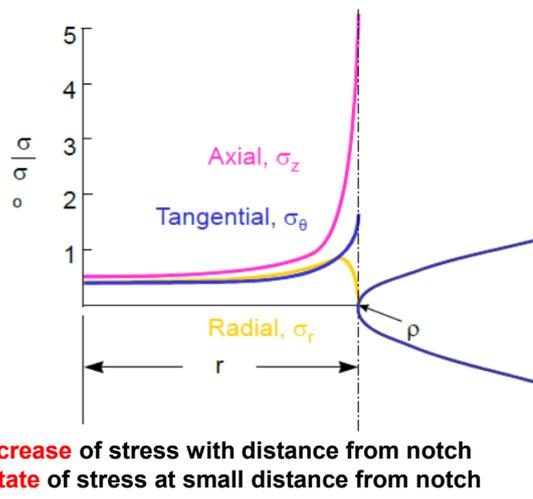
- Rapid **decrease** of stress with distance from notch
- **Biaxial state** of stress at small distance from notch

$$\frac{\sigma_r}{\sigma} = \frac{1+\lambda}{2} \left(1 - \left(\frac{r}{a}\right)^2 \right) + \frac{1-\lambda}{2} \left(1 + 3 \left(\frac{r}{a}\right)^4 - 4 \left(\frac{r}{a}\right)^2 \right) \cos 2\theta$$

$$\frac{\sigma_\theta}{\sigma} = \frac{1+\lambda}{2} \left(1 + \left(\frac{r}{a}\right)^2 \right) + \frac{1-\lambda}{2} \left(1 + 3 \left(\frac{r}{a}\right)^4 \right) \cos 2\theta$$

$$\frac{\tau_{\theta\phi}}{\sigma} = \frac{1-\lambda}{2} \left(1 - 3 \left(\frac{r}{a}\right)^4 + 2 \left(\frac{r}{a}\right)^2 \right) \sin 2\theta$$

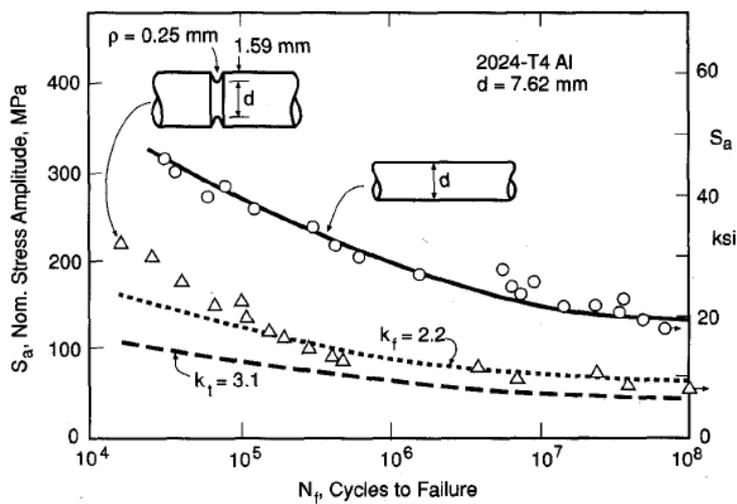
NOTCH EFFECTS



- Rapid **decrease** of stress with distance from notch
- **Triaxial state** of stress at small distance from notch

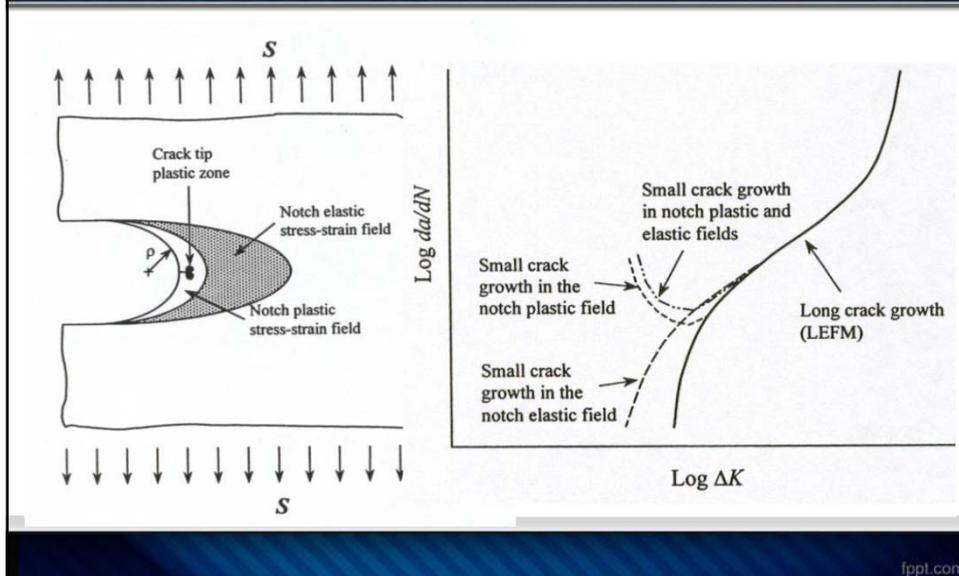
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NOTCH EFFECTS



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CRACK GROWTH AT NOTCHES

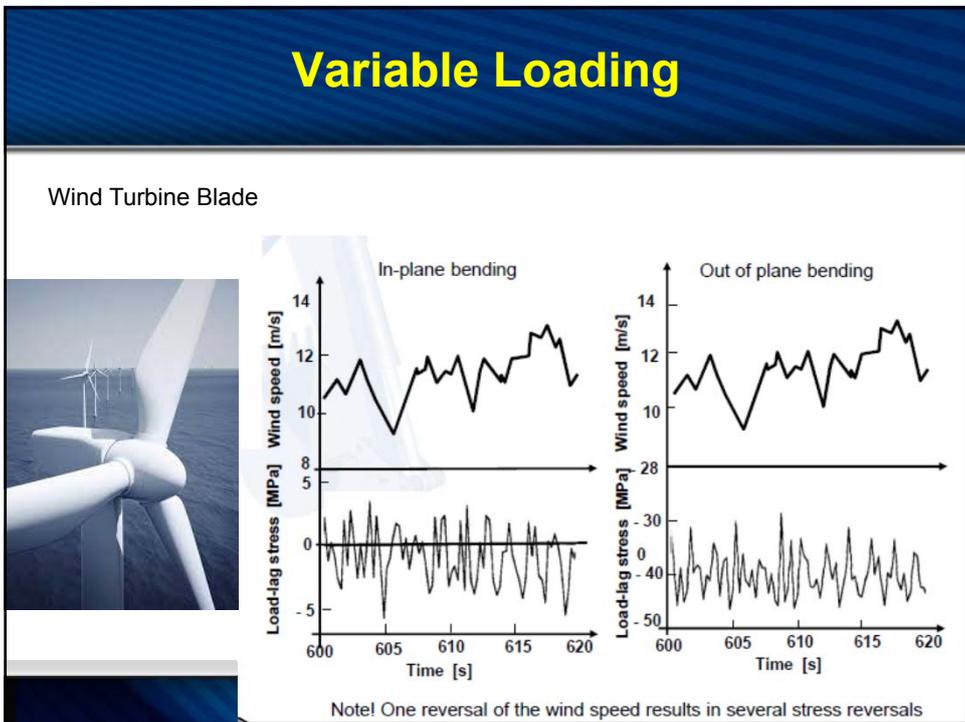
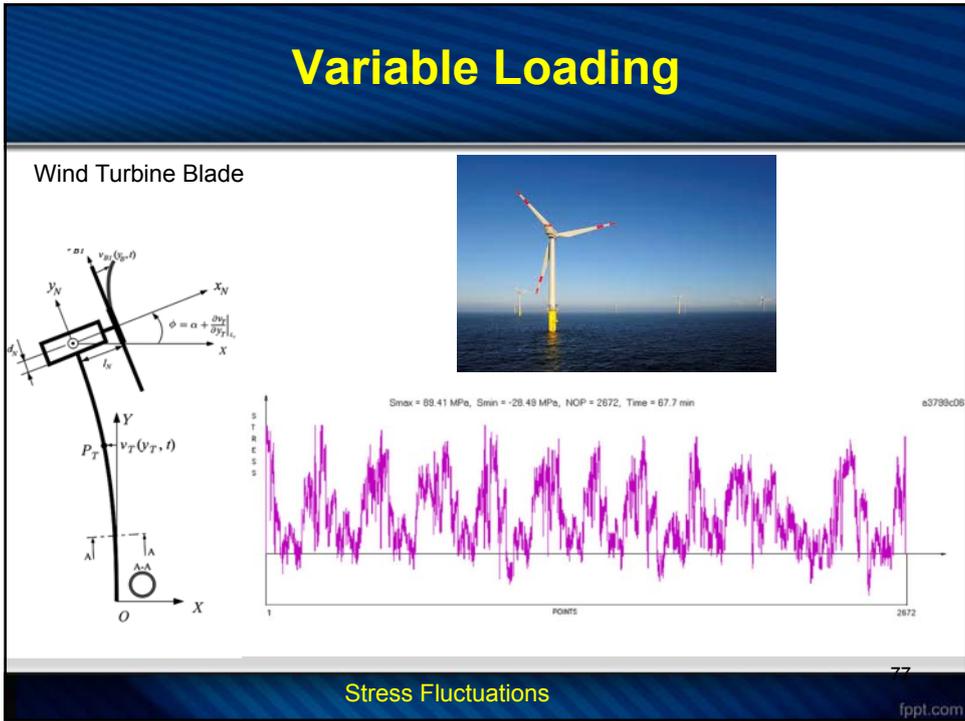


AGENDA

4. Metodologias para Avaliação da Vida à Fadiga (Fatigue Methodologies)
 - Carregamento Constante (Constant Amplitude)
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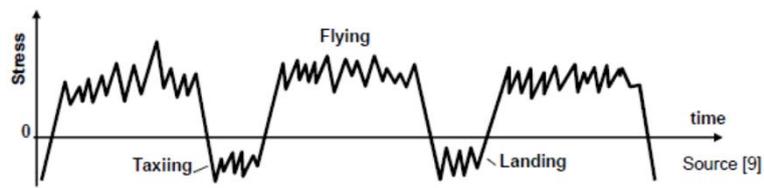
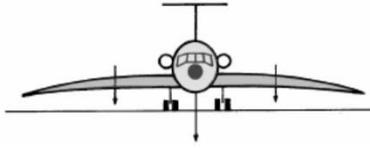
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Variable Loading

Aircraft wing skin



Stress Fluctuations

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Variable Loading

Ship

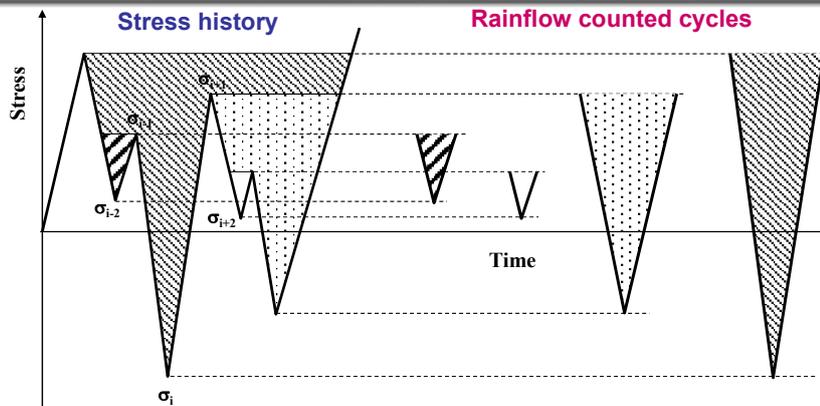


Stress Fluctuations

80

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Rainflow Counted Cycles



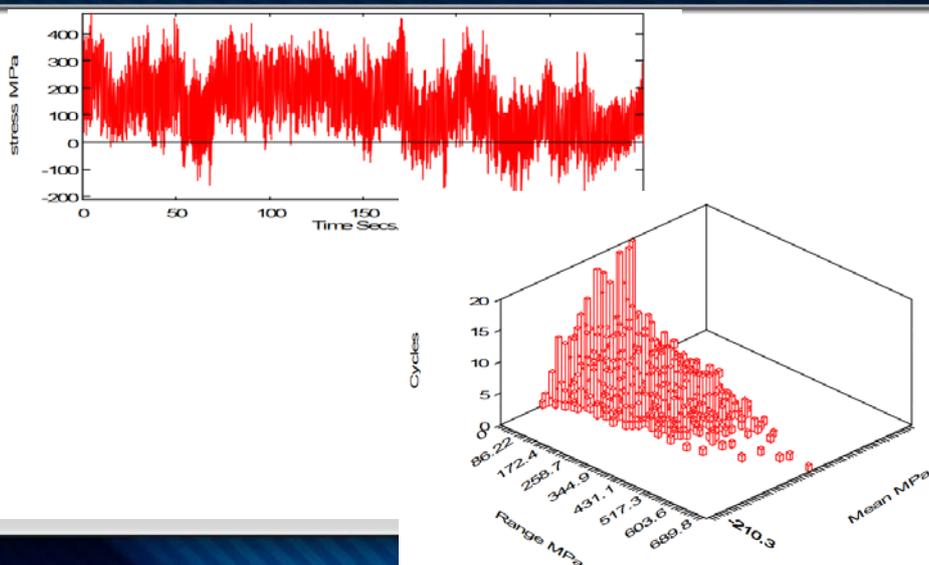
A *rainflow counted cycle* is identified when any two adjacent reversals in the stress history satisfy the following relation:

$$ABS|\sigma_{i-1} - \sigma_i| < ABS|\sigma_i - \sigma_{i+1}|$$

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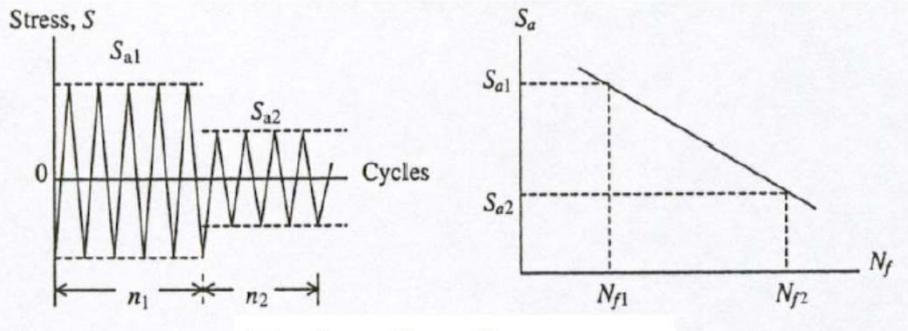
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Range-mean histogram by rainflow



DAMAGE EVOLUTION

Palmgren-Miner Linear Damage Rule

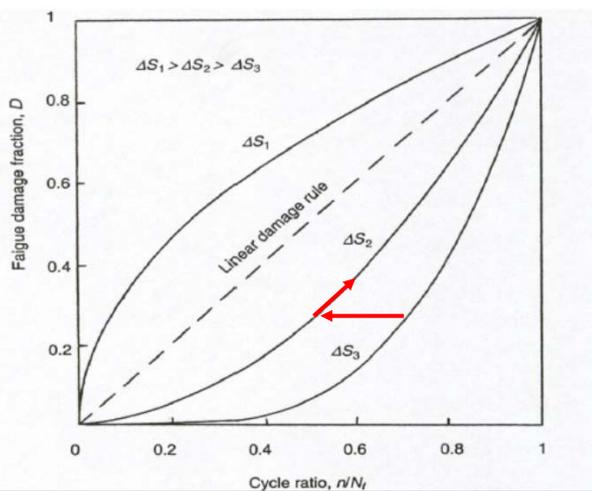


$$\sum \frac{n_i}{N_{fi}} = \frac{n_1}{N_{f1}} + \frac{n_2}{N_{f2}} + \dots = 1$$

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DAMAGE EVOLUTION

Nonlinear Damage Rule



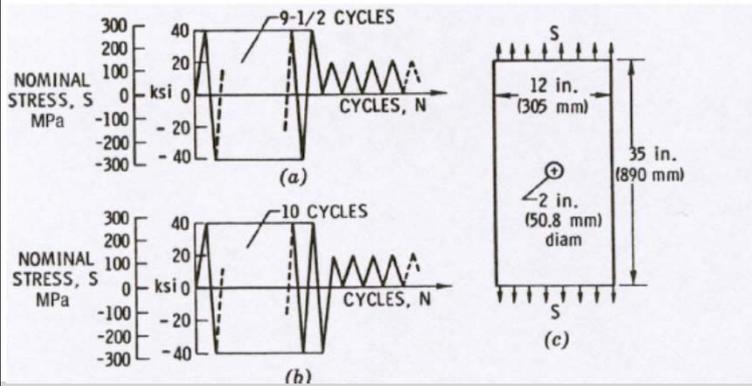
$$D = \sum_i \left(\frac{n}{N} \right)^\alpha$$

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DAMAGE EVOLUTION

Nonlinear Damage Rule (Initiation)

$$D = \sum_i \left(\frac{n}{N} \right)^\alpha$$



Cycles

460×10^3

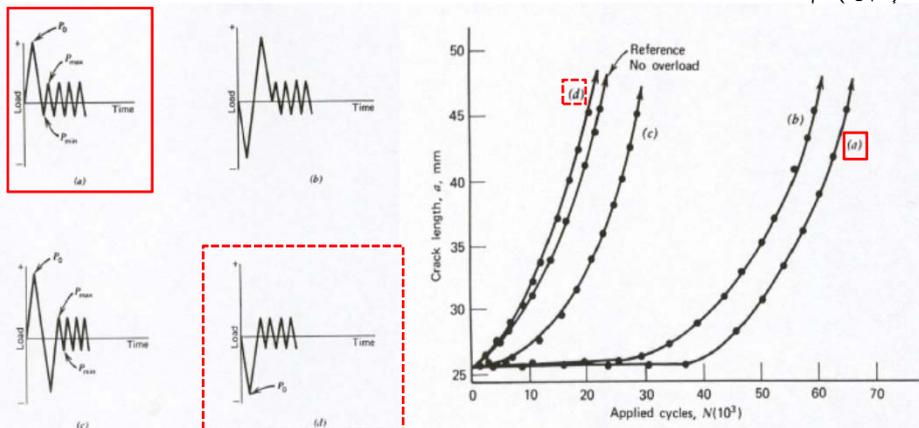
63×10^3

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DAMAGE EVOLUTION

Nonlinear Damage Rule (Propagation)

$$D = \sum_i \left(\frac{n}{N} \right)^\alpha$$

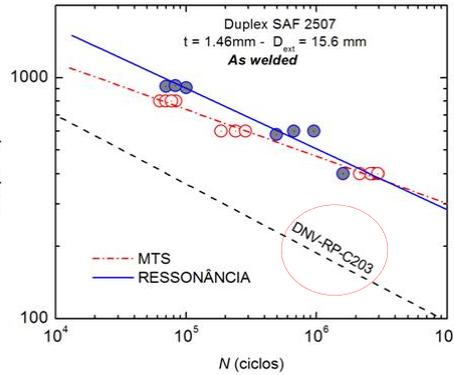
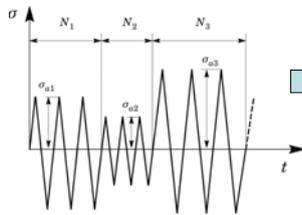


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Rainflow + Damage

– Análise dos procedimentos correntes de avaliação usando normas de construção naval e de estruturas oceânicas.

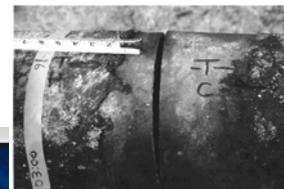
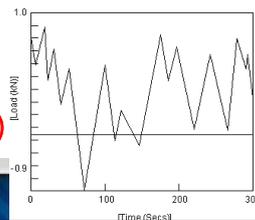
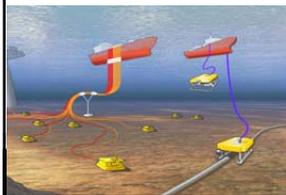
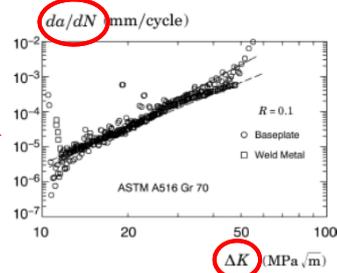
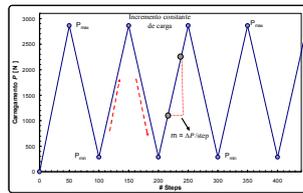
$$D_{mp} = \sum_i^m \frac{n_i}{N_{fi}}$$



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Rainflow + Damage

• Forças Motrizes Cíclicas (efetivas) e Taxas de Propagação



AGENDA

4. Metodologias para Avaliação da Vida à Fadiga (Fatigue Methodologies)

- Carregamento Constante (Constant Amplitude)
 - S-N
 - ϵ -N
 - $da/dN-\Delta K$
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Fatigue of Welds

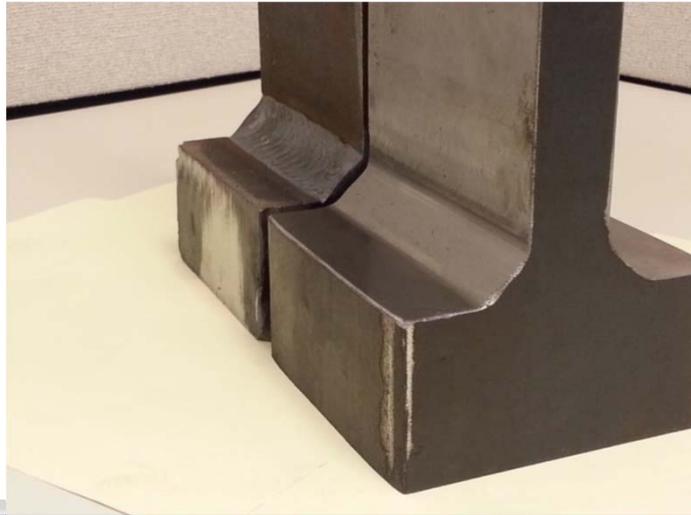
Weld Problems



NYS&DOT

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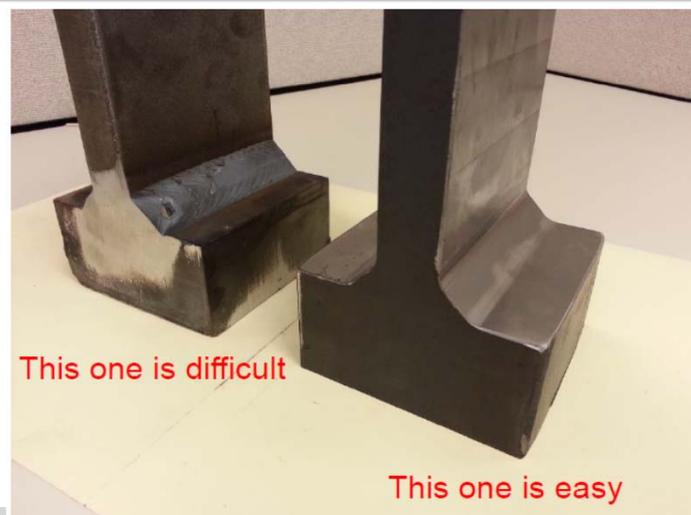
Fatigue of Welds



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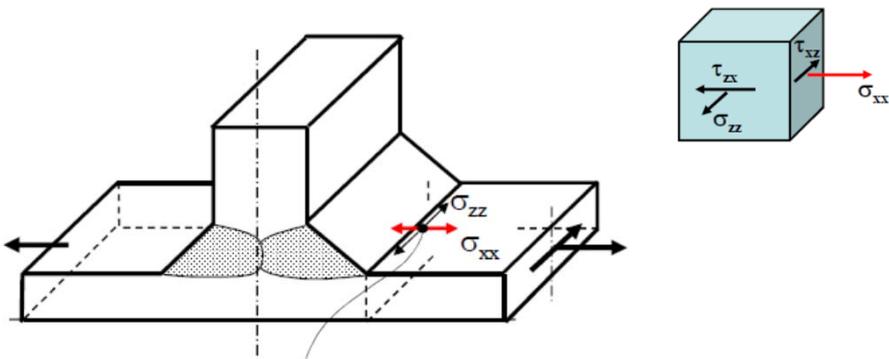
Fatigue of Welds



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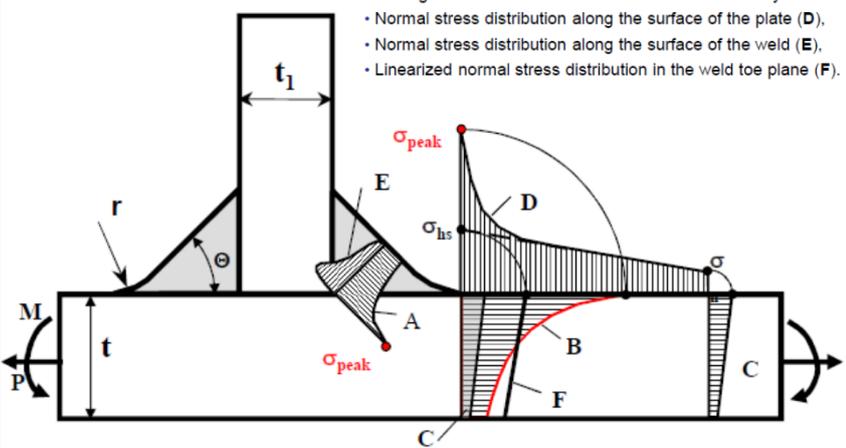
Stress State



- Multiaxial State of Stress at the weld toe
- Due to notch σ_{xx} is the largest component and responsible for fatigue damage

2008 Grzegorz Glinka

Stress Distribution in Welds



- Normal stress distribution in the weld throat plane (A),
- Through the thickness normal stress distribution in the weld toe plane (B),
- Through the thickness normal stress distribution away from the weld (C),
- Normal stress distribution along the surface of the plate (D),
- Normal stress distribution along the surface of the weld (E),
- Linearized normal stress distribution in the weld toe plane (F).

Various stress distributions in a T-butt weldment with transverse fillet welds; 2008 Grzegorz Glinka

Design Fatigue Curves

Tubular Welded Joint under Torsion and Bending

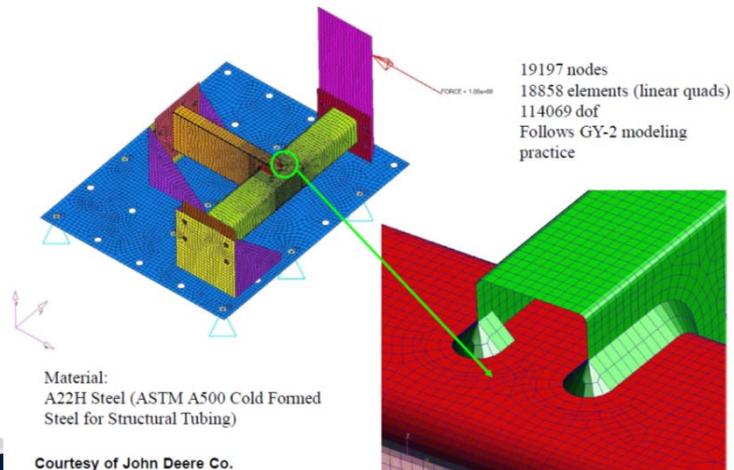


Courtesy of John Deere Co.

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Design Fatigue Curves

Shell Element Model Details



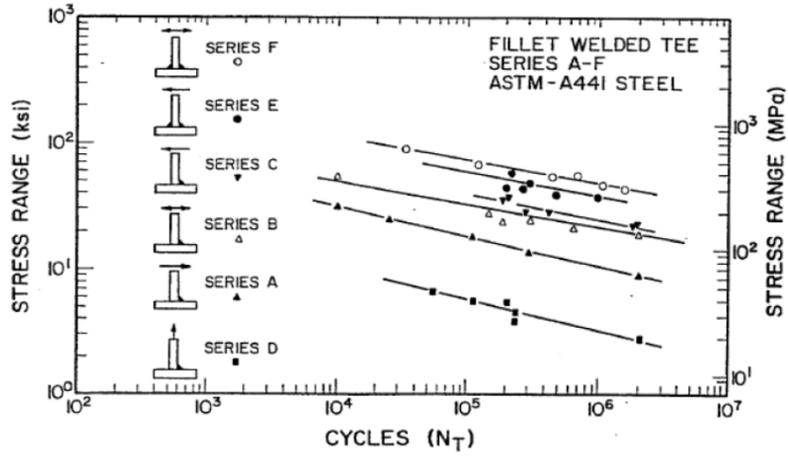
Courtesy of John Deere Co.

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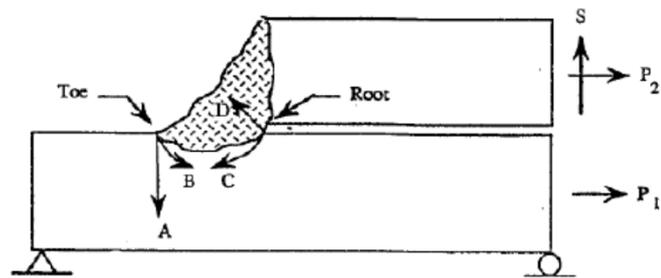
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Design Curves



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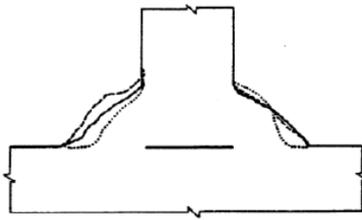
Failure Locations



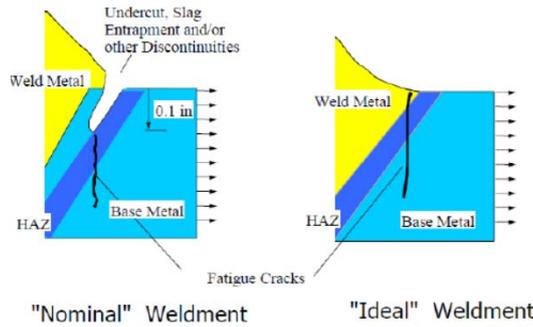
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Fatigue of Welds

Weld Shape?

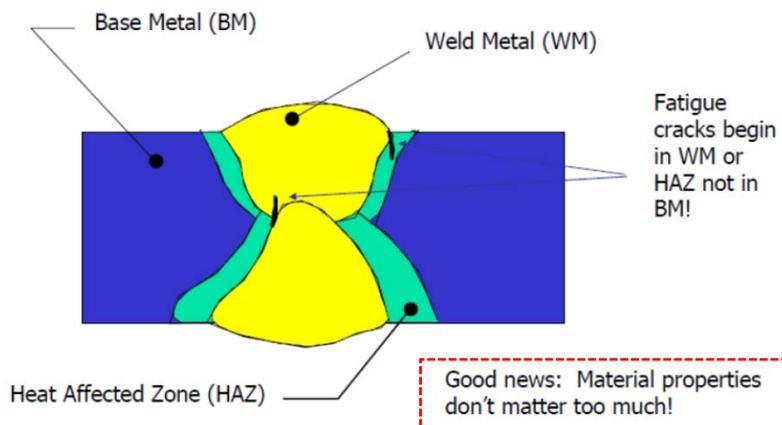


Weld Quality?



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Material Properties



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Fatigue of Welds

The variables influencing weldment fatigue life can be thought of as being only two:

- the magnitude of the notch root stresses.
- the properties of the notch root material.

In this sense, the applied stresses, the degree of bending, the welding residual stresses, the fabrication residual stresses, the applied mean stresses, the weldment geometry, the notch root weld defects, and the weldment size all influence the magnitude of the notch root stresses.

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Fatigue of Welds

The fatigue behavior of a weldment is controlled by the local (notch root, hot-spot) stress-strain history.

For structural steel weldments: material properties are of minor importance except (as we shall see) to the degree that they determine and limit the value of the residual stresses.

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AGENDA

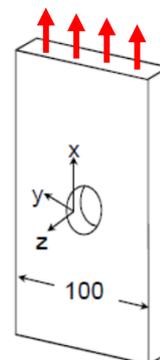
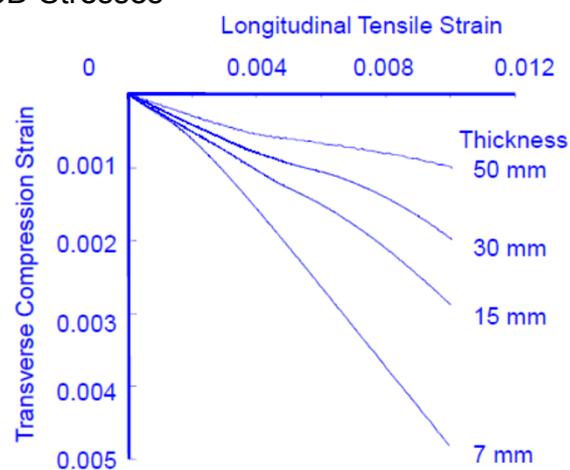
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Multiaxial Fatigue

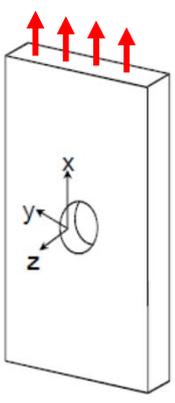
3D Stresses



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Multiaxial Fatigue

3D Stresses

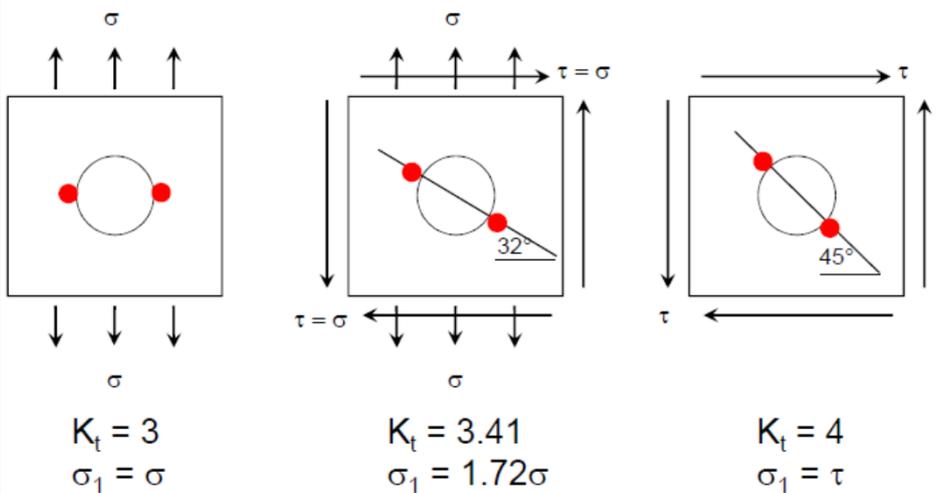


| t | ϵ_x | ϵ_z | σ_x | σ_z |
|----|--------------|--------------|------------|------------|
| 7 | 0.01 | -0.005 | 63.5 | 0 |
| 15 | 0.01 | -0.003 | 70.6 | 14.1 |
| 30 | 0.01 | -0.002 | 73.0 | 21.8 |
| 50 | 0.01 | -0.001 | 75.1 | 29.3 |

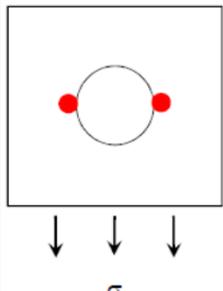
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Multiaxial Fatigue

Maximum Stress (Plane)



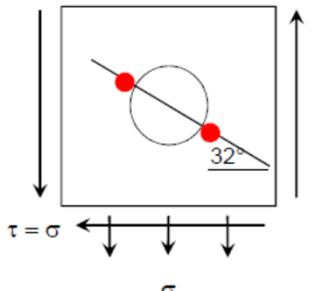
σ



σ

$K_t = 3$
 $\sigma_1 = \sigma$

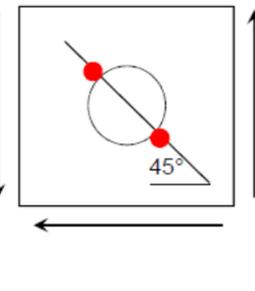
σ



$\tau = \sigma$

$K_t = 3.41$
 $\sigma_1 = 1.72\sigma$

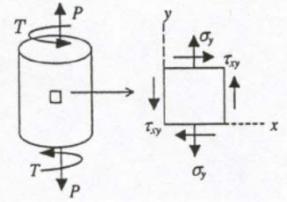
τ



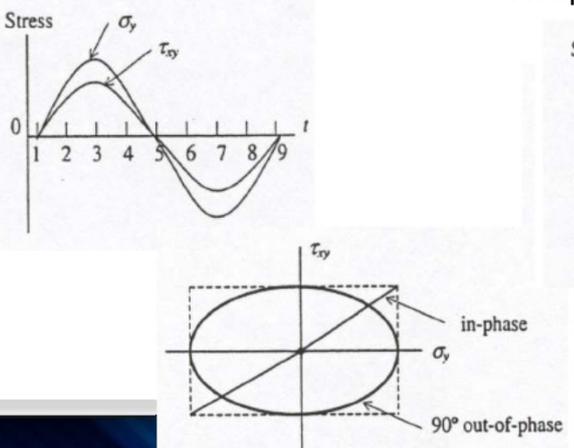
τ

$K_t = 4$
 $\sigma_1 = \tau$

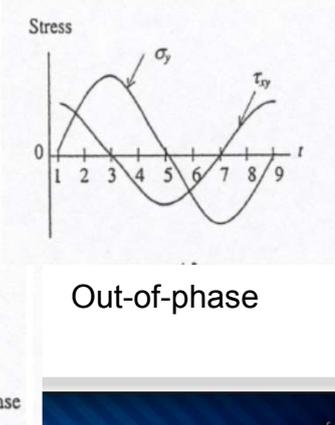
Multiaxial Fatigue



Proportional Loading

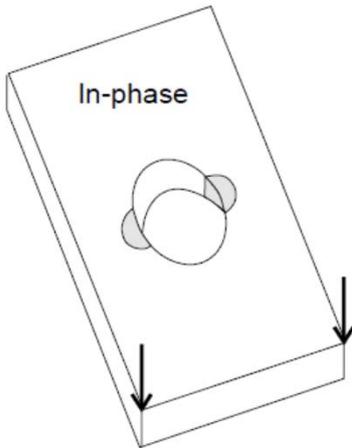


Nonproportional Loading



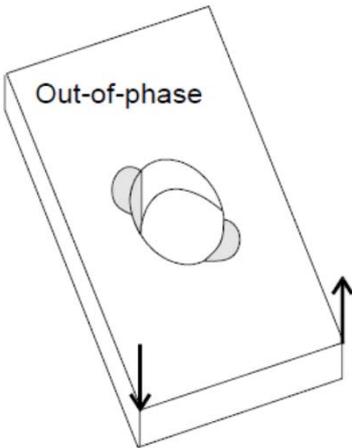
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Multiaxial Fatigue



In-phase

$K_t = 3$



Out-of-phase

$K_t = 4$

Damage location changes with load phasing

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Obrigado!

Diego F. B. Sarzosa
Universidade de São Paulo - USP