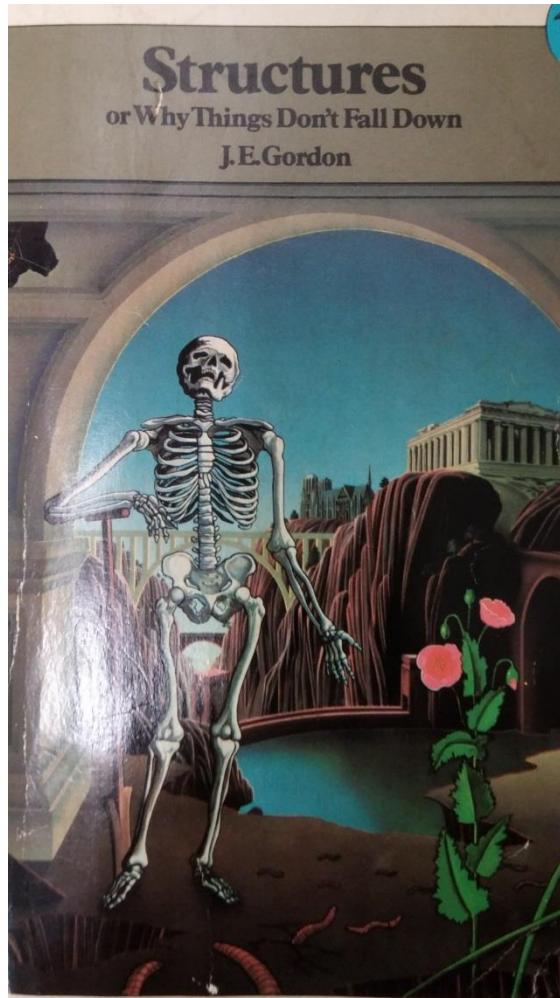
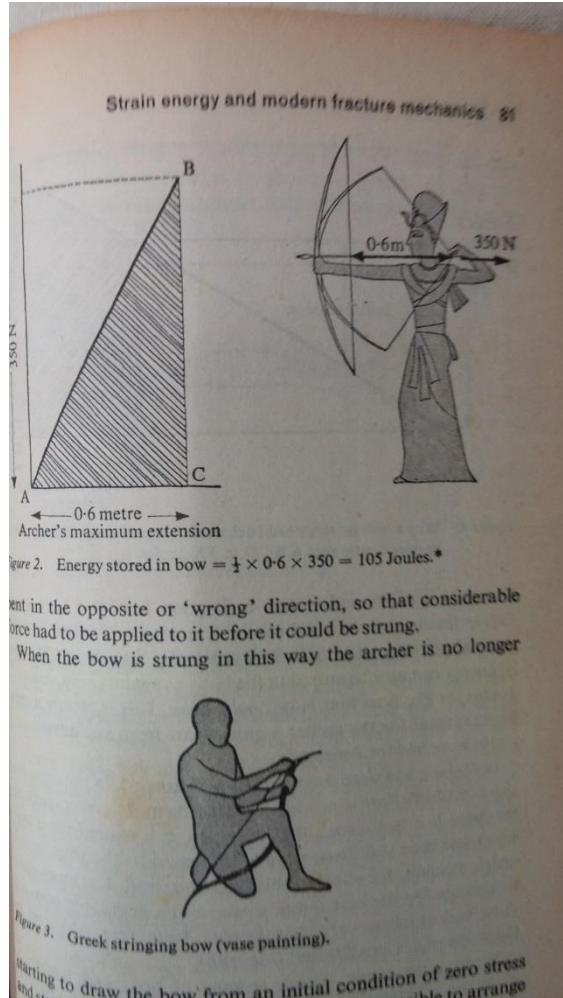


Teoremas de Energia

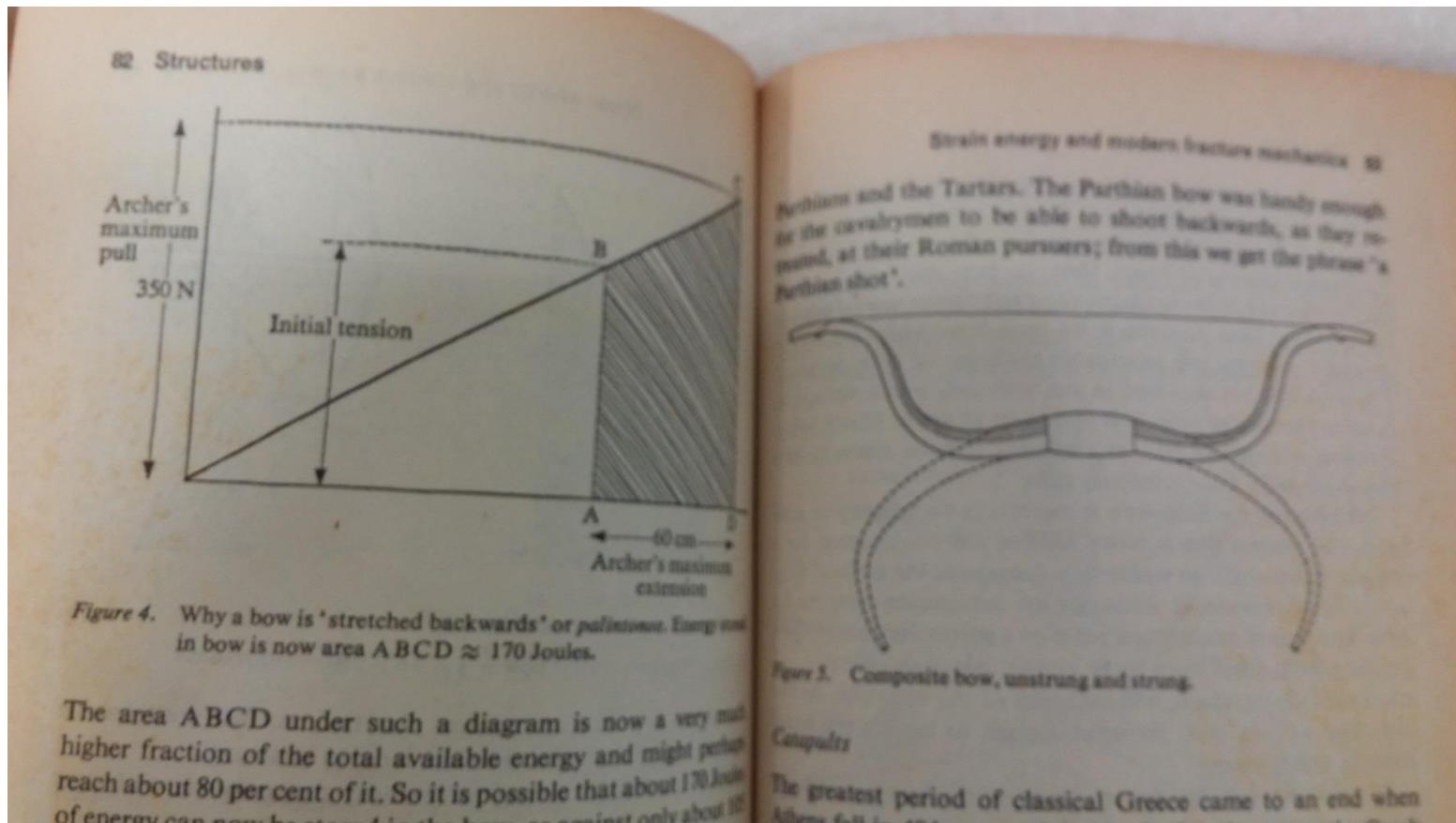
Energia de deformação



Energia de deformação



Energia de deformação



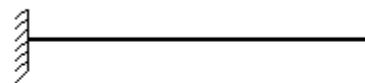
Energia de deformação

TABLE 3

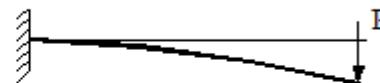
Approximate strain energy storage capacities of various solids

Material	Working strain %	Working stress		Strain energy stored Joules $\times 10^6$ per cubic metre	Density kilograms per cubic metre	Energy stored Joules per kilogram
		p.s.i.	MN/m ²			
Ancient iron	0.03	10,000	70	0.01	7,800	1.3
Modern spring steel	0.3	100,000	700	1.0	7,800	130
Bronze	0.3	60,000	400	0.6	8,700	70
Yew wood	0.9	18,000	120	0.5	600	900
Tendon	8.0	10,000	70	2.8	1,100	2,500
Horn	4.0	13,000	90	1.8	1,200	1,500
Rubber	300	1,000	7	10.0	1,200	8,000

Energia de deformação



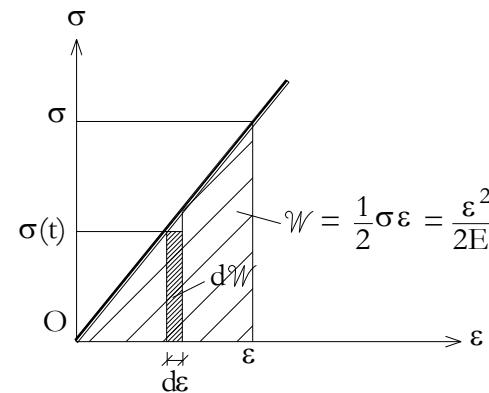
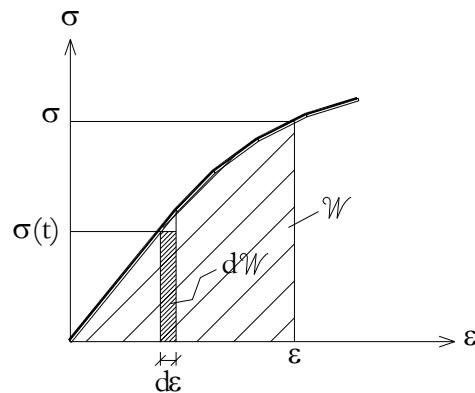
configuração de referência



configuração deformada

$$\mathcal{U} = T_{\text{int}}$$

$$\mathcal{U} = \int_V \mathcal{W} dV$$



Energia de deformação

Teoria elementar de barra plana

$$\mathcal{U} = \frac{1}{2} \int_V \sigma \epsilon dV = \frac{1}{2} \int_V E \epsilon^2 dV = \frac{1}{2} \int_V E (u' - z w'')^2 dV = \frac{1}{2} \int_{est A} \int E (u' - z w'')^2 dA dx$$

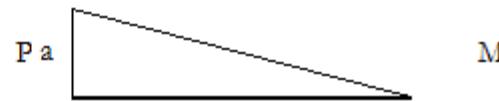
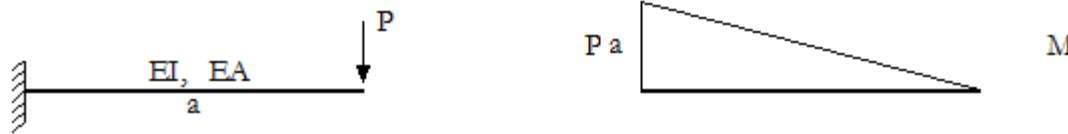
$$\mathcal{U} = \frac{1}{2} \int_{est} EI_y (w'')^2 ds + \frac{1}{2} \int_{est} EA (u')^2 ds = \int_{est} \frac{M_y^2}{2EI_y} ds + \int_{est} \frac{N^2}{2EA} ds$$

Teoria elementar de barra espacial

$$\mathcal{U} = \frac{1}{2} \int_{est} EI_y (w'')^2 ds + \frac{1}{2} \int_{est} EI_z (v'')^2 ds + \frac{1}{2} \int_{est} EA (u')^2 ds + \frac{1}{2} \int_{est} GI_T (\theta')^2 ds$$

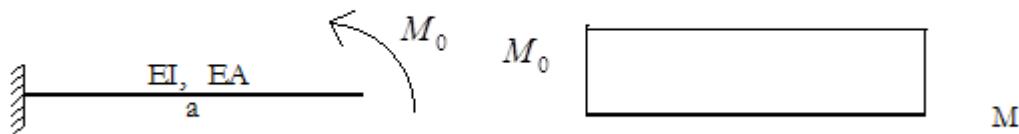
$$\mathcal{U} = \int_{est} \frac{M_y^2}{2EI_y} ds + \int_{est} \frac{M_z^2}{2EI_z} ds + \int_{est} \frac{N^2}{2EA} ds + \int_{est} \frac{T^2}{2GI_T} ds$$

Exemplo 1 - Cálculo de energia de deformação



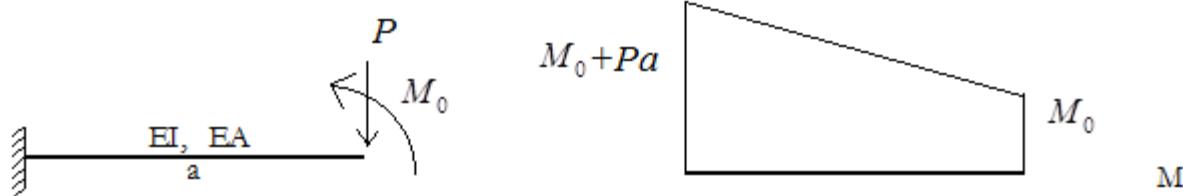
$$\mathcal{U} = \int_{est} \frac{M_y^2}{2EI_y} ds = \frac{P^2 a^3}{3EI}$$

Exemplo 1 - Cálculo de energia de deformação



$$\mathcal{U} = \int_{est} \frac{M_y^2}{2EI_y} ds = \frac{M_0^2 a}{2EI}$$

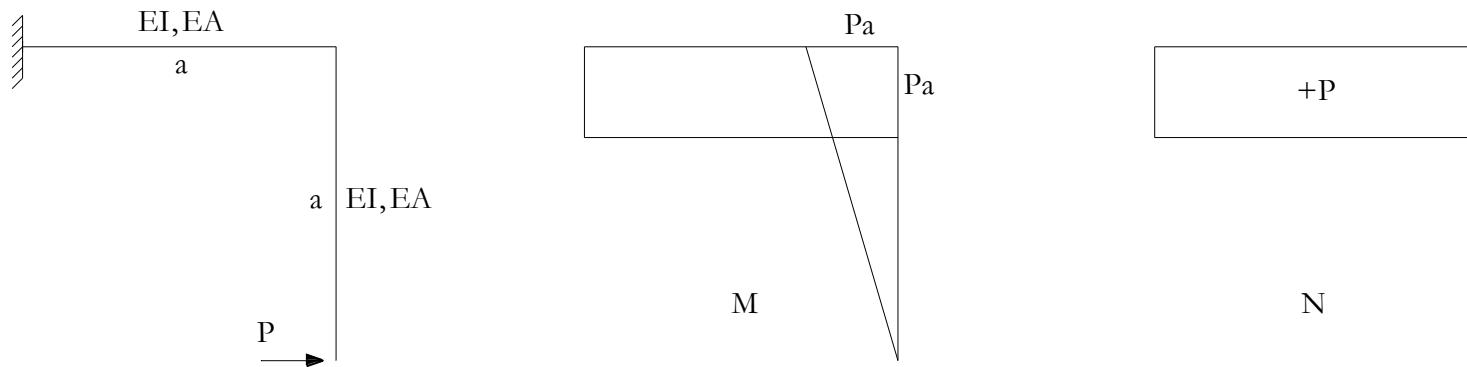
Exemplo 1 - Cálculo de energia de deformação



$$\mathcal{U} = \int_{est} \frac{M_y^2}{2EI_y} ds = \frac{P^2 a^3}{6EI} + \frac{M_0^2 a}{2EI} + \underbrace{\frac{M_0 Pa^2}{2EI}}_{\text{trabalho cruzado}}$$

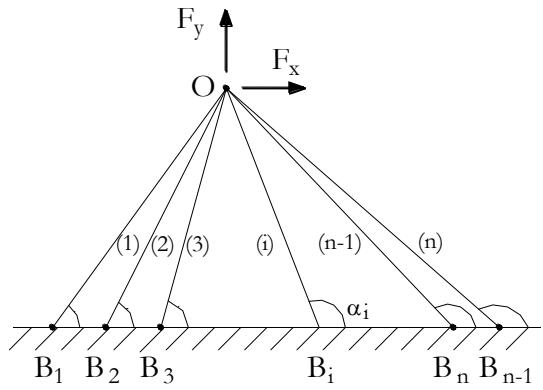
Cuidado! Em geral não vale superposição de efeitos!

Exemplo 2 - Cálculo de energia de deformação



$$\mathcal{U} = \int_{est} \frac{M_y^2}{2EI_y} ds + \int_{est} \frac{N^2}{2EA} ds = \frac{2P^2a^3}{3EI} + \frac{P^2a}{2EA} = \frac{2P^2a^3}{3EI} \left(1 + \frac{h^2}{16a^2} \right)$$

Exemplo 3 - Cálculo de energia de deformação



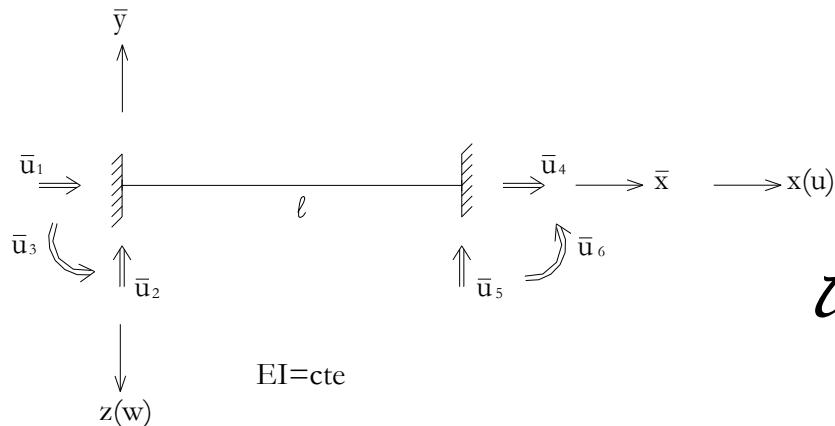
$$\mathcal{U} = \int_{est} \frac{N^2}{2EA} ds = \sum_{i=1}^n \int_0^{\ell_i} \frac{N^2}{2EA} ds = \sum_{i=1}^n \frac{N_i^2 \ell_i}{2EA_i}$$

$$N_i = \frac{EA_i}{\ell_i} (U_1 \cos \alpha_i + U_2 \sin \alpha_i)$$

$$\mathcal{U} = \frac{1}{2} (K_{11} U_1^2 + K_{12} U_1 U_2 + K_{21} U_2 U_1 + K_{22} U_2^2) = \frac{1}{2} \{U\}^T [K] \{U\}$$

$$[K] = \begin{bmatrix} \sum_{i=1}^n \frac{EA_i}{\ell_i} \cos^2 \alpha_i & \sum_{i=1}^n \frac{EA_i}{\ell_i} \cos \alpha_i \sin \alpha_i \\ \sum_{i=1}^n \frac{EA_i}{\ell_i} \cos \alpha_i \sin \alpha_i & \sum_{i=1}^n \frac{EA_i}{\ell_i} \sin^2 \alpha_i \end{bmatrix}$$

Exemplo 4 - Cálculo de energia de deformação



$$\mathcal{U} = \frac{1}{2} \int_{est} EI_y (w'')^2 ds + \frac{1}{2} \int_{est} EA (u')^2 ds$$

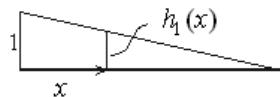
$$w = h_2(x)\bar{u}_2 + h_3(x)\bar{u}_3 + h_5(x)\bar{u}_5 + h_6(x)\bar{u}_6$$

$$u = h_1(x)\bar{u}_1 + h_4(x)\bar{u}_4$$

$$\mathcal{U}_M = \frac{1}{2} \int_0^\ell EI_y (w'')^2 ds = \frac{EI_y}{2} \left(\sum_{i=2,3,5,6} \sum_{j=2,3,5,6} \left(\int_0^\ell h_i'' h_j'' dx \right) \bar{u}_i \bar{u}_j \right)$$

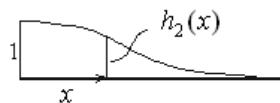
$$\mathcal{U}_N = \frac{1}{2} \int_0^\ell EA (u')^2 ds = \frac{EA}{2} \left(\sum_{i=1,4} \sum_{j=1,4} \left(\int_0^\ell h_i' h_j' dx \right) \bar{u}_i \bar{u}_j \right)$$

Exemplo 4 - Cálculo de energia de deformação



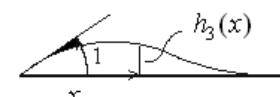
$$h_1(x) = 1 - \frac{x}{\ell}$$

$\pi(x) = h_1(x)$ para $\bar{U}_1 = 1$



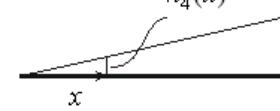
$$h_2(x) = 1 - 3\frac{x^2}{\ell^2} + 2\frac{x^3}{\ell^3}$$

$\bar{w}(x) = h_2(x)$ para $\bar{U}_2 = 1$



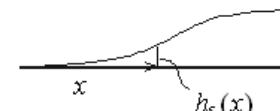
$$h_3(x) = x - 2\frac{x^2}{\ell} + \frac{x^3}{\ell^2}$$

$\bar{w}(x) = h_3(x)$ para $\bar{U}_3 = 1$



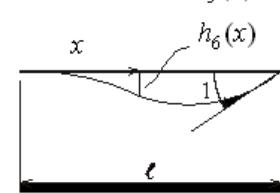
$$h_4(x) = \frac{x}{\ell}$$

$\pi(x) = h_4(x)$ para $\bar{U}_4 = 1$



$$h_5(x) = 3\frac{x^2}{\ell^2} - 2\frac{x^3}{\ell^3}$$

$\bar{w}(x) = h_5(x)$ para $\bar{U}_5 = 1$



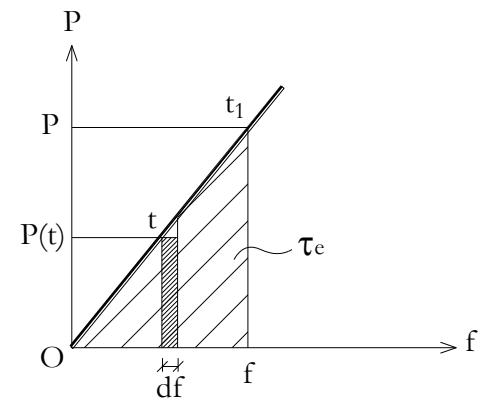
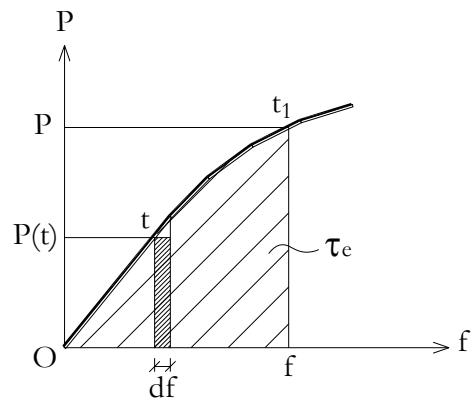
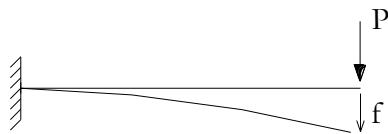
$$h_6(x) = -\frac{x^2}{\ell} + \frac{x^3}{\ell^2}$$

$\bar{w}(x) = h_6(x)$ para $\bar{U}_6 = 1$

Exemplo 4 - Cálculo de energia de deformação

$$\mathcal{U} = \frac{1}{2} \{\bar{u}\}^T [\bar{k}] \{\bar{u}\} \text{ com } [\bar{k}] = \begin{bmatrix} \frac{EA}{\ell} & 0 & 0 & -\frac{EA}{\ell} & 0 & 0 \\ 0 & \frac{12EI}{\ell^3} & \frac{6EI}{\ell^2} & 0 & -\frac{12EI}{\ell^3} & \frac{6EI}{\ell^2} \\ 0 & \frac{6EI}{\ell^2} & \frac{4EI}{\ell} & 0 & -\frac{6EI}{\ell^2} & \frac{2EI}{\ell} \\ -\frac{EA}{\ell} & 0 & 0 & \frac{EA}{\ell} & 0 & 0 \\ 0 & -\frac{12EI}{\ell^3} & -\frac{6EI}{\ell^2} & 0 & \frac{12EI}{\ell^3} & -\frac{6EI}{\ell^2} \\ 0 & -\frac{6EI}{\ell^2} & \frac{2EI}{\ell} & 0 & -\frac{6EI}{\ell^2} & \frac{4EI}{\ell} \end{bmatrix}$$

Teorema de Clapeyron



Para comportamento linear:

$$T_e = \frac{1}{2} Pf$$

Generalizando:

$$T_e = \frac{1}{2} \sum_{i=1}^n R_i U_i = \frac{1}{2} \{U\}^T \{R\}$$

Teorema do Trabalho

Particularizando para teoria de barras:

$$T_{int} = T_{ext}$$

$$T_{int} = \mathcal{U} = \frac{1}{2} \{U\}^T [K] \{U\}$$

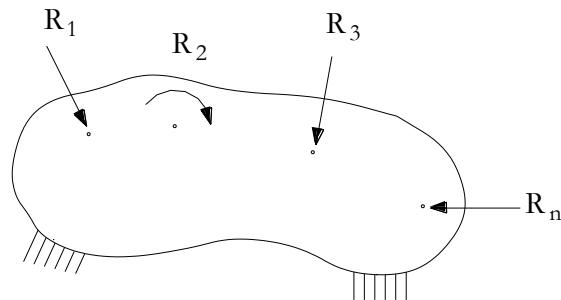
$$T_e = \frac{1}{2} \sum_{i=1}^n R_i U_i = \frac{1}{2} \{U\}^T \{R\}$$

$$\{U\}^T ([K] \{U\} - \{R\}) = \{0\} \xrightarrow{\{U\} \neq \{0\}} [K] \{U\} = \{R\}$$

Energia potencial total

$$\Pi = \mathcal{U}(U_i) + \mathcal{P}(U_i) = \mathcal{U}(U_i) - \sum_{i=1}^n R_i U_i$$

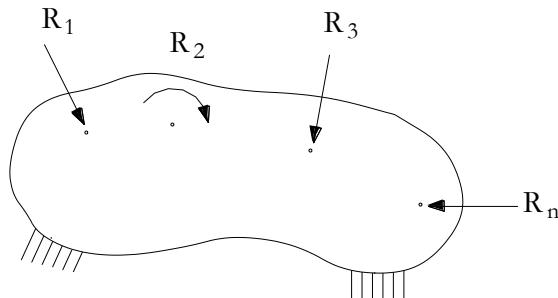
Teorema: “entre todas as soluções compatíveis, aquela que também é equilibrada torna estacionária a energia potencial total”



$$\frac{\partial \Pi}{\partial U_k} = \frac{\partial \mathcal{U}}{\partial U_k} - R_k = 0$$

Primeiro teorema de Castigliano

(por Alberto Castigliano em 1873)



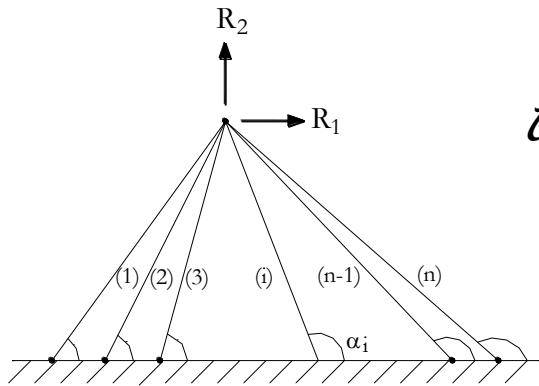
$$\frac{\partial \mathcal{U}}{\partial U_k} = R_k$$

Teorema: “Se a energia de deformação for expressa em função de n deslocamentos independentes entre si, então a sua derivada parcial em relação a um desses deslocamentos é igual ao esforço conjugado”

Aplicações do primeiro teorema de Castigliano

- Estabelecer equações de equilíbrio
- análise de estruturas pelo método dos deslocamentos que permite escolher entre todas as soluções compatíveis aquela também equilibrada
- Nas duas aplicações é importante observar que os deslocamentos devem se independentes

Exemplo: Aplicação do primeiro teorema de Castigliano



$$\mathcal{U} = \frac{1}{2} (K_{11}U_1^2 + K_{12}U_1U_2 + K_{21}U_2U_1 + K_{22}U_2^2) = \frac{1}{2} \{\mathbf{U}\}^T [\mathbf{K}] \{\mathbf{U}\}$$

$$\mathcal{P} = -R_1 U_1 - R_2 U_2$$

$$\Pi = \frac{1}{2} (K_{11}U_1^2 + K_{12}U_1U_2 + K_{21}U_2U_1 + K_{22}U_2^2) - R_1 U_1 - R_2 U_2$$

$$\begin{aligned} \frac{\partial \mathcal{U}}{\partial U_1} &= R_1 \quad \text{ou} \quad \frac{\partial \Pi}{\partial U_1} = 0 \quad \Rightarrow \quad K_{11}U_1 + K_{12}U_2 = R_1 \\ \frac{\partial \mathcal{U}}{\partial U_2} &= R_2 \quad \text{ou} \quad \frac{\partial \Pi}{\partial U_2} = 0 \quad \Rightarrow \quad K_{21}U_1 + K_{22}U_2 = R_2 \end{aligned} \quad \rightarrow [\mathbf{K}] \{\mathbf{U}\} = \{\mathbf{R}\}$$

Método dos deslocamentos

- Formulação direta das equações de equilíbrio, que envolve grandezas vetoriais - forças e deslocamentos
- Formulação baseada no teorema dos deslocamentos virtuais que envolve grandeza escalar - trabalho
- Formulação variacional baseada no teorema da energia potencial total ou no primeiro teorema de Castigliano que envolve grandeza escalar - energia